**Illinois Statewide**

**Technical Reference Manual**

**for Energy Efficiency**

**Version 4.0**

**December 19, 2014**

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**June 1st, 2015**

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**Acknowledgements**

This document was created through a collaboration amongst the members of the Illinois Energy Efficiency Stakeholder Advisory Group (SAG). The SAG is an open forum where interested parties may participate in the evolution of Illinois’ energy efficiency programs. Parties wishing to participate in the SAG process may do so by visiting <http://www.ilsag.info/questions.html> and contacting the Independent Facilitator at [Annette.Beitel@FutEE.biz](mailto:Annette.Beitel@FutEE.biz). Parties wishing to participate in the Technical Advisory Committee (TAC), a subcommittee of the SAG, may do so by contacting the TRM Administrator at [iltrmadministrator@veic.org](mailto:iltrmadministrator@veic.org).

|  |
| --- |
| **SAG Stakeholders[[1]](#footnote-2)** |
| Ameren Illinois Company (Ameren) |
| Center for Neighborhood Technology (CNT) |
| Citizen's Utility Board (CUB) |
| City of Chicago |
| Commonwealth Edison Company (ComEd) |
| Energy Resources Center at the University of Illinois, Chicago (ERC) |
| Environment IL |
| Environmental Law and Policy Center (ELPC) |
| Future Energy Enterprises LLC |
| Illinois Attorney General's Office (AG) |
| Illinois Commerce Commission Staff (ICC Staff) |
| Illinois Department of Commerce and Economic Opportunity (DCEO) |
| Independent Evaluators (ADM, Cadmus, Itron, Navigant) |
| Integrys (Peoples Gas and North Shore Gas) |
| Metropolitan Mayor's Caucus (MMC) |
| Midwest Energy Efficiency Association (MEEA) |
| Natural Resources Defense Council (NRDC) |
| Nicor Gas |

Table 1.: Document Revision History

| **Document Title** | **Applicable to PY Beginning** |
| --- | --- |
| Illinois\_Statewide\_TRM\_Effective\_060112\_Version\_1.0\_091412\_Clean.doc | 6/1/12 |
| Illinois\_Statewide\_TRM\_Effective\_060113\_Version\_2.0\_060713\_Clean.docx | 6/1/13 |
| Illinois\_Statewide\_TRM\_Effective\_060114\_Version\_3.0\_022414\_Clean.docx | 6/1/14 |
| Illinois\_Statewide\_TRM\_Effective\_060115\_Version\_4.0\_121914\_Clean.docx | 6/1/15 |

**Summary of Measure Revisions**

The following tables summarize the evolution of measures that are new, revised or errata. This version of the TRM contains 80 measure-level changes as described in the following table.

Table 1.2: Summary of Measure-Level Changes

|  |  |
| --- | --- |
| **Change Type** | **# Changes** |
| Errata | 16 |
| Revision | 43 |
| New Measure | 21 |
| Total Changes | 80 |

The ‘Change Type’ column indicates what kind of change each measure has gone through. Specifically, when a measure error was identified and the TAC process resulted in a consensus, the measure is identified here as an ‘Errata’. In these instances the measure code indicates that a new version of the measure has been published, and that the effective date of the measure dates back to June 1st, 2014. Measures that are identified as ‘Revised’ were included in the third edition of the TRM, and have been updated for this edition of the TRM. Both ‘Revised’ and ‘New Measure(s)’ have an effective date of June 1st, 2015.

The following table provides an overview of the 80 measure-level changes that are included in this version of the TRM.

Table 1.3: Summary of Measure Revisions

| **Mkt** | **End Use** | **Measure Name** | **Measure Code** | **Change Type** | **Explanation** | **Impact on Savings** |
| --- | --- | --- | --- | --- | --- | --- |
| C&I | 4.2 Food Service Equipment | 4.2.19 ENERGY STAR Electric Convection Oven | CI-FSE-ECON-V01-150601 | New | n/a | n/a |
| C&I | 4.3 Hot Water | 4.3.2 Low Flow Faucet Aerators | CI-HWE-LFFA-V05-140601 | Errata | Fixing Reference | None |
| 4.3.7 Multifamily Central Domestic Hot Water Plants | CI-HW\_-MDHW-V01-150601 | New | n/a | n/a |
| 4.3.8 Controls for Central Domestic Hot Water | CI-HW\_-CDHW-V01-150601 | New | n/a | n/a |
| C&I | 4.4 HVAC | 4.4 HVAC End Use |  | Errata | Added EFLH for Heat Pump Systems, PTAC/PTHP and Unitary AC | Unknown |
| 4.4 HVAC End Use |  | Revision | Updated EFLH | Dependent on building type |
| 4.4.1 Air Conditioner Tune-Up | CI-HVC-ACTU-V02-150601 | Revision | Removed some tune-up requirements Removing deemed savings assumption - replaced with algorithm | Unknown |
| 4.4.2 Space Heating Boiler Tune-Up | CI-HVC-BLRT-V05-150601 | Revision | Removing deemed savings factor | Unknown |
| 4.4.3 Process Boiler Tune-Up | CI-HVC-PBTU-V04-150601 | Revision | Removing deemed savings factor | Unknown |
| 4.4.4 Boiler Lockout/Reset Controls | CI-HVC-BLRC-V03-150601 | Revision | Updated example with new EFLH | Dependent on building type |
| 4.4.6 Electric Chiller | CI-HVC-CHIL-V03-150601 | Revision | Updated example with new EFLH | Dependent on building type |
| 4.4.8 Guest Room Energy Management | CI-HVC-GREM-V05-150601 | Revision | Updated Hotel savings values based on modeling | Dependent on inputs |
| 4.4.9 Heat Pump Systems | CI-HVC-HPSY-V03-150601 | Revision | Updated code reference Updated example with new EFLH | Dependent on building type |
| 4.4.10 High Efficiency Boiler | CI-HVC-BOIL-V05-150601 | Revision | Updated example with new EFLH | Dependent on building type |
| 4.4.11 High Efficiency Furnace | CI-HVC-FRNC-V04-150601 | Revision | Updated example with new EFLH | Dependent on building type |
| 4.4.13 Package Terminal Air Conditioner and Package Terminal Heat Pump | CI-HVC-PTAC-V05-140601 | Errata | Retrofit cost information updated | None |
| 4.4.13 Package Terminal Air Conditioner and Package Terminal Heat Pump | CI-HVC-PTAC-V05-150601 | Revision | Updated example with new EFLH Added default early replacement costs | Dependent on building type |
| 4.4.14 Pipe Insulation | CI-HVC-PINS-V03-150601 | Revision | Clarifications of algorithm Model results updated with new EFLH | Dependent on building type |
| 4.4.15 Single-Package and Split System Unitary Air Conditioning | CI-HVC-SPUA-V03-150601 | Revision | Updated code reference Updated example with new EFLH | Dependent on building type |
| 4.4.17 Variable Speed Drives for HVAC Pumps and Cooling Tower Fans | CI-HVC-VSDHP-V02-150601 | Revision | Seperated Supply / Return fans in to separate measure. Updated Hours table | Dependent on building type |
| 4.4.18 Small Commercial Programmable Thermostats | CI-HVC-PROG-V02-150601 | Revision | Costs clarified. Complete re-work of savings estimate | Unknown |
| 4.4.19 Demand Control Ventilation | CI-HVC-DCV-V02-140601 | Errata | Therm\_Saving\_Factor and Elec\_Saving\_Factor updated with final values | Unknown |
| 4.4.24 Small Pipe Insulation | CI-HVC-SPIN-V01-150601 | New | n/a | n/a |
| 4.4.25 Small Programmable Thermostat Adjustments | CI-HVC- PRGA -V01-150601 | New | n/a | n/a |
| 4.4.26 Variable Speed Drives for HVAC Supply and Return Fans | CI-HVC-VSDF-V01-150601 | New | n/a | n/a |
| 4.4.27 Energy Recovery Ventilator | CI-HVC-ERVE-V01-150601 | New | n/a | n/a |
| 4.4.28 Stack Economizer for Boilers Serving HVAC Loads | CI-HVC-BECO-V01-150601 | New | n/a | n/a |
| 4.4.29 Stack Economizer for Boilers Serving Process Loads | CI-HVC-PECO-V01-150601 | New | n/a | n/a |
| 4.4.30 Notched V Belts for HVAC Systems | CI-MSC-NVBE-V01-150601 | New | n/a | n/a |
| 4.4.31 Small Business Furnace Tune Up | CI-HVC-FTUN-V01-150601 | New | n/a | n/a |
| C&I | 4.5 Lighting | 4.5 Lighting |  | Revision | Update of WHF to match new models | Dependent on building type |
| 4.5.1 Commercial ENERGY STAR Compact Fluorescent | CI-LTG-CCFL-V04-140601 | Errata | Update to RES v C&I Split | Increase in kWh savings (more C&I) |
| 4.5.1 Commercial ENERGY STAR Compact Fluorescent | CI-LTG-CCFL-V05-150601 | Revision | Update to RES v C&I Split, ISR | Increase in kWh savings (more C&I) |
| 4.5.3 High Performance and Reduced Wattage T8 Fixtures | CI-LTG-T8FX-V03-140601 | Errata | Update to RES v C&I Split | Increase in kWh savings (more C&I) |
| 4.5.3 High Performance and Reduced Wattage T8 Fixtures | CI-LTG-T8FX-V04-150601 | Revision | Clarification of Direct Install assumptions. Measure life clarification Update to ISR | Increase in kWh savings (higher ISR) |
| 4.5.4 LED Bulbs and Fixtures | CI-LTG-LEDB-V03-140601 | Errata | Update to RES v C&I Split | Increase in kWh savings (more C&I) |
| 4.5.4 LED Bulbs and Fixtures | CI-LTG-LEDB-V04-150601 | Revision | Update to RES v C&I Split | Increase in kWh savings (more C&I) |
| C&I | 4.6 Refrigeration | 4.6.6 Evaporator Fan Control | CI-RFG-EVPF-V02-140601 | Errata | Replacing CA estimates with Illinois | Approximately the same |
| 4.6.9 Night Covers for Open Refrigerated Display Cases | CI-RFG-NCOV-V01-150601 | New | n/a | n/a |
| C&I | 4.7 Miscellaneous | 4.7.4 Pump Optimization | CI-MSC-PMPO-V01-150601 | New | n/a | n/a |
| 4.7.5 Efficient Compressed Air Nozzles | CI-MSC-CNOZ-V01-150601 | New | n/a | n/a |
| 4.7.6 Roof Insulation for C&I Facilities | CI-MSC-RINS-V01-150601 | New | n/a | n/a |
| 4.7.7 Computer Power Management Software | CI-MSC-CPMS-V01-150601 | New | n/a | n/a |
| Res | 5.1 Appliances | 5.1.2 ENERGY STAR and ENERGY STAR Most Efficient Clothes Washer | RS-APL-ESCL-V03-150601 | Revision | Updatated methodology based on new Federal and ESTAR specifications | Reduction in savings |
| 5.1.8 Refrigerator and Freezer Recycling | RS-APL-RFRC-V04-140601 | Errata | Fixing typo in Freezer coefficient table. | Unknown |
| 5.1.8 Refrigerator and Freezer Recycling | RS-APL-RFRC-V05-150601 | Revision | Updated coefficient values | Dependent on inputs |
| 5.1.10 Residential ENERGY STAR Clothes Dryer | RS-APL-ESDR-V01-150601 | New | n/a | n/a |
| Res | 5.3 HVAC | 5.3.1 Air Source Heat Pump | RS-HVC-ASHP-V04-150601 | Revision | Added deemed early replacement rate. Updated Federal Standard and costs | Reduction in savings |
| 5.3.3 Central Air Conditioning | RS-HVC-CAC1-V04-150601 | Revision | Added deemed early replacement rate. | None |
| 5.3.4 Duct Insulation and Sealing | RS-HVC-DINS-V03-140601 | Errata | Input capacity update  Addition of furnace fan savings | Addition of kWh savings |
| 5.3.4 Duct Insulation and Sealing | RS-HVC-DINS-V05-150601 | Revision | Updated HP Federal Standard | Reduction in savings |
| 5.3.6 Gas High Efficiency Boiler | RS-HVC-GHEB-V03-150601 | Revision | Added deemed early replacement rate. | None |
| 5.3.7 Gas High Efficiency Furnace | RS-HVC-GHEF-V04-150601 | Revision | Added deemed early replacement rate. | None |
| 5.3.8 Ground Source Heat Pump | RS-HVC-GSHP-V04-150601 | Revision | Complete rework of methodology | Increase in savings |
| 5.3.12 Ductless Heat Pumps | RS-HVC-DHP-V02-150601 | Revision | Updated HP Federal Standard | Reduction in savings |
| 5.3.13 Residential Furnace Tune up | RS-HVC-FTUN-V01-150601 | New | n/a | n/a |
| 5.3.14 Boiler Reset Controls | RS-HVC-BREC-V01-150601 | New | n/a | n/a |
| 5.3.15 ENERGY STAR Ceiling Fan | RS-HVC-CFAN-V01-150601 | New | n/a | n/a |
| Res | 5.4 Hot Water | 5.4.2 Gas Water Heater | RS-HWE-GWHT-V03-140601 | Errata | Removing link and reference to DeOreo study | None |
| 5.4.2 Gas Water Heater | RS-HWE-GWHT-V04-150601 | Revision | Added Early Replacement Updated Federal Baseline | Reduction in savings |
| 5.4.3 Heat Pump Water Heaters | RS-HWE-HPWH-V03-140601 | Errata | Coincidence factor reference update  Removing link and reference to DeOreo study | None |
| 5.4.3 Heat Pump Water Heaters | RS-HWE-HPWH-V04-150601 | Revision | Updated Federal Baseline | Reduction in savings |
| 5.4.4 Low Flow Faucet Aerators | RS-HWE-LFFA-V04-140601 | Errata | Removing link and reference to DeOreo study | None |
| 5.4.6 Water Heater Temperature Setback | RS-HWE-TMPS-V04-150601 | Revision | Complete rework of methodology | Unknown |
| 5.4.7 Water Heater Wrap | RS-HWE-WRAP-V02-150601 | revision | Fixed algorithm typo | None |
| 5.4.8 Thermostatic Restrictor Shower Valve | RS-HWE-TRVA-V01-150601 | New | n/a | n/a |
| Res | 5.5 Lighting | 5.5.1 ENERGY STAR Compact Fluorescent Lamp | RS-LTG-ESCF-V04-150601 | Revision | Update to RES v C&I Split, ISR, Hours, Coincidence Factors. Added leakage variable Added Efficiency Kit ISRs | Unknown |
| 5.5.2 ENERGY STAR Specialty Compact Fluorescent Lamp | RS-LTG-ESCC-V03-150601 | Revision | Update to RES v C&I Split, ISR, Hours, Coincidence Factors. Added leakage variable Added Efficiency Kit ISRs | Unknown |
| 5.5.3 ENERGY STAR Torchiere | RS-LTG-ESTO-V02-150601 | Revision | Update to Coincidence Factors. Added leakage variable | Unknown |
| 5.5.4 Exterior Hardwired Compact Fluorescent Lamp | RS-LTG-EFIX-V04-150601 | Revision | Update to Hours, Coincidence Factors. Added leakage variable | Increase in savings |
| 5.5.5 Interior Hardwired Compact Fluorescent Lamp | RS-LTG-IFIX-V04-150601 | Revision | Update to Hours, Coincidence Factors. Added leakage variable | Reduction in savings |
| 5.5.6 LED Downlights | RS-LTG-LEDD-V03-140601 | Errata | Fixing typo in delta watts table | None |
| 5.5.6 LED Downlights | RS-LTG-LEDD-V04-150601 | Revision | Update to Hours, Coincidence Factors. Added leakage variable | Dependent on inputs |
| 5.5.8 LED Screw Based Omnidirectional Bulbs | RS-LTG-LEDA-V03-150601 | Revision | Update to ISR, Hours, Coincidence Factors. Added leakage variable Added Efficiency Kit ISRs | Unknown |
| Res | 5.6 Shell | 5.6.1 Air Sealing | RS-SHL-AIRS-V03-150601 | Revision | Updated HP Federal Standard | Reduction in savings |
| 5.6.2 Basement Sidewall Insulation | RS-SHL-BINS-V05-140601 | Errata | Removing Low Income distinction due to very small sample size. | Increase in LI savings |
| 5.6.2 Basement Sidewall Insulation | RS-SHL-BINS-V06-150601 | Revision | Updated HP Federal Standard | Reduction in savings |
| 5.6.3 Floor Insulation Above Crawlspace | RS-SHL-FINS-V05-140601 | Errata | Removing Low Income distinction due to very small sample size. | Increase in LI savings |
| 5.6.3 Floor Insulation Above Crawlspace | RS-SHL-FINS-V06-150601 | Revision | Updated HP Federal Standard | Reduction in savings |
| 5.6.4 Wall and Ceiling/Attic Insulation | RS-SHL-AINS-V05-150201 | Revision | Updated HP Federal Standard | Reduction in savings |

# Purpose of the TRM

The purpose of the Illinois Statewide Technical Reference Manual (TRM) is to provide a transparent and consistent basis for calculating energy (electric kilowatt-hours (kWh) and natural gas therms) and capacity (electric kilowatts (kW)) savings generated by the State of Illinois’ energy efficiency programs[[2]](#footnote-3) which are administered by the Department of Commerce and Economic Opportunity (DCEO) and the state’s largest electric and gas Utilities[[3]](#footnote-4) (collectively, Program Administrators).

The TRM is a technical document that is filed with the Illinois Commerce Commission (Commission or ICC) and is intended to fulfill a series of objectives, including:

* “Serve as a common reference document for all… stakeholders, [Program Administrators], and the Commission, so as to provide transparency to all parties regarding savings assumptions and calculations and the underlying sources of those assumptions and calculations.
* Support the calculation of the Illinois Total Resource Cost test[[[4]](#footnote-5)] (“TRC”), as well as other cost-benefit tests in support of program design, evaluation and regulatory compliance. Actual cost-benefit calculations and the calculation of avoided costs will not be part of this TRM.
* Identify gaps in robust, primary data for Illinois, that can be addressed via evaluation efforts and/or other targeted end-use studies.
* [Provide] a process for periodically updating and maintaining records, and preserve a clear record of what deemed parameters are/were in effect at what times to facilitate evaluation and data accuracy reviews.
* …[S]upport coincident peak capacity (for electric) savings estimates and calculations for electric utilities in a manner consistent with the methodologies employed by the utility’s Regional Transmission Organization (“RTO”), as well as those necessary for statewide Illinois tracking of coincident peak capacity impacts.”[[5]](#footnote-6)

* 1. Enabling ICC Policy

This Illinois Statewide Technical Reference Manual (TRM) was developed to comply with the Illinois Commerce Commission (ICC or Commission) Final Orders from the electric and gas Utilities’[[6]](#footnote-7) Energy Efficiency Plan dockets. In the Final Orders, the ICC required the utilities to work with DCEO and the Illinois Energy Efficiency Stakeholder Advisory Group (SAG) to develop a statewide TRM. *See, e.g.,* ComEd’s Final Order *(Docket No. 10-0570, Final Order[[7]](#footnote-8) at 59-60, December 21, 2010);* Ameren’s Final Order *(Docket No. 10-0568, Order on Rehearing[[8]](#footnote-9) at 19, May 24, 2011);* Peoples Gas/North Shore Gas’ Final Order *(Docket No. 10-0564, Final Order[[9]](#footnote-10)at 76, May 24, 2011),* and Nicor’s Final Order *(Docket No. 10-0562, Final Order[[10]](#footnote-11) at 30, May 24, 2011).*

As directed in the Utilities’ Efficiency Plan Orders, the SAG had the opportunity to, and also participated in, every aspect of the development of the TRM. Interested members of the SAG participated in weekly teleconferences to review, comment, and participate in the development of the TRM. The active participants in the TRM were designated as the “Technical Advisory Committee” (TAC). The TAC participants include representatives from the following organizations:

* the Utilities (ComEd, Ameren IL, Nicor Gas, Peoples Gas/North Shore Gas),
* DCEO, Implementation contractors (Applied Proactive Technologies (APT), CLEAResult, Conservation Services Group, Elevate Energy, Franklin Energy, GDS Associates, PECI, 360 Energy Group),
* Illinois Department of Commerce and Economic Opportunity (DCEO),
* the independent evaluators (ADM Associates, The Cadmus Group, Itron, Navigant Consulting, Michael’s Engineering, Opinion Dynamics Corporation),
* ICC Staff,
* the Illinois Attorney General’s Office (AG),
* Natural Resources Defense Council (NRDC),
* the Environmental Law and Policy Center (ELPC),
* the Citizen’s Utility Board (CUB),
* CNT Energy, The University of Illinois at Chicago,
* Future Energy Enterprises,
* Geothermal Alliance of Illinois,
* the Geothermal Exchange Organization.

* 1. Development Process

The first edition of the IL-TRM was approved by the Commission in ICC Docket No. 12-0528[[11]](#footnote-12). The second edition of the IL-TRM was approved by the Commission in ICC Docket No. 13-0437[[12]](#footnote-13). The policies surrounding the applicability and use of the IL-TRM in planning, implementation, and evaluation were established by the Commission in ICC Docket No. 13-0077[[13]](#footnote-14). The third edition of the IL-TRM was approved by the Commission in ICC Docket No. 14-0189[[14]](#footnote-15). This document represents the fourth edition of the IL-TRM. It contains a series of new measures, as well as a series of errata items[[15]](#footnote-16) and updates to existing measures that were already present in the first, second and third editions. Like the previous editions, it is a result of an ongoing review process involving the Illinois Commerce Commission (ICC) Staff (Staff or ICC Staff), the Utilities, DCEO, the Evaluators, the SAG TAC, and the SAG. VEIC meets with the SAG and/or the TRM TAC at least once each month to create a high level of transparency and vetting in the development of this TRM.

Measure requests that are submitted by interested parties are ranked based on the following criteria to determine the approximate priority level for order of inclusion in the TRM:

1. High Priority

* For those existing measures that make up a significant portion of a utilities’ portfolio and/or where the impact of the requested change is high
* For new measures where plans are in place to implement in the next program year

1. Medium Priority

* For existing measures that are a less significant percent of a utilities portfolio and value change will not have a significant impact
* For new measures where a savings value is estimated but implementation plans not yet developed

1. Low Priority

* For existing measures that represent a very small percent of a utility’s portfolio
* For new measures that are just beginning to be explored and will not be implemented in the next program year

These rankings are used to align budget and schedule constraints with desired updates from the TRM.

As measure requests are finalized leading up to the next update of the TRM, weekly TAC meetings are often scheduled to maximize the level of collaboration and visibility into the measure characterization process. Where consensus does not emerge on specific measures or issues, those items are identified in a memo, and are not included in the TRM. As a result, this TRM represents a broad consensus amongst the SAG and TAC participants. In keeping with the goal of transparency, all of the comments and their status to‐date are available through the TAC SharePoint web site, [https://portal.veic.org](https://portal.veic.org/).

For each measure characterization, this TRM includes engineering algorithm(s) and a value(s) for each parameter in the equation(s). These parameters have values that fall into one of three categories: a single deemed value, a lookup table of deemed values or an actual value such as the capacity of the equipment. The TRM makes extensive use of lookup tables because they allow for an appropriate level of measure streamlining and customization within the context of an otherwise prescriptive measure.

Accuracy is the overarching principle that governs what value to use for each parameter. When it is explicitly allowed within the text of the measure characterization, the preferred value is the actual or on-site value for the individual measure being implemented. The *deemed values[[16]](#footnote-17)* in the lookup tables are the next most accurate choice, and in the absence of either an actual value or an appropriate value in a lookup table, the single, *deemed value* should be used. As a result, this single, *deemed value* can be thought of as a default value for that particular input to the algorithm.

A single *deemed savings estimate* is produced by any given combination of an algorithm and the allowable input values for each of its parameters. In cases where lookup tables are provided, there is a range of deemed savings estimates that are possible, depending on site-specific factors such as equipment capacity, location and building type.

Algorithms and their parameter values are included for calculating estimated:

* Gross annual electric energy savings (kWh)
* Gross annual natural gas energy savings (therms)
* Gross electric summer coincident peak demand savings (kW)

To support cost-effectiveness calculations, parameter values are also included for:

* Incremental costs ($)
* Measure life (years)
* Operation and maintenance costs ($)
* Water (gal) and other resource savings where appropriate.

To facilitate the use of the TRM as measures are revised, updated, and removed, a unique code is provided for each measure that identifies the measure and the applicable installed program year.



## Organizational Structure

The organization of this document follows a three-level format, each of which is a major heading in the Table of Contents. These levels are designed to define and clarify what the measure is and where it is applied.

1. **Market Sectors[[17]](#footnote-18)** 
   * This level of organization specifies the type of customer the measure applies to, either Commercial and Industrial or Residential.
   * Answers the question, “What category best describes the customer?”
2. **End-use Category**
   * This level of organization represents most of the major end-use categories for which an efficient alternative exists. The following table lists all of the end-use categories in this version of the TRM.
   * Answers the question, “To what end-use category does the measure apply?”

**Table 1.1: End-Use Categories in the TRM[[18]](#footnote-19)**

|  |  |
| --- | --- |
| **Residential Market Sector** | **Commercial and Industrial Market Sector** |
| Appliances | Agricultural Equipment |
| Consumer Electronics | Food Service Equipment |
| Hot Water | Hot Water |
| HVAC | HVAC |
| Lighting | Lighting |
| Shell | Miscellaneous |
|  | Refrigeration |

1. **Measure & Technology**
   * This level of organization represents individual efficient measures such as CFL lighting and LED lighting, both of which are individual technologies within the Lighting end-use category.
   * Answers the question, “What technology defines the measure?”

This organizational structure is silent on which fuel the measure is designed to save; electricity or natural gas. By organizing the TRM this way, measures that save on both fuels do not need to be repeated. As a result, the TRM will be easier to use and to maintain.

* 1. Measure Code Specification

In order to uniquely identify each measure in the TRM, abbreviations for the major organizational elements of the TRM have been established. When these abbreviations are combined and delimited by a dash (‘-‘) a unique, 18-character alphanumeric code is formed that can be used for tracking the measures and their associated savings estimates. Measure codes appear at the end of each measure and are structured using five parts.

**Code Structure = Market + End-use Category + Measure + Version # + Effective Date**

For example, the commercial boiler measure is coded: “CI-HVC-BLR\_-V01-120601”

**Table 1.2: Measure Code Specification Key**

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
| **Market (@@)** | **End-use (@@@)** | **Measure (@@@@)** | **Version (V##)** | **Effective Date** |
| CI (C&I) | AGE (Agricultural Equipment) | BLR\_ | V01 | YYMMDD |
| RS (Residential) | APL (Appliances) | T5F\_ | V02 | YYMMDD |
|  | CEL (Consumer Electronics) | T8F\_ | V03 | YYMMDD |
|  | FSE (Food Service Equipment) | … | … | … |
|  | HVC (HVAC) |  |  |  |
|  | HW\_ (Hot Water) |  |  |  |
|  | LTG (Lighting) |  |  |  |
|  | MSC (Miscellaneous) |  |  |  |
|  | RFG (Refrigeration) |  |  |  |
|  | SHL (Shell) |  |  |  |

* 1. Components of TRM Measure Characterizations

Each measure characterization uses a standardized format that includes at least the following components. Measures that have a higher level of complexity may have additional components, but also follow the same format, flow and function.

**Description**

Brief description of measure stating how it saves energy, the markets it serves and any limitations to its applicability.

**Definition of Efficient Equipment**

Clear definition of the criteria for the efficient equipment used to determine delta savings. Including any standards or ratings if appropriate*.*

**Definition of Baseline Equipment**

Clear definition of the efficiency level of the baseline equipment used to determine delta savings including any standards or ratings if appropriate. If a Time of Sale measure the baseline will be new base level equipment (to replace existing equipment at the end of its useful life or for a new building). For Early Replacement or Early Retirement measures the baseline is the existing working piece of equipment that is being removed.

**Deemed Lifetime of Efficient Equipment**

The expected duration in years (or hours) of the savings. If an early replacement measure, the assumed life of the existing unit is also provided.

**Deemed Measure Cost**

For time of sale measures, incremental cost from baseline to efficient is provided. Installation costs should only be included if there is a difference between each level. For Early Replacement the full equipment and install cost of the efficient installation is provided in addition to the full deferred hypothetical baseline replacement cost.

**Loadshape**

The appropriate loadshape to apply to electric savings is provided.

**Coincidence Factor**

The summer coincidence factor is provided to estimate the impact of the measure on the utility’s system peak – defined as 1PM to hour ending 5PM on non-holiday weekdays, June through August.

**Algorithm**

**Calculation of Energy Savings**

Algorithms are provided followed by list of assumptions with their definition.

If there are no Input Variables, there will be a finite number of Output values. These will be identified and listed in a table. Where there are custom inputs, an example calculation is often provided to illustrate the algorithm and provide context.

**Electric Energy Savings**

**Summer Coincident Peak Demand Savings**

**Natural Gas Savings**

**Water Impact Descriptions and Calculation**

**Deemed O&M Cost Adjustment Calculation**

Only required if the operation and maintenance cost for the efficient case is different to the baseline

* 1. Variable Input Tables

Many of the measures in this TRM require the user to select the appropriate input value from a list of inputs for a given parameter in the savings algorithm. Where the TRM asks the user to select the input, look-up tables of allowable values are provided. For example, a set of input parameters may depend on building type; while a range of values may be given for each parameter, only one value is appropriate for any specific building type. If no table of alternative inputs is provided for a particular parameter, then the single deemed value will be used, unless the measure has a custom allowable input.

* + 1. C&I Custom Value Use in Measure Implementation

This section defines the requirements for capturing Custom variables that can be used in place of defaults for select assumptions within the prescriptive measures defined in this statewide TRM. This approach is to be used when a variable in a measure formula can be replaced by a verifiable and documented value that is not presented in the TRM. This approach assumes that the algorithms presented in the measure are used as stated and only allows changes to certain variable values and is not a replacement algorithm for the measure. A custom variable is when customer input is provided to define the number or the value is measured at the site. Custom data values can also be supplied from product data of the measure installed. In certain cases the custom data can be provided from a documented study or report that is applicable to the measure. Custom variables and potential sources are clearly defined in the specific measures where “Actual” or “Custom” is noted.

* 1. Program Delivery & Baseline Definitions

The measure characterizations in this TRM are not grouped by program delivery type. As a result, the measure characterizations provided include information and assumptions to support savings calculations for the range of program delivery options commonly used for the measure. The organizational significance of this approach is that multiple baselines, incremental costs, O&M costs, measure lives and in-service rates are included in the measure characterization(s) that are delivered under two or more different program designs. Values appropriate for each given program delivery type are clearly specified in the algorithms or in look-up tables within the characterization.

Care has been taken to clearly define in the measure’s description the types of program delivery that the measure characterization is designed to support. However, there are no universally accepted definitions for a particular program type, and the description of the program type(s) may differ by measure. Nevertheless, program delivery types can be generally defined according to the following table. These are the definitions used in the measure descriptions, and, when necessary, individual measure descriptions may further refine and clarify these definitions of program delivery type.

**Table 1.3: Program Delivery Types**

| **Program** | **Attributes** |
| --- | --- |
| Time of Sale (TOS) | Definition: A program in which the customer is incented to purchase or install higher efficiency equipment than if the program had not existed. This may include retail rebate (coupon) programs, upstream buydown programs, online store programs or contractor based programs as examples.  Baseline = New equipment.  Efficient Case = New, premium efficiency equipment above federal and state codes and standard industry practice.  Example: CFL rebate |
| New Construction (NC) | Definition: A program that intervenes during building design to support the use of more-efficient equipment and construction practices.  Baseline = Building code or federal standards.  Efficient Case = The program’s level of building specification  Example: Building shell and mechanical measures |
| Retrofit (RF) | Definition: A program that upgrades existing equipment before the end of its useful life.  Baseline = Existing equipment or the existing condition of the building or equipment. A single baseline applies over the measure’s life.  Efficient Case = New, premium efficiency equipment above federal and state codes and standard industry practice.  Example: Air sealing and insulation |
| Early Replacement (EREP) | Definition: A program that replaces existing equipment before the end of its expected life.  Baseline = Dual; it begins as the existing equipment and shifts to new baseline equipment after the expected life of the existing equipment is over.  Efficient Case = New, premium efficiency equipment above federal and state codes and standard industry practice.  Example: Refrigerators, freezers |
| Early Retirement (ERET) | Definition: A program that retires duplicative equipment before its expected life is over.  Baseline = The existing equipment, which is retired and not replaced.  Efficient Case = Zero because the unit is retired.  Example: Appliance recycling |
| Direct Install (DI) | Definition: A program where measures are installed during a site visit.  Baseline = Existing equipment.  Efficient Case = New, premium efficiency equipment above federal and state codes and standard industry practice.  Example: Lighting and low-flow hot water measures |
| Efficiency Kits (KITS) | Definition: A program where measures are provided free of charge to a customer in an Efficiency Kit.  Baseline = Existing equipment.  Efficient Case = New, premium efficiency equipment above federal and state codes and standard industry practice.  Example: Lighting and low-flow hot water measures |

The concept and definition of the baseline is a key element of every measure characterization and is directly related to the program delivery type. Without a clear definition of the baseline, the savings algorithms cannot be adequately specified and subsequent evaluation efforts would be hampered. As a result, each measure has a detailed description (and in many cases, specification) of the specific baseline that should be used to calculate savings. Baselines in this TRM fall into one of the following four categories, and are organized within each measure characterization by the program delivery type to which it applies.

1. **Building Code:** As defined by the minimum specifications required under state energy code or applicable federal standards.
2. **Existing Equipment**: As determined by the most representative (or average) example of equipment that is in the existing stock. Existing equipment baselines apply over the equipment’s remaining useful life.
3. **New Equipment:** As determined by the equipment that represents standard practice in the current market environment. New equipment baselines apply over the effective useful life of the measure.
4. **Dual Baseline:** A baseline that begins as the existing equipment and shifts to new equipment after the expected life of the existing equipment is over.

# Assumptions

The information contained in this TRM contains VEIC’s recommendations for the content of the Illinois TRM. Sources that are cited within the TRM have been chosen based on two priorities, geography and age. Whenever possible and appropriate, VEIC has incorporated Illinois-specific information into each measure characterization. The Business TRM documents from Ameren and ComEd were reviewed, as well as program and measure specific data from evaluations, efficiency plans, and working documents.

The assumptions for these characterizations rest on our understanding of the information available. In each case, the available Illinois and Midwest-specific information was reviewed, including evaluations and support material provided by the Illinois Utilities.

When Illinois or region-specific evaluations or data were not available, best practice research and data from other jurisdictions was used, often from west and east-coast states that have allocated large amounts of funding to evaluation work and to refining their measure characterization parameters. As a result, much of the most-defensible information originates from these regions. In every case, VEIC used the most recent, well-designed, and best-supported studies and only if it was appropriate to generalize their conclusions to the Illinois programs.

## Footnotes & Documentation of Sources

Each new and updated measure characterization is supported by a work paper, which is posted to the SharePoint web site ([https://portal.veic.org](https://portal.veic.org/)).[[19]](#footnote-20) Both the work paper and the measure characterizations themselves use footnotes to document the references that have been used to characterize the technology. The reference documents are too numerous to include in an Appendix and have instead been posted to the TRM’s Sharepoint website. These files can be found in the ‘Sources and Reference Documents’ folder in the main directory, and may also be posted to the SAG’s public web site ([www.ilsag.info](http://www.ilsag.info)).

## General Savings Assumptions

The TRM savings estimates are expected to serve as average, representative values, or ways to calculate savings based on program-specific information. All information is presented on a per-measure basis. In using the measure-specific information in the TRM, it is helpful to keep the following notes in mind.

* All estimates of energy (kWh or therms) and peak (kW) savings are for first-year savings, not lifetime savings.
* Unless otherwise noted, measure life is defined to be the life of an energy consuming measure, including its equipment life and measure persistence.
* Where deemed values for savings are provided, they represent the average energy (kWh or therms) or peak (kW) savings that could be expected from the average of all measures that might be installed in Illinois in the program year.
* In general, the baselines included in the TRM are intended to represent average conditions in Illinois. Some are based on data from the state, such as household consumption characteristics provided by the Energy Information Administration. Some are extrapolated from other areas, when Illinois data are not available.

## Shifting Baseline Assumptions

The TRM anticipates the effects of changes in efficiency codes and standards on affected measures. When these changes take effect, a shift in the baseline is usually required. This complicates the measure savings estimation somewhat, and will be handled in future versions of the TRM by describing the choice of and reasoning behind a shifting baseline assumption. In this version of the TRM, this applies to CFLs and T5/T8 Linear Fluorescents, Furnaces and Early Replacement Measures.

### CFL and T5/T8 Linear Fluorescents Baseline Assumptions

Specific reductions in savings have been incorporated for CFL measures that relate to the shift in appropriate baseline due to changes in Federal Standards for lighting products. Federal legislation (stemming from the Energy Independence and Security Act of 2007) mandates a phase-in process beginning in 2012 for all general-purpose light bulbs between 40W and 100W to be approximately 30% more energy efficient than current incandescent bulbs, in essence beginning the phase-out of the current style, or “standard”, incandescent bulbs. In 2012, standard 100W incandescent bulbs will no longer be manufactured, followed by restrictions on standard 75W bulbs in 2013 and 60W and 40W bulbs in 2014. The baseline for the CFL measure in the corresponding program years starting June 1 each year will therefore become bulbs (improved or “efficient” incandescent, or halogen) that meet the new standard and have the same lumen equivalency. Those products can take several different forms we can envision now and perhaps others we do not yet know about. Halogens are one of those possibilities and have been chosen to represent a baseline at that time. To account for this shifting baseline, annual savings are reduced within the lifetime of the measure.

Other lighting measures will also have baseline shifts (for example screw based LED and CFL fixtures) that will result in significant impacts to annual estimated savings in later years. Finally, as of July 14, 2012, Federal Standards will require that practically all linear fluorescents meet strict performance requirements essentially requiring all T12 users, when they need to purchase new bulbs, to upgrade to high performance T8 lamps and ballasts[[20]](#footnote-21). We have assumed that this standard will become fully effective in 2016. To account for this, we have included a methodology to address the shifting baseline in the high performance T8 measure and T5 measure which is defined specifically in each measure characterization.

### Early Replacement Baseline Assumptions

A series of measures have an option to choose an Early Replacement Baseline. For these measures, the baseline assumption of the existing unit efficiency is based upon the average efficiency of units that were classified in Ameren’s PY3-PY4 as functioning and that meet efficiency and cost of replacement criteria in the following table.

Table 3.: Early Replacement Baseline Criteria[[21]](#footnote-22)

|  |  |  |
| --- | --- | --- |
| **Measure** | **Section** | **Criteria** |
| Air Source Heap Pump | 5.3.1 | SEER <=10 and cost of any repairs <$249 per ton |
| Central Air Conditioner | 5.3.3 | SEER <=10 and cost of any repairs <$190 per ton |
| Boiler | 5.3.6 | AFUE <= 75% and cost of any repairs <$709 |
| Furnace | 4.4.11, 5.3.7 | AFUE <= 75% and cost of any repairs <$528 |
| Ground Source Heat Pump | 5.3.8 | SEER <=10 and cost of any repairs <$249 per ton |

It is only appropriate to use these Early Replacement assumptions where these conditions are met. The TAC defined “functioning” as the unit is fully operational – providing sufficient space conditioning (i.e. heat exchanger, compressors, pumps work effectively) and/or the cost of repair is under 20% of the new baseline replacement cost. Therefore in order to apply early replacement assumptions the programs should apply the following eligibility criteria for the existing heating or cooling system in the home:

### Furnace Baseline

“The prior national standard for residential oil and gas furnaces was 78% AFUE. DOE raised the standard in 2007 to 80% AFUE, effective 2015. However, virtually all furnaces on the market have an AFUE of 80% or better, which prompted states and environmental and consumer groups to sue DOE over its 2007 decision. In April 2009, DOE accepted a “voluntary remand” in that litigation. In October 2009, manufacturers and efficiency advocates negotiated an agreement that, for the first time, included different standard levels in three climate regions: the North, South, and Southwest. DOE issued a direct final rule (DFR) in June 2011 reflecting the standard levels in the consensus agreement. The DFR became effective on October 25, 2011 establishing new standards: In the North, most furnaces will be required to have an AFUE of 90%.The 80% AFUE standard for the South and Southwest will remain unchanged at 80%. Oil furnaces will be required to have an AFUE of 83% in all three regions. The amended standards will become effective in May 2013 for non-weatherized furnaces and in January 2015 for weatherized furnaces. DOE estimates that the standards will save about 3.3 quads (quadrillion Btu) of energy over 30 years and yield a net present value of about $14 billion at a 3 percent discount rate.

Updat*e:*On January 14th, the U.S. Department of Energy (DOE) proposed to settle a lawsuit brought by the American Public Gas Association (APGA) that seeks to roll back gas furnace efficiency standards. As a result, the new standards, completed in 2011 and slated to take effect in May 2013, would be eliminated in favor of yet another round of DOE hearings and studies. Even if DOE completes a new rulemaking in two years, it's unlikely to take effect before 2020.”[[22]](#footnote-23)

As a result, each of the furnace measures contain the following language describing the baseline assumption.

“Although the current Federal Standard for gas furnaces is an AFUE rating of 78%, based upon review of available product in the AHRI database, the baseline efficiency for this characterization is assumed to be 80%. The baseline will be adjusted when the Federal Standard is updated.”[[23]](#footnote-24)

## Glossary

**Baseline Efficiency:** The assumed standard efficiency of equipment, absent an efficiency program.

**Building Types[[24]](#footnote-25):**

| **Building Type** | **Definition** |
| --- | --- |
| Assisted Living MultiFamily | Applies to residential buildings of three of more units with staff to assist the occupants. Gross Floor Area should include all fully-enclosed space within the exterior walls of the building(s) including individual rooms or units, wellness centers, exam rooms, community rooms, small shops or service areas for residents and visitors (e.g. hair salons, convenience stores), staff offices, lobbies, atriums, cafeterias, kitchens, storage areas, hallways, basements, stairways, corridors between buildings, and elevator shafts. |
| Auditorium/Assembly | Applies to any performance space such as a theater, arena, or hall. Gross Floor Area should include all space within the building(s), including seating, stage and backstage areas, food service areas, retail areas, rehearsal studios, administrative/office space, mechanical rooms, storage areas, elevator shafts, and stairwells. |
| College/University | Applies to facility space used for higher education. Relevant buildings include administrative headquarters, residence halls, athletic and recreation facilities, laboratories, etc. The total gross floor area should include all supporting functions such as kitchens used by staff, lobbies, atria, conference rooms and auditoria, fitness areas for staff, storage areas, stairways, elevator shafts, etc. |
| Convenience Store | Applies to facility space used for the retail sale of a limited selection of food and beverage products. The total gross floor area should include all supporting functions such as kitchens and break rooms used by staff, storage areas (refrigerated and non-refrigerated), and administrative areas. |
| Elementary School | Applies to a school serving children In any grades from Kindergarten through sixth grade. The total gross floor area should include all supporting functions such as administrative space, conference rooms, kitchens used by staff, lobbies, cafeterias, gymnasiums, auditoria, laboratory classrooms, portable classrooms,  greenhouses, stairways, atria, elevator shafts, small landscaping sheds, storage areas, etc. |
| Exterior | Applies to unconditioned spaces that are outside of the building envelope. |
| Garage | Applies to unconditioned spaces either attached or detached from the primary building envelope that are not used for living space. |
| Grocery | Applies to facility space used for the retail sale of food and beverage products. It should not be used by restaurants. The total gross floor area should include all supporting functions such as kitchens and break rooms used by staff, storage areas (refrigerated and non-refrigerated), administrative areas, stairwells, atria, lobbies, etc. |
| Healthcare Clinic | Applies to a facility space used to provide diagnosis and treatment for medical, dental, or psychiatric outpatient care. Gross Floor Area should include all space within the building(s) including offices, exam rooms, laboratories, lobbies, atriums, conference rooms and auditoriums, employee break rooms and kitchens, rest rooms, elevator shafts, stairways, mechanical rooms, and storage areas. |
| Heavy Industry | Heavy industry buildings are typically characterized by a plant that includes a main production area that has high-ceilings and contains heavy equipment used for assembly line production. These building types may be distinguished by categorizing NIACS (SIC) codes according to the needs of the Program Administrator. |
| High School/Middle School | Applies to facility space used as a school building for 7th through 12th grade students. This does not include college or university classroom facilities and laboratories, vocational, technical, or trade schools. The total gross floor area should include all supporting functions such as administrative space, conference rooms, kitchens used by staff, lobbies, cafeterias, gymnasiums, auditoria, laboratory classrooms, portable classrooms,  greenhouses, stairways, atria, elevator shafts, small landscaping sheds, storage areas, etc. |
| Hospital | Applies to a general medical and surgical hospital (including critical access hospitals and children’s hospitals) that is either a stand-alone building or a campus of buildings. Spaces more accurately characterized as a Healthcare Clinic should use that definition.  The definition of Hospital accounts for all space types that are located within the Hospital building/campus, such as medical offices, administrative offices, and skilled nursing.  The total floor area should include the aggregate floor area of all buildings on the campus as well as all supporting functions such as: stairways, connecting corridors between buildings, medical offices, exam rooms, laboratories, lobbies, atria, cafeterias, storage areas, elevator shafts, and any space affiliated with emergency medical care, or diagnostic care. |
| Hotel/Motel Combined  (All Spaces) | Applies to buildings that rent overnight accommodations on a room/suite basis, typically including a bath/shower and other facilities in guest rooms.  The total gross floor area should include all interior space, including guestrooms, halls, lobbies, atria, food preparation and restaurant space, conference and banquet space, health clubs/spas, indoor pool areas, and laundry facilities, as well as all space used for supporting functions such as elevator shafts, stairways, mechanical rooms, storage areas, employee break rooms, back-of-house offices, etc.  Hotel does not apply to fractional ownership properties such as condominiums or vacation timeshares.  Hotel properties should be owned by a single entity and have rooms available on a nightly basis. |
| Hotel/Motel Common Areas | All the common areas open to guests of the hotel such as the lobby, corridors and stairways, and other spaces that may have continuous or large lighting and HVAC hours. |
| Hotel/Motel Guest Room | Applies to the guest rooms of the hotel or motel. These spaces are occupied intermittantly. |
| Light Industry | Applies to buildings that are dedicated to manufacturing activities. Light industry buildings are characterized by consumer product and component manufacturing .These building types may be distinguished by categorizing NIACS (SIC) codes according to the needs of the Program Administrator. |
| Miscellaneous | Applies to spaces that do not fit clearly within any available categories should be designated as “miscellaneous”. |
| MedicalMultifamily-Mid Rise |  |
| Multifamily-High Rise Combined  (All Spaces) | Applies to residential buildings with five or more floors, including all public and multiuse spaces within the building envelope. Gross Floor Area should include all fully-enclosed space within the exterior walls of the building(s) including living space in each unit (including occupied and unoccupied units), interior common areas (e.g. lobbies, offices, community rooms, common kitchens, fitness rooms, indoor pools), hallways, stairwells, elevator shafts, connecting corridors between buildings, storage areas, and mechanical space such as a boiler room. Open air stairwells, breezeways, and other similar areas that are not fully-enclosed should not be included in the Gross Floor Area. |
| Multifamily-High Rise  Common Areas | All the common areas open to occupants of the building such as the lobby, corridors and stairways, and other spaces that may have continuous or high lighting and HVAC hours. |
| Multifamily-High Rise  Residential Units | Applies to the residential units in the building only. |
| MiscellaneousMovie Theater | Applies to buildings used for public or private film screenings. Gross Floor Area should include all space within the building(s), including seating areas, lobbies, concession stands, bathrooms, administrative/office space, mechanical rooms, storage areas, elevator shafts, and stairwells. |
| Office-Low Rise | Applies to facility spaces in buildings with four floors or fewer used for general office, professional, and administrative purposes. The total gross floor area should include all supporting functions such as kitchens used by staff, lobbies, atria, conference rooms and auditoria, fitness areas for staff, storage areas, stairways, elevator shafts, etc. |
| Office-Mid Rise | Applies to facility spaces in buildings with ffive to nine floors used for general office, professional, and administrative purposes. The total gross floor area should include all supporting functions such as kitchens used by staff, lobbies, atria, conference rooms and auditoria, fitness areas for staff, storage areas, stairways, elevator shafts, etc. |
| Office-High Rise | Applies to facility spaces in buildings with ten floors or more used for general office, professional, and administrative purposes. The total gross floor area should include all supporting functions such as kitchens used by staff, lobbies, atria, conference rooms and auditoria, fitness areas for staff, storage areas, stairways, elevator shafts, etc. |
| Religious Worhip/Church | Applies to buildings that are used as places of worship. This includes churches, temples, mosques, synagogues, meetinghouses, or any other buildings that primarily function as a place of religious worship. Gross Floor Area should include all areas inside the building that includes the primary worship area, including food preparation, community rooms, classrooms, and supporting areas such as restrooms, storage areas, hallways, and elevator shafts. |
| Restaurant | Applies to a subcategory of Retail/Service space that is used to provide commercial food services to individual customers, and includes kitchen, dining, and common areas. |
| Retail/Service-  Department store | Applies to facility space used to conduct the retail sale of consumer product goods.  Stores must be at least 30,000 square feet and have an exterior entrance to the public. The total gross floor area should include all supporting functions such as kitchens and break rooms used by staff, storage areas, administrative areas, elevators, stairwells, etc. Retail segments typically included under this definition are: Department Stores, Discount Stores, Supercenters, Warehouse Clubs, Drug Stores, Dollar Stores, Home Center/Hardware Stores, and Apparel/Hard Line Specialty Stores (e.g., books, clothing, office products, toys, home goods, electronics). Retail segments excluded under this definition are: Grocery, Convenience Stores, Automobile Dealerships, and Restaurants. |
| Retail/Service- Strip Mall | Applies to facility space used to conduct the retail sale of consumer product goods.  Stores must less than 30,000 square feet and have an exterior entrance to the public. The total gross floor area should include all supporting functions such as kitchens and break rooms used by staff, storage areas, administrative areas, elevators, stairwells, etc. Retail segments excluded under this definition are: Grocery, Convenience Stores, Automobile Dealerships, and Restaurants. |
| Warehouse | Applies to unrefrigerated or refrigerated buildings that are used to store goods, manufactured products, merchandise or raw materials. The total gross floor area of Refrigerated Warehouses should include all temperature controlled area designed to store perishable goods or merchandise under refrigeration at temperatures below 50 degrees Fahrenheit. The total gross floor area of Unrefrigerated Warehouses should include space designed to store non-perishable goods and merchandise. Unrefrigerated warehouses also include distribution centers. The total gross floor area of refrigerated and unrefrigerated warehouses should include all supporting functions such as offices, lobbies, stairways, rest rooms, equipment storage areas, elevator shafts, etc. Existing atriums or areas with high ceilings should only include the base floor area that they occupy. The total gross floor area of refrigerated or unrefrigerated warehouse should not include outside loading bays or docks. Self-storage facilities, or facilities that rent individual storage units, are not eligible for a rating using the warehouse model. |

**Coincidence** **Factor** (CF): Coincidence factors represent the fraction of connected load expected to be coincident with a particular system peak period, on a diversified basis. Coincidence factors are provided for summer peak periods.

**Commercial & Industrial:** The market sector that includes measures that apply to any of the building types defined in this TRM, which includes multifamily common areas and public housing[[25]](#footnote-26).

**Connected Load**: The maximum wattage of the equipment, under normal operating conditions.

**Deemed Value:** A value that has been assumed to be representative of the average condition of an input parameter.

**Default Value**: When a measure indicates that an input to a prescriptive saving algorithm may take on a range of values, an average value is also provided in many cases. This value is considered the default input to the algorithm, and should be used when the other alternatives listed in the measure are not applicable.

**End-use Category:** A general term used to describe the categories of equipment that provide a service to an individual or building. See Table 2.1.1 for a list of the end-use categories that are incorporated in this TRM.

**Energy Efficiency:** "Energy efficiency" means measures that reduce the amount of electricity or natural gas required to achieve a given end use. "Energy efficiency" also includes measures that reduce the total Btus of electricity and natural gas needed to meet the end use or uses (20 ILCS 3855/1-10). For purposes of this Section, "energy efficiency" means measures that reduce the amount of energy required to achieve a given end use. "Energy efficiency" also includes measures that reduce the total Btus of electricity and natural gas needed to meet the end use or uses (220 ILCS 5/8-104(b)).

**Equivalent Full Load Hours** (EFLH): The equivalent hours that equipment would need to operate at its peak capacity in order to consume its estimated annual kWh consumption (annual kWh/connected kW) or therms.

**High Efficiency**: General term for technologies and processes that require less energy, water, or other inputs to operate.

**Lifetime**: The number of years (or hours) that the new high efficiency equipment is expected to function. These are generally based on engineering lives, but sometimes adjusted based on expectations about frequency of removal, remodeling or demolition. Two important distinctions fall under this definition; Effective Useful Life (EUL) and Remaining Useful Life (RUL).

**EUL** – EUL is based on the manufacturers rating of the effective useful life; how long the equipment will last. For example, a CFL that operates x hours per year will typically have an EUL of y. A house boiler may have a lifetime of 20 years but the EUL is only 15 years since after that time it may be operating at a non-efficient point. An estimate of the median number of years that the measures installed under a program are still in place and operable.

**RUL** – Applies to retrofit or replacement measures.  For example, if an existing working refrigerator is replaced with a high efficiency unit, the RUL is an assumption of how many more years the existing unit would have lasted. As a general rule the RUL is usually assumed to be 1/3 of the EUL.

**Load Factor** (LF): The fraction of full load (wattage) for which the equipment is typically run.

**Measure Cost**: The incremental (for time of sale measures) or full cost (both capital and labor for retrofit measures) of implementing the High Efficiency equipment.

**Measure Description**: A detailed description of the technology and the criteria it must meet to be eligible as an energy efficient measure.

**Measure:** An efficient technology or procedure that results in energy savings as compared to the baseline efficiency.

**Residential:** The market sector that includes measures that apply only to detached, residential buildings or duplexes.

**Operation and Maintenance (O&M) Cost Adjustments:** The dollar impact resulting from differences between baseline and efficient case Operation and Maintenance costs.

**Operating Hours** (HOURS): The annual hours that equipment is expected to operate.

**Program:** The mode of delivering a particular measure or set of measures to customers. See Table 2.4 for a list of program descriptions that are presently operating in Illinois.

**Rating Period Factor** (RPF): Percentages for defined times of the year that describe when energy savings will be realized for a specific measure.

**Stakeholder Advisory Group (SAG):** The Illinois Energy Efficiency Stakeholder Advisory Group (SAG) was first defined in the electric utilities’ first energy efficiency Plan Orders to include “… the Utility, DCEO, Staff, the Attorney General, BOMA and CUB and representation from a variety of interests, including residential consumers, business consumers, environmental and energy advocacy organizations, trades and local government... [and] a representative from the ARES (alternative retail electric supplier) community should be included.”[[26]](#footnote-27) A group of stakeholders who have an interest in Illinois’ energy efficiency programs and who meet regularly to share information and work toward consensus on various energy efficiency issues. The Utilities in Illinois have been directed by the ICC to work with the SAG on the development of a statewide TRM.

**Table 3.2: Degree-Day Zones and Values by Market Sector**

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
|  | **Residential** | | **C&I** | |  |
| **Zone** | **HDD** | **CDD** | **HDD** | **CDD** | **Weather Station / City** |
| 1 | 5,352 | 820 | 4,272 | 2,173 | Rockford AP / Rockford |
| 2 | 5,113 | 842 | 4,029 | 2,181 | Chicago O'Hare AP / Chicago |
| 3 | 4,379 | 1,108 | 3,406 | 2,666 | Springfield #2 / Springfield |
| 4 | 3,378 | 1,570 | 2,515 | 3,358 | Belleville SIU RSCH / Belleville |
| 5 | 3,438 | 1,370 | 2,546 | 3,090 | Carbondale Southern IL AP / Marion |
| Average | 4,860 | 947 | 3,812 | 2,362 | Weighted by occupied housing units |
| Base Temp | 60F | 65F | 55F | 55F | Year climate normals, 1981-2010 |

## Electrical Loadshapes (kWh)

Loadshapes are an integral part of the measure characterization and are used to divide energy savings into appropriate periods using Rating Period Factors (RPFs) such that each have variable avoided cost values allocated to them for the purpose of estimating cost effectiveness.

For the purposes of assigning energy savings (kWh) periods, the TRM TAC has agreed to use the industry standards for wholesale power market transactions as shown in the following table.

Table 3.: On and Off Peak Energy Definitions

|  |  |
| --- | --- |
| **Period Category** | **Period Definition (Central Prevailing Time)** |
| Winter On-Peak Energy | 8AM - 11PM, weekdays, Oct – Apr, No NERC holidays |
| Winter Off-Peak Energy | All other hours |
| Summer On-Peak Energy | 8AM - 11PM, weekdays, May – Sept, No NERC holidays |
| Summer Off-Peak Energy | All other hours |

Loadshapes have been developed for each end-use by assigning Rating Period Factor percentages to each of the four periods above. Two methodologies were used:

1. Itron eShapes[[27]](#footnote-28) data for Missouri, reconciled to Illinois loads and provided by Ameren, were used to calculate the percentage of load in to the four categories above.
2. Where the Itron eShapes data did not provide a particular end-use or specific measure load profile, loadshapes that have been developed over many years by Efficiency Vermont and that have been reviewed by the Vermont Department of Public Service, were adjusted to match Illinois period definitions. Note – no weather sensitive loadshapes were based on this method. Any of these load profiles that relate to High Impact Measures should be an area of future evaluation.

The following pages provide the loadshape values for all measures provided in the TRM. To distinguish the source of the loadshape, they are color coded. Rows that are shaded in green are Efficiency Vermont loadshapes adjusted for Illinois periods. Rows that are unshaded and are left in white are Itron eShapes data provided by Ameren.

The Illinois electric utilities use the DSMore™ (Integral Analytics DSMore™ Demand Side Management Option/Risk Evaluator) software to screen the efficiency measures for cost effectiveness. Since this tool requires a loadshape value for weekdays and weekends in each month (i.e., 24 inputs), the percentages for the four period categories above were calculated by weighting the proportion of weekdays/weekends in each month to the total within each period. The results of these calculations are also provided below.

Table 3.: Loadshapes by Season

|  |  | Winter Peak | Winter  Off-peak | Summer  Peak | Summer  Off-peak |
| --- | --- | --- | --- | --- | --- |
|  | Loadshape Reference Number | Oct-Apr, M-F, non-holiday, 8AM - 11PM | Oct-Apr, All other time | May-Sept, M-F, non-holiday, 8AM - 11PM | May- Sept, All other time |
| Residential Clothes Washer | R01 | 47.0% | 11.1% | 34.0% | 8.0% |
| Residential Dish Washer | R02 | 49.3% | 8.7% | 35.7% | 6.3% |
| Residential Electric DHW | R03 | 43.2% | 20.6% | 24.5% | 11.7% |
| Residential Freezer | R04 | 38.9% | 16.4% | 31.5% | 13.2% |
| Residential Refrigerator | R05 | 37.0% | 18.1% | 30.1% | 14.7% |
| Residential Indoor Lighting | R06 | 48.1% | 15.5% | 26.0% | 10.5% |
| Residential Outdoor Lighting | R07 | 18.0% | 44.1% | 9.4% | 28.4% |
| Residential Cooling | R08 | 4.1% | 0.7% | 71.3% | 23.9% |
| Residential Electric Space Heat | R09 | 57.8% | 38.8% | 1.7% | 1.7% |
| Residential Electric Heating and Cooling | R10 | 35.2% | 22.8% | 31.0% | 11.0% |
| Residential Ventilation | R11 | 25.8% | 32.3% | 18.9% | 23.0% |
| Residential - Dehumidifier | R12 | 12.9% | 16.2% | 31.7% | 39.2% |
| Residential Standby Losses - Entertainment Center | R13 | 26.0% | 32.5% | 18.9% | 22.6% |
| Residential Standby Losses - Home Office | R14 | 23.9% | 34.6% | 17.0% | 24.5% |
|  |  |  |  |  |  |
| Commercial Electric Cooking | C01 | 40.6% | 18.2% | 28.7% | 12.6% |
| Commercial Electric DHW | C02 | 40.5% | 18.2% | 28.5% | 12.8% |
| Commercial Cooling | C03 | 4.9% | 0.8% | 66.4% | 27.9% |
| Commercial Electric Heating | C04 | 53.5% | 43.2% | 1.9% | 1.4% |
| Commercial Electric Heating and Cooling | C05 | 19.4% | 13.5% | 47.1% | 19.9% |
| Commercial Indoor Lighting | C06 | 40.1% | 18.6% | 28.4% | 12.9% |
| Grocery/Conv. Store Indoor Lighting | C07 | 31.4% | 26.4% | 22.8% | 19.3% |
| Hospital Indoor Lighting | C08 | 29.1% | 29.0% | 21.0% | 20.9% |
| Office Indoor Lighting | C09 | 42.1% | 16.0% | 30.4% | 11.5% |
| Restaurant Indoor Lighting | C10 | 32.1% | 25.7% | 23.4% | 18.8% |
| Retail Indoor Lighting | C11 | 35.5% | 22.3% | 25.8% | 16.3% |
| Warehouse Indoor Lighting | C12 | 39.4% | 18.5% | 28.6% | 13.5% |
| K-12 School Indoor Lighting | C13 | 45.8% | 22.6% | 20.2% | 11.4% |
| Indust. 1-shift (8/5) (e.g., comp. air, lights) | C14 | 50.5% | 7.2% | 37.0% | 5.3% |
| Indust. 2-shift (16/5) (e.g., comp. air, lights) | C15 | 47.5% | 10.2% | 34.8% | 7.4% |
| Indust. 3-shift (24/5) (e.g., comp. air, lights) | C16 | 34.8% | 23.2% | 25.5% | 16.6% |
| Indust. 4-shift (24/7) (e.g., comp. air, lights) | C17 | 25.8% | 32.3% | 18.9% | 23.0% |
| Industrial Indoor Lighting | C18 | 44.3% | 13.6% | 32.4% | 9.8% |
| Industrial Outdoor Lighting | C19 | 18.0% | 44.1% | 9.4% | 28.4% |
| Commercial Outdoor Lighting | C20 | 23.4% | 35.3% | 13.0% | 28.3% |
| Commercial Office Equipment | C21 | 37.7% | 20.9% | 26.7% | 14.7% |
| Commercial Refrigeration | C22 | 38.5% | 20.6% | 26.7% | 14.2% |
| Commercial Ventilation | C23 | 38.1% | 20.6% | 29.7% | 11.6% |
| Traffic Signal - Red Balls, always changing or flashing | C24 | 25.8% | 32.3% | 18.9% | 23.0% |
| Traffic Signal - Red Balls, changing day, off night | C25 | 37.0% | 20.9% | 27.1% | 14.9% |
| Traffic Signal - Green Balls, always changing | C26 | 25.8% | 32.3% | 18.9% | 23.0% |
| Traffic Signal - Green Balls, changing day, off night | C27 | 37.0% | 20.9% | 27.1% | 14.9% |
| Traffic Signal - Red Arrows | C28 | 25.8% | 32.3% | 18.9% | 23.0% |
| Traffic Signal - Green Arrows | C29 | 25.8% | 32.3% | 18.9% | 23.0% |
| Traffic Signal - Flashing Yellows | C30 | 25.8% | 32.3% | 18.9% | 23.0% |
| Traffic Signal - “Hand” Don’t Walk Signal | C31 | 25.8% | 32.3% | 18.9% | 23.0% |
| Traffic Signal - “Man” Walk Signal | C32 | 25.8% | 32.3% | 18.9% | 23.0% |
| Traffic Signal - Bi-Modal Walk/Don’t Walk | C33 | 25.8% | 32.3% | 18.9% | 23.0% |
| Industrial Motor | C34 | 47.5% | 10.2% | 34.8% | 7.4% |
| Industrial Process | C35 | 47.5% | 10.2% | 34.8% | 7.4% |
| HVAC Pump Motor (heating) | C36 | 38.7% | 48.6% | 5.9% | 6.8% |
| HVAC Pump Motor (cooling) | C37 | 7.8% | 9.8% | 36.8% | 45.6% |
| HVAC Pump Motor (unknown use) | C38 | 23.2% | 29.2% | 21.4% | 26.2% |
| VFD - Supply fans <10 HP | C39 | 38.8% | 16.1% | 28.4% | 16.7% |
| VFD - Return fans <10 HP | C40 | 38.8% | 16.1% | 28.4% | 16.7% |
| VFD - Exhaust fans <10 HP | C41 | 34.8% | 23.2% | 20.3% | 21.7% |
| VFD - Boiler feedwater pumps <10 HP | C42 | 42.9% | 44.2% | 6.6% | 6.3% |
| VFD - Chilled water pumps <10 HP | C43 | 11.2% | 5.5% | 40.7% | 42.6% |
| VFD Boiler circulation pumps <10 HP | C44 | 42.9% | 44.2% | 6.6% | 6.3% |
| Refrigeration Economizer | C45 | 36.3% | 50.8% | 5.6% | 7.3% |
| Evaporator Fan Control | C46 | 24.0% | 35.9% | 16.7% | 23.4% |
| Standby Losses - Commercial Office | C47 | 8.2% | 50.5% | 5.6% | 35.7% |
| VFD Boiler draft fans <10 HP | C48 | 37.3% | 48.9% | 6.4% | 7.3% |
| VFD Cooling Tower Fans <10 HP | C49 | 7.9% | 5.2% | 54.0% | 32.9% |
| Engine Block Heater Timer | C50 | 26.5% | 61.0% | 4.1% | 8.5% |
| Door Heater Control | C51 | 30.4% | 69.6% | 0.0% | 0.0% |
| Beverage and Snack Machine Controls | C52 | 10.0% | 48.3% | 7.4% | 34.3% |
| Flat | C53 | 36.3% | 21.8% | 26.2% | 15.7% |
| Religious Indoor Lighting | C54 | 26.8% | 31.4% | 18.9% | 22.8% |

Table 3.: Loadshapes by Month and Day of Week

|  |  | Jan | | Feb | | Mar | | Apr | | May | | Jun | | Jul | | Aug | | Sep | | Oct | | Nov | | Dec | |
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
|  | M-F | S-S | M-F | S-S | M-F | S-S | M-F | S-S | M-F | S-S | M-F | S-S | M-F | S-S | M-F | S-S | M-F | S-S | M-F | S-S | M-F | S-S | M-F | S-S | |
| Residential Clothes Washer | R01 | 7.0% | 1.6% | 6.3% | 1.5% | 6.6% | 1.7% | 6.7% | 1.5% | 6.9% | 1.6% | 6.5% | 1.6% | 7.1% | 1.5% | 6.8% | 1.7% | 6.6% | 1.6% | 7.0% | 1.5% | 6.5% | 1.7% | 6.9% | 1.6% | |
| Residential Dish Washer | R02 | 7.3% | 1.2% | 6.6% | 1.2% | 7.0% | 1.4% | 7.1% | 1.2% | 7.3% | 1.2% | 6.9% | 1.3% | 7.4% | 1.2% | 7.1% | 1.3% | 7.0% | 1.2% | 7.4% | 1.2% | 6.8% | 1.3% | 7.2% | 1.3% | |
| Residential Electric DHW | R03 | 6.4% | 2.9% | 5.8% | 2.7% | 6.1% | 3.3% | 6.2% | 2.8% | 5.0% | 2.3% | 4.7% | 2.4% | 5.1% | 2.2% | 4.9% | 2.5% | 4.8% | 2.3% | 6.5% | 2.8% | 6.0% | 3.1% | 6.3% | 3.0% | |
| Residential Freezer | R04 | 5.8% | 2.3% | 5.2% | 2.2% | 5.5% | 2.6% | 5.6% | 2.2% | 6.4% | 2.6% | 6.1% | 2.7% | 6.6% | 2.5% | 6.3% | 2.8% | 6.1% | 2.6% | 5.8% | 2.2% | 5.4% | 2.4% | 5.7% | 2.4% | |
| Residential Refrigerator | R05 | 5.5% | 2.6% | 4.9% | 2.4% | 5.2% | 2.9% | 5.3% | 2.5% | 6.2% | 2.9% | 5.8% | 3.0% | 6.3% | 2.8% | 6.0% | 3.1% | 5.9% | 2.9% | 5.5% | 2.5% | 5.1% | 2.7% | 5.4% | 2.6% | |
| Residential Indoor Lighting | R06 | 7.1% | 2.2% | 6.4% | 2.1% | 6.8% | 2.4% | 6.9% | 2.1% | 5.3% | 2.1% | 5.0% | 2.2% | 5.4% | 2.0% | 5.2% | 2.2% | 5.1% | 2.1% | 7.2% | 2.1% | 6.6% | 2.3% | 7.0% | 2.2% | |
| Residential Outdoor Lighting | R07 | 2.7% | 6.2% | 2.4% | 5.9% | 2.6% | 7.0% | 2.6% | 6.0% | 1.9% | 5.7% | 1.8% | 5.8% | 2.0% | 5.3% | 1.9% | 6.0% | 1.8% | 5.7% | 2.7% | 6.0% | 2.5% | 6.6% | 2.6% | 6.4% | |
| Residential Cooling | R08 | 0.6% | 0.1% | 0.5% | 0.1% | 0.6% | 0.1% | 0.6% | 0.1% | 14.6% | 4.8% | 13.7% | 4.9% | 14.9% | 4.5% | 14.2% | 5.0% | 13.9% | 4.8% | 0.6% | 0.1% | 0.6% | 0.1% | 0.6% | 0.1% | |
| Residential Electric Space Heat | R09 | 8.6% | 5.5% | 7.7% | 5.1% | 8.2% | 6.1% | 8.3% | 5.3% | 0.3% | 0.3% | 0.3% | 0.3% | 0.4% | 0.3% | 0.3% | 0.4% | 0.3% | 0.3% | 8.7% | 5.3% | 8.0% | 5.8% | 8.5% | 5.6% | |
| Residential Electric Heating and Cooling | R10 | 5.2% | 3.2% | 4.7% | 3.0% | 5.0% | 3.6% | 5.0% | 3.1% | 6.3% | 2.2% | 6.0% | 2.3% | 6.5% | 2.1% | 6.2% | 2.3% | 6.0% | 2.2% | 5.3% | 3.1% | 4.9% | 3.4% | 5.2% | 3.3% | |
| Residential Ventilation | R11 | 3.8% | 4.6% | 3.4% | 4.3% | 3.6% | 5.1% | 3.7% | 4.4% | 3.8% | 4.6% | 3.6% | 4.7% | 3.9% | 4.3% | 3.8% | 4.8% | 3.7% | 4.6% | 3.9% | 4.4% | 3.6% | 4.8% | 3.8% | 4.7% | |
| Residential - Dehumidifier | R12 | 1.9% | 2.3% | 1.7% | 2.2% | 1.8% | 2.6% | 1.8% | 2.2% | 6.5% | 7.8% | 6.1% | 8.0% | 6.6% | 7.3% | 6.3% | 8.2% | 6.2% | 7.8% | 1.9% | 2.2% | 1.8% | 2.4% | 1.9% | 2.4% | |
| Residential Standby Losses - Entertainment Center | R13 | 3.8% | 4.6% | 3.5% | 4.3% | 3.7% | 5.1% | 3.7% | 4.4% | 3.9% | 4.5% | 3.7% | 4.6% | 4.0% | 4.2% | 3.8% | 4.8% | 3.7% | 4.5% | 3.9% | 4.4% | 3.6% | 4.8% | 3.8% | 4.7% | |
| Residential Standby Losses - Home Office | R14 | 3.5% | 4.9% | 3.2% | 4.6% | 3.4% | 5.5% | 3.4% | 4.7% | 3.5% | 4.9% | 3.3% | 5.0% | 3.5% | 4.6% | 3.4% | 5.2% | 3.3% | 4.9% | 3.6% | 4.7% | 3.3% | 5.2% | 3.5% | 5.0% | |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | |
| Commercial Electric Cooking | C01 | 6.0% | 2.6% | 5.4% | 2.4% | 5.7% | 2.9% | 5.8% | 2.5% | 5.9% | 2.5% | 5.5% | 2.6% | 6.0% | 2.4% | 5.7% | 2.6% | 5.6% | 2.5% | 6.1% | 2.5% | 5.6% | 2.7% | 5.9% | 2.6% | |
| Commercial Electric DHW | C02 | 6.0% | 2.6% | 5.4% | 2.4% | 5.7% | 2.9% | 5.8% | 2.5% | 5.8% | 2.5% | 5.5% | 2.6% | 6.0% | 2.4% | 5.7% | 2.7% | 5.6% | 2.5% | 6.1% | 2.5% | 5.6% | 2.7% | 5.9% | 2.6% | |
| Commercial Cooling | C03 | 0.7% | 0.1% | 0.6% | 0.1% | 0.7% | 0.1% | 0.7% | 0.1% | 13.6% | 5.5% | 12.8% | 5.7% | 13.9% | 5.2% | 13.3% | 5.9% | 13.0% | 5.5% | 0.7% | 0.1% | 0.7% | 0.1% | 0.7% | 0.1% | |
| Commercial Electric Heating | C04 | 7.9% | 6.1% | 7.1% | 5.7% | 7.6% | 6.8% | 7.7% | 5.9% | 0.4% | 0.3% | 0.4% | 0.3% | 0.4% | 0.3% | 0.4% | 0.3% | 0.4% | 0.3% | 8.0% | 5.9% | 7.4% | 6.5% | 7.8% | 6.3% | |
| Commercial Electric Heating and Cooling | C05 | 2.9% | 1.9% | 2.6% | 1.8% | 2.8% | 2.1% | 2.8% | 1.9% | 9.6% | 4.0% | 9.1% | 4.1% | 9.8% | 3.7% | 9.4% | 4.2% | 9.2% | 4.0% | 2.9% | 1.9% | 2.7% | 2.0% | 2.8% | 2.0% | |
| Commercial Indoor Lighting | C06 | 5.9% | 2.6% | 5.3% | 2.5% | 5.7% | 2.9% | 5.7% | 2.6% | 5.8% | 2.6% | 5.5% | 2.6% | 5.9% | 2.4% | 5.7% | 2.7% | 5.5% | 2.6% | 6.0% | 2.6% | 5.5% | 2.8% | 5.9% | 2.7% | |
| Grocery/Conv. Store Indoor Lighting | C07 | 4.7% | 3.7% | 4.2% | 3.5% | 4.4% | 4.2% | 4.5% | 3.6% | 4.7% | 3.8% | 4.4% | 3.9% | 4.8% | 3.6% | 4.6% | 4.1% | 4.5% | 3.8% | 4.7% | 3.6% | 4.3% | 3.9% | 4.6% | 3.8% | |
| Hospital Indoor Lighting | C08 | 4.3% | 4.1% | 3.9% | 3.8% | 4.1% | 4.6% | 4.2% | 4.0% | 4.3% | 4.2% | 4.0% | 4.3% | 4.4% | 3.9% | 4.2% | 4.4% | 4.1% | 4.2% | 4.4% | 4.0% | 4.0% | 4.3% | 4.3% | 4.2% | |
| Office Indoor Lighting | C09 | 6.2% | 2.3% | 5.6% | 2.1% | 6.0% | 2.5% | 6.0% | 2.2% | 6.2% | 2.3% | 5.9% | 2.4% | 6.4% | 2.2% | 6.1% | 2.4% | 5.9% | 2.3% | 6.3% | 2.2% | 5.8% | 2.4% | 6.2% | 2.3% | |
| Restaurant Indoor Lighting | C10 | 4.8% | 3.6% | 4.3% | 3.4% | 4.5% | 4.1% | 4.6% | 3.5% | 4.8% | 3.7% | 4.5% | 3.8% | 4.9% | 3.5% | 4.7% | 4.0% | 4.6% | 3.7% | 4.8% | 3.5% | 4.4% | 3.8% | 4.7% | 3.7% | |
| Retail Indoor Lighting | C11 | 5.3% | 3.1% | 4.7% | 3.0% | 5.0% | 3.5% | 5.1% | 3.1% | 5.3% | 3.2% | 5.0% | 3.3% | 5.4% | 3.1% | 5.2% | 3.4% | 5.0% | 3.2% | 5.3% | 3.1% | 4.9% | 3.3% | 5.2% | 3.2% | |
| Warehouse Indoor Lighting | C12 | 5.8% | 2.6% | 5.2% | 2.5% | 5.6% | 2.9% | 5.6% | 2.5% | 5.8% | 2.7% | 5.5% | 2.8% | 6.0% | 2.5% | 5.7% | 2.8% | 5.6% | 2.7% | 5.9% | 2.5% | 5.4% | 2.8% | 5.8% | 2.7% | |
| K-12 School Indoor Lighting | C13 | 6.8% | 3.2% | 6.1% | 3.0% | 6.5% | 3.6% | 6.6% | 3.1% | 4.1% | 2.3% | 3.9% | 2.3% | 4.2% | 2.1% | 4.0% | 2.4% | 3.9% | 2.3% | 6.9% | 3.1% | 6.3% | 3.4% | 6.7% | 3.3% | |
| Indust. 1-shift (8/5) (e.g., comp. air, lights) | C14 | 7.5% | 1.0% | 6.7% | 1.0% | 7.1% | 1.1% | 7.2% | 1.0% | 7.5% | 1.1% | 7.1% | 1.1% | 7.7% | 1.0% | 7.4% | 1.1% | 7.2% | 1.1% | 7.6% | 1.0% | 7.0% | 1.1% | 7.4% | 1.0% | |
| Indust. 2-shift (16/5) (e.g., comp. air, lights) | C15 | 7.0% | 1.4% | 6.3% | 1.4% | 6.7% | 1.6% | 6.8% | 1.4% | 7.1% | 1.5% | 6.7% | 1.5% | 7.3% | 1.4% | 6.9% | 1.6% | 6.8% | 1.5% | 7.1% | 1.4% | 6.6% | 1.5% | 7.0% | 1.5% | |
| Indust. 3-shift (24/5) (e.g., comp. air, lights) | C16 | 5.1% | 3.3% | 4.6% | 3.1% | 4.9% | 3.7% | 5.0% | 3.2% | 5.2% | 3.3% | 4.9% | 3.4% | 5.3% | 3.1% | 5.1% | 3.5% | 5.0% | 3.3% | 5.2% | 3.2% | 4.8% | 3.5% | 5.1% | 3.4% | |
| Indust. 4-shift (24/7) (e.g., comp. air, lights) | C17 | 3.8% | 4.6% | 3.4% | 4.3% | 3.6% | 5.1% | 3.7% | 4.4% | 3.8% | 4.6% | 3.6% | 4.7% | 3.9% | 4.3% | 3.8% | 4.8% | 3.7% | 4.6% | 3.9% | 4.4% | 3.6% | 4.8% | 3.8% | 4.7% | |
| Industrial Indoor Lighting | C18 | 6.6% | 1.9% | 5.9% | 1.8% | 6.3% | 2.1% | 6.3% | 1.9% | 6.6% | 1.9% | 6.2% | 2.0% | 6.8% | 1.8% | 6.5% | 2.0% | 6.3% | 1.9% | 6.6% | 1.9% | 6.1% | 2.0% | 6.5% | 2.0% | |
| Industrial Outdoor Lighting | C19 | 2.7% | 6.2% | 2.4% | 5.9% | 2.6% | 7.0% | 2.6% | 6.0% | 1.9% | 5.7% | 1.8% | 5.8% | 2.0% | 5.3% | 1.9% | 6.0% | 1.8% | 5.7% | 2.7% | 6.0% | 2.5% | 6.6% | 2.6% | 6.4% | |
| Commercial Outdoor Lighting | C20 | 3.5% | 5.0% | 3.1% | 4.7% | 3.3% | 5.6% | 3.3% | 4.8% | 2.7% | 5.6% | 2.5% | 5.8% | 2.7% | 5.3% | 2.6% | 5.9% | 2.5% | 5.6% | 3.5% | 4.8% | 3.2% | 5.3% | 3.4% | 5.1% | |
| Commercial Office Equipment | C21 | 5.6% | 3.0% | 5.0% | 2.8% | 5.3% | 3.3% | 5.4% | 2.9% | 5.4% | 2.9% | 5.1% | 3.0% | 5.6% | 2.7% | 5.3% | 3.1% | 5.2% | 2.9% | 5.6% | 2.9% | 5.2% | 3.1% | 5.5% | 3.0% | |
| Commercial Refrigeration | C22 | 5.7% | 2.9% | 5.1% | 2.7% | 5.4% | 3.2% | 5.5% | 2.8% | 5.5% | 2.8% | 5.1% | 2.9% | 5.6% | 2.7% | 5.3% | 3.0% | 5.2% | 2.8% | 5.8% | 2.8% | 5.3% | 3.1% | 5.6% | 3.0% | |
| Commercial Ventilation | C23 | 5.6% | 2.9% | 5.1% | 2.7% | 5.4% | 3.3% | 5.4% | 2.8% | 6.1% | 2.3% | 5.7% | 2.4% | 6.2% | 2.2% | 5.9% | 2.4% | 5.8% | 2.3% | 5.7% | 2.8% | 5.3% | 3.1% | 5.6% | 3.0% | |
| Traffic Signal - Red Balls, always changing or flashing | C24 | 3.8% | 4.6% | 3.4% | 4.3% | 3.6% | 5.1% | 3.7% | 4.4% | 3.8% | 4.6% | 3.6% | 4.7% | 3.9% | 4.3% | 3.8% | 4.8% | 3.7% | 4.6% | 3.9% | 4.4% | 3.6% | 4.8% | 3.8% | 4.7% | |
| Traffic Signal - Red Balls, changing day, off night | C25 | 5.5% | 2.9% | 4.9% | 2.8% | 5.2% | 3.3% | 5.3% | 2.9% | 5.5% | 3.0% | 5.2% | 3.1% | 5.7% | 2.8% | 5.4% | 3.1% | 5.3% | 3.0% | 5.5% | 2.9% | 5.1% | 3.1% | 5.4% | 3.0% | |
| Traffic Signal - Green Balls, always changing | C26 | 3.8% | 4.6% | 3.4% | 4.3% | 3.6% | 5.1% | 3.7% | 4.4% | 3.8% | 4.6% | 3.6% | 4.7% | 3.9% | 4.3% | 3.8% | 4.8% | 3.7% | 4.6% | 3.9% | 4.4% | 3.6% | 4.8% | 3.8% | 4.7% | |
| Traffic Signal - Green Balls, changing day, off night | C27 | 5.5% | 2.9% | 4.9% | 2.8% | 5.2% | 3.3% | 5.3% | 2.9% | 5.5% | 3.0% | 5.2% | 3.1% | 5.7% | 2.8% | 5.4% | 3.1% | 5.3% | 3.0% | 5.5% | 2.9% | 5.1% | 3.1% | 5.4% | 3.0% | |
| Traffic Signal - Red Arrows | C28 | 3.8% | 4.6% | 3.4% | 4.3% | 3.6% | 5.1% | 3.7% | 4.4% | 3.8% | 4.6% | 3.6% | 4.7% | 3.9% | 4.3% | 3.8% | 4.8% | 3.7% | 4.6% | 3.9% | 4.4% | 3.6% | 4.8% | 3.8% | 4.7% | |
| Traffic Signal - Green Arrows | C29 | 3.8% | 4.6% | 3.4% | 4.3% | 3.6% | 5.1% | 3.7% | 4.4% | 3.8% | 4.6% | 3.6% | 4.7% | 3.9% | 4.3% | 3.8% | 4.8% | 3.7% | 4.6% | 3.9% | 4.4% | 3.6% | 4.8% | 3.8% | 4.7% | |
| Traffic Signal - Flashing Yellows | C30 | 3.8% | 4.6% | 3.4% | 4.3% | 3.6% | 5.1% | 3.7% | 4.4% | 3.8% | 4.6% | 3.6% | 4.7% | 3.9% | 4.3% | 3.8% | 4.8% | 3.7% | 4.6% | 3.9% | 4.4% | 3.6% | 4.8% | 3.8% | 4.7% | |
| Traffic Signal - “Hand” Don’t Walk Signal | C31 | 3.8% | 4.6% | 3.4% | 4.3% | 3.6% | 5.1% | 3.7% | 4.4% | 3.8% | 4.6% | 3.6% | 4.7% | 3.9% | 4.3% | 3.8% | 4.8% | 3.7% | 4.6% | 3.9% | 4.4% | 3.6% | 4.8% | 3.8% | 4.7% | |
| Traffic Signal - “Man” Walk Signal | C32 | 3.8% | 4.6% | 3.4% | 4.3% | 3.6% | 5.1% | 3.7% | 4.4% | 3.8% | 4.6% | 3.6% | 4.7% | 3.9% | 4.3% | 3.8% | 4.8% | 3.7% | 4.6% | 3.9% | 4.4% | 3.6% | 4.8% | 3.8% | 4.7% | |
| Traffic Signal - Bi-Modal Walk/Don’t Walk | C33 | 3.8% | 4.6% | 3.4% | 4.3% | 3.6% | 5.1% | 3.7% | 4.4% | 3.8% | 4.6% | 3.6% | 4.7% | 3.9% | 4.3% | 3.8% | 4.8% | 3.7% | 4.6% | 3.9% | 4.4% | 3.6% | 4.8% | 3.8% | 4.7% | |
| Industrial Motor | C34 | 7.0% | 1.4% | 6.3% | 1.4% | 6.7% | 1.6% | 6.8% | 1.4% | 7.1% | 1.5% | 6.7% | 1.5% | 7.3% | 1.4% | 6.9% | 1.6% | 6.8% | 1.5% | 7.1% | 1.4% | 6.6% | 1.5% | 7.0% | 1.5% | |
| Industrial Process | C35 | 7.0% | 1.4% | 6.3% | 1.4% | 6.7% | 1.6% | 6.8% | 1.4% | 7.1% | 1.5% | 6.7% | 1.5% | 7.3% | 1.4% | 6.9% | 1.6% | 6.8% | 1.5% | 7.1% | 1.4% | 6.6% | 1.5% | 7.0% | 1.5% | |
| HVAC Pump Motor (heating) | C36 | 5.7% | 6.9% | 5.2% | 6.4% | 5.5% | 7.7% | 5.5% | 6.6% | 1.2% | 1.4% | 1.1% | 1.4% | 1.2% | 1.3% | 1.2% | 1.4% | 1.2% | 1.4% | 5.8% | 6.6% | 5.3% | 7.3% | 5.7% | 7.1% | |
| HVAC Pump Motor (cooling) | C37 | 1.2% | 1.4% | 1.0% | 1.3% | 1.1% | 1.5% | 1.1% | 1.3% | 7.5% | 9.1% | 7.1% | 9.3% | 7.7% | 8.5% | 7.3% | 9.6% | 7.2% | 9.1% | 1.2% | 1.3% | 1.1% | 1.5% | 1.1% | 1.4% | |
| HVAC Pump Motor (unknown use) | C38 | 3.4% | 4.1% | 3.1% | 3.9% | 3.3% | 4.6% | 3.3% | 4.0% | 4.4% | 5.2% | 4.1% | 5.4% | 4.5% | 4.9% | 4.3% | 5.5% | 4.2% | 5.2% | 3.5% | 4.0% | 3.2% | 4.4% | 3.4% | 4.2% | |
| VFD - Supply fans <10 HP | C39 | 5.7% | 2.3% | 5.2% | 2.1% | 5.5% | 2.5% | 5.6% | 2.2% | 5.8% | 3.3% | 5.5% | 3.4% | 5.9% | 3.1% | 5.7% | 3.5% | 5.5% | 3.3% | 5.8% | 2.2% | 5.4% | 2.4% | 5.7% | 2.3% | |
| VFD - Return fans <10 HP | C40 | 5.7% | 2.3% | 5.2% | 2.1% | 5.5% | 2.5% | 5.6% | 2.2% | 5.8% | 3.3% | 5.5% | 3.4% | 5.9% | 3.1% | 5.7% | 3.5% | 5.5% | 3.3% | 5.8% | 2.2% | 5.4% | 2.4% | 5.7% | 2.3% | |
| VFD - Exhaust fans <10 HP | C41 | 5.1% | 3.3% | 4.6% | 3.1% | 4.9% | 3.7% | 5.0% | 3.2% | 4.1% | 4.3% | 3.9% | 4.4% | 4.2% | 4.1% | 4.1% | 4.6% | 4.0% | 4.3% | 5.2% | 3.2% | 4.8% | 3.5% | 5.1% | 3.4% | |
| VFD - Boiler feedwater pumps <10 HP | C42 | 6.4% | 6.2% | 5.7% | 5.9% | 6.1% | 7.0% | 6.1% | 6.0% | 1.3% | 1.3% | 1.3% | 1.3% | 1.4% | 1.2% | 1.3% | 1.3% | 1.3% | 1.3% | 6.4% | 6.0% | 5.9% | 6.6% | 6.3% | 6.4% | |
| VFD - Chilled water pumps <10 HP | C43 | 1.7% | 0.8% | 1.5% | 0.7% | 1.6% | 0.9% | 1.6% | 0.8% | 8.3% | 8.5% | 7.8% | 8.7% | 8.5% | 8.0% | 8.1% | 8.9% | 7.9% | 8.5% | 1.7% | 0.8% | 1.6% | 0.8% | 1.6% | 0.8% | |
| VFD Boiler circulation pumps <10 HP | C44 | 6.4% | 6.2% | 5.7% | 5.9% | 6.1% | 7.0% | 6.1% | 6.0% | 1.3% | 1.3% | 1.3% | 1.3% | 1.4% | 1.2% | 1.3% | 1.3% | 1.3% | 1.3% | 6.4% | 6.0% | 5.9% | 6.6% | 6.3% | 6.4% | |
| Refrigeration Economizer | C45 | 5.4% | 7.2% | 4.8% | 6.7% | 5.1% | 8.0% | 5.2% | 7.0% | 1.1% | 1.5% | 1.1% | 1.5% | 1.2% | 1.4% | 1.1% | 1.5% | 1.1% | 1.5% | 5.4% | 7.0% | 5.0% | 7.6% | 5.3% | 7.4% | |
| Evaporator Fan Control | C46 | 3.6% | 5.1% | 3.2% | 4.8% | 3.4% | 5.7% | 3.4% | 4.9% | 3.4% | 4.7% | 3.2% | 4.8% | 3.5% | 4.4% | 3.3% | 4.9% | 3.3% | 4.7% | 3.6% | 4.9% | 3.3% | 5.4% | 3.5% | 5.2% | |
| Standby Losses - Commercial Office | C47 | 1.2% | 7.1% | 1.1% | 6.7% | 1.2% | 8.0% | 1.2% | 6.9% | 1.1% | 7.1% | 1.1% | 7.3% | 1.2% | 6.7% | 1.1% | 7.5% | 1.1% | 7.1% | 1.2% | 6.9% | 1.1% | 7.5% | 1.2% | 7.3% | |
| VFD Boiler draft fans <10 HP | C48 | 5.5% | 6.9% | 5.0% | 6.5% | 5.3% | 7.7% | 5.3% | 6.7% | 1.3% | 1.5% | 1.2% | 1.5% | 1.3% | 1.4% | 1.3% | 1.5% | 1.2% | 1.5% | 5.6% | 6.7% | 5.2% | 7.3% | 5.5% | 7.1% | |
| VFD Cooling Tower Fans <10 HP | C49 | 1.2% | 0.7% | 1.1% | 0.7% | 1.1% | 0.8% | 1.1% | 0.7% | 11.0% | 6.5% | 10.4% | 6.7% | 11.3% | 6.2% | 10.8% | 6.9% | 10.5% | 6.5% | 1.2% | 0.7% | 1.1% | 0.8% | 1.2% | 0.8% | |
| Engine Block Heater Timer | C50 | 3.9% | 8.6% | 3.5% | 8.1% | 3.7% | 9.6% | 3.8% | 8.3% | 0.8% | 1.7% | 0.8% | 1.7% | 0.8% | 1.6% | 0.8% | 1.8% | 0.8% | 1.7% | 4.0% | 8.3% | 3.7% | 9.1% | 3.9% | 8.9% | |
| Door Heater Control | C51 | 4.5% | 9.8% | 4.0% | 9.2% | 4.3% | 11.0% | 4.3% | 9.5% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 4.5% | 9.5% | 4.2% | 10.4% | 4.4% | 10.1% | |
| Beverage and Snack Machine Controls | C52 | 1.5% | 6.8% | 1.3% | 6.4% | 1.4% | 7.6% | 1.4% | 6.6% | 1.5% | 6.8% | 1.4% | 7.0% | 1.5% | 6.4% | 1.5% | 7.2% | 1.4% | 6.8% | 1.5% | 6.6% | 1.4% | 7.2% | 1.5% | 7.0% | |
| Flat | C53 | 5.4% | 3.1% | 4.8% | 2.9% | 5.1% | 3.4% | 5.2% | 3.0% | 5.3% | 3.1% | 5.0% | 3.2% | 5.5% | 2.9% | 5.2% | 3.3% | 5.1% | 3.1% | 5.4% | 3.0% | 5.0% | 3.3% | 5.3% | 3.2% | |
| Religious Indoor Lighting | C54 | 4.0% | 4.4% | 3.6% | 4.2% | 3.8% | 5.0% | 3.8% | 4.3% | 3.9% | 4.5% | 3.6% | 4.7% | 3.9% | 4.3% | 3.8% | 4.8% | 3.7% | 4.5% | 4.0% | 4.3% | 3.7% | 4.7% | 3.9% | 4.6% | |

## Summer Peak Period Definition (kW)

To estimate the impact that an efficiency measure has on a utility’s system peak, the peak itself needs to be defined. Illinois spans two different electrical control areas, the Pennsylvania – Jersey – Maryland (PJM) and the Midwest Independent System Operators (MISO). As a result, there is some disparity in the peak definition across the state. However, only PJM has a forward capacity market where an efficiency program can potentially participate. Because ComEd is part of the PJM control area, their definition of summer peak is being applied statewide in this TRM.

Because Illinois is a summer peaking state, only the summer peak period is defined for the purpose of this TRM. The coincident summer peak period is defined as 1:00-5:00 pm Central Prevailing Time on non-holiday weekdays, June through August.

Summer peak coincidence factors can be found within each measure characterization. The source is provided and is based upon evaluation results, analysis of load shape data (e.g., the Itron eShapes data provided by Ameren), or through a calculation using stated assumptions.

For measures that are not weather-sensitive, the summer peak coincidence factor is estimated whenever possible as the average of savings within the peak period defined above. For weather sensitive measures such as cooling, the summer peak coincidence factor is provided in two different ways. The first method is to estimate demand savings during the utility’s peak hour (as provided by Ameren). This is likely to be the most indicative of actual peak benefits. The second way represents the average savings over the summer peak period, consistent with the non-weather sensitive end uses, and is presented so that savings can be bid into PJM’s Forward Capacity Market.

## Heating and Cooling Degree-Day Data

Many measures are weather sensitive. Because there is a range of climactic conditions across the state, VEIC engaged the Utilities to provide their preferences for what airports and cities are the best proxies for the weather in their service territories. The result of this engagement is in the table below. All of the data represents 30-year normals[[28]](#footnote-29) from the National Climactic Data Center (NCDC). Note that the base temperature for the calculation of heating degree-days in this document does not follow the historical 65F degree base temperature convention. Instead VEIC used several different temperatures in this TRM to more accurately reflect the outdoor temperature when a heating or cooling system turns on.

Residential heating is based on 60F, in accordance with regression analysis of heating fuel use and weather by state by the Pacific Northwest National Laboratory[[29]](#footnote-30). Residential cooling is based on 65F in agreement with a field study in Wisconsin[[30]](#footnote-31). These are lower than typical thermostat set points because internal gains such as appliances, lighting, and people provide some heating. In C&I settings, internal gains are often much higher; the base temperatures for both heating and cooling is 55F[[31]](#footnote-32). Custom degree-days with building specific base temperatures are recommended for large C&I projects.

Table 3.: Degree-Day Zones and Values by Market Sector

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
|  | **Residential** | | **C&I** | |  |
| **Zone** | **HDD** | **CDD** | **HDD** | **CDD** | **Weather Station / City** |
| 1 | 5,352 | 820 | 4,272 | 2,173 | Rockford AP / Rockford |
| 2 | 5,113 | 842 | 4,029 | 3,357 | Chicago O'Hare AP / Chicago |
| 3 | 4,379 | 1,108 | 3,406 | 2,666 | Springfield #2 / Springfield |
| 4 | 3,378 | 1,570 | 2,515 | 3,090 | Belleville SIU RSCH / Belleville |
| 5 | 3,438 | 1,370 | 2,546 | 2,182 | Carbondale Southern IL AP / Marion |
| Average | 4,860 | 947 | 3,812 | 3,051 | Weighted by occupied housing units |
| Base Temp | 60F | 65F | 55F | 55F | 30 year climate normals, 1981-2010 |

This table assigns each of the proxy cities to one of five climate zones. The following graphics from the Illinois State Water Survey show isobars (lines of equal degree-days) and we have color-coded the counties in each of these graphics using those isobars as a dividing line. Using this approach, the state divides into five cooling degree-day zones and five heating degree-day zones. Note that although the heating and cooling degree-day maps are similar, they are not the same, and the result is that there are a total of 10 climate zones in the state. The counties are listed in the tables following the figures for ease of reference.

Figure 1: Cooling Degree-Day Zones by County



**Zone 1**

**Zone 2**

**Zone 3**

**Zone 4**

**Zone 5**

Figure 2: Heating Degree-Day Zones by County



**Zone 1**

**Zone 2**

**Zone 3**

**Zone 4**

**Zone 5**

Table 3.: Heating Degree-Day Zones by County

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
| Zone 1 | Zone 2 | Zone 3 | Zone 4 | Zone 5 |
| Boone County | Bureau County | Adams County | Clinton County | Alexander County |
| Jo Daviess County | Carroll County | Bond County | Edwards County | Massac County |
| Stephenson County | Cook County | Brown County | Franklin County | Pulaski County |
| Winnebago County | DeKalb County | Calhoun County | Gallatin County | Union County |
|  | DuPage County | Cass County | Hamilton County |  |
|  | Grundy County | Champaign County | Hardin County |  |
|  | Henderson County | Christian County | Jackson County |  |
|  | Henry County | Clark County | Jefferson County |  |
|  | Iroquois County | Clay County | Johnson County |  |
|  | Kane County | Coles County | Lawrence County |  |
|  | Kankakee County | Crawford County | Madison County |  |
|  | Kendall County | Cumberland County | Marion County |  |
|  | Knox County | De Witt County | Monroe County |  |
|  | Lake County | Douglas County | Perry County |  |
|  | LaSalle County | Edgar County | Pope County |  |
|  | Lee County | Effingham County | Randolph County |  |
|  | Livingston County | Fayette County | Richland County |  |
|  | Marshall County | Ford County | Saline County |  |
|  | McHenry County | Fulton County | St. Clair County |  |
|  | Mercer County | Greene County | Wabash County |  |
|  | Ogle County | Hancock County | Washington County |  |
|  | Peoria County | Jasper County | Wayne County |  |
|  | Putnam County | Jersey County | White County |  |
|  | Rock Island County | Logan County | Williamson County |  |
|  | Stark County | Macon County |  |  |
|  | Warren County | Macoupin County |  |  |
|  | Whiteside County | Mason County |  |  |
|  | Will County | McDonough County |  |  |
|  | Woodford County | McLean County |  |  |
|  |  | Menard County |  |  |
|  |  | Montgomery County |  |  |
|  |  | Morgan County |  |  |
|  |  | Moultrie County |  |  |
|  |  | Piatt County |  |  |
|  |  | Pike County |  |  |
|  |  | Sangamon County |  |  |
|  |  | Schuyler County |  |  |
|  |  | Scott County |  |  |
|  |  | Shelby County |  |  |
|  |  | Tazewell County |  |  |
|  |  | Vermilion County |  |  |

Table 3.: Cooling Degree-day Zones by County

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
| Zone 1 | Zone 2 | Zone 3 | Zone 4 | Zone 5 |
| Boone County | Bureau County | Adams County | Bond County | Alexander County |
| Carroll County | Cook County | Brown County | Clay County | Hardin County |
| DeKalb County | DuPage County | Calhoun County | Clinton County | Johnson County |
| Jo Daviess County | Grundy County | Cass County | Edwards County | Massac County |
| Kane County | Henderson County | Champaign County | Fayette County | Pope County |
| Lake County | Henry County | Christian County | Franklin County | Pulaski County |
| McHenry County | Iroquois County | Clark County | Gallatin County | Randolph County |
| Ogle County | Kankakee County | Coles County | Hamilton County | Union County |
| Stephenson County | Kendall County | Crawford County | Jackson County |  |
| Winnebago County | Knox County | Cumberland County | Jefferson County |  |
|  | LaSalle County | De Witt County | Jersey County |  |
|  | Lee County | Douglas County | Lawrence County |  |
|  | Livingston County | Edgar County | Macoupin County |  |
|  | Marshall County | Effingham County | Madison County |  |
|  | Mercer County | Ford County | Marion County |  |
|  | Peoria County | Fulton County | Monroe County |  |
|  | Putnam County | Greene County | Montgomery County |  |
|  | Rock Island County | Hancock County | Perry County |  |
|  | Stark County | Jasper County | Richland County |  |
|  | Warren County | Logan County | Saline County |  |
|  | Whiteside County | Macon County | St. Clair County |  |
|  | Will County | Mason County | Wabash County |  |
|  | Woodford County | McDonough County | Washington County |  |
|  |  | McLean County | Wayne County |  |
|  |  | Menard County | White County |  |
|  |  | Morgan County | Williamson County |  |
|  |  | Moultrie County |  |  |
|  |  | Piatt County |  |  |
|  |  | Pike County |  |  |
|  |  | Sangamon County |  |  |
|  |  | Schuyler County |  |  |
|  |  | Scott County |  |  |
|  |  | Shelby County |  |  |
|  |  | Tazewell County |  |  |
|  |  | Vermilion County |  |  |

## O&M Costs and the Weighted Average Cost of Capital (WACC)

Some measures specify an operations and maintenance (O&M) parameter that describes the incremental O&M cost savings that can be expected over the measure’s lifetime. When estimating the cost effectiveness of these measures, it is necessary to calculate the net present value (NPV) of O&M costs over the life of the measure, which requires an appropriate discount rate. The utility’s weighted average cost of capital (WACC) is the most commonly used discount rate that is used in this context.

Each utility has a unique WACC that will vary over time. As a result, the TRM does not specify the NPV of the O&M costs. Instead, the necessary information required to calculate the NPV is included. An example is provided below to demonstrate how to calculate the NPV of O&M costs.

EXAMPLE

Baseline Case: O&M costs equal $150 every two years.

Efficient Case: O&M costs equal $50 every five years.

Given this information, the incremental O&M costs can be determined by discounting the cash flows in the Baseline Case and the Efficient Case separately using the applicable WACC. Then the NPV of the incremental O&M costs is calculated by subtracting one NPV from the other. This value is then used in each utility’s cost-effectiveness screening process.

Those measures that include baseline shifts that result in multiple component costs and lifetimes cannot be calculated by this standard method. In only these cases, the O&M costs are presented both as Annual Levelized equivalent cost (i.e., the annual payment that results in an equivalent NPV to the actual stream of O&M costs) and as NPVs using a statewide average real discount rate of 5.23%.

## Interactive Effects

The TRM presents engineering equations for most measures. This approach is desirable because it conveys information clearly and transparently, and is widely accepted in the industry. Unlike simulation model results, engineering equations also provide flexibility and the opportunity for users to substitute local, specific information for specific input values. Furthermore, the parameters can be changed in TRM updates to be applied in future years as better information becomes available.

One limitation is that some interactive effects between measures are not automatically captured. Because we cannot know what measures will be implemented at the same time with the same customer, we cannot always capture the interactions between multiple measures within individual measure characterizations. However, interactive effects with different end-uses are included in individual measure characterizations whenever possible[[32]](#footnote-33). For instance, waste heat factors are included in the lighting characterizations to capture the interaction between more-efficient lighting measures and the amount of heating and/or cooling that is subsequently needed in the building.

By contrast, no effort is made to account for interactive effects between an efficient air conditioning measure and an efficient lighting measure, because it is impossible to know the specifics of the other measure in advance of its installation. For custom measures and projects where a bundle of measures is being implemented at the same time, these kinds of interactive effects should be estimated.

# Commercial and Industrial Measures

## Agricultural End Use

### Engine Block Timer for Agricultural Equipment

###### Description

The measure is a plug-in timer that is activated below a specific outdoor temperature to control an engine block heater in agricultural equipment. Engine block heaters are typically used during cold weather to pre-warm an engine prior to start, for convenience heaters are typically plugged in considerably longer than necessary to improve startup performance. A timer allows a user to preset the heater to come on for only the amount of time necessary to pre-warm the engine block, reducing unnecessary run time even if the baseline equipment has an engine block temperature sensor.

This measure was developed to be applicable to the following program types: RF. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The efficient measure is an engine block heater operated by an outdoor plug-in timer (15 amp or greater) that turns on the heater only when the outdoor temperature is below 25 °F.

###### Definition of Baseline Equipment

The baseline scenario is an engine block heater that is manually plugged in by the farmer to facilitate equipment startup at a later time.

###### Deemed Lifetime of Efficient Equipment

The expected measure life if assumed to be 3 years[[33]](#footnote-34)

###### Deemed Measure Cost

The incremental cost per installed plug-in timer is $10.19[[34]](#footnote-35).

###### Coincidence Factor

Engine block timers only operate in the winter so the summer peak demand savings is zero.

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh*=* ISR \* Use Season \* %Days \* HrSave/Day \* kWheater - ParaLd

= 78.39% \* 87 days \* 84.23% \* 7.765 Hr/Day \* 1.5 kW - 5.46 kWh

= 664 kWh

###### Summer Coincident Peak Demand Savings

N/A

###### NATURAL GAS ENERGY SAVINGS

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-APL-ESDH-V01-120601

### High Volume Low Speed Fans

###### Description

The measure applies to 20-24 foot diameter horizontally mounted ceiling high volume low speed (HVLS) fans that are replacing multiple non HVLS fans that have reached the end of useful life in agricultural applications.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the efficient equipment is assumed to be classified as HVLS and have a VFD[[35]](#footnote-36).

###### Definition of Baseline Equipment

In order for this characterization to apply, the baseline condition is assumed to be multiple non HVLS existing fans that have reached the end of s useful life.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 10 years[[36]](#footnote-37).

###### Deemed Measure Cost

The incremental capital cost for the fans are as follows[[37]](#footnote-38):

|  |  |
| --- | --- |
| **Fan Diameter Size (feet)** | **Incremental Cost** |
| 20 | $4150 |
| 22 | $4180 |
| 24 | $4225 |

###### Loadshape

Loadshape C34 - Industrial Motor

###### Coincidence Factor

The measure has deemed kW savings therefor a coincidence factor is not applied.

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings [[38]](#footnote-39)

The annual electric savings from this measure are deemed values depending on fan size and apply to all building types:

|  |  |
| --- | --- |
| **Fan Diameter Size (feet)** | **kWh Savings** |
| 20 | 6576.85 |
| 22 | 8543.34 |
| 24 | 10018.22 |

###### Summer Coincident Peak Demand Savings[[39]](#footnote-40)

The annual kW savings from this measure are deemed values depending on fan size and apply to all building types:

|  |  |
| --- | --- |
| Fan Diameter Size (feet) | kW Savings |
| 20 | 2.408 |
| 22 | 3.128 |
| 24 | 3.668 |

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-AGE-HVSF-V01-120601

### High Speed Fans

###### Description

The measure applies to high speed exhaust, ventilation and circulation fans that are replacing an existing unit that reached the end of its useful life in agricultural applications.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the efficient equipment is assumed to be diffuser equipped and meet the following criteria[[40]](#footnote-41).

|  |  |  |
| --- | --- | --- |
| Diameter of Fan (inches) | Minimum Efficiency for Exhasut & Ventilation Fans | Minimum Efficiency for Circulation Fans |
| 24 through 35 | 14.0 cfm/W at 0.10 static pressure | 12.5 lbf/kW |
| 36 through 47 | 17.1 cfm/W at 0.10 static pressure | 18.2 lbf/kW |
| 48 through 71 | 20.3 cfm/W at 0.10 static pressure | 23.0 lbf/kW |

###### Definition of Baseline Equipment

In order for this characterization to apply, the baseline condition is assumed to be an existing fan that reached the end of its useful life.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 7 years[[41]](#footnote-42).

###### Deemed Measure Cost

The incremental capital cost for all fan sizes is $150[[42]](#footnote-43).

###### Loadshape

Loadshape C34 - Industrial Motor

###### Coincidence Factor

The measure has deemed kW savings therefor a coincidence factor is not applied.

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings [[43]](#footnote-44)

The annual electric savings from this measure are deemed values depending on fan size and apply to all building types:

|  |  |
| --- | --- |
| Diameter of Fan (inches) | kWh |
| 24 through 35 | 372.14 |
| 36 through 47 | 625.23 |
| 48 through 71 | 1122.36 |

###### Summer Coincident Peak Demand Savings[[44]](#footnote-45)

The annual kW savings from this measure are deemed values depending on fan size and apply to all building types:

|  |  |
| --- | --- |
| Diameter of Fan (inches) | kW |
| 24 through 35 | 0.118 |
| 36 through 47 | 0.198 |
| 48 through 71 | 0.356 |

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-AGE-HSF\_-V01-120601

### Live Stock Waterer

###### Description

This measure applies to the replacement of electric open waterers with sinking or floating water heaters with equivalent herd size watering capacity of the old unit.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the efficient equipment is assumed to an electrically heated thermally insulated waterer with minimum 2 inches of insulation. A thermostat is required on unit with heating element greater than or equal to 250 watts[[45]](#footnote-46).

###### Definition of Baseline Equipment

In order for this characterization to apply, the baseline equipment is assumed to be an electric open waterer with sinking or floating water heaters that have reached the end of useful life.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 10 years[[46]](#footnote-47).

###### Deemed Measure Cost

The incremental capital cost for the waters are $787.50:[[47]](#footnote-48)

###### Loadshape

Loadshape C04 - Non-Residential Electric Heating

###### Coincidence Factor

The measure has deemed kW savings therefor a coincidence factor is not applied

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings [[48]](#footnote-49)

The annual electric savings from this measure is a deemed value and assumed to be 1592.85 kWh.

###### Summer Coincident Peak Demand Savings

The annual kW savings from this measure is a deemed value and assumed to be 0.525 kW. [[49]](#footnote-50)

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-AGE-LSW1-V01-120601

## Food Service Equipment End Use

### Combination Oven

###### Description

This measure applies to natural gas fired high efficiency combination convection and steam ovens installed in a commercial kitchen replacing existing equipment at the end of its useful life.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a new natural gas combination convection with steam oven cooking efficiency ≥ 38% and convection mode cooking efficiency ≥ 44% utilizing ASTM standard F2861 and meet idle requirements below[[50]](#footnote-51):

Idle Rate Requirements for Commercial Combination Ovens/Steamers

|  |  |  |
| --- | --- | --- |
| Combi Oven Type | Steam Mode Idle Rate | Convection Mode Idle Rate |
| Gas Combi < 15 pan capacity  Gas Combi 15-28 pan capacity  Gas Combi > 28 pan capacity | 15,000 Btu/hr  18,000 Btu/hr  28,000 Btu/hr | 9,000 Btu/hr  11,000 Btu/hr  17,000 Btu/hr |

###### Definition of Baseline Equipment

The baseline equipment is a new or existing natural gas combination convection and steam ovens that do not meet the efficient equipment criteria

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 12 years[[51]](#footnote-52)

###### Deemed Measure Cost

The incremental capital cost for this measure is $4300[[52]](#footnote-53)

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

The annual natural gas energy savings from this measure is a deemed value equaling 644 therms.[[53]](#footnote-54)

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-CBOV-V01-120601

### Commercial Solid and Glass Door Refrigerators & Freezers

###### Description

This measure relates to the installation of a new reach-in commercial refrigerator or freezer meeting ENERGY STAR efficiency standards. ENERGY STAR labeled commercial refrigerators and freezers are more energy efficient because they are designed with components such as ECM evaporator and condenser fan motors, hot gas anti-sweat heaters, or high-efficiency compressors, which will significantly reduce energy consumption.

This measure was developed to be applicable to the following program types: TOS and NC. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the efficient equipment is assumed to be a new vertical solid or glass door refrigerator or freezer or vertical chest freezer meeting the minimum ENERGY STAR efficiency level standards.

###### Definition of Baseline Equipment

In order for this characterization to apply, the baseline equipment is assumed to be an existing solid or glass door refrigerator or freezer meeting the minimum federal manufacturing standards as specified by the Energy Policy Act of 2005.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 12 years [[54]](#footnote-55).

###### Deemed Measure Cost

The incremental capital cost for this measure is provided below[[55]](#footnote-56).

|  |  |  |
| --- | --- | --- |
| Type | Refrigerator incremental Cost, per unit | Freezer Incremental Cost, per unit |
| Solid or Glass Door | | |
| 0 < V < 15 | $143 | $142 |
| 15 ≤ V < 30 | $164 | $166 |
| 30 ≤ V < 50 | $164 | $166 |
| V ≥ 50 | $249 | $407 |

###### Loadshape

Loadshape C23 - Commercial Refrigeration

###### Coincidence Factor

The summer peak coincidence factor for this measure is assumed to be 0.937.[[56]](#footnote-57)

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = (kWhbase – kWhee) \* 365.25

Where:

kWhbase= baseline maximum daily energy consumption in kWh

= calculated using actual chilled or frozen compartment volume (V) of the efficient unit as shown in the table below.

|  |  |
| --- | --- |
| Type | kWhbase[[57]](#footnote-58) |
| Solid Door Refrigerator | 0.10 \* V + 2.04 |
| Glass Door Refrigerator | 0.12 \* V + 3.34 |
| Solid Door Freezer | 0.40 \* V + 1.38 |
| Glass Door Freezer | 0.75 \* V + 4.10 |

kWhee[[58]](#footnote-59) = efficient maximum daily energy consumption in kWh

= calculated using actual chilled or frozen compartment volume (V) of the efficient unit as shown in the table below.

|  |  |  |
| --- | --- | --- |
| Type | Refrigerator  kWhee | Freezer  kWhee |
| Solid Door | | |
| 0 < V < 15 | ≤ 0.089V + 1.411 | ≤ 0.250V + 1.250 |
| 15 ≤ V < 30 | ≤ 0.037V + 2.200 | ≤ 0.400V – 1.000 |
| 30 ≤ V < 50 | ≤ 0.056V + 1.635 | ≤ 0.163V + 6.125 |
| V ≥ 50 | ≤ 0.060V + 1.416 | ≤ 0.158V + 6.333 |
| Glass Door | | |
| 0 < V < 15 | ≤ 0.118V + 1.382 | ≤ 0.607V + 0.893 |
| 15 ≤ V < 30 | ≤ 0.140V + 1.050 | ≤ 0.733V – 1.000 |
| 30 ≤ V < 50 | ≤ 0.088V + 2.625 | ≤ 0.250V + 13.500 |
| V ≥ 50 | ≤ 0.110V + 1.500 | ≤ 0.450V + 3.500 |

V = the chilled or frozen compartment volume (ft3) (as defined in the Association of Home Appliance Manufacturers Standard HRF1–1979)

= Actual installed

365.25 = days per year

For example a solid door refrigerator with a volume of 15 would save

ΔkWh = (3.54 – 2.76) \* 365.25

= 285 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = ΔkWh / HOURS \* CF

Where:

HOURS = equipment is assumed to operate continuously, 24 hours per day, 365.25 days per year.

= 8766

CF = Summer Peak Coincidence Factor for measure

= 0.937

For example a solid door refrigerator with a volume of 15 would save

ΔkW = 285/ 8766 \* .937

=0.030 kW

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-CSDO-V01-120601

### Commercial Steam Cooker

###### Description

To qualify for this measure the installed equipment must be an ENERGY STAR® steamer in place of a standard steamer in a commercial kitchen. Savings are presented dependent on the pan capacity and corresponding idle rate at heavy load cooking capacity and if the steamer is gas or electric.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

To qualify for this measure the installed equipment must be as follows:

|  |  |
| --- | --- |
| **Gas** | **Electric** |
| ENERGY STAR® qualified with 38% minimum cooking energy efficiency at heavy load (potato) cooking capacity for gas steam cookers. | ENERGY STAR® qualified with 50% minimum cooking energy efficiency at heavy load (potato) cooking capacity for electric steam cookers. |

**Definition of Baseline Equipment**

The baseline condition is assumed to be a non-ENERGY STAR® commercial steamer at end of life. It is assumed that the efficient equipment and baseline equipment have the same number of pans.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 12 years[[59]](#footnote-60)

**Deemed Measure Cost**

The incremental capital cost for this measure is $998[[60]](#footnote-61) for a natural gas steam cooker or $2490[[61]](#footnote-62) for an electric steam cooker.

**Loadshape**

Loadshape C01 - Commercial Electric Cooking

**Coincidence Factor**

Summer Peak Coincidence Factor for measure is provided below for different building type[[62]](#footnote-63):

|  |  |
| --- | --- |
| **Location** | **CF**  **CF** |
| Fast Food Limited Menu | 0.32 |
| Fast Food Expanded Menu | 0.41 |
| Pizza | 0.46 |
| Full Service Limited Menu | 0.51 |
| Full Service Expanded Menu | 0.36 |
| Cafeteria | 0.36 |
| Unknown | 0.40 |

**Algorithm**

**Calculation of Savings**

Formulas below are applicable to both gas and electric steam cookers. Please use appropriate lookup values and identified flags.

**Energy Savings**

ΔSavings = (ΔIdle Energy + ΔPreheat Energy + ΔCooking Energy) \* Z

For a gas cooker: ΔSavings = ΔBtu \* 1/100,000 \*Z

For an electric steam cooker: ΔSavings = ΔkWh \*Z

Where:

Z = days/yr steamer operating (use 365.25 days/yr if heavy use restaurant and exact number unknown)

ΔIdle Energy = ((((1- CSM%Baseline)\* IDLEBASE + CSM%Baseline \* PCBASE \* EFOOD / EFFBASE)\*(HOURSday - (F / PCBase) - ( PREnumber \*0.25))) - (((1- CSM%ENERGYSTAR) \* IDLEENERGYSTAR + CSM%ENERGYSTAR \* PCENERGY \* EFOOD / EFFENERGYSTAR) \* (HOURSDay - (F l/ PCENERGY ) - (PREnumber \* 0.25 ))))

Where:

CSM%Baseline = Baseline Steamer Time in Manual Steam Mode (% of time)

= 90%[[63]](#footnote-64)

IDLEBase = Idle Energy Rate of Base Steamer[[64]](#footnote-65)

|  |  |  |
| --- | --- | --- |
| **Number of Pans** | **IDLEBASE - Gas, Btu/hr** | **IDLEBASE - Electric, kw** |
| 3 | 11,000 | 1.0 |
| 4 | 14,667 | 1.33 |
| 5 | 18,333 | 1.67 |
| 6 | 22,000 | 2.0 |

PCBase = Production Capacity of Base Steamer[[65]](#footnote-66)

|  |  |  |
| --- | --- | --- |
| **Number of Pans** | **PCBASE, gas (lbs/hr)** | **PCBASE, electric (lbs/hr)** |
| 3 | 65 | 70 |
| 4 | 87 | 93 |
| 5 | 108 | 117 |
| 6 | 130 | 140 |

EFOOD= Amount of Energy Absorbed by the food during cooking known as ASTM Energy to Food (Btu/lb or kW/lb)

=105 Btu/lb[[66]](#footnote-67) (gas steamers) or 0.03088 (electric steamers)

EFFBASE =Heavy Load Cooking Efficiency for Base Steamer

=15%[[67]](#footnote-68) (gas steamers) or 26%9 (electric steamers)

HOURSday  = Average Daily Operation (hours)

|  |  |
| --- | --- |
| **Type of Food Service** | **Hoursday[[68]](#footnote-69)** |
| Fast Food, limited menu | 4 |
| Fast Food, expanded menu | 5 |
| Pizza | 8 |
| Full Service, limited menu | 8 |
| Full Service, expanded menu | 7 |
| Cafeteria | 6 |
| Unknown | 6[[69]](#footnote-70) |
| Custom | Varies |

F = Food cooked per day (lbs/day)

= custom or if unknown, use 100 lbs/day[[70]](#footnote-71)

CSM%ENERGYSTAR = ENERGY STAR Steamer's Time in Manual Steam Mode (% of time)[[71]](#footnote-72)

= 0%

IDLEENERGYSTAR = Idle Energy Rate of ENERGY STAR®[[72]](#footnote-73)

|  |  |  |
| --- | --- | --- |
| **Number of Pans** | **IDLEENERGY STAR – gas, (Btu/hr)** | **IDLEENERGY STAR – electric, (kW)** |
| 3 | 6250 | 0.40 |
| 4 | 8333 | 0.53 |
| 5 | 10417 | 0.67 |
| 6 | 12500 | 0.80 |

PCENERGY = Production Capacity of ENERGY STAR® Steamer[[73]](#footnote-74)

|  |  |  |
| --- | --- | --- |
| **Number of Pans** | **PCENERGY - gas(lbs/hr)** | **PCENERGY – electric (lbs/hr)** |
| 3 | 55 | 50 |
| 4 | 73 | 67 |
| 5 | 92 | 83 |
| 6 | 110 | 100 |

EFFENERGYSTAR = Heavy Load Cooking Efficiency for ENERGY STAR® Steamer(%)

=38%[[74]](#footnote-75) (gas steamer) or 50%15 (electric steamer)

PREnumber = Number of preheats per day

=1[[75]](#footnote-76) (if unknown, use 1)

Where:

ΔPreheat Energy = ( PREnumber \* Δ Preheat)

Where:

PREnumber = Number of Preheats per Day

=1[[76]](#footnote-77)(if unknown, use 1)

PREheat = Preheat energy savings per preheat

= 11,000 Btu/preheat[[77]](#footnote-78) (gas steamer) or 0.5 kWh/preheat[[78]](#footnote-79) (electric steamer)

Where:

ΔCooking Energy = ((1/ EFFBASE) - (1/ EFFENERGY STAR®)) \* F \* EFOOD

Where:

EFFBASE =Heavy Load Cooking Efficiency for Base Steamer

=15%[[79]](#footnote-80) (gas steamer) or 26%28 (electric steamer)

EFFENERGYSTAR =Heavy Load Cooking Efficiency for ENERGY STAR® Steamer

=38%[[80]](#footnote-81) (gas steamer) or 50%23 (electric steamer)

F = Food cooked per day (lbs/day)

= custom or if unknown, use 100 lbs/day[[81]](#footnote-82)

EFOOD = Amount of Energy Absorbed by the food during cooking known as ASTM Energy to Food[[82]](#footnote-83)

|  |  |
| --- | --- |
| **EFOOD  - gas(Btu/lb)** | **EFOOD  (kWh/lb)** |
| 105[[83]](#footnote-84) | 0.0308[[84]](#footnote-85) |

EXAMPLE

For a gas steam cooker: A 3 pan steamer in a restaurant

ΔSavings = ΔIdle Energy + ΔPreheat Energy + ΔCooking Energy \*Z \* 1/100.000

ΔIdle Energy = ((((1- .9)\* 11000 + .9 \* 65 \* 105 /.15 )\*(12 - (100 / 65)-(1-.25))) - (((1-0) \* 6250 + 0 \* 55 \* 105 / 0.38) \* (12 - (100 / 55) - (1-0.25)))) +

ΔPreheat Energy = (1 \*11,000) +

ΔCooking Energy = (((1/ 0.15) - (1/ 0.38)) \* (100 lb/day \* 105 btu/lb)))

\* 365.25 days)) \*1/100,000 =

=1536 therms

For an electric steam cooker: A 3 pan steamer in a restaurant

ΔSavings = ΔIdle Energy + ΔPreheat Energy + ΔCooking Energy \*Z

ΔIdle Energy = ((((1- .9)\* 1.0 + .9 \* 70 \* 0.0308 /.26 )\*(12 - (100 / 70)-(1\*.25))) - (((1-0) \* 0.4 + 0 \* 50 \* .0308 / 0.50) \* (12 - (100 / 50) - (1\*.25)))) +

ΔPreheat Energy = (1 \*0.5)) +

ΔCooking Energy = (((1/ 0.26) - (1/ 0.5)) \* (100 \* 0.0308 )))

\* 365.25 days=

30,533kWh

**Summer Coincident Peak Demand Savings**

This is only applicable to the electric steam cooker.

ΔkW = (ΔkWh/(HOURSDay \*DaysYear)) \* CF

Where:

|  |  |
| --- | --- |
| **Location** | **CF**  **CF** |
| Fast Food Limited Menu | 0.32 |
| Fast Food Expanded Menu | 0.41 |
| Pizza | 0.46 |
| Full Service Limited Menu | 0.51 |
| Full Service Expanded Menu | 0.36 |
| Cafeteria | 0.36 |

CF =Summer Peak Coincidence Factor for measure is provided below for different locations[[85]](#footnote-86):

DaysYear =Annual Days of Operation

=custom or 365.25 days a year

Other values as defined above

EXAMPLE

For 3 pan electric steam cooker located in a cafeteria:

ΔkW = (ΔkWh/(HOURSDay \*DaysYear)) \* CF

= (30,533/(12\*365.25))\*.36

= 2.51 kW

**Water Impact Descriptions and Calculation**

This is applicable to both gas and electric steam cookers.

ΔWater = [(WBASE -WENERGYSTAR®)\*HOURSDay \*DaysYear

Where

WBASE = Water Consumption Rate of Base Steamer (gal/hr)

= 40[[86]](#footnote-87)

WENERGYSTAR = Water Consumption Rate of ENERGY STAR® Steamer look up[[87]](#footnote-88)

|  |  |
| --- | --- |
| **CEE Tier** | **gal/hr** |
| Tier 1A | 15 |
| Tier 1B | 4 |
| Avg Efficient | 10 |
| Avg Most Efficient | 3 |

DaysYear =Annual Days of Operation

=custom or 365.25 days a year[[88]](#footnote-89)

EXAMPLE

For example, an electric 3 pan steamer with average efficiency in a restaurant

ΔWater = [(40 -10)\*12\*365.25

= 131,490 gallons

**Deemed O&M Cost Adjustment Calculation**

N/A

###### Measure Code: CI-FSE-STMC-V02-120601

### Conveyor Oven

###### Description

This measure applies to natural gas fired high efficiency conveyor ovens installed in commercial kitchens replacing existing natural gas units with conveyor width greater than 25 inches.

Conveyor ovens are available using four different heating processes: infrared, natural convection with a ceramic baking hearth, forced convection or air impingement, or a combination of infrared and forced convection. Conveyor ovens are typically used for producing a limited number of products with similar cooking requirements at high production rates. They are highly flexible and can be used to bake or roast a wide variety of products including pizza, casseroles, meats, breads, and pastries.

Some manufacturers offer an air-curtain feature at either end of the cooking chamber that helps to keep the heated air inside the conveyor oven. The air curtain operates as a virtual oven wall and helps reduce both the idle energy of the oven and the resultant heat gain to the kitchen.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a natural gas conveyor oven with a tested baking energy efficiency > 42% and an idle energy consumption rate < 57,000 Btu/hr utilizing ASTM standard F1817.

###### Definition of Baseline Equipment

The baseline equipment is an existing pizza deck oven at end of life.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 17 years.[[89]](#footnote-90)

###### Deemed Measure Cost

The incremental capital cost for this measure is $1800[[90]](#footnote-91).

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

The annual natural gas energy savings from this measure is a deemed value equaling 733 Therms[[91]](#footnote-92).

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-CVOV-V01-120601

### ENERGY STAR Convection Oven

###### Description

This measure applies to natural gas fired ENERGY STAR convection ovens installed in a commercial kitchen.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a natural gas convection oven with a cooking efficiency ≥ 44% utilizing ASTM standard 1496 and an idle energy consumption rate < 13,000 Btu/hr

###### Definition of Baseline Equipment

The baseline equipment is a natural gas convection oven that is not ENERGY STAR certified and is at end of life.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 12 years[[92]](#footnote-93)

###### Deemed Measure Cost

The incremental capital cost for this measure is $50[[93]](#footnote-94)

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

Custom calculation below, otherwise use deemed value of 306 therms. [[94]](#footnote-95)

ΔTherms = (ΔDailyIdle Energy + ΔDailyPreheat Energy + ΔDailyCooking Energy) \* Days /100000

Where:

ΔDailyIdleEnergy = (IdleBase\* IdleBaseTime)- (IdleENERGYSTAR \* IdleENERGYSTARTime)

ΔDailyPreheatEnergy = (PreHeatNumberBase \* PreheatTimeBase / 60 \* PreheatRateBase) – (PreheatNumberENERGYSTAR \* PreheatTimeENERGYSTAR/60 \* PreheatRateENERGYSTAR)

ΔDailyCookingEnergy = (LB \* EFOOD/ EffBase) - (LB \* EFOOD/ EffENERGYSTAR)

Where:

HOURSday = Average Daily Operation

= custom or if unknown, use 12 hours

Days = Annual days of operation

= custom or if unknown, use 365.25 days a year

LB = Food cooked per day

= custom or if unknown, use 100 pounds

EffENERGYSTAR = Cooking Efficiency ENERGY STAR

= custom or if unknown, use 44%

EffBase = Cooking Efficiency Baseline

= custom or if unknown, use 30%

PCENERGYSTAR = Production Capacity ENERGY STAR

= custom or if unknown, use 80 pounds/hr

PCBase = Production Capacity base

= custom or if unknown, use 70 pounds/hr

PreheatNumberENERGYSTAR = Number of preheats per day

= custom or if unknown, use 1

PreheatNumberBase = Number of preheats per day

= custom or if unknown, use 1

PreheatTimeENERGYSTAR = preheat length

= custom or if unknown, use 15 minutes

PreheatTimeBase = preheat length

= custom or if unknown, use 15 minutes

PreheatRateENERGYSTAR = preheat energy rate high efficiency

= custom or if unknown, use 44000 btu/h

PreheatRateBase = preheat energy rate baseline

= custom or if unknown, use 76000 btu/h

IdleENERGYSTAR = Idle energy rate

= custom or if unknown, use 13000 btu/h

IdleBase = Idle energy rate

= custom or if unknown, use 18000 btu/h

IdleENERGYSTARTime = ENERGY STAR Idle Time

=HOURsday-LB/PCENERGYSTAR –PreHeatTimeENERGYSTAR/60

=12 – 100/80 – 15/60

=10.5 hours

IdleBaseTime = BASE Idle Time

= HOURsday-LB/PCbase –PreHeatTimeBase/60

=Custom or if unknown, use

=12 – 100/70-15/60

=10.3 hours

EFOOD = ASTM energy to food

= 250 btu/pound

EXAMPLE

For example, an ENERGY STAR Oven with a cooking energy efficiency of 44% and default values from above would save.

ΔTherms = (ΔIdle Energy + ΔPreheat Energy + ΔCooking Energy) \* Days /100000

Where:

ΔDailyIdleEnergy =(18000\*10.3)- (13000\*10.5)

= 49286 btu

ΔDailyPreheatEnergy = (1 \* 15 / 60 \*76000) – (1 \* 15 / 60 \*44000)

= 8000 btu

ΔDailyCookingEnergy = (100 \* 250/ .30) - (100 \* 250/ .44)

=26515 btu

ΔTherms = (49286+8000+26515)\* 365.25 /100000

=306 therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-ESCV-V01-120

### ENERGY STAR Dishwasher

###### Description

This measure applies to ENERGY STAR high and low temp under counter single tank door type, single tank conveyor, and multiple tank conveyor dishwashers installed in a commercial kitchen.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be an ENERGY STAR certified dishwasher meeting idle energy rate (kW) and water consumption (gallons/rack) limits, as determined by both machine type and sanitation approach (chemical/low temp versus high temp).

###### Definition of Baseline Equipment

The baseline equipment is a dishwasher that’s not ENERGY STAR certified and at end of life.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be[[95]](#footnote-96)

|  |  |  |
| --- | --- | --- |
| Dishwasher type | | Equipment Life |
| Low Temp | Under Counter | 10 |
| Door Type | 15 |
| Single Tank Conventional | 20 |
| Multi Tank Conventional | 20 |
| High Temp | Under Counter | 10 |
| Door Type | 15 |
| Single Tank Conventional | 20 |
| Multi Tank Conventional | 20 |

###### Deemed Measure Cost

The incremental capital cost for this measure is[[96]](#footnote-97)

|  |  |  |
| --- | --- | --- |
| Dishwasher type | | Incremental Cost |
| Low Temp | Under Counter | $530 |
| Door Type | $530 |
| Single Tank Conventional | $170 |
| Multi Tank Conventional | $0 |
| High Temp | Under Counter | $1000 |
| Door Type | $500 |
| Single Tank Conventional | $270 |
| Multi Tank Conventional | $0 |

###### Loadshape

Loadshape C01 - Commercial Electric Cooking

###### Summer Coincident Peak Demand Savings

Summer Peak Coincidence Factor for measure is provided below for different restaurant types[[97]](#footnote-98):

|  |  |
| --- | --- |
| Location | CF  CF |
| Fast Food Limited Menu | 0.32 |
| Fast Food Expanded Menu | 0.41 |
| Pizza | 0.46 |
| Full Service Limited Menu | 0.51 |
| Full Service Expanded Menu | 0.36 |
| Cafeteria | 0.36 |

**Algorithm**

###### Energy Savings

ENERGY STAR dishwashers save energy in three categories, building water heating, booster water heating and idle energy. Building water heating and booster water heating could be either electric or natural gas. These deemed values are presented in a table format. Savings all water heating combinations are found in the tables below. [[98]](#footnote-99)

Electric building and booster water heating

|  |  |  |  |
| --- | --- | --- | --- |
| Dishwasher type | | kWh | Therms |
| Low Temp | Under Counter | 1,213 | 0 |
| Door Type | 12,135 | 0 |
| Single Tank Conventional | 11,384 | 0 |
| Multi Tank Conventional | 17,465 | 0 |
| High Temp | Under Counter | 7471 | 0 |
| Door Type | 14143 | 0 |
| Single Tank Conventional | 19235 | 0 |
| Multi Tank Conventional | 34153 | 0 |

Electric building and natural gas booster water heating

|  |  |  |  |
| --- | --- | --- | --- |
| Dishwasher type | | kWh | Therms |
| Low Temp | Under Counter | 9089 | 0 |
| Door Type | 21833 | 0 |
| Single Tank Conventional | 24470 | 0 |
| Multi Tank Conventional | 29718 | 0 |
| High Temp | Under Counter | 7208 | 110 |
| Door Type | 19436 | 205 |
| Single Tank Conventional | 29792 | 258 |
| Multi Tank Conventional | 34974 | 503 |

Natural Gas building and electric booster water heating

|  |  |  |  |
| --- | --- | --- | --- |
| Dishwasher type | | kWh | Therms |
| Low Temp | Under Counter | 0 | 56 |
| Door Type | 0 | 562 |
| Single Tank Conventional | 0 | 527 |
| Multi Tank Conventional | 0 | 809 |
| High Temp | Under Counter | 2717 | 220 |
| Door Type | 5269 | 441 |
| Single Tank Conventional | 8110 | 515 |
| Multi Tank Conventional | 12419 | 1007 |

Natural Gas building and booster water heating

|  |  |  |  |
| --- | --- | --- | --- |
| Dishwasher type | | kWh | Therms |
| Low Temp | Under Counter | 0 | 56 |
| Door Type | 0 | 562 |
| Single Tank Conventional | 0 | 527 |
| Multi Tank Conventional | 0 | 809 |
| High Temp | Under Counter | 0 | 330 |
| Door Type | 198 | 617 |
| Single Tank Conventional | 1752 | 773 |
| Multi Tank Conventional | 0 | 1510 |

###### Water Savings

Using standard assumptions water savings would be:

|  |  |  |
| --- | --- | --- |
| Dishwasher type | | Savings (gallons) |
| Low Temp | Under Counter | 6,844 |
| Door Type | 6,8474 |
| Single Tank Conventional | 64,240 |
| Multi Tank Conventional | 98,550 |
| High Temp | Under Counter | 26,828 |
| Door Type | 50,078 |
| Single Tank Conventional | 62,780 |
| Multi Tank Conventional | 122,640 |

###### Summer Coincident Peak Demand Savings

ΔkW = ΔkWh/ AnnualHours

Where:

AnnualHours = Hours \* Days

= 365.25 \* 18

= 6575 annual hours

Example:

A low temperature undercounter dishwasher with electric building and booster water heaters would save:

ΔkW = ΔkWh/ AnnualHours

= 1213/6575

= 0.184 kW

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-ESDW-V01-120601

### ENERGY STAR Fryer

###### Description

This measure applies to natural gas fired ENERGY STAR fryer installed in a commercial kitchen.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a natural gas fryer with a heavy load cooking efficiency ≥ 50% utilizing ASTM standard F1361 or F2144.

###### Definition of Baseline Equipment

The baseline equipment is a natural gas fryer that is not ENERGY STAR certified at end of life.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 15 years.[[99]](#footnote-100)

###### Deemed Measure Cost

The incremental capital cost for this measure is $1200.[[100]](#footnote-101)

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings[[101]](#footnote-102)

Custom calculation below, otherwise use deemed value of 505 Therms.

ΔTherms = (ΔDailyIdle Energy + ΔDailyPreheat Energy + ΔDailyCooking Energy) \* Days /100000

Where:

ΔDailyIdleEnergy =(IdleBase\* IdleBaseTime) – (IdleENERGYSTAR \* IdleENERGYSTARTime)

ΔDailyPreheatEnergy = (PreHeatNumberBase \* PreheatTimeBase / 60 \* PreheatRateBase) – (PreheatNumberENERGYSTAR\* PreheatTimeENERGYSTAR/60 \* PreheatRateENERGYSTAR)

ΔDailyCookingEnergy = (LB \* EFOOD/ EffBase) - (LB \* EFOOD/ EffENERGYSTAR)

Where:

HOURSday = Average Daily Operation

= custom or if unknown, use 16 hours

Days = Annual days of operation

= custom or if unknown, use 365.25 days a year

LB = Food cooked per day

= custom or if unknown, use 150 pounds

EffENERGYSTAR = Cooking Efficiency ENERGY STAR

= custom or if unknown, use 50%

EffBase = Cooking Efficiency Baseline

= custom or if unknown, use 35%

PCENERGYSTAR = Production Capacity ENERGY STAR

= custom or if unknown, use 65 pounds/hr

PCBase = Production Capacity base

= custom or if unknown, use 60 pounds/hr

PreheatNumberENERGYSTAR = Number of preheats per day

= custom or if unknown, use 1

PreheatNumberBase = Number of preheats per day

= custom or if unknown, use 1

PreheatTimeENERGYSTAR = preheat length

= custom or if unknown, use 15 minutes

PreheatTimeBase = preheat length

= custom or if unknown, use 15 minutes

PreheatRateENERGYSTAR = preheat energy rate high efficiency

= custom or if unknown, use 62000 btu/h

PreheatRateBase = preheat energy rate baseline

= custom or if unknown, use 64000 btu/h

IdleENERGYSTAR = Idle energy rate

= custom or if unknown, use 9000 btu/h

IdleBase = Idle energy rate

= custom or if unknown, use 14000 btu/h

IdleENERGYSTARTime = ENERGY STAR Idle Time

= HOURsday-LB/PCENERGYSTAR –PreHeatTimeENERGYSTAR/60

=Custom or if unknown, use

=16 – 150/65-15/60

=13.44 hours

IdleBaseTime = BASE Idle Time

= HOURsday-LB/PCbase –PreHeatTimeBase/60

=Custom or if unknown, use

=16 – 150/60-15/60

=13.25 hours

EFOOD = ASTM energy to food

= 570 btu/pound

EXAMPLE

For example, an ENERGY STAR fryer with a tested heavy load cooking energy efficiency of 50% and an idle energy rate of 120,981 btu and an Idle Energy Consumption Rate 9000 btu would save.

ΔTherms = (ΔIdle Energy + ΔPreheat Energy + ΔCooking Energy) \* Days /100000

Where:

ΔDailyIdleEnergy =(18550\*13.25)- (120981 \* 13.44)

= 64519 btu

ΔDailyPreheatEnergy = (1 \* 15 / 60 \*64000) – (1 \* 15 / 60 \*62000)

= 500 btu

ΔDailyCookingEnergy = (150 \* 570/ .35) - (150 \* 570/ .5)

=73286 btu

ΔTherms = (64519+500+73286)\* 365.25 /100000

=508 therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-ESFR-V01-120601

### ENERGY STAR Griddle

###### Description

This measure applies to electric and natural gas fired high efficiency griddle installed in a commercial kitchen.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be an ENERGY STAR natural gas or electric griddle with a tested heavy load cooking energy efficiency of 70 percent (electric) 38 percent (gas) or greater and an idle energy rate of 2,650 Btu/hr per square foot of cooking surface or less, utilizing ASTM F1275. The griddle must have an Idle Energy Consumption Rate < 2,600 Btu/hr per square foot of cooking surface.

###### Definition of Baseline Equipment

The baseline equipment is an existing natural gas or electric griddle that’s not ENERGY STAR certified and is at end of use.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 12 years[[102]](#footnote-103)

###### Deemed Measure Cost

The incremental capital cost for this measure is $0 for and electric griddle and $60 for a gas griddle.[[103]](#footnote-104)

###### Loadshape

Loadshape C01 - Commercial Electric Cooking

###### Coincidence Factor

Summer Peak Coincidence Factor for measure is provided below for different building type[[104]](#footnote-105):

|  |  |
| --- | --- |
| Location | CF  CF |
| Fast Food Limited Menu | 0.32 |
| Fast Food Expanded Menu | 0.41 |
| Pizza | 0.46 |
| Full Service Limited Menu | 0.51 |
| Full Service Expanded Menu | 0.36 |
| Cafeteria | 0.36 |

**Algorithm**

###### Calculation of Savings [[105]](#footnote-106)

###### Electric Energy Savings

ΔkWh = (ΔIdle Energy + ΔPreheat Energy + ΔCooking Energy) \* Days /1000

Where:

ΔDailyIdleEnergy =[ IdleBase \* Width \* Length (LB/ PCBase) – (PreheatNumberBase\* PreheatTimeBase/60)]- IdleENERGYSTAR \* Width \* Length (LB/ PCENERGYSTAR) – (PreheatNumberENERGYSTAR\* PreheatTimeENERGYSTAR/60]

ΔDailyPreheatEnergy = (PreHeatNumberBase \* PreheatTimeBase / 60 \* PreheatRateBase \* Width \* Depth) – (PreheatNumberENERGYSTAR\* PreheatTimeENERGYSTAR/60 \* PreheatRateENERGYSTAR \* Width \* Depth)

ΔDailyCookingEnergy = (LB \* EFOOD/ EffBase) - (LB \* EFOOD/ EffENERGYSTAR)

Where:

HOURSday = Average Daily Operation

= custom or if unknown, use 12 hours

Days = Annual days of operation

= custom or if unknown, use 365.25 days a year

LB = Food cooked per day

= custom or if unknown, use 100 pounds

Width = Griddle Width

= custom or if unknown, use 3 feet

Depth = Griddle Depth

= custom or if unknown, use 2 feet

EffENERGYSTAR = Cooking Efficiency ENERGY STAR

= custom or if unknown, use 70%

EffBase = Cooking Efficiency Baseline

= custom or if unknown, use 65%

PCENERGYSTAR = Production Capacity ENERGY STAR

= custom or if unknown, use 6.67 pounds/hr/sq ft

PCBase = Production Capacity base

= custom or if unknown, use 5.83 pounds/hr/sq ft

PreheatNumberENERGYSTAR = Number of preheats per day

= custom or if unknown, use 1

PreheatNumberBase = Number of preheats per day

= custom or if unknown, use 1

PreheatTimeENERGYSTAR = preheat length

= custom or if unknown, use 15 minutes

PreheatTimeBase = preheat length

= custom or if unknown, use 15 minutes

PreheatRateENERGYSTAR = preheat energy rate high efficiency

= custom or if unknown, use 1333 W/sq ft

PreheatRateBase = preheat energy rate baseline

= custom or if unknown, use 2667 W/sq ft

IdleENERGYSTAR = Idle energy rate

= custom or if unknown, use 320 W/sq ft

IdleBase = Idle energy rate

= custom or if unknown, use 400 W/sq ft

EFOOD = ASTM energy to food

= 139 w/pound

For example, an ENERGY STAR griddle with a tested heavy load cooking energy efficiency of 70 percent or greater and an idle energy rate of 320 W per square foot of cooking surface or less would save.

ΔDailyIdleEnergy =[ 400\* 3 \* 2 (100/5.83) – (1\* 15/60)]- [320\* 3 \* 2 (100/6.67) – (1\* 15/60]

= 3583 W

ΔDailyPreheatEnergy = (1\* 15 / 60 \* 2667 \* 3 \* 2) – (1\* 15/60 \* 1333 \* 3 \* 2)

=2000 W

ΔDailyCookingEnergy = (100 \* 139/ .65) - (100 \* 139/ .70)

=1527 W

ΔkWh = (2000+1527+3583) \* 365.25 /1000

=2597 kWh

###### Summer Coincident Peak Demand Savings

kW = ΔkWh/Hours \* CF

For example, an ENERGY STAR griddle in a cafeteria with a tested heavy load cooking energy efficiency of 70 percent or greater and an idle energy rate of 320 W per square foot of cooking surface or less would save

=2595 kWh/4308 \* .36

= 0.22 kW

###### Natural Gas Energy Savings

Custom calculation below, otherwise use deemed value of 149 therms.

ΔTherms = (ΔIdle Energy + ΔPreheat Energy + ΔCooking Energy) \* Days /100000

Where:

ΔDailyIdleEnergy =[ IdleBase \* Width \* Length (LB/ PCBase) – (PreheatNumberBase\* PreheatTimeBase/60)]- IdleENERGYSTAR \* Width \* Length (LB/ PCENERGYSTAR) – (PreheatNumberENERGYSTAR\* PreheatTimeENERGYSTAR/60]

ΔDailyPreheatEnergy = (PreHeatNumberBase \* PreheatTimeBase / 60 \* PreheatRateBase \* Width \* Depth) – (PreheatNumberENERGYSTAR\* PreheatTimeENERGYSTAR/60 \* PreheatRateENERGYSTAR \* Width \* Depth)

ΔDailyCookingEnergy = (LB \* EFOOD/ EffBase) - (LB \* EFOOD/ EffENERGYSTAR)

Where (new variables only):

EffENERGYSTAR = Cooking Efficiency ENERGY STAR

= custom or if unknown, use 38%

EffBase = Cooking Efficiency Baseline

= custom or if unknown, use 32%

PCENERGYSTAR = Production Capacity ENERGY STAR

= custom or if unknown, use 7.5 pounds/hr/sq ft

PCBase = Production Capacity base

= custom or if unknown, use 4.17 pounds/hr/sq ft

PreheatRateENERGYSTAR = preheat energy rate high efficiency

= custom or if unknown, use 10000 btu/h/sq ft

PreheatRateBase = preheat energy rate baseline

= custom or if unknown, use 14000 btu/h/sq ft

IdleENERGYSTAR = Idle energy rate

= custom or if unknown, use 2650 btu/h/sq ft

IdleBase = Idle energy rate

= custom or if unknown, use 3500 btu/h/sq ft

EFOOD = ASTM energy to food

= 475 btu/pound

For example, an ENERGY STAR griddle with a tested heavy load cooking energy efficiency of 38 percent or greater and an idle energy rate of 2,650 Btu/h per square foot of cooking surface or less and an Idle Energy Consumption Rate < 2,600 Btu/h per square foot of cooking surface would save.

ΔDailyIdleEnergy =[ 3500\* 3 \* 2 (100/4.17) – (1\* 15/60)]- 2650\* 3 \* 2 (100/7.5) – (1\* 15/60]

= 11258 Btu

ΔDailyPreheatEnergy = (1\* 15 / 60 \* 14,000 \* 3 \* 2) – (1\* 15/60 \* 10000 \* 3 \* 2)

=6000 btu

ΔDailyCookingEnergy = (100 \* 475/ .32) - (100 \* 475/ .38)

=23438 btu

ΔTherms = (11258 + 6000 + 23438) \* 365.25 /100000

=149 therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-ESGR-V01-120601

### ENERGY STAR Hot Food Holding Cabinets

###### Description

This measure applies to electric ENERGY STAR hot food holding cabinets (HFHC) installed in a commercial kitchen.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be an ENERGY STAR certified HFHC.

###### Definition of Baseline Equipment

The baseline equipment is an electric HFHC that’s not ENERGY STAR certified and at end of life.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 12 years[[106]](#footnote-107)

###### Deemed Measure Cost

The incremental capital cost for this measure is[[107]](#footnote-108)

|  |  |
| --- | --- |
| **HFHC Size** | **Incremental Cost** |
| Full Size (20 cubic feet) | $1200 |
| ¾ Size (12 cubic feet) | $1800 |
| ½ Size (8 cubic feet) | $1500 |

###### Loadshape

Loadshape C01 - Commercial Electric Cooking

###### Coincidence Factor

Summer Peak Coincidence Factor for measure is provided below for different building type[[108]](#footnote-109):

|  |  |
| --- | --- |
| Location | CF  CF |
| Fast Food Limited Menu | 0.32 |
| Fast Food Expanded Menu | 0.41 |
| Pizza | 0.46 |
| Full Service Limited Menu | 0.51 |
| Full Service Expanded Menu | 0.36 |
| Cafeteria | 0.36 |

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

Custom calculation below, otherwise use deemed values depending on HFHC size[[109]](#footnote-110)

|  |  |
| --- | --- |
| **Cabinet Size** | **Savings (kWh)** |
| Full Size HFHC | 9308 |
| ¾ Size HFHC | 3942 |
| ½ Size HFHC | 2628 |

ΔkWh = HFHCBaselinekWh – HFHCENERGYSTARkWh

Where:

HFHCBaselinekWh = PowerBaseline\* HOURSday \* Days/1000

PowerBaseline = Custom, otherwise

|  |  |
| --- | --- |
| Cabinet Size | Power (W) |
| Full Size HFHC | 2500 |
| ¾ Size HFHC | 1200 |
| ½ Size HFHC | 800 |

HOURSday = Average Daily Operation

= custom or if unknown, use 15 hours

Days = Annual days of operation

= custom or if unknown, use 365.25 days a year

HFHCENERGYSTARkWh = PowerENERGYSTAR\* HOURSday \* Days/1000

PowerENERGYSTAR = Custom, otherwise

|  |  |
| --- | --- |
| **Cabinet Size** | **Power (W)** |
| Full Size HFHC | 800 |
| ¾ Size HFHC | 480 |
| ½ Size HFHC | 320 |

HOURSday = Average Daily Operation

= custom or if unknown, use 15 hours

Days = Annual days of operation

= custom or if unknown, use 365.25 days a year

For example, if a full size HFHC is installed the measure would save:

ΔkWh = (PowerBaseline\* HOURSday \* Days)/1000– (PowerENERGYSTAR\* HOURSday \* Days)/1000

= (2500\*15\*365.25)/1000 – (800\*15\*365.25)/1000

= 9,314 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = ΔkWh/Hours \* CF

Where:

Hours = Hoursday \*Days

For example, if a full size HFHC is installed in a cafeteria the measure would save:

= 9,314 kWh / (15\*365.25)\* .36

=0 .61 kW

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-ESHH-V01-120601

### ENERGY STAR Ice Maker

###### Description

This measure relates to the installation of a new ENERGY STAR qualified commercial ice machine. The ENERGY STAR label applied to air-cooled, cube-type machines including ice-making head, self-contained, and remote-condensing units. This measure excludes flake and nugget type ice machines. This measure could relate to the replacing of an existing unit at the end of its useful life, or the installation of a new system in a new or existing building.

This measure was developed to be applicable to the following program types: TOS and NC. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the efficient equipment is assumed to be a new commercial ice machine meeting the minimum ENERGY STAR efficiency level standards.

###### Definition of Baseline Equipment

In order for this characterization to apply, the baseline equipment is assumed to be a commercial ice machine meeting federal equipment standards established January 1, 2010.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 10 years[[110]](#footnote-111).

###### Deemed Measure Cost

The incremental capital cost for this measure is provided below.[[111]](#footnote-112)

|  |  |
| --- | --- |
| Harvest Rate (H) | Incremental Cost |
| 100-200 lb ice machine | $296 |
| 201-300 lb ice machine | $312 |
| 301-400 lb ice machine | $559 |
| 401-500 lb ice machine | $981 |
| 501-1000 lb ice machine | $1,485 |
| 1001-1500 lb ice machine | $1,821 |
| >1500 lb ice machine | $2,194 |

###### Loadshape

Loadshape C23 - Commercial Refrigeration

###### Coincidence Factor

The Summer Peak Coincidence Factor is assumed to equal 0.937

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWH = [(kWhbase – kWhee) / 100] \* (DC \* H) \* 365.25

Where:

kWhbase  = maximum kWh consumption per 100 pounds of ice for the baseline equipment

= calculated as shown in the table below using the actual Harvest Rate (H) of the efficient equipment.

kWhee = maximum kWh consumption per 100 pounds of ice for the efficient equipment

= calculated as shown in the table below using the actual Harvest Rate (H) of the efficient equipment.

|  |  |  |
| --- | --- | --- |
| Ice Machine Type | kWhbase[[112]](#footnote-113) | kWhee[[113]](#footnote-114) |
| Ice Making Head (H < 450) | 10.26 - 0.0086\*H | 9.23 - 0.0077\*H |
| Ice Making Head (H ≥ 450) | 6.89 – 0.0011\*H | 6.20 - 0.0010\*H |
| Remote Condensing Unit, without remote compressor (H < 1000) | 8.85 – 0.0038\*H | 8.05 - 0.0035\*H |
| Remote Condensing Unit, without remote compressor (H ≥ 1000) | 5.1 | 4.64 |
| Remote Condensing Unit, with remote compressor (H < 934) | 8.85 – 0.0038\*H | 8.05 - 0.0035\*H |
| Remote Condensing Unit, with remote compressor (H ≥ 934) | 5.3 | 4.82 |
| Self Contained Unit (H < 175) | 18 - 0.0469\*H | 16.7 - 0.0436\*H |
| Self Contained Unit (H ≥ 175) | 9.8 | 9.11 |

100 = conversion factor to convert kWhbase and kWhee into maximum kWh consumption per pound of ice.

DC = Duty Cycle of the ice machine

= 0.57[[114]](#footnote-115)

H = Harvest Rate (pounds of ice made per day)

= Actual installed

365.35 = days per year

For example an ice machine with an ice making head producing 450 pounds of ice would save

ΔkWH = [(6.4 – 5.8) / 100] \* (0.57 \* 450) \* 365.25

= 562 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = ΔkWh / (HOURS \* DC) \* CF

Where:

HOURS = annual operating hours

= 8766[[115]](#footnote-116)

CF = 0.937

For example an ice machine with an ice making head producing 450 pounds of ice would save

ΔkW = 562/(8766 \* 0.57) \* .937

= 0.105 kW

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

While the ENERGY STAR labeling criteria require that certified commercial ice machines meet certain “maximum potable water use per 100 pounds of ice made” requirements, such requirements are intended to prevent equipment manufacturers from gaining energy efficiency at the cost of water consumptions. A review of the AHRI Certification Directory[[116]](#footnote-117) indicates that approximately 81% of air-cooled, cube-type machines meet the ENERGY STAR potable water use requirement. Therefore, there are no assumed water impacts for this measure.

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-ESIM-V01-120601

### High Efficiency Pre-Rinse Spray Valve

**Description**

Pre-rise valves use a spray of water to remove food waste from dishes prior to cleaning in a dishwasher. More efficient spray valves use less water thereby reducing water consumption, water heating cost, and waste water (sewer) charges. Pre-rinse spray valves include a nozzle, squeeze lever, and dish guard bumper. The primary impacts of this measure are water savings. Reduced hot water consumption saves either natural gas or electricity, depending on the type of energy the hot water heater uses.

This measure was developed to be applicable to the following program types: TOS, RF, and DI. If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

To qualify for this measure, the new or replacement pre-rinse spray nozzle must use less than 1.6 gallons per minute with a cleanability performance of 26 seconds per plate or less.

**Definition of Baseline Equipment**

The baseline equipment will vary based on the delivery method and is defined below:

|  |  |
| --- | --- |
| **Time of Sale** | **Retrofit, Direct Install** |
| The baseline equipment is assumed to be 1.6 gallons per minute. The Energy Policy Act (EPAct) of 2005 sets the maximum flow rate for pre-rinse spray valves at 1.6 gallons per minute at 60 pounds per square inch of water pressure when tested in accordance with ASTM F2324-03. This performance standard went into effect January 1, 2006. | The baseline equipment is assumed to be an existing pre-rinse spray valve with a flow rate of 1.9 gallons per minute.[[117]](#footnote-118) If existing pre-rinse spray valve flow rate is unknown, then existing pre-rinse spray valve must have been installed prior to 2006. The Energy Policy Act (EPAct) of 2005 sets the maximum flow rate for pre-rinse spray valves at 1.6 gallons per minute at 60 pounds per square inch of water pressure when tested in accordance with ASTM F2324-03. This performance standard went into effect January 1, 2006. However, field data shows that not all nozzles in use have been replaced with the newer flow rate nozzle. Products predating this standard can use up to five gallons per minute |

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 5 years[[118]](#footnote-119)

**Deemed Measure Cost**

The cost of this measure is assumed to be $100[[119]](#footnote-120)

**Loadshape**

Loadshape C01 - Commercial Electric Cooking

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings (note water savings must first be calculated)**

ΔkWH = ΔGallons x 8.33 x 1 x (Tout - Tin) x (1/EFF electric) /3,413 x FLAG

Where:

ΔGallons = amount of water saved as calculated below

8.33 lbm/gal = specific mass in pounds of one gallon of water

1 Btu/lbm°F = Specific heat of water: 1 Btu/lbm/°F

Tout = Water Heater Outlet Water Temperature

= custom, otherwise assume Tin + 70°F temperature rise from Tin[[120]](#footnote-121)

Tin = Inlet Water Temperature

= custom, otherwise assume 54.1 °F[[121]](#footnote-122)

EFF = Efficiency of electric water heater supplying hot water to pre-rinse spray valve

=custom, otherwise assume 97%[[122]](#footnote-123)

Flag = 1 if electric or 0 if gas

EXAMPLE

Time of Sale: For example, a new spray nozzle with 1.06 gal/min flow replacing a nozzle with 1.6 gal/min flow at a large institutional establishments with a cafeteria with 70 degree temperature rise of water used by the pre-rinse spray valve that is heated by electric hot water saves annually :

ΔkWH = 30,326x 8.33 x 1 x ((70+54.1) - 54.1) x (1/.97) /3,413 x 1

= 5,341kWh

Retrofit: For example, a new spray nozzle with 1.06 gal/min flow replacing a nozzle with 1.9 gal/min flow at a large institutional establishments with a cafeteria with 70 degree temperature rise of water used by the pre-rinse spray valve that is heated by electric hot water equals:

ΔkWH = 47,175 x 8.33 x 1 x ((70+ 54.1) - 54.1) x (1/.97) /3,413 x 1

=8309 kWh

**Summer Coincident Peak Demand Savings**

N/A

**Natural Gas Energy Savings**

ΔTherms = ΔGallons x 8.33 x 1 x (Tout - Tin) x (1/EFF) /100,000 Btu

Where (new variables only):

EFF = Efficiency of gas water heater supplying hot water to pre-rinse spray valve

= custom, otherwise assume 75%[[123]](#footnote-124)

EXAMPLE

Time of Sale: For example, a new spray nozzle with 1.06 gal/min flow replacing a nozzle with 1.6 gal/min flow at a large institutional establishments with a cafeteria with 70 degree temperature of water used by the pre-rinse spray valve that is heated by fossil fuel hot water saves annually:

ΔTherms = 30,326 x 8.33 x 1 x ((70+54.1) - 54.1) x (1/.75)/100,000 x 1.0

= 236 Therms

Retrofit: For example, a new spray nozzle with 1.06 gal/min flow replacing a nozzle with 1.9 gal/min flow at a busy large institutional establishments with a cafeteria with 70 degree temperature rise of water used by the pre-rinse spray valve that is heated by fossil fuel hot water saves annually:

ΔTherms = 47,175 x 8.33 x 1 x ((70+54.1) - 54.1) x (1/.75)/100,000 x (1-0)

=368 Therms

**Water Impact Calculation[[124]](#footnote-125)**

ΔGallons = (FLObase - FLOeff)gal/min x 60 min/hr x HOURSday x DAYSyear

FLObase = Base case flow in gallons per minute, or custom

|  |  |
| --- | --- |
| **Time of Sale** | **Retrofit, Direct Install** |
| 1.6 gal/min[[125]](#footnote-126) | 1.9 gal/min[[126]](#footnote-127) |

FLOeff = Efficient case flow in gallons per minute or custom

|  |  |
| --- | --- |
| **Time of Sale** | **Retrofit, Direct Install** |
| 1.06 gal/min[[127]](#footnote-128) | 1.06 gal/min[[128]](#footnote-129) |

HOURSday = Hours per day that the pre-rinse spray valve is used at the site, custom, otherwise[[129]](#footnote-130):

|  |  |
| --- | --- |
| **Application** | **Hours/day** |
| Small, quick- service restaurants | 1/2 |
| Medium-sized casual dining restaurants | 1.5 |
| Large institutional establishments with cafeteria | 3 |

DAYSyear = Days per year pre-rinse spray valve is used at the site, custom, otherwise 312 days/yr based on assumed 6 days/wk x 52 wk/yr = 312 day/yr.

EXAMPLE

Time of Sale: For example, a new spray nozzle with 1.06 gal/min flow replacing a nozzle with 1.6 gal/min flow at a large institutional establishment with a cafeteria equals

= (1.6 – 1.06) \* 60 \* 3 \* 312

= 30,326 gal/yr

Retrofit: For example, a new spray nozzle with 106 gal/min flow replacing a nozzle with 1.9 gal/min flow at a large institutional establishments with a cafeteria equals

= (1.9 – 1.06) \* 60 \* 3 \* 312

= 47,175 gal/yr

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-FSE-SPRY-V02-120601**

### Infrared Charbroiler

###### Description

This measure applies to natural gas fired charbroilers that utilize infrared burners installed in a commercial kitchen

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a new natural gas charbroiler with infrared burners.

###### Definition of Baseline Equipment

The baseline equipment is an existing natural gas charbroiler without infrared burners.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 12 years[[130]](#footnote-131)

###### Deemed Measure Cost

The incremental capital cost for this measure is $2200[[131]](#footnote-132)

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

The annual natural gas energy savings from this measure is a deemed value equaling 661 Therms.[[132]](#footnote-133)

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-IRCB-V01-120601

### Infrared Rotisserie Oven

###### Description

This measure applies to natural gas fired high efficiency rotisserie ovens utilizing infrared burners and installed in a commercial kitchen.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a new natural gas rotisserie oven with infrared burners.

###### Definition of Baseline Equipment

The baseline equipment is an existing natural gas rotisserie oven without infrared burners.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 12 years[[133]](#footnote-134)

###### Deemed Measure Cost

The incremental capital cost for this measure is $2700[[134]](#footnote-135)

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

The annual natural gas energy savings from this measure is a deemed value equaling 554 Therms[[135]](#footnote-136)

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-IROV-V01-120601

### Infrared Salamander Broiler

###### Description

This measure applies to natural gas fired high efficiency salamander broilers utilizing infrared burners installed in a commercial kitchen.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a new natural gas salamander broiler with infrared burners

###### Definition of Baseline Equipment

The baseline equipment is an existing natural gas salamander broiler without infrared burners

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 12 years[[136]](#footnote-137)

###### Deemed Measure Cost

The incremental capital cost for this measure is $1000[[137]](#footnote-138)

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

The annual natural gas energy savings from this measure is a deemed value equaling 239 therms[[138]](#footnote-139)

###### Water Impact Descriptions and Calculation

###### Deemed O&M Cost Adjustment Calculation

###### Measure Code: CI-FSE-IRBL-V01-120601

### Infrared Upright Broiler

###### Description

This measure applies to natural gas fired high efficiency upright broilers utilizing infrared burners and installed in a commercial kitchen.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a new natural gas upright broiler with infrared burners.

###### Definition of Baseline Equipment

The baseline equipment is an existing natural gas upright broiler without infrared burners.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 10 years[[139]](#footnote-140)

###### Deemed Measure Cost

The incremental capital cost for this measure is $5900[[140]](#footnote-141)

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

The annual natural gas energy savings from this measure is a deemed value equaling 1089 therms[[141]](#footnote-142).

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-IRUB-V01-120601

### Kitchen Demand Ventilation Controls

###### Description

Installation of commercial kitchen demand ventilation controls that vary the ventilation based on cooking load and/or time of day.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a control system that varies the exhaust rate of kitchen ventilation (exhaust and/or makeup air fans) based on the energy and effluent output from the cooking appliances (i.e., the more heat and smoke/vapors generated, the more ventilation needed). This involves installing a new temperature sensor in the hood exhaust collar and/or an optic sensor on the end of the hood that sense cooking conditions which allows the system to automatically vary the rate of exhaust to what is needed by adjusting the fan speed accordingly.

###### Definition of Baseline Equipment

The baseline equipment is kitchen ventilation that has constant speed ventilation motor.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 15 years.[[142]](#footnote-143)

###### Deemed Measure Cost

The incremental capital cost for this measure is[[143]](#footnote-144)

|  |  |
| --- | --- |
| Measure Category | Incremental Cost , $/fan |
| DVC Control Retrofit | $1,988 |
| DVC Control New | $1,000 |

###### Loadshape

Loadshape C23 - Commercial Ventilation

###### Coincidence Factor

The measure has deemed peak kW savings therefore a coincidence factor does not apply

**Algorithm**

###### Calculation of Savings

Annual energy use was based on monitoring results from five different types of sites, as summarized in PG&E Food Service Equipment work paper.

###### Electric Energy Savings

The following table provides the kWh savings

|  |  |
| --- | --- |
| Measure Name | Annual Energy Savings Per Unit (kWh/fan) |
| DVC Control Retrofit | 4,486 |
| DVC Control New | 4,486 |

###### Summer Coincident Peak Demand Savings

The following table provides the kW savings

|  |  |
| --- | --- |
| Measure Name | Coincident Peak Demand Reduction (kW) |
| DVC Control Retrofit | 0.76 |
| DVC Control New | 0.76 |

###### Natural Gas Energy Savings

ΔTherms = CFM \* HP\* Annual Heating Load /(Eff(heat) \* 100,000)

Where:

CFM = the average airflow reduction with ventilation controls per hood

= 611 cfm/HP[[144]](#footnote-145)

HP = actual if known, otherwise assume 7.75 HP

Annual Heating Load = Annual heating energy required to heat fan exhaust make-up air, Btu/cfm dependent on location[[145]](#footnote-146):

|  |  |
| --- | --- |
| Zone | Annual Heating Load, Btu/cfm |
| 1 (Rockford) | 154,000 |
| 2-(Chicago) | 144,000 |
| 3 (Springfield) | 132,000 |
| 4-(Belleville) | 102,000 |
| 5-(Marion) | 104,000 |

Eff(heat) = Heating Efficiency

= actual if known, otherwise assume 80%[[146]](#footnote-147)

100,000 = conversion from Btu to Therm

EXAMPLE

For example, a kitchen hood in Rockford, IL with a 7.75 HP ventilation motor

ΔTherms = 611 \* 7.75\*154,000 / (0.80 \* 100,000)

= 9,115 Therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-VENT-V02-140601

### Pasta Cooker

###### Description

This measure applies to natural gas fired dedicated pasta cookers as determined by the manufacturer and installed in a commercial kitchen.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a new natural gas fired paste cooker.

###### Definition of Baseline Equipment

The baseline equipment is an existing natural gas fired stove where pasta is cooked in a pan.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 12[[147]](#footnote-148).

###### Deemed Measure Cost

The incremental capital cost for this measure is $2400[[148]](#footnote-149).

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

The annual natural gas energy savings from this measure is a deemed value equaling 1380 Therms[[149]](#footnote-150).

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-PCOK-V01-120601

### Rack Oven - Double Oven

###### Description

This measure applies to natural gas fired high efficiency rack oven - double oven installed in a commercial kitchen.

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a new natural gas rack oven –double oven with a baking efficiency ≥ 50% utilizing ASTM standard 2093

###### Definition of Baseline Equipment

The baseline equipment is an existing natural gas rack oven – double oven with a baking efficiency < 50%.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 12 years.[[150]](#footnote-151)

###### Deemed Measure Cost

The incremental capital cost for this measure is $8646.[[151]](#footnote-152)

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

The annual natural gas energy savings from this measure is a deemed value equaling 2064 therms[[152]](#footnote-153)

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-FSE-RKOV-V01-120601

### ENERGY STAR Electric Convection Oven

**Description**

Commercial convection ovens that are ENERGY STAR certified have higher heavy load cooking efficiencies, and lower idle energy rates, making them on average about 20 percent more efficient than standard models. Energy savings estimates are for ovens using full size (18” x 36”) sheet pans.

This measure was developed to be applicable to the following program types; TOS.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

The efficient equipment is assumed to be an ENERGY STAR qualified electric convection oven.

**Definition of Baseline Equipment**

The baseline equipment is assumed to be a standard convection oven with a heavy load efficiency of 65%.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 12 years.[[153]](#footnote-154)

**Deemed Measure Cost**

The incremental cost for this measure is assumed to be $800 for half size units and $1000 for full size[[154]](#footnote-155)

**Loadshape**

Loadshape C01 - Commercial Electric Cooking

**Coincidence Factor**

Summer Peak Coincidence Factor for measure is provided below for different building type[[155]](#footnote-156):

|  |  |
| --- | --- |
| **Location** | **CF**  **CF** |
| Fast Food Limited Menu | 0.32 |
| Fast Food Expanded Menu | 0.41 |
| Pizza | 0.46 |
| Full Service Limited Menu | 0.51 |
| Full Service Expanded Menu | 0.36 |
| Cafeteria | 0.36 |
| Unknown | 0.40 |

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

ΔkWh = kWHbase - kWheff

kWh = [(LB \* EFOOD/EFF) + (IDLE \* (HOURSDAY – LB/PC – PRETIME/60)) + PREENERGY] \* DAYS

Where:

kWHbase = the annual energy usage of the baseline equipment calculated using baseline values

kWHeff = the annual energy usage of the efficient equipment calculated using efficient values

HOURSDAY = daily operating hours

= Actual, defaults:

|  |  |
| --- | --- |
| **Type of Food Service** | **HOURSDAY [[156]](#footnote-157)** |
| Fast Food, limited menu | 4 |
| Fast Food, expanded menu | 5 |
| Pizza | 8 |
| Full Service, limited menu | 8 |
| Full Service, expanded menu | 7 |
| Cafeteria | 6 |
| Unknown | 6[[157]](#footnote-158) |
| Custom | Varies |

DAYS = Days per year of operation

= Actual, default = 365[[158]](#footnote-159)

PRETIME = Preheat time (min/day), the amount of time it takes a steamer to reach operating temperature when turned on

= 15 min/day[[159]](#footnote-160)

EFOOD = ASTM Energy to Food (kWh/lb); the amount of energy absorbed by the food during cooking, per pound of food

= 0.0732[[160]](#footnote-161)

LB = pounds of food cooked per day (lb/day)

= Actual, default = 100[[161]](#footnote-162)

EFF = Heavy load cooking energy efficiency (%). See table below.

IDLE = Idle energy rate. See table below.

PC = Production capacity (lbs/hr). See table below.

PREENERGY = Preheat energy (kWh/day). See table below.

Performance Metrics: Baseline and Efficient Values

|  |  |  |
| --- | --- | --- |
| **Metric** | **Baseline Model [[162]](#footnote-163)** | **Energy Efficient Model [[163]](#footnote-164)** |
| PREENERGY (kWh) | 1.5 | 1 |
| IDLE (kW) | 2 | Actual, default = 1.0 |
| EFF | 65% | Actual, default = 74% |
| PC (lb/hr) | 70 | Actual, default = 79 |

EXAMPLE

Using defaults provided above, the savings for a ENERGY STAR Electric Convection Oven in unknown location are:

kWHbase = [(100 \* 0.0732/0.65) + (2 \* (6 – 100/70 – 15/60)) + 1.5] \* 365

= 12,193 kWh

kWheff  = [(100 \* 0.0732/0.74) + (1 \* (6 – 100/79 – 15/60)) + 1.0] \* 365

= 11,629 kWh

ΔkWh = kWHbase - kWheff

= 7,813 – 5,612

= 2200 kWh

**Summer Coincident Peak Demand Savings**

ΔkW = (ΔkWh / (HOURSDAY \* DAYS)) \* CF

Where:

ΔkWh = Annual energy savings (kWh)

CF = Summer Peak Coincidence Factor for measure is provided below for different building type[[164]](#footnote-165):

|  |  |
| --- | --- |
| **Location** | **CF**  **CF** |
| Fast Food Limited Menu | 0.32 |
| Fast Food Expanded Menu | 0.41 |
| Pizza | 0.46 |
| Full Service Limited Menu | 0.51 |
| Full Service Expanded Menu | 0.36 |
| Cafeteria | 0.36 |
| Unknown | 0.40 |

EXAMPLE

Using defaults provided above, the savings for a ENERGY STAR Electric Convection Oven in unknown location are:

ΔkW = (2200 / (6 \* 365)) \* 0.40

= 0.40

**Fossil Fuel Impact Descriptions and Calculation**

N/A

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

###### Measure Code: CI-FSE-ECON-V01-150601

## Hot Water

### Storage Water Heater

###### Description

This measure is for upgrading from minimum code to a storage-type water heaters. Storage water heaters are used to supply hot water for a variety of commercial building types. Storage capacities vary greatly depending on the application. Large consumers of hot water include (but not limited to) industries, hotels/motels and restaurants.

This measure was developed to be applicable to the following program types: TOS, RF, ER.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

|  |  |  |
| --- | --- | --- |
| Gas, High Efficiency | Gas, Standard | Electric |
| In order for this characterization to apply, the efficient equipment is assumed to have heating capacity over 75,000 Btu/hr and a Thermal Efficiency (TE) greater than or equal to 88% | In order for this characterization to apply, the efficient equipment is assumed to be a gas-fired storage water heaters with 0.67 EF or better installed in a non-residential application  Primary applications would include (but not limited to) hotels/motels, small commercial spaces, offices and restaurants | In order for this characterization to apply, the efficient equipment is assumed to have[[165]](#footnote-166).:  Energy factor greater than or equal to 0.95 Minimum Thermal Efficiency of 0.98  Less than 3% standby loss (standby loss is calculated as percentage of annual (energy usage)  Equivalent storage capacity to unit being replaced  Qualified units must be GAMA/AHRI efficiency rating certified |

###### Definition of Baseline Equipment

|  |  |  |
| --- | --- | --- |
| Gas, High Efficiency | Gas, Standard | Electric |
| In order for this characterization to apply, the baseline condition is assumed to be a water heater with heating capacity over 75,000 Btu/hr and a Thermal Efficiency (TE) of 80% | In order for this characterization to apply, the baseline condition is assumed to be the minimum code compliant unit with 0.575 EF. | In order for this characterization to apply, the baseline equipment is assumed to be an electric storage water heater with 50 or more gallon capacity in input wattage between 12kW and 54kW. |

###### Deemed Lifetime of Efficient Equipment

|  |  |  |
| --- | --- | --- |
| Gas, High Efficiency | Gas, Standard | Electric |
| The expected measure life is assumed to be 15 Years[[166]](#footnote-167) | The expected measure life is assumed to be 15 years[[167]](#footnote-168) | The expected measure life is assumed to be 5 years[[168]](#footnote-169). |

###### Deemed Measure Cost

|  |  |  |
| --- | --- | --- |
| Gas, High Efficiency | Gas, Standard | Electric |
| The incremental capital cost for this measure is $209 | The deemed measure cost is assumed to be $400 | The incremental capital cost for this measure is assumed to be[[169]](#footnote-170)   |  |  | | --- | --- | | Tank Size | Incremental Cost | | 50 gallons | $1050 | | 80 gallons | $1050 | | 100 gallons | $1950 | |

###### Loadshape

|  |  |  |
| --- | --- | --- |
| Gas, High Efficiency | Gas, Standard | Electric |
| N/A | N/A | Loadshape C02 - Non-Residential Electric DHW |

###### Coincidence Factor

|  |  |  |
| --- | --- | --- |
| Gas, High Efficiency | Gas, Standard | Electric |
| N/A | N/A | The measure has deemed kW savings therefor a coincidence factor is not applied |

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings [[170]](#footnote-171)

The annual electric savings the electric water storage tank and heater is a deemed value and assumed to be:

|  |  |
| --- | --- |
| Tank Size | Savings (kWh) |
| 50 gallons | 1780.85 |
| 80 gallons | 4962.69 |
| 100 gallons | 8273.63 |

###### Summer Coincident Peak Demand Savings[[171]](#footnote-172)

The annual kW savings from this measure is a deemed value and assumed to be:

|  |  |
| --- | --- |
| Tank Size | Savings (kW) |
| 50 gallons | 0.20 |
| 80 gallons | 0.57 |
| 100 gallons | 0.94 |

###### Natural Gas Energy Savings

|  |  |
| --- | --- |
| Gas, High Efficiency | Gas, Standard |
| The annual natural gas energy savings from this measure is a deemed value equaling 251[[172]](#footnote-173) | Gas savings depend on building type and are based on measure case energy factor of 0.67 and a heating capacity of 75 MBtu/hr. These values are averages of qualifying units. Savings values are derived from 2008 DEER Miser, which provides MBtu/hr gas savings per MBtu/hr capacity. Savings presented here are per water heater.[[173]](#footnote-174)   |  |  | | --- | --- | | Building Type | Energy Savings (therms/unit) | | Assembly | 185 | | Education – Primary/Secondary | 124 | | Education – Post Secondary | 178 | | Grocery | 191 | | Health/Medical - Hospital | 297 | | Lodging - Hotel | 228 | | Manufacturing - Light Industrial | 140 | | Office – > 60,000 sq-ft | 164 | | Office – < 60,000 sq-ft | 56 | | Restaurant - FastFood | 109 | | Restaurant – Sit Down | 166 | | Retail | 105 | | Storage | 150 | | Multi-Family | 119 | | Other | 148 | |

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-HW\_-STWH-V01-120601

* + 1. Low Flow Faucet Aerators

**Description**

This measure relates to the direct installation of a low flow faucet aerator in a commercial building. Expected applications include small business, office, restaurant, or motel. For multifamily or senior housing, the residential low flow faucet aerator should be used.

This measure was developed to be applicable to the following program types, DI.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

To qualify for this measure the installed equipment must be an energy efficient faucet aerator, for bathrooms rated at 1.5 gallons per minute (GPM) or less, or for kitchens rated at 2.2 GPM or less. Savings are calculated on an average savings per faucet fixture basis.

**Definition of Baseline Equipment**

The baseline condition is assumed to be a standard bathroom faucet aerator rated at 2.25 GPM or more, or a standard kitchen faucet aerator rated at 2.75 GPM or more. Note if flow rates are measured, for example through a Direct Install program, then actual baseline flow rates should be used as opposed to the deemed values.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 9 years.[[174]](#footnote-175)

**Deemed Measure Cost**

The incremental cost for this measure is $8[[175]](#footnote-176) or program actual.

**Loadshape**

Loadshape C02 - Commercial Electric DHW

**Coincidence Factor**

The coincidence factor for this measure is dependent on building type as presented below.

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

**Note these savings are *per* faucet retrofitted[[176]](#footnote-177).**

ΔkWh = %ElectricDHW  \* ((GPM\_base - GPM\_low)/GPM\_base) \* Usage \* EPG\_electric \* ISR

Where:

%ElectricDHW = proportion of water heating supplied by electric resistance heating

|  |  |
| --- | --- |
| DHW fuel | %Electric\_DHW |
| Electric | 100% |
| Fossil Fuel | 0% |

GPM\_base = Average flow rate, in gallons per minute, of the baseline faucet “as-used”

= 1.39[[177]](#footnote-178) or custom based on metering studies[[178]](#footnote-179) or if measured during DI:

= Measured full throttle flow \* 0.83 throttling factor[[179]](#footnote-180)

GPM\_low = Average flow rate, in gallons per minute, of the low-flow faucet aerator “as-used”

= 0.94[[180]](#footnote-181) or custom based on metering studies[[181]](#footnote-182) or if measured during DI:

= Rated full throttle flow \* 0.95 throttling factor[[182]](#footnote-183)

Usage = Estimated usage of mixed water (mixture of hot water from water heater line and cold water line) per faucet (gallons per year)

= If data is available to provide a reasonable custom estimate it should be used, if not use the following defaults (or substitute custom information in to the calculation):

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| **Building Type** | **Gallons hot water per unit per day[[183]](#footnote-184)**  **(A)** | **Unit** | **Estimated % hot water from Faucets [[184]](#footnote-185)**  **(B)** | **Multiplier [[185]](#footnote-186)**  **(C)** | **Unit** | **Days per year**  **(D)** | **Annual gallons mixed water per faucet**  **(A\*B\*C\*D)** |
| Small Office | 1 | person | 100% | 10 | employees per faucet | 250 | 2,500 |
| Large Office | 1 | person | 100% | 45 | employees per faucet | 250 | 11,250 |
| Fast Food Rest | 0.7 | meal/day | 50% | 75 | meals per faucet | 365 | 9,581 |
| Sit-Down Rest | 2.4 | meal/day | 50% | 36 | meals per faucet | 365 | 15,768 |
| Retail | 2 | employee | 100% | 5 | employees per faucet | 365 | 3,650 |
| Grocery | 2 | employee | 100% | 5 | employees per faucet | 365 | 3,650 |
| Warehouse | 2 | employee | 100% | 5 | employees per faucet | 250 | 2,500 |
| Elementary School | 0.6 | person | 50% | 50 | students per faucet | 200 | 3,000 |
| Jr High/High School | 1.8 | person | 50% | 50 | students per faucet | 200 | 9,000 |
| Health | 90 | patient | 25% | 2 | Patients per faucet | 365 | 16,425 |
| Motel | 20 | room | 25% | 1 | faucet per room | 365 | 1,825 |
| Hotel | 14 | room | 25% | 1 | faucet per room | 365 | 1,278 |
| Other | 1 | employee | 100% | 20 | employees per faucet | 250 | 5,000 |

EPG\_electric = Energy per gallon of mixed water used by faucet (electric water heater)

= (8.33 \* 1.0 \* (WaterTemp - SupplyTemp)) / (RE\_electric \* 3412)

= (8.33 \* 1.0 \* (90 – 54.1)) / (0.98 \* 3412)

= 0.0894 kWh/gal

8.33 = Specific weight of water (lbs/gallon)

1.0 = Heat Capacity of water (btu/lb-°F)

WaterTemp = Assumed temperature of mixed water

= 86F for Bath, 93F for Kitchen 91F for Unknown[[186]](#footnote-187)

SupplyTemp = Assumed temperature of water entering building

= 54.1°F [[187]](#footnote-188)

RE\_electric = Recovery efficiency of electric water heater

= 98% [[188]](#footnote-189)

3412 = Converts Btu to kWh (Btu/kWh)

ISR = In service rate of faucet aerators dependant on install method as listed in table below[[189]](#footnote-190)

|  |  |
| --- | --- |
| **Selection** | **ISR** |
| Direct Install - Deemed | 0.95 |

EXAMPLE

For example, a direct installed faucet in a large office with electric DHW:

ΔkWh = 1 \* ((1.39 – 0.94)/1.39) \* 11,250 \* 0.0894 \* 0.95

= 309 kWh

For example, a direct installed faucet in an Elementary School with electric DHW:

ΔkWh = 1 \* ((1.39 – 0.94)/1.39) \* 3,000 \* 0.0894 \* 0.95

= 82.5 kWh

**Summer Coincident Peak Demand Savings**

ΔkW = (ΔkWh / Hours) \* CF

Where:

ΔkWh = calculated value above on a per faucet basis

Hours = Annual electric DHW recovery hours for faucet use

= (Usage \* 0.545[[190]](#footnote-191) )/GPH

= Calculate if usage is custom, if using default usage use:

|  |  |
| --- | --- |
| **Building Type** | **Annual Recovery Hours** |
| Small Office | 24 |
| Large Office | 109 |
| Fast Food Rest | 93 |
| Sit-Down Rest | 153 |
| Retail | 36 |
| Grocery | 36 |
| Warehouse | 24 |
| Elementary School | 29 |
| Jr High/High School | 88 |
| Health | 160 |
| Motel | 18 |
| Hotel | 12 |
| Other | 49 |

Where:

GPH = Gallons per hour recovery of electric water heater calculated for 85.9F temp rise (140-54.1), 98% recovery efficiency, and typical 12kW electric resistance storage tank.

= 56

CF = Coincidence Factor for electric load reduction

= Dependent on building type[[191]](#footnote-192)

|  |  |
| --- | --- |
| **Building Type** | **Coincidence Factor** |
| Small Office | 0.0064 |
| Large Office | 0.0288 |
| Fast Food Rest | 0.0084 |
| Sit-Down Rest | 0.0184 |
| Retail | 0.0043 |
| Grocery | 0.0043 |
| Warehouse | 0.0064 |
| Elementary School | 0.0096 |
| Jr High/High School | 0.0288 |
| Health | 0.0144 |
| Motel | 0.0006 |
| Hotel | 0.0004 |
| Other | 0.0128 |

EXAMPLE

For example, a direct installed faucet in a large office with electric DHW:

ΔkW = 309/109 \* 0.0288

= 0.0816 kW

For example, a direct installed faucet in an Elementary School with electric DHW:

ΔkW = 82.5/29 \* 0.0096

= 0.0273 kW

**Fossil Fuel Impact Descriptions and Calculation**

ΔTherms = %FossilDHW \* ((GPM\_base - GPM\_low)/GPM\_base) \* Usage \* EPG\_gas \* ISR

Where:

%FossilDHW = proportion of water heating supplied by fossil fuel heating

|  |  |
| --- | --- |
| **DHW fuel** | **%Fossil\_DHW** |
| Electric | 0% |
| Fossil Fuel | 100% |

EPG\_gas = Energy per gallon of mixed water used by faucet (gas water heater)

= (8.33 \* 1.0 \* (WaterTemp - SupplyTemp)) / (RE\_gas \* 100,000)

= 0.00446 Therm/gal

Where:

RE\_gas = Recovery efficiency of gas water heater

` = 67% [[192]](#footnote-193)

100,000 = Converts Btus to Therms (Btu/Therm)

Other variables as defined above.

EXAMPLE

For example, a direct installed faucet in a large office with gas DHW:

ΔTherms = 1 \* ((1.39 – 0.94)/1.39) \* 11,250 \* 0.00446 \* 0.95

= 15.4 Therms

For example, a direct installed faucet in a Elementary School with gas DHW:

ΔTherms = 1 \* ((1.39 – 0.94)/1.39) \* 3,000 \* 0.00446 \* 0.95

= 4.12 Therms

**Water Impact Descriptions and Calculation**

Δgallons = ((GPM\_base - GPM\_low)/GPM\_base) \* Usage \* ISR

Variables as defined above

EXAMPLE

For example, a direct installed faucet in a large office:

Δgallons = ((1.39 – 0.94)/1.39) \* 11,250 \* 0.95

= 3,640 gallons

For example, a direct installed faucet in a Elementary School:

Δgallons = ((1.39 – 0.94)/1.39) \* 3,000 \* 0.95

= 971 gallons

**Deemed O&M Cost Adjustment Calculation**

N/A

**Sources used for GPM assumptions**

|  |  |
| --- | --- |
| **Source ID** | **Reference** |
| 1 | 2011, DeOreo, William. California Single Family Water Use Efficiency Study. April 20, 2011. |
| 2 | 2000, Mayer, Peter, William DeOreo, and David Lewis. Seattle Home Water Conservation Study. December 2000. |
| 3 | 1999, Mayer, Peter, William DeOreo. Residential End Uses of Water. Published by AWWA Research Foundation and American Water Works Association. 1999. |
| 4 | 2003, Mayer, Peter, William DeOreo. Residential Indoor Water Conservation Study. Aquacraft, Inc. Water Engineering and Management. Prepared for East Bay Municipal Utility District and the US EPA. July 2003. |
| 5 | 2011, DeOreo, William. Analysis of Water Use in New Single Family Homes. By Aquacraft. For Salt Lake City Corporation and US EPA. July 20, 2011. |
| 6 | 2011, Aquacraft. Albuquerque Single Family Water Use Efficiency and Retrofit Study. For Albuquerque Bernalillo County Water Utility Authority. December 1, 2011. |
| 7 | 2008, Schultdt, Marc, and Debra Tachibana. Energy related Water Fixture Measurements: Securing the Baseline for Northwest Single Family Homes. 2008 ACEEE Summer Study on Energy Efficiency in Buildings. |

**Measure Code: CI-HWE-LFFA-V05-140601**

### Low Flow Showerheads

**Description**

This measure relates to the direct installation of a low flow showerhead in a commercial building. Expected applications include small business, office, restaurant, or small motel. For multifamily or senior housing, the residential low flow showerhead should be used.

This measure was developed to be applicable to the following program types: DI.

If applied to other program types, the measure savings should be verified

**Definition of Efficient Equipment**

To qualify for this measure the installed equipment must be an energy efficient showerhead rated at 2.0 gallons per minute (GPM) or less. Savings are calculated on a per showerhead fixture basis.

**Definition of Baseline Equipment**

The baseline condition is assumed to be a standard showerhead rated at 2.5 GPM.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 10 years.[[193]](#footnote-194)

**Deemed Measure Cost**

The incremental cost for this measure is $12[[194]](#footnote-195) or program actual.

**Loadshape**

Loadshape C02 - Commercial Electric DHW

**Coincidence Factor**

The coincidence factor for this measure is assumed to be 2.78%[[195]](#footnote-196).

**Algorithm**

**Calculation of Savings [[196]](#footnote-197)**

**Electric Energy Savings**

Note these savings are per showerhead fixture

ΔkWh =

%ElectricDHW \* ((GPM\_base \* L\_base - GPM\_low \* L\_low) \* NSPD \* 365.25) \* EPG\_electric \* ISR

Where:

%ElectricDHW = proportion of water heating supplied by electric resistance heating

= 1 if electric DHW, 0 if fuel DHW, if unknown assume 16% [[197]](#footnote-198)

GPM\_base = Flow rate of the baseline showerhead

= 2.67 for Direct-install programs[[198]](#footnote-199)

GPM\_low = As-used flow rate of the low-flow showerhead, which may, as a result of measurements of program evaulations deviate from rated flows, see table below:

|  |
| --- |
| **Rated Flow** |
| 2.0 GPM |
| 1.75 GPM |
| 1.5 GPM |
| Custom or Actual[[199]](#footnote-200) |

L\_base = Shower length in minutes with baseline showerhead

= 8.20 min[[200]](#footnote-201)

L\_low = Shower length in minutes with low-flow showerhead

= 8.20 min[[201]](#footnote-202)

365.25 = Days per year, on average.

NSPD = Estimated number of showers taken per day for one showerhead

EPG\_electric = Energy per gallon of hot water supplied by electric

= (8.33 \* 1.0 \* (ShowerTemp - SupplyTemp)) / (RE\_electric \* 3412)

= (8.33 \* 1.0 \* (105 – 54.1)) / (0.98 \* 3412)

= 0.127 kWh/gal

8.33 = Specific weight of water (lbs/gallon)

1.0 = Heat Capacity of water (btu/lb-°F)

ShowerTemp = Assumed temperature of water

= 105°F [[202]](#footnote-203)

SupplyTemp = Assumed temperature of water entering house

= 54.1°F [[203]](#footnote-204)

RE\_electric = Recovery efficiency of electric water heater

= 98% [[204]](#footnote-205)

3412 = Converts Btu to kWh (btu/kWh)

ISR = In service rate of showerhead

= Dependant on program delivery method as listed in table below

|  |  |
| --- | --- |
| **Selection** | **ISR[[205]](#footnote-206)** |
| Direct Install - Deemed | 0.98 |

EXAMPLE

For example, a direct-installed 1.5 GPM showerhead in an office with electric DHW where the number of showers is estimated at 3 per day:

ΔkWh = 1 \* ((2.67\*8.20)- (1.5\*8.20)) \* 3\*365.25) \*0.127 \* 0.98

= 1308.4 kWh

**Summer Coincident Peak Demand Savings**

ΔkW = ΔkWh/Hours \* CF

Where:

ΔkWh = calculated value above

Hours = Annual electric DHW recovery hours for showerhead use

= ((GPM\_base \* L\_base) \*NSPD \* 365.25 ) \* 0.773[[206]](#footnote-207) / GPH

Where:

GPH = Gallons per hour recovery of electric water heater calculated for 65.9F temp rise (120-54.1), 98% recovery efficiency, and typical 4.5kW electric resistance storage tank.

= 27.51

CF = Coincidence Factor for electric load reduction

= 0.0278[[207]](#footnote-208)

EXAMPLE

For example, a direct-installed 1.5 GPM showerhead in an office with electric DHW where the number of showers is estimated at 3 per day:

ΔkW = (1308.4 / 674.1)\*0.0278

= 0.162 kW

**Fossil Fuel Impact Descriptions and Calculation**

ΔTherms = %FossilDHW \* ((GPM\_base \* L\_base - GPM\_low \* L\_low) \* NSPD\* 365.25) \* EPG\_gas \* ISR

Where:

%FossilDHW = proportion of water heating supplied by fossil fuel heating

|  |  |
| --- | --- |
| **DHW fuel** | **%Fossil\_DHW** |
| Electric | 0% |
| Fossil Fuel | 100% |
| Unknown | 84%[[208]](#footnote-209) |

EPG\_gas = Energy per gallon of Hot water supplied by gas

= (8.33 \* 1.0 \* (ShowerTemp - SupplyTemp)) / (RE\_gas \* 100,000)

= 0.0063 Therm/gal

Where:

RE\_gas = Recovery efficiency of gas water heater

= 67% [[209]](#footnote-210)

100,000 = Converts Btus to Therms (btu/Therm)

Other variables as defined above.

EXAMPLE

For example, a direct-installed 1.5 GPM showerhead in an office with gas DHW where the number of showers is estimated at 3 per day:

ΔTherms = 1.0 \* (( 2.67 \*8.2) – (1.5 \* 8.2)) \* 3 \* 365.25 \* 0.0063 \* 0.98

= 64.9 therms

**Water Impact Descriptions and Calculation**

Δgallons = ((GPM\_base \* L\_base - GPM\_low \* L\_low) \* NSPD \* 365.25 \* ISR

Variables as defined above

EXAMPLE

For example, a direct-installed 1.5 GPM showerhead in an office with where the number of showers is estimated at 3 per day:

Δgallons = ((2.67 \* 8.20)-(1.5 \* 8.20)) \* 3 \* 365.25 \* 0.98

= 10,302 gallons

**Deemed O&M Cost Adjustment Calculation**

N/A

**Sources**

|  |  |
| --- | --- |
| **Source ID** | **Reference** |
| 1 | 2011, DeOreo, William. California Single Family Water Use Efficiency Study. April 20, 2011. |
| 2 | 2000, Mayer, Peter, William DeOreo, and David Lewis. Seattle Home Water Conservation Study. December 2000. |
| 3 | 1999, Mayer, Peter, William DeOreo. Residential End Uses of Water. Published by AWWA Research Foundation and American Water Works Association. 1999. |
| 4 | 2003, Mayer, Peter, William DeOreo. Residential Indoor Water Conservation Study. Aquacraft, Inc. Water Engineering and Management. Prepared for East Bay Municipal Utility District and the US EPA. July 2003. |
| 5 | 2011, DeOreo, William. Analysis of Water Use in New Single Family Homes. By Aquacraft. For Salt Lake City Corporation and US EPA. July 20, 2011. |
| 6 | 2011, Aquacraft. Albuquerque Single Family Water Use Efficiency and Retrofit Study. For Albuquerque Bernalillo County Water Utility Authority. December 1, 2011. |
| 7 | 2008, Schultdt, Marc, and Debra Tachibana. Energy related Water Fixture Measurements: Securing the Baseline for Northwest Single Family Homes. 2008 ACEEE Summer Study on Energy Efficiency in Buildings. |

###### Measure Code: CI-HW\_-LFSH-V02-120601

### Commercial Pool Covers

**Description**

This measure refers to the installation of covers on commercial use pools that are heated with gas-fired equipment located either indoors or outdoors. By installing pool covers, the heating load on the pool boiler will be reduced by reducing the heat loss from the water to the environment and the amount of actual water lost due to evaporation (which then requires additional heated water to make up for it).

The main source of energy loss in pools is through evaporation. This is particularly true of outdoor pools where wind plays a larger role. The point of installing pool covers is threefold. First, it will reduce convective losses due to the wind by shielding the water surface. Second, it will insulate the water from the colder surrounding air. And third, it will reduce radiative losses to the night sky. In doing so, evaporative losses will also be minimized, and the boiler will not need to work as hard in replenishing the pool with hot water to keep the desired temperature.

This measure can be used for pools that (1) currently do not have pool covers, (2) have pool covers that are past the useful life of the existing cover, or (3) have pool covers that are past their warranty period and have failed.

**Definition of Efficient Equipment**

For indoor pools, the efficient case is the installation of an indoor pool cover with a 5 year warranty on an indoor pool that operates all year.

For outdoor pools, the efficient case is the installation of an outdoor pool cover with a 5 year warranty on an outdoor pool that is open through the summer season.

**Definition of Baseline Equipment**

For indoor pools, the base case is an uncovered indoor pool that operates all year.

For outdoor pools, the base case is an outdoor pool that is uncovered and is open through the summer season.

**Deemed Lifetime of Efficient Equipment**

The useful life of this measure is assumed to be 6 years [[210]](#footnote-211)

**Deemed Measure Cost**

The table below shows the costs for the various options and cover sizes. Since this measure covers a mix of various sizes, the average cost of these options is taken to be the incremental measure cost. [[211]](#footnote-212).

|  |  |  |
| --- | --- | --- |
| **Cover Size** | **Edge Style** | |
| **Hemmed (indoor)** | **Weighted (outdoor)** |
| 1000-1,999 sq. ft. | $2.19 | $2.24 |
| 2,000-2,999 sq. ft. | $2.01 | $2.06 |
| 3,000+ sq. ft. | $1.80 | $1.83 |
| **Average** | **$2.00** | **$2.04** |

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Net To Gross Ratio**

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

N/A

**Summer Coincident Peak Demand Savings**

N/A

**Natural Gas Savings**

The calculations are based on modeling runs using RSPEC! Energy Smart Pools Software that was created by the U.S. Department of Energy. [[212]](#footnote-213)

ΔTherms = SavingFactor x Size of Pool

Where

Savings factor = dependant on pool location and listed in table below[[213]](#footnote-214)

|  |  |
| --- | --- |
| **Location** | **Therm / sq-ft** |
| Chicago - indoor | 2.61 |
| Chicago - outdoor | 1.01 |

Size of Pool = custom input

**Water Impact Descriptions and Calculation**

ΔTherms = WaterSavingFactor x Size of Pool

Where

WaterSavingFactor = Water savings for this measure dependant on pool location and listed in table below.[[214]](#footnote-215).

|  |  |
| --- | --- |
| **Location** | **Annual Savings**  **Gal / sq-ft** |
| Chicago - indoor | 15.28 |
| Chicago - outdoor | 8.94 |

Size of Pool = Custom input

**Deemed O&M Cost Adjustment Calculation**

There are no O&M cost adjustments for this measure.

###### Measure code: CI-HW\_-PLCV-V01-130601

### Tankless Water Heater

###### Description

This measure covers the installation of on-demand or instantaneous tankless water heaters. Tankless water heaters function similar to standard hot water heaters except they do not have a storage tank. When there is a call for hot water, the water is heated instantaneously as it passes through the heating element and then proceeds to the user or appliance calling for hot water. Tankless water heaters achieve savings by eliminating the standby losses that occur in stand-alone or tank-type water heaters and by being more efficient than the baseline storage hot water heater.

This measure was developed to be applicable to the following program types: TOS, RF, ER.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

|  |  |
| --- | --- |
| Electric | Gas |
| To qualify for this measure, the tankless water heater shall be a new electric powered tankless hot water heater with an energy factor greater than or equal to 0.98 with an output greater than or equal to 5 GPM output at 70° F temperature rise | To qualify for this measure, the tankless water heater shall meet or exceed the efficiency requirements for tankless hot water heaters mandated by the International Energy Conservation Code (IECC) 2012, Table C404.2. |

###### Definition of Baseline Equipment

|  |  |
| --- | --- |
| Electric | Gas |
| The baseline condition is assumed to be an electric commercial-grade tanked water heater 50 or more gallon storage capacity with an energy factor less than or equal to 0.9 or the water heater is five or more years old | The baseline condition is assumed to be a gas-fired tank-type water heater meeting the efficiency requirements mandated by the International Energy conservation Code (IECC) 2012, Table C404.2. |

###### Deemed Lifetime of Efficient Equipment

|  |  |
| --- | --- |
| Electric | Gas |
| The expected measure life is assumed to be 5 years[[215]](#footnote-216). | The expected measure life is assumed to be 20 years[[216]](#footnote-217) |

###### Deemed Measure Cost

The incremental capital cost for an electric tankless heater this measure is assumed to be[[217]](#footnote-218)

|  |  |
| --- | --- |
| **Output (gpm) at delta T 70** | **Incremental Cost** |
| 5 | $1050 |
| 10 | $1050 |
| 15 | $1950 |

The incremental capital cost for a gas fired tankless heater is as follows:

|  |  |
| --- | --- |
| Program | Capital Cost, $ per unit |
| Retrofit | $3,255[[218]](#footnote-219) |
| Time of Sale or New Construction | $2,526[[219]](#footnote-220) |

###### Deemed O&M Cost Adjustments

$100[[220]](#footnote-221)

###### Loadshape

Loadshape C02 - Commercial Electric DHW

###### Coincidence Factor

The measure has deemed kW savings therefor a coincidence factor is not applied

**Algorithm**

###### Calculation of Energy Savings

###### Electric Energy Savings [[221]](#footnote-222)

The annual electric savings from an electric tankless heater is a deemed value and assumed to be:

|  |  |
| --- | --- |
| Output (gpm) at delta T 70 | Savings (kWh) |
| 5.0 | 2,991.98 |
| 10.0 | 7,904.82 |
| 15.0 | 12,878.51 |

###### Summer Coincident Peak Demand Savings[[222]](#footnote-223)

The annual kW savings from an electric tankless heater is a deemed value and assumed to be:

|  |  |
| --- | --- |
| Output (gpm) at delta T 70 | Savings (kW) |
| 5.0 | 0.34 |
| 10.0 | 0.90 |
| 15.0 | 1.47 |

###### Natural Gas Savings

ΔTherms=[[Wgal x 8.33 x 1 x (Tout - Tin) x [(1/Eff base) - (1/Eff ee)]]/100,000] +[[(SL x 8,766)/Eff base]] / 100,000 Btu/Therms]

Where:

Wgal = Annual water use for equipment in gallons

= custom, otherwise assume 21,915 gallons [[223]](#footnote-224)

8.33 lbm/gal = weight in pounds of one gallon of water

1 Btu/lbm°F = Specific heat of water: 1 Btu/lbm/°F

8,766 hr/yr = hours a year

Tout = Unmixed Outlet Water Temperature

= custom, otherwise assume 130 °F[[224]](#footnote-225)

Tin = Inlet Water Temperature

= custom, otherwise assume 54.1 °F[[225]](#footnote-226)

Eff base = Rated efficiency of baseline water heater expressed as Energy Factor (EF) or Thermal Efficiency (Et); see table below[[226]](#footnote-227)

|  |  |  |
| --- | --- | --- |
| Input Btu/hr of existing, tanked water heater | Eff base | Units |
| Size: ≤ 75,000 Btu/hr | 0.67 -0.0019\*Tank Volume | Energy Factor |
| Size: >75,000 Btu/hr and ≤ 155,000 Btu/hr | 80% | Thermal Efficiency |
| Size: >155,000 Btu/hr | 80% | Thermal Efficiency |

Where Tank Volume = custom input, if unknown assume 60 gallons for Size: ≤ 75,000 Btu/hr

Please note: Units in base case must match units in efficient case. If Energy Factor used in base case, Energy Factor to be used in efficient case. If Themal Efficiency is used in base case, Thermal Efficiency must be used in efficient case.

Eff ee = Rated efficiency of efficient water heater expressed as Energy Factor (EF) or Thermal Efficiency (Eff t)

= custom input, if unknown assume 0.84[[227]](#footnote-228)

SL = Stand-by Loss in Base Case Btu/hr

= custom input based on formula in table below, if unknown assume unit size in table below[[228]](#footnote-229)

|  |  |
| --- | --- |
| **Input Btu/h of new, tankless water heater** | **Standby Loss (SL)** |
| Size: ≤ 75,000 Btu/hr | 0 |
| Size: >75,000 Btu/hr | (Input rating/800)+(110\*√Tank Volume)) |

Where:

Tank Volume = custom input, if unknown assume, 60 gallons for <75,000 Btu/hr, 75 gallons for >75,000 Btu/hr and ≤ 155,000 Btu/hr and 150 for Size >155,000 Btu/hr

Input Value = nameplate Btu/hr rating of water heater

EXAMPLE

For example, a 75,000 Btu/hr tankless unit using 21,915 gal/yr with outlet temperature at 130.0 and inlet temperature at 54.1, replacing a baseline unit with 0.8 thermal efficiency and standby losses of 1008.3 btu/hr:

ΔTherms =[[(21,915 x 8.33x 1 x (130 – 54.1) x [(1/.8) - (1/.84)]/100,000] +[(1008.3 x 8,766)/.8]] / 100,000

=115 Therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

The deemed O&M cost adjustment for a gas fired tankless heater is $100

###### Reference Tables

Minimum Performance Water Heating Equipment[[229]](#footnote-230)



###### Measure Code: CI-HW\_-TKWH-V02-120601

### Ozone Laundry

###### Description

A new ozone laundry system(s) is added-on to new or existing commercial washing machine(s) using hot water heated with natural gas. The system generates ozone (O3), a naturally occurring molecule, which helps clean fabrics by chemically reacting with soils in cold water. Adding an ozone laundry system(s) will reduce the amount of chemicals, detergents, and hot water needed to wash linens. Using ozone also reduces the total amount of water consumed, saving even more in energy.

Natural gas energy savings will be achieved at the hot water heater/boiler as they will be required to produce less hot water to wash each load of laundry. The decrease in hot water usage will increase cold water usage, but overall water usage at the facility will decrease.

Electric savings can be realized through reduced washer cycle length and reduced pumping load at the boiler feeding the commercial washers. The increased usage associated with operating the ozone system should also be accounted for when determining total kWh impact. Data reviewed for this measure characterization indicated that pumping savings should be accounted for, but washer savings and ozone generator consumption are comparatively so small that they can be ignored.

The reduced washer cycle length may decrease the dampness of the clothes when they move to the dryer. This can result in shorter runtimes which result in gas and electrical savings. However, at this time, there is inconclusive evidence that energy savings are achieved from reduced dryer runtimes so the resulting dryer effects are not included in this analysis. Additionally, there would be challenges verifying that dryer savings will be achieved throughout the life of the equipment.

This incentive only applies to the following facilities with on-premise laundry operations:

* + Hotels/motels
  + Fitness and recreational sports centers.
  + Healthcare (excluding hospitals)
  + Assisted living facilities

Ozone laundry system(s) could create significant energy savings opportunities at other larger facility types with on-premise laundry operations (such as correctional facilities, universities, and staff laundries), however, the results included in this analysis are based heavily on past project data for the applicable facility types listed above and may not apply to facilities outside of this list due to variances in number of loads and average pound (lbs.)-capacity per project site. Projects at these facilities should continue to be evaluated through custom programs and the applicable facility types and the resulting analysis should be updated based on new information.

This measure was developed to be applicable to the following program types:  TOS, RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

A new ozone laundry system(s) is added-on to new or existing commercial washing machine(s) using hot water heated with natural gas. The ozone laundry system(s) must transfer ozone into the water through:

* + Venturi Injection
  + Bubble Diffusion
  + Additional applications may be considered upon program review and approval on a case by case basis

###### Definition of Baseline Equipment

The base case equipment is a conventional washing machine system with no ozone generator installed. The washing machines are provided hot water from a gas-fired boiler.

###### Deemed Lifetime of Efficient Equipment

The measure equipment effective useful life (EUL) is estimated at 10 years based on typical lifetime of the ozone generator’s corona discharge unit.[[230]](#footnote-231)

###### Deemed Measure Cost

The actual measure costs should be used if available. If not a deemed value of $79.84 / lbs capacity should be used[[231]](#footnote-232).

###### Loadshape

Loadshape C53 – Flat

###### Coincidence Factor

Past project documentation and data collection is not sufficient to determine a coincidence factor for this measure. Value should continue to be studied and monitored through additional studies due to limited data points used for this determination

Algorithm

###### Calculation of Energy Savings

###### Electric Energy Savings

Electric savings can be realized through reduced washer cycle length and reduced pumping load at the boiler feeding the commercial washers. There is also an increased usage associated with operating the ozone system. Data reviewed for this measure characterization indicated that while pumping savings is significant and should be accounted for, washer savings and ozone generator consumption are negligible, counter each other out and are well within the margin of error so these are not included to simplify the characterization[[232]](#footnote-233).

∆kWhPUMP = HP \* HPCONVERSION \* Hours \* %water\_savings

Where:

∆kWhPUMP = Electric savings from reduced pumping load

HP = Brake horsepower of boiler feed water pump;

= Actual or use 5 HP if unknown[[233]](#footnote-234)

HPCONVERSION = Conversion from Horsepower to Kilowatt

= 0.746

Hours = Actual associated boiler feed water pump hours

= 800 hours if unknown[[234]](#footnote-235)

%water\_savings = water reduction factor: how much more efficient an ozone injection washing machine is compared to a typical conventional washing machine as a rate of hot and cold water reduction.

= 25%[[235]](#footnote-236)

Using defaults above:

∆kWhPUMP = 5 \* 0.746 \* 800 \* 0.25

= 746 kWh

Default per lb capacity: = ∆kWhPUMP / lb capacity

Where:

Lbs-Capacity = Average Capacity in lbs of washer

=254.38[[236]](#footnote-237)

∆kWhPUMP / lb capacity = 746/254.38

= 2.93 kWh/lb-capacity

###### Summer Coincident Peak Demand Savings

Past project documentation and data collection is not sufficient to determine summer coincident peak demand savings for this measure. Value should continue to be studied and monitored through additional studies due to limited data points used for this determination. In absence of site-specific data, the summer coincident peak demand savings should be assumed to be zero.

∆kW = 0

###### Natural Gas Savings

∆Therm = ThermBaseline \* %hot\_water\_savings

Where:

∆Therm = Gas savings resulting from a reduction in hot water use, in therm.

ThermBaseline = Annual Baseline Gas Consumption

= WHE \* WUtiliz \* WUsage\_hot

Where:

WHE = water heating energy: energy required to heat the hot water used

= 0.00885 therm/gallon[[237]](#footnote-238)

WUtiliz = washer utilitzation factor: the annual pounds of clothes washed per year

= actual, if unknown use 916,150 lbs laundry[[238]](#footnote-239), approximately equivalent to 13 cycles/day

WUsage\_hot = hot water usage factor: how much hot water a typical conventional washing machine utilizes, normalized per pounds of clothes washed

= 1.19 gallons/lbs laundry[[239]](#footnote-240)

Using defaults above:

ThermBaseline = 0.00885 \* 916,150 \* 1.19

= 9,648 therms

Default per lb capacity:

ThermBaseline / lb capacity= 9,648 / 254.38

= 37.9 therms / lb-capacity

%hot\_water\_savings = hot water reduction factor: how much more efficient an ozone injection washing machine is, compared to a typical conventional washing machine, as a rate of hot water reduction

= 81%[[240]](#footnote-241)

Savings using defaults above:

∆Therm = ThermBaseline \* %hot\_water\_savings

= 9648 \* 0.81

= 7,815 therms

Default per lb capacity:

∆Therm / lb-capacity = 7815 / 254.38

= 30.7 therms / lb-capacity

###### Water Impact Descriptions and Calculation

The water savings calculations listed here account for the combination of hot and cold water used. Savings calculations for this measure were based on the reduction in total water use from implementing an ozone washing system to the base case. There are three main components in obtaining this value:

Δgallons = WUsage \* WUtiliz \* %water\_savings

Where:

Δgallons = reduction in total water use from implementing an ozone washing system to the base case

WUsage = water usage factor: how efficiently a typical conventional washing machine utilized hot and cold water normalized per unit of clothes washed

= 2.03 gallons/lbs laundry[[241]](#footnote-242)

WUtiliz = washer utilitzation factor: the annual pounds of clothes washed per year

= actual, if unknown use 916,150 lbs laundry[[242]](#footnote-243), approximately equivalent to 13 cycles/day

%water\_savings = water reduction factor: how much more efficient an ozone injection washing machine is compared to a typical conventional washing machine as a rate of hot and cold water reduction.

= 25%[[243]](#footnote-244)

Savings using defaults above:

∆Gallons = WUsage \* WUtiliz \* %water\_savings

= 2.03 \* 916,150 \* 0.25

= 464,946 gallons

Default per lb capacity:

∆ Gallons / lb-capacity = 464,946 / 254.38

= 1,828 gallons / lb-capacity

###### Deemed O&M Cost Adjustment Calculation

Maintenance is required for the following components annually:[[244]](#footnote-245)

* Ozone Generator: filter replacement, check valve replacement, fuse replacement, reaction chamber inspection/cleaning, reaction chamber o-ring replacement
* Air Preparation – Heat Regenerative: replacement of two medias
* Air Preparation – Oxygen Concentrators: filter replacement, pressure relief valve replacement, compressor rebuild
* Venturi Injector: check valve replacement

Maintenance is expected to cost $0.79 / lbs capacity.

###### References

1 "Lodging Report", December 2008, California Travel & Tourism Commission, <http://tourism.visitcalifornia.com/media/uploads/files/editor/Research/CaliforniaTourism_200812.pdf>

2 "Health, United States, 2008" Table 120, U.S. Department of Health & Human Services, Centers for Disease Control & Prevention, National Center for Health Statistics, <http://www.cdc.gov/nchs/data/hus/hus08.pdf#120>

3 [Fourth Quarter 2008 Facts and Fictures, California Department of Corrections & Rehabilitation (CDCR)](http://www.cdcr.ca.gov/Divisions_Boards/Adult_Operations/docs/Fourth_Quarter_2008_Facts_and_Figures.pdf), <http://www.cdcr.ca.gov/Divisions_Boards/Adult_Operations/docs/Fourth_Quarter_2008_Facts_and_Figures.pdf>

4 [Jail Profile Survey (2008), California Department of Corrections & Rehabilitation (CDCR)](http://www.cdcr.ca.gov/Divisions_Boards/CSA/FSO/Docs/2008_4th_Qtr_JPS_full_report.pdf), <http://www.cdcr.ca.gov/Divisions_Boards/CSA/FSO/Docs/2008_4th_Qtr_JPS_full_report.pdf>

5 DEER2011\_NTGR\_2012-05-16.xls from DEER Database for Energy-Efficient Resources; Version 2011 4.01 found at :<http://www.deeresources.com/index.php?option=com_content&view=article&id=68&Itemid=60>

Under: DEER2011 Update Documentation linked at: [DEER2011 Update Net-To-Gross table](http://www.deeresources.com/DEER2011/download/DEER2011_NTGR_2012-05-16.xls) Cells: T56 and U56

6 The Benefits of Ozone in Hospitality On-Premise Laundry Operations, PG&E Emerging Technologies Program, Application Assessment Report #0802, April 2009.

7 Federal Register, Vol. 52, No. 166

8 2009 ASHRAE Handbook – Fundamentals, Thermodynamic Properties of Water at Saturation, Section 1.1 (Table 3), 2009

9 Table 2 through 6: Excel file summarizing data collected from existing ozone laundry projects that received incentives under the NRR-DR program

###### Measure code CI-HW-OZLD-V01-140601

### Multifamily Central Domestic Hot Water Plants

**Description**

This measure covers multifamily central domestic hot water (DHW) plants with thermal efficiencies greater than or equal to 88%. This measure is applicable to any combination of boilers and storage tanks provided the thermal efficiency of the boilers is greater than 88%. Plants providing other than solely DHW are not applicable to this measure.

This measure was developed to be applicable to the following program types: TOS, NC, ER.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

To qualify the boiler(s) must have a Thermal Efficiency of 88% or greater and supply domestic hot water to multi-family buildings.

**Definition of Baseline Equipment**

For TOS the baseline boiler is assumed to have a Thermal Efficiency of 80%.[[245]](#footnote-246)

For Early Replacement the savings are calculated between existing unit and efficient unit consumption during the remaining life of the existing unit, and between new baseline unit as above and efficient unit consumption for the remainder of the measure life.

**Deemed Lifetime of Efficient Equipment**

The measure life for the domestic hot water boilers is 15 years.[[246]](#footnote-247)

**Deemed Measure Cost**

TOS: The actual install cost should be used for the efficient case, minus the baseline cost assumption provided below:

|  |  |
| --- | --- |
| **Capacity Range** | **Baseline Installed Cost per kBtuh[[247]](#footnote-248)** |
| <300kBtuh | $65 per kBTUh |
| 300 – 2500 kBtuh | $38 per kBTUh |
| >2500 kBtuh | $32 per kBTUh |

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

There are no anticipated electrical savings from this measure.

**Summer Coincident Peak Demand Savings**

N/A

**Natural Gas Savings**

Time of Sale:

ΔTherms = Hot Water Savings + Standby Loss Savings

= [(MFHH \* #Units \* GPD \* Days/yr \* עWater \* (Tout – Tin) \* (1/Eff\_base – 1/Eff\_ee)) / 100,000] + [((SL \* Hours/yr \* (1/Eff\_base – 1/Eff\_ee)) / 100,000]

Early Replacment[[248]](#footnote-249):

ΔTherms for remaining life of existing unit (1st 5 years):

= [(MFHH \* #Units \* GPD \* Days/yr \* עWater \* (Tout – Tin) \* (1/Eff\_exist – 1/Eff\_ee)) / 100,000] + [((SL \* Hours/yr \* (1/Eff\_exist – 1/Eff\_ee)) / 100,000]

ΔTherms for remaining measure life (next 10 years):

= [(MFHH \* #Units \* GPD \* Days/yr \* עWater \* (Tout – Tin) \* (1/Eff\_base – 1/Eff\_ee)) / 100,000] + [((SL \* Hours/yr \* (1/Eff\_base – 1/Eff\_ee)) / 100,000]

Where:

MFHH = number of people in Multi-Family House Hold

= Actual. If unknown assume 2.1 persons/unit[[249]](#footnote-250)

#Units = Number of units served by hot water boiler

= Actual

GPD = Gallons of hot water used per person per day

= Actual. If unknown assume 17.6 gallons per person per day[[250]](#footnote-251)

Days/yr = 365.25

עWater = Specific Weight of Water

= 8.33 gal/lb

Tout = tank temperature of hot water

= 125°F or custom

Tin = Incoming water temperature from well or municiple system

= 54°F[[251]](#footnote-252)

Eff\_base = thermal efficiency of base unit

= 80%[[252]](#footnote-253)

Eff\_ee = thermal efficiency of efficient unit complying with this measure

= Actual. If unknown assume 88%

Eff\_exist = thermal efficiency of existing unit

= Actual. If unknown assume 73%[[253]](#footnote-254)

SL = Standby Loss[[254]](#footnote-255)

= (Input rating / 800) + (110 \* √Tank Volume)

Input rating = Name plate input capacity in Btuh

Tank Volume = Rated volume of the tank in gallons

Hours / yr = 8766 hours

100,000 = btu/therm

**EXAMPLES**

Time of Sale:

For example, an 88% 1000 gallon boiler with 150,000 Btuh input rating installed serving 50 units.

ΔTherms = Hot Water Savings + Standby Loss Savings

= [(MFHH \* #Units \* GPD \* Days/yr \* עWater \* (Tout – Tin) \* (1/Eff\_base – 1/Eff\_ee)) / 100,000] + [((SL \* Hours/yr \* (1/Eff\_base – 1/Eff\_ee)) / 100,000]

=[(2.1 \* 50 \* 17.6 \* 8.33 \* 365.25 \* 1.0 \* (125-54) \* (1/0.8 – 1/0.88)) / 100000] + [((150000/800 + (110 \* √1000)) \* 8766 \* (1/0.8 – 1/0.88)) / 100000]

= 454 + 37

= 490 therms

Early Replacement:

For example, an 88% 1000 gallon boiler with 150,000 Btuh input rating installed serving 50 units replaces a working unit with unknown efficiency.

ΔTherms for remaining life of existing unit (1st 5 years):

=[(2.1 \* 50 \* 17.6 \* 8.33 \* 365.25 \* 1.0 \* (125-54) \* (1/0.73 – 1/0.88)) / 100000] + [((150000/800 + (110 \* √1000)) \* 8766 \* (1/0.73 – 1/0.88)) / 100000]

= 932 + 75

= 1007 therms

ΔTherms for remaining measure life (next 10 years):

= 454 + 37 (as above)

= 490 therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

###### Measure code: CI-HW\_-MDHW-V01-150601

### Controls for Central Domestic Hot Water

**Description**

Demand control recirculation pumps seek to reduce inefficiency by combining control via temperature and demand inputs, whereby the controller will not activate the recirculation pump unless both (a) the recirculation loop return water has dropped below a prescribed temperature (e.g. 100°F) and (b) a CDHW demand is sensed as water flow through the CDHW system.

This measure was developed to be applicable to the following program types: TOS, RF, NC. If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

Re-circulating pump shall cycle on based on (a) the recirculation loop return water dropping below a prescribed temperature (e.g. 100°F) and (b) a CDHW demand is sensed as water flow through the CDHW system.

**Definition of Baseline Equipment**

The base case for this measure category are existing, un-controlled Recirculation Pumps on gas-fired Central Domestic Hot Water Systems.

**Deemed Lifetime of Efficient Equipment**

The effective useful life is 15 years[[255]](#footnote-256).

**Deemed Measure Cost**

Incremental Cost: $1,200 [[256]](#footnote-257)

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Energy Savings[[257]](#footnote-258)**

**Electric Energy Savings**

Deemed at 651 kWh[[258]](#footnote-259).

**Summer Coincident Peak Demand Savings**

N/A

**Natural Gas Savings**

∆Therms = 55.9[[259]](#footnote-260) \* number of dwelling units

**EXAMPLE**

For example, an apartment building with 53 units:

∆Therms = 55.9 \* 53

= 2,962.7 therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

###### Measure Code: CI-HW\_-CDHW-V01-150601

4.4 HVAC End Use

Many of the commercial HVAC measures use equivalent full load hours (EFLH) to calculate heating and cooling savings. The tables with these values are included in this section and referenced in each measure.

Equivalent Full Load Hours is calculated using the annual energy use divided by the peak load. The team identified 15 building types to calculate EFLH. The method establish was to obtain energy models for typical building stock and then run the energy models to establish annual energy use and peak load to then calculate EFLH.

The goal was to find pre-developed energy models that could be run through eQuest software and output reports would provide the energy use and peak load. The team explored using California DEER models or ComEd models. It was determined that the ComEd models better represented IL building stock and equipment vintages than the California models[[260]](#footnote-261).

A summary of the inputs to the building models is summarized in Building Descriptions.xls. After the buildings were run through eQuest, “Space Heating" value in MBtu/y found on the "Building Energy Performance Summary" was divided by "Maximum Heating Load" in kBtu/y found on the "Building HVAC Load Summary" to calculate hours.

The building characteristics can be found in the reference table named “EFLH Building Descriptions Updated 2014-11-21.xlsx”.

| **Building Type** | **Heating EFLH** | | | | |
| --- | --- | --- | --- | --- | --- |
| **Zone 1 (Rockford)** | **Zone 2 (Chicago)** | **Zone 3 (Springfield)** | **Zone 4 (Belleville)** | **Zone 5 (Marion)** |
| Assembly | 1,787 | 1,831 | 1,635 | 1,089 | 1,669 |
| Assisted Living | 1,683 | 1,646 | 1,446 | 1,063 | 1,277 |
| College | 1,530 | 1,430 | 1,276 | 709 | 849 |
| Convenience Store | 1,481 | 1,368 | 1,214 | 871 | 973 |
| Elementary School | 1,781 | 1,736 | 1,531 | 1,057 | 1,283 |
| Garage | 985 | 969 | 852 | 680 | 752 |
| Grocery | 1,608 | 1,602 | 1,404 | 876 | 1,047 |
| Healthcare Clinic | 1,579 | 1,620 | 1,414 | 963 | 1,019 |
| High School | 1,845 | 1,857 | 1,666 | 1,187 | 1,388 |
| Hospital - CAV no econ | 1,764 | 1,818 | 1,549 | 1,332 | 1,512 |
| Hospital - CAV econ | 1,788 | 1,853 | 1,580 | 1,369 | 1,555 |
| Hospital - VAV econ | 731 | 695 | 522 | 314 | 340 |
| Hospital - FCU | 1,325 | 1,512 | 1,232 | 1,448 | 1,946 |
| Hotel/Motel | 1,761 | 1,712 | 1,544 | 1,056 | 1,290 |
| Hotel/Motel - Common | 1,601 | 1,626 | 1,548 | 1,260 | 1,323 |
| Hotel/Motel - Guest | 1,758 | 1,702 | 1,521 | 1,018 | 1,252 |
| Manufacturing Facility | 1,048 | 1,013 | 939 | 567 | 634 |
| MF - High Rise | 1,526 | 1,506 | 1,373 | 1,169 | 1,172 |
| MF - High Rise - Common | 1,815 | 1,762 | 1,580 | 1,089 | 1,406 |
| MF - High Rise - Residential | 1,475 | 1,464 | 1,330 | 1,152 | 1,123 |
| MF - Mid Rise | 1,666 | 1,685 | 1,450 | 1,067 | 1,216 |
| Movie Theater | 1,916 | 1,905 | 1,718 | 1,288 | 1,538 |
| Office - High Rise - CAV no econ | 2,020 | 2,050 | 1,869 | 1,252 | 1,363 |
| Office - High Rise - CAV econ | 2,089 | 2,132 | 1,960 | 1,351 | 1,487 |
| Office - High Rise - VAV econ | 1,528 | 1,558 | 1,284 | 759 | 846 |
| Office - High Rise - FCU | 1,118 | 1,102 | 952 | 505 | 530 |
| Office - Low Rise | 1,428 | 1,425 | 1,132 | 692 | 793 |
| Office - Mid Rise | 1,585 | 1,587 | 1,342 | 855 | 950 |
| Religious Building | 1,603 | 1,504 | 1,440 | 1,054 | 1,205 |
| Restaurant | 1,350 | 1,354 | 1,216 | 920 | 1,091 |
| Retail - Department Store | 1,392 | 1,278 | 1,200 | 781 | 891 |
| Retail - Strip Mall | 1,332 | 1,233 | 1,090 | 751 | 810 |
| Warehouse | 1,456 | 1,357 | 1,400 | 875 | 1,078 |
| Unknown | 1,553 | 1,539 | 1,369 | 982 | 1,139 |

Equivalent Full Load Hours for Cooling (EFLHcooling) :

| **Building Type** | **Cooling EFLH** | | | | |
| --- | --- | --- | --- | --- | --- |
| **Zone 1 (Rockford)** | **Zone 2 (Chicago)** | **Zone 3 (Springfield)** | **Zone 4 (Belleville)** | **Zone 5 (Marion)** |
| Assembly | 725 | 796 | 937 | 1,183 | 932 |
| Assisted Living | 1,475 | 1,457 | 1,773 | 2,110 | 1,811 |
| College | 475 | 481 | 662 | 746 | 806 |
| Convenience Store | 1,088 | 1,067 | 1,368 | 1,541 | 1,371 |
| Elementary School | 725 | 764 | 905 | 1,142 | 956 |
| Garage | 934 | 974 | 1,226 | 1,582 | 1,383 |
| Grocery | 1,033 | 1,000 | 1,236 | 1,499 | 1,286 |
| Healthcare Clinic | 1,282 | 1,305 | 1,519 | 1,767 | 1,571 |
| High School | 675 | 721 | 840 | 1,060 | 920 |
| Hospital - CAV no econ | 4,166 | 4,275 | 4,319 | 4,692 | 4,445 |
| Hospital - CAV econ | 1,751 | 1,814 | 2,120 | 2,411 | 2,112 |
| Hospital - VAV econ | 1,531 | 1,592 | 1,853 | 2,163 | 1,876 |
| Hospital - FCU | 3,245 | 3,291 | 3,451 | 4,128 | 3,806 |
| Hotel/Motel | 1,233 | 1,186 | 1,436 | 1,274 | 1,616 |
| Hotel/Motel - Common | 2,186 | 2,103 | 2,344 | 1,391 | 2,651 |
| Hotel/Motel - Guest | 1,042 | 1,019 | 1,269 | 1,216 | 1,418 |
| Manufacturing Facility | 1,010 | 1,055 | 1,209 | 1,453 | 1,273 |
| MF - High Rise | 921 | 845 | 1,048 | 1,779 | 1,099 |
| MF - High Rise - Common | 914 | 839 | 1,055 | 2,893 | 1,132 |
| MF - High Rise - Residential | 899 | 831 | 1,011 | 1,569 | 1,055 |
| MF - Mid Rise | 809 | 767 | 992 | 1,119 | 993 |
| Movie Theater | 876 | 745 | 1,036 | 1,178 | 1,010 |
| Office - High Rise - CAV no econ | 1,688 | 1,708 | 1,811 | 1,865 | 1,725 |
| Office - High Rise - CAV econ | 1,454 | 1,452 | 1,551 | 1,568 | 1,416 |
| Office - High Rise - VAV econ | 875 | 919 | 1,057 | 1,275 | 1,077 |
| Office - High Rise - FCU | 1,117 | 1,170 | 1,277 | 1,642 | 1,412 |
| Office - Low Rise | 949 | 1,010 | 1,182 | 1,452 | 1,281 |
| Office - Mid Rise | 883 | 938 | 1,072 | 1,286 | 1,083 |
| Religious Building | 861 | 817 | 967 | 1,159 | 1,067 |
| Restaurant | 1,074 | 1,134 | 1,279 | 1,627 | 1,325 |
| Retail - Department Store | 949 | 889 | 1,124 | 1,367 | 1,157 |
| Retail - Strip Mall | 950 | 919 | 1,149 | 1,351 | 1,215 |
| Warehouse | 357 | 338 | 422 | 647 | 533 |
| Unknown | 1,215 | 1,221 | 1,408 | 1,670 | 1,480 |



### Air Conditioner Tune-up

###### Description

An air conditioning system that is operating as designed saves energy and provides adequate cooling and comfort to the conditioned space

###### Definition of Efficient Equipment

In order for this characterization to apply, the efficient equipment is assumed to be a unitary or split system air conditioner least 3 tons and preapproved by program. The measure requires that a certified technician performs the following items:

* Check refrigerant charge
* Identify and repair leaks if refrigerant charge is low
* Measure and record refrigerant pressures
* Measure and record temperature drop at indoor coil
* Clean condensate drain line
* Clean outdoor coil and straighten fins
* Clean indoor and outdoor fan blades
* Clean indoor coil with spray-on cleaner and straighten fins
* Repair damaged insulation – suction line
* Change air filter
* Measure and record blower amp draw

A copy of contractor invoices that detail the work performed to identify tune-up items, as well as additional labor and parts to improve/repair air conditioner performance must be submitted to the program

###### Definition of Baseline Equipment

In order for this characterization to apply, the baseline condition is assumed to be an AC system that that does not have a standing maintenance contract or a tune up within in the past 36 months.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 3 years.[[261]](#footnote-262)

###### Deemed Measure Cost

The incremental capital cost for this measure is $35[[262]](#footnote-263) per ton.

###### Loadshape

Loadshape C03 - Commercial Cooling

###### Coincidence Factor

CFSSP = Summer System Peak Coincidence Factor for Commercial cooling (during system peak hour)

= 91.3% [[263]](#footnote-264)

CFPJM = PJM Summer Peak Coincidence Factor for Commercial cooling (average during peak period)

= 47.8%[[264]](#footnote-265)

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

For units with cooling capacities less than 65 kBtu/hr:

ΔkWH = (kBtu/hr) \* [(1/SEERbefore) – (1/SEERafter)] \* EFLH

For units with cooling capacities equal to or greater than 65 kBtu/hr:

ΔkWH = (kBtu/hr) \* [(1/EERbefore) – (1/EERafter)] \* EFLH

Where:

kBtu/hr = capacity of the cooling equipment actually installed in kBtu per hour (1 ton of cooling capacity equals 12 kBtu/hr).

=Actual

SEERbefore = Seasonal Energy Efficiency Ratio of the equipment prior to tune-up

=Actual

SEERafter = Seasonal Energy Efficiency Ratio of the equipment after to tune-up

=Actual

EERbefore = Energy Efficiency Ratio of the baseline equipment prior to tune-up

=Actual

EERafter = Energy Efficiency Ratio of the baseline equipment after to tune-up

=Actual

EFLH = Equivalent Full Load Hours for cooling are provided in section 4.4 HVAC End Use

###### Summer Coincident Peak Demand Savings

ΔkWSSP = (kBtu/hr \* (1/EERbefore - 1/EERafter)) \* CFSSP

ΔkWPJM = (kBtu/hr \* (1/ EERbefore - 1/EERafter)) \* CFPJM

Where:

CFSSP = Summer System Peak Coincidence Factor for Commercial cooling (during system peak hour)

= 91.3% [[265]](#footnote-266)

CFPJM = PJM Summer Peak Coincidence Factor for Commercial cooling (average during peak period)

= 47.8%[[266]](#footnote-267)

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-HVC-ACTU-V02-150601

### Space Heating Boiler Tune-up [[267]](#footnote-268)

**Description**

This measure is for a non-residential boiler that provides space heating. The tune-up will improve boiler efficiency by cleaning and/or inspecting burners, combustion chamber, and burner nozzles. Adjust air flow and reduce excessive stack temperatures, adjust burner and gas input. Check venting, safety controls, and adequacy of combustion air intake. Combustion efficiency should be measured before and after tune-up using an electronic flue gas analyzer.

**Definition of Efficient Equipment**

To qualify for this measure the facility must, as applicable, complete the tune-up requirements[[268]](#footnote-269) listed below, by approved technician:

* Measure combustion efficiency using an electronic flue gas analyzer
* Adjust airflow and reduce excessive stack temperatures
* Adjust burner and gas input, manual or motorized draft control
* Check for proper venting
* Complete visual inspection of system piping and insulation
* Check safety controls
* Check adequacy of combustion air intake
* Clean fireside surfaces.
* Inspect all refractory. Patch and wash coat as required.
* Inspect gaskets on front and rear doors and replace as necessary.
* Seal and close front and rear doors properly.
* Clean low and auxiliary low water cut-off controls, then re-install using new gaskets.
* Clean plugs in control piping.
* Remove all hand hole and man hole plates. Flush boiler with water to remove loose scale and sediment.
* Replace all hand hole and man hole plates with new gaskets.
* Open feedwater tank manway, inspect and clean as required. Replace manway plate with new gasket.
* Clean burner and burner pilot.
* Check pilot electrode and adjust or replace.
* Clean air damper and blower assembly.
* Clean motor starter contacts and check operation.
* Make necessary adjustments to burner for proper combustion.
* Perform all flame safeguard and safety trip checks.
* Check all hand hole plates and man hole plates for leaks at normal operating temperatures and pressures.
* Troubleshoot any boiler system problems as requested by on-site personnel

**Definition of Baseline Equipment**

The baseline condition of this measure is a boiler that has not had a tune-up within the past 36 months

**Deemed Lifetime of Efficient Equipment**

The life of this measure is 3 years[[269]](#footnote-270)

**Deemed Measure Cost**

The cost of this measure is $0.83/MBtu/hr[[270]](#footnote-271) per tune-up

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

N/A

**Summer Coincident Peak Demand Savings**

N/A

**Natural Gas Energy Savings**

Δtherms =(Capacity \* EFLH \* (((Effbefore + Ei)/ Effbefore) – 1)) / 100,000

Where:

Capacity = Boiler gas input size (Btu/hr)

= custom

EFLH = Equivalent Full Load Hours for heating are provided in section 4.4 HVAC End Use

Effbefore= Efficiency of the boiler before the tune-up

SF Ei = Efficiency Improvement of the boiler tune-up measure

100,000 = Converts Btu to therms

EXAMPLE

For example, a 1050 kBtu boiler in a Chicago high rise office records an efficiency prior to tune up of 82% AFUE and a 1.8% improvement in efficiency are tune up:

Δtherms = (1050 \* 2050h \* ((0.82 + 0.018)/ 0.82 – 1)) /100.000

= 688 Therms

**Summer Coincident Peak Demand Savings**

N/A

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code:** **CI-HVC-BLRT-V05-150601**

### Process Boiler Tune-up

**Description**

This measure is for a non-residential boiler for process loads. For space heating, see measure 5.2.1. .The tune-up will improve boiler efficiency by cleaning and/or inspecting burners, combustion chamber, and burner nozzles. Adjust air flow and reduce excessive stack temperatures, adjust burner and gas input. Check venting, safety controls, and adequacy of combustion air intake. Combustion efficiency should be measured before and after tune-up using an electronic flue gas analyzer.

**Definition of Efficient Equipment**

To qualify for this measure the facility must, as applicable, complete the tune-up requirements[[271]](#footnote-272) by approved technician, as specified below:

* Measure combustion efficiency using an electronic flue gas analyzer
* Adjust airflow and reduce excessive stack temperatures
* Adjust burner and gas input, manual or motorized draft control
* Check for proper venting
* Complete visual inspection of system piping and insulation
* Check safety controls
* Check adequacy of combustion air intake
* Clean fireside surfaces
* Inspect all refractory. Patch and wash coat as required.
* Inspect gaskets on front and rear doors and replace as necessary.
* Seal and close front and rear doors properly.
* Clean low and auxiliary low water cut-off controls, then re-install using new gaskets.
* Clean plugs in control piping.
* Remove all hand hole and man hole plates. Flush boiler with water to remove loose scale and sediment.
* Replace all hand hole and man hole plates with new gaskets.
* Open feedwater tank manway, inspect and clean as required. Replace manway plate with new gasket.
* Clean burner and burner pilot.
* Check pilot electrode and adjust or replace.
* Clean air damper and blower assembly.
* Clean motor starter contacts and check operation.
* Make necessary adjustments to burner for proper combustion.
* Perform all flame safeguard and safety trip checks.
* Check all hand hole plates and man hole plates for leaks at normal operating temperatures and pressures.
* Troubleshoot any boiler system problems as reQuested by on-site personnel

**Definition of Baseline Equipment**

The baseline condition of this measure is a boiler that has not had a tune-up within the past 36 months

**Deemed Lifetime of Efficient Equipment**

The life of this measure is 3 years[[272]](#footnote-273)

**Deemed Measure Cost**

The cost of this measure is $0.83/MBtu/hr[[273]](#footnote-274) per tune-up

**Deemed O&M Cost Adjustments**

N/A

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

N/A

**Summer Coincident Peak Demand Savings**

N/A

**Natural Gas Energy Savings**

Δtherms=((Ngi \* 8766\*UF)/100) \* (1- (Effpre/Effmeasured))

Where:

Ngi = Boiler gas input size (kBtu/hr)

= custom

UF = Utilization Factor

= 41.9%[[274]](#footnote-275) or custom

Effpre = Boiler Combustion Efficiency Before Tune-Up

= Actual

Effmeasured = Boiler Combustion Efficiency After Tune-Up

= Actual

100 =converstion from kBtu to therms

8766 = hours a year

EXAMPLE

For example, a 80% 1050 kBtu boiler is tuned-up resulting in final efficiency of 81.3%:

Δtherms =((1050 \* 8766\*0.419)/100) \* (1- (0.80/0.813))

= 617 therms

Δtherms =(1050 \*8766 \* .419)/100)\*(1-\*(0.80 /.813))

= 617 therms

**Summer Coincident Peak Demand Savings**

N/A

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-HVC-PBTU-V04-150601**

### Boiler Lockout/Reset Controls

**Description**

This measure relates to improving combustion efficiency by adding controls to non-residential building heating boilers to vary the boiler entering water temperature relative to heating load as a function of the outdoor air temperature to save energy. Energy is saved by increasing the temperature difference between the water temperature entering the boiler in the boiler's heat exchanger and the boiler's burner flame temperature. The flame temperature remains the same while the water temperature leaving the boiler decreases with the decrease in heating load due to an increase in outside air temperature. A lockout temperature is also set to prevent the boiler from turning on when it is above a certain temperature outdoors.

This measure was developed to be applicable to the following program types: RF. If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

Natural gas customer adding boiler reset controls capable of resetting the boiler supply water temperature in an inverse linear fashion with outdoor air temperature. Boiler lockout temperatures should be set to 55 °F at this time as well, to turn the boiler off when the temperature goes above a certain setpoint.

**Definition of Baseline Equipment**

Existing boiler without boiler reset controls, any size with constant hot water flow.

**Deemed Lifetime of Efficient Equipment**

The life of this measure is 20 years***[[275]](#footnote-276)***

**Deemed Measure Cost**

The cost of this measure is $612[[276]](#footnote-277)

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

N/A

**Summer Coincident Peak Demand Savings**

N/A

**Natural Gas Energy Savings**

Therm Savings = Binput \* SF \* EFLH /( 100)

Where:

Binput = Boiler Input Capacity (kBtu/hr)

= custom

SF = Savings factor

= 8%[[277]](#footnote-278) or custom

EFLH = Equivalent Full Load Hours for heating are provided in section 4.4 HVAC End Use

100 = conversion from kBtu to therms

EXAMPLE

For example, a 800 kBtu/hr boiler at a restaurant in Rockford, IL

ΔTherms = 800 \* 0.08 \* 1,350 / (100)

= 864 Therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-HVC-BLRC-V03-150601**

### Condensing Unit Heaters

###### Description

This measure applies to a gas fired condensing unit heater installed in a commercial application.

This measure was developed to be applicable to the following program types: TOS, NC. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the efficient equipment is assumed to be a condensing unit heater up to 300 MBH with a Thermal Efficiency > 90% and the heater must be vented, and condensate drained per manufacturer specifications. The unit must be replacing existing natural gas equipment.

###### Definition of Baseline Equipment

In order for this characterization to apply, the baseline condition is assumed to be a non-condensing natural gas unit heater at end of life.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 12 years[[278]](#footnote-279)

###### Deemed Measure Cost

The incremental capital cost for a unit heater is $676[[279]](#footnote-280)

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

The annual natural gas energy savings from this measure is a deemed value equaling 266 Therms.

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-HVC-CUHT-V01-120601

### Electric Chiller

**Description**

This measure relates to the installation of a new electric chiller meeting the efficiency standards presented below. This measure could relate to the replacement of an existing unit at the end of its useful life, or the installation of a new system in an existing building (i.e. time of sale). Only single-chiller applications should be assessed with this methodology. The characterization is not suited for multiple chillers projects or chillers equipped with variable speed drives (VSDs).

This measure was developed to be applicable to the following program types: TOS, NC. If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

In order for this characterization to apply, the efficient equipment is assumed to exceed the efficiency requirements of the 2009 International Energy Conservation Code, Table 503.2.3(7)

**Definition of Baseline Equipment**

In order for this characterization to apply, the baseline equipment is assumed to meet the efficiency requirements of the2009 International Energy Conservation Code, Table 503.2.3(7).

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 20 years [[280]](#footnote-281).

**Deemed Measure Cost**

The incremental capital cost for this measure is provided below.

| **Equipment Type** | **Size Category** | **Incremental Cost ($/ton)****[[281]](#footnote-282)** |
| --- | --- | --- |
| Air cooled, electrically operated | All capacities | $127/ton[[282]](#footnote-283) |
| Water cooled, electrically operated, positive displacement (reciprocating) | All capacities | $22/ton |
| Water cooled, electrically operated, positive displacement (rotary screw and scroll) | < 150 tons | $128/ton |
| >= 150 tons and < 300 tons | $70/ton |
| >= 300 tons | $48/ton |

**Loadshape**

Loadshape C03 - Commercial Cooling

**Coincidence Factor**

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.  Both values provided are based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren.

CFSSP = Summer System Peak Coincidence Factor for Commercial cooling (during system peak hour)

= 91.3% [[283]](#footnote-284)

CFPJM = PJM Summer Peak Coincidence Factor for Commercial cooling (average during peak period)

= 47.8% [[284]](#footnote-285)

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

ΔkWH = TONS \* ((IPLVbase) – (IPLVee)) \* EFLH

Where:

TONS = chiller nominal cooling capacity in tons (note: 1 ton = 12,000 Btu/hr)

= Actual installed

IPLVbase = efficiency of baseline equipment expressed as Integrated Part Load Value(kW/ton). Chiller units are dependent on chiller type. See Chiller Units, Convertion Values and Baseline Efficiency Values by Chiller Type and Capacity in the Reference Tables section.

IPLVee[[285]](#footnote-286) = efficiency of high efficiency equipment expressed as Integrated Part Load Value (kW/ton)[[286]](#footnote-287)

= Actual installed

EFLH = Equivalent Full Load Hours for cooling are provided in section 4.4 HVAC End Use:

For example, a 100 ton air-cooled electrically operated chiller in a high-rise office building with IPLV of 14 EER (0.86 kW/ton) and baseline EER of 12.5 (0.96 kW/ton) in Rockford would save:

ΔkWH = 100 \* ((0.96) – (0.86)) \* 923

= 9,230 kWh

**Summer Coincident Peak Demand Savings**

ΔkWSSP = TONS \* ((PEbase) – (PEee)) \* CFSSP

ΔkWPJM = TONS \* ((PEbase) – (PEee)) \* CFPJM

Where:

PEbase = Peak efficiency of baseline equipment expressed as Full Load (kW/ton)

PEee = Peak efficiency of high efficiency equipment expressed as Full Load (kW/ton)

= Actual installed

CFSSP = Summer System Peak Coincidence Factor for Commercial cooling (during system peak hour)

= 91.3%

CFPJM = PJM Summer Peak Coincidence Factor for Commercial cooling (average during peak period)

= 47.8%

For example, a 100 ton air-cooled electrically operated chiller in a high-rise office building with a full load IPLV of 12 EER ( 0.86 kW/ton) with baseline full load IPLV 9.56 EER (1.3 kW/ton) in Rockford would save:

ΔkWSSP = 100 \* ((1.3) – (1.0)) \* .913

=23 kW

**Natural Gas Energy Savings**

N/A

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Reference Tables**

Chillers Ratings- Chillers are rated with different units depending on equipment type as shown below

|  |  |
| --- | --- |
| **Equipment Type** | **Unit** |
| Air cooled, electrically operated | EER |
| Water cooled, electrically operated, positive displacement (reciprocating) | kW/ton |
| Water cooled, electrically operated, positive displacement (rotary screw and scroll) | kW/ton |

In order to convert chiller equipment ratings to IPLV the following relationships are provided

kW/ton = 12 / EER

kW/ton = 12 / (COP x 3.412)

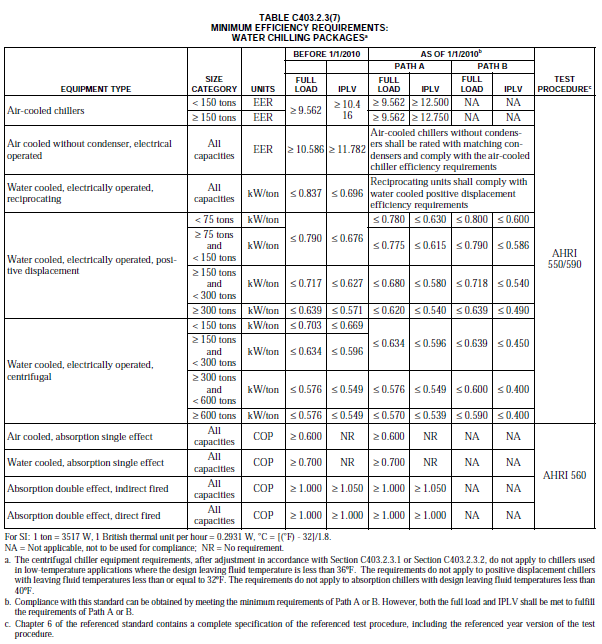
COP = EER / 3.412

COP = 12 / (kW/ton) / 3.412

EER = 12 / kW/ton

EER = COP x 3.412

Baseline Efficiency Values by Chiller Type and Capacity[[287]](#footnote-288)



###### Measure Code: CI-HVC-CHIL-V03-150601

### ENERGY STAR and CEE Tier 1 Room Air Conditioner

###### Description

This measure relates to the purchase and installation of a room air conditioning unit that meets either the ENERGY STAR or CEE TIER 1 minimum qualifying efficiency specifications, in place of a baseline unit meeting minimum Federal Standard efficiency ratings presented below:[[288]](#footnote-289)

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
| Product Class (Btu/H) | Federal Standard EER, with louvered sides | Federal Standard EER, without louvered sides | ENERGY STAR EER, with louvered sides | ENERGY STAR EER, without louvered sides | CEE TIER 1  EER |
| < 8,000 | 9.7 | 9 | 10.7 | 9.9 | 11.2 |
| 8,000 to 13,999 | 9.8 | 8.5 | 10.8 | 9.4 | 11.3 |
| 14,000 to 19,999 | 9.7 | 8.5 | 10.7 | 9.4 | 11.2 |
| >= 20,000 | 8.5 | 8.5 | 9.4 | 9.4 | 9.8 |

|  |  |  |
| --- | --- | --- |
| **Casement** | **Federal Standard (EER)** | **ENERGY STAR (EER)** |
| Casement-only | 8.7 | 9.6 |
| Casement-slider | 9.5 | 10.5 |

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
| Reverse Cycle -  Product Class (Btu/H) | Federal Standard EER, with louvered sides | Federal Standard EER, without louvered sides | ENERGY STAR EER, with louvered sides | ENERGY STAR EER, without louvered sides |
| < 14,000 | N/A | 8.5 | N/A | 9.4 |
| >= 14,000 | N/A | 8 | N/A | 8.8 |
| < 20,000 | 9 | N/A | 9.9 | N/A |
| >= 20,000 | 8.5 | N/A | 9.4 | N/A |

This measure was developed to be applicable to the following program types: TOS. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the new room air conditioning unit must meet the ENERGY STAR efficiency standards presented above.

###### Definition of Baseline Equipment

The baseline assumption is a new room air conditioning unit that meets the current minimum federal efficiency standards presented above.

###### Deemed Lifetime of Efficient Equipment

The measure life is assumed to be 9 years.[[289]](#footnote-290)

###### Deemed Measure Cost

The incremental cost for this measure is assumed to be $40 for an ENERGY STAR unit and $80 for a CEE TIER 1 unit.[[290]](#footnote-291)

###### Loadshape

Loadshape C03 - Commercial Cooling

###### Coincidence Factor

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.  Both values provided are based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren.

CFSSP = Summer System Peak Coincidence Factor for Commercial cooling (during system peak hour)

= 91.3% [[291]](#footnote-292)

CFPJM = PJM Summer Peak Coincidence Factor for Commercial cooling (average during peak period)

= 47.8%[[292]](#footnote-293)

**Algorithm**

###### Calculation of Savings

###### Energy Savings

ΔkWh = (FLHRoomAC \* Btu/H \* (1/EERbase - 1/EERee))/1000

Where:

FLHRoomAC = Full Load Hours of room air conditioning unit

= dependent on location:[[293]](#footnote-294)

|  |  |
| --- | --- |
| Zone | FLHRoomAC |
| 1 (Rockford) | 253 |
| 2-(Chicago) | 254 |
| 3 (Springfield) | 310 |
| 4-(Belleville) | 391 |
| 5-(Marion) | 254 |

Btu/H = Size of unit

= Actual. If unknown assume 8500 Btu/hr [[294]](#footnote-295)

EERbase = Efficiency of baseline unit

= As provided in tables above

EERee = Efficiency of ENERGY STAR or CEE Tier 1 unit

= Actual. If unknown assume minimum qualifying standard as provided in tables above

For example for an 8,500 Btu/H capacity ENERGY STAR unit, with louvered sides, in Rockford:

ΔkWHENERGY STAR = (253 \* 8500 \* (1/9.8 – 1/10.8)) / 1000

= 20.3 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = Btu/H \* ((1/EERbase - 1/EERee))/1000) \* CF

Where:

CFSSP = Summer System Peak Coincidence Factor for Commercial cooling (during system peak hour)

= 91.3% [[295]](#footnote-296)

CFPJM = PJM Summer Peak Coincidence Factor for Commercial cooling (average during peak period)

= 47.8%[[296]](#footnote-297)

Other variable as defined above

For example for an 8,500 Btu/H capacity ENERGY STAR unit, with louvered sides, in Rockford during system peak

ΔkWENERGY STAR = (8500 \* (1/9.8 – 1/10.8)) / 1000 \* 0.913

= 0.073 kW

###### Fossil Fuel Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-HVC-ESRA-V01-120601

### Guest Room Energy Management (PTAC & PTHP)

**Description**

This measure applied to the installation of a temperature setback and lighting control system for individual guest rooms. The savings are achieved based on Guest Room Energy Management’s (GREM’s) ability to automatically adjust the guest room’s set temperatures and control the HVAC unit for various occupancy modes.

This measure was developed to be applicable to the following program types: TOS, NC. If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

Guest room temperature set point must be controlled by automatic occupancy detectors or keycard that indicates the occupancy status of the room. During unoccupied periods the default setting for controlled units differs by at least 5 degrees from the operating set point. Theoretically, the control system may also be tied into other electric loads, such as lighting and plug loads to shut them off when occupancy is not sensed. This measure bases savings on improved HVAC controls. If system is connected to lighting and plug loads, additional savings would be realized. The incentive is per guestroom controlled, rather than per sensor, for multi-room suites. Replacement or upgrades of existing occupancy-based controls are not eligible for an incentive.

**Definition of Baseline Equipment**

Guest room energy management thermostats replace manual heating/cooling temperature set-point and fan On/Off/Auto thermostat controls. Two possible baselines exist based on whether housekeeping staff are directed to set-back (or turn off) thermostats when rooms are not rented.

**Deemed Lifetime of Efficient Equipment**

The measure life for GREM is 15 years [[297]](#footnote-298).

**Deemed Measure Cost**

$260/unit

The IMC documented for this measure is $260 per room HVAC controller, which is the cost difference between a non-programmable thermostat and a GREM[[298]](#footnote-299).

**Deemed O&M Cost Adjustments**

N/A

**Loadshape**

Loadshape C03 - Commercial Cooling

**Coincidence Factor**

A coincidence factor is not used in the determination of coincident peak kW savings.

**Algorithm**

**Calculation of Savings**

Below are the annual kWh savings per installed EMS for different sizes and types of HVAC units. The savings are achieved based on GREM’s ability to automatically adjust the guest room’s set temperatures and control the HVAC unit to maintain set temperatures for various occupancy modes. Note that care should be taken in selecting a value consistent with actual baseline conditions (e.g. whether housekeeping staff are directed to set-back/turn-off the thermostats when rooms are unrented). Different values are provided for Motels and Hotels since significant differences in shell performance, number of external walls per room and typical heating and cooling efficiencies result in significantly different savings estimates. Energy savings estimates are derived using a prototypical EnergyPlus simulation of a motel and a hotel[[299]](#footnote-300). Model outputs are normalized to the installed capacity and reported here as kWh/Ton, coincident peak kW/Ton and Therms/Ton.

**Electric Energy Savings**

| **Motel Electric Energy Savings** | | | |
| --- | --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **Heating Source** | **Baseline** | **Electric Savings**  **(kWh/Ton)** |
| 1 (Rockford) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 744 |
| No Housekeeping Setback | 1,786 |
| PTAC w/ Gas Heating | Housekeeping Setback | 63 |
| No Housekeeping Setback | 155 |
| PTHP | Housekeeping Setback | 385 |
| No Housekeeping Setback | 986 |
| 2 (Chicago) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 506 |
| No Housekeeping Setback | 1,582 |
| PTAC w/ Gas Heating | Housekeeping Setback | 51 |
| No Housekeeping Setback | 163 |
| PTHP | Housekeeping Setback | 211 |
| No Housekeeping Setback | 798 |
| 3 (Springfield) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 462 |
| No Housekeeping Setback | 1,382 |
| PTAC w/ Gas Heating | Housekeeping Setback | 65 |
| No Housekeeping Setback | 198 |
| PTHP | Housekeeping Setback | 202 |
| No Housekeeping Setback | 736 |
| 4 (Belleville) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 559 |
| No Housekeeping Setback | 1,877 |
| PTAC w/ Gas Heating | Housekeeping Setback | 85 |
| No Housekeeping Setback | 287 |
| PTHP | Housekeeping Setback | 260 |
| No Housekeeping Setback | 1,023 |
| 5 (Marion-Williamson) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 388 |
| No Housekeeping Setback | 1,339 |
| PTAC w/ Gas Heating | Housekeeping Setback | 81 |
| No Housekeeping Setback | 274 |
| PTHP | Housekeeping Setback | 174 |
| No Housekeeping Setback | 682 |
|  |  |  |  |

| **Hotel Electric Energy Savings** | | | |
| --- | --- | --- | --- |
| **Climate Zone (City based upon)** | **Heating Source** | **Baseline** | **Electric Savings (kWh/Ton)** |
| 1 (Rockford) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 204 |
| No Housekeeping Setback | 345 |
| PTAC w/ Gas Heating | Housekeeping Setback | 121 |
| No Housekeeping Setback | 197 |
| PTHP | Housekeeping Setback | 152 |
| No Housekeeping Setback | 253 |
| Central Hot Water Fan Coil w/ Electric Resistance Heating | Housekeeping Setback | 177 |
| No Housekeeping Setback | 296 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 94 |
| No Housekeeping Setback | 148 |
| 2 (Chicago) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 188 |
| No Housekeeping Setback | 342 |
| PTAC w/ Gas Heating | Housekeeping Setback | 119 |
| No Housekeeping Setback | 195 |
| PTHP | Housekeeping Setback | 145 |
| No Housekeeping Setback | 250 |
| Central Hot Water Fan Coil w/ Electric Resistance Heating | Housekeeping Setback | 161 |
| No Housekeeping Setback | 294 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 92 |
| No Housekeeping Setback | 147 |
| 3 (Springfield) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 182 |
| No Housekeeping Setback | 291 |
| PTAC w/ Gas Heating | Housekeeping Setback | 123 |
| No Housekeeping Setback | 197 |
| PTHP | Housekeeping Setback | 145 |
| No Housekeeping Setback | 233 |
| Central Hot Water Fan Coil w/ Electric Resistance Heating | Housekeeping Setback | 153 |
| No Housekeeping Setback | 240 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 94 |
| No Housekeeping Setback | 146 |
| 4 (Belleville) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 182 |
| No Housekeeping Setback | 308 |
| PTAC w/ Gas Heating | Housekeeping Setback | 125 |
| No Housekeeping Setback | 199 |
| PTHP | Housekeeping Setback | 146 |
| No Housekeeping Setback | 240 |
| Central Hot Water Fan Coil w/ Electric Resistance Heating | Housekeeping Setback | 152 |
| No Housekeeping Setback | 255 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 95 |
| No Housekeeping Setback | 147 |
| 5 (Marion-Williamson) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 171 |
| No Housekeeping Setback | 295 |
| PTAC w/ Gas Heating | Housekeeping Setback | 122 |
| No Housekeeping Setback | 199 |
| PTHP | Housekeeping Setback | 140 |
| No Housekeeping Setback | 235 |
| Central Hot Water Fan Coil w/ Electric Resistance Heating | Housekeeping Setback | 141 |
| No Housekeeping Setback | 243 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 92 |
| No Housekeeping Setback | 146 |

**Summer Coincident Peak Demand Savings**

| **Motel Coincident Peak Demand Savings** | | | |
| --- | --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **Heating Source** | **Baseline** | **Coincident Peak Demand Savings**  **(kW/Ton)** |
| 1 (Rockford) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.17 |
| PTAC w/ Gas Heating | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.17 |
| PTHP | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.17 |
| 2 (Chicago) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 0.06 |
| No Housekeeping Setback | 0.17 |
| PTAC w/ Gas Heating | Housekeeping Setback | 0.06 |
| No Housekeeping Setback | 0.17 |
| PTHP | Housekeeping Setback | 0.06 |
| No Housekeeping Setback | 0.17 |
| 3 (Springfield) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 0.07 |
| No Housekeeping Setback | 0.17 |
| PTAC w/ Gas Heating | Housekeeping Setback | 0.07 |
| No Housekeeping Setback | 0.17 |
| PTHP | Housekeeping Setback | 0.07 |
| No Housekeeping Setback | 0.17 |
| 4 (Belleville) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 0.10 |
| No Housekeeping Setback | 0.28 |
| PTAC w/ Gas Heating | Housekeeping Setback | 0.10 |
| No Housekeeping Setback | 0.28 |
| PTHP | Housekeeping Setback | 0.10 |
| No Housekeeping Setback | 0.28 |
| 5 (Marion-Williamson) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.21 |
| PTAC w/ Gas Heating | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.21 |
| PTHP | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.21 |

| **Hotel Coincident Peak Demand Savings** | | | |
| --- | --- | --- | --- |
| **Climate Zone (City based upon)** | **Heating Source** | **Baseline** | **Coincident Peak Demand Savings (kW/Ton)** |
| 1 (Rockford) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.11 |
| PTAC w/ Gas Heating | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.11 |
| PTHP | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.11 |
| Central Hot Water Fan Coil w/ Electric Resistance Heating | Housekeeping Setback | 0.05 |
| No Housekeeping Setback | 0.08 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 0.05 |
| No Housekeeping Setback | 0.08 |
| 2 (Chicago) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 0.07 |
| No Housekeeping Setback | 0.11 |
| PTAC w/ Gas Heating | Housekeeping Setback | 0.07 |
| No Housekeeping Setback | 0.11 |
| PTHP | Housekeeping Setback | 0.07 |
| No Housekeeping Setback | 0.11 |
| Central Hot Water Fan Coil w/ Electric Resistance Heating | Housekeeping Setback | 0.05 |
| No Housekeeping Setback | 0.07 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 0.05 |
| No Housekeeping Setback | 0.07 |
| 3 (Springfield) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.11 |
| PTAC w/ Gas Heating | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.11 |
| PTHP | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.11 |
| Central Hot Water Fan Coil w/ Electric Resistance Heating | Housekeeping Setback | 0.05 |
| No Housekeeping Setback | 0.07 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 0.05 |
| No Housekeeping Setback | 0.07 |
| 4 (Belleville) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.11 |
| PTAC w/ Gas Heating | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.11 |
| PTHP | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.11 |
| Central Hot Water Fan Coil w/ Electric Resistance Heating | Housekeeping Setback | 0.05 |
| No Housekeeping Setback | 0.08 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 0.05 |
| No Housekeeping Setback | 0.08 |
| 5 (Marion-Williamson) | PTAC w/ Electric Resistance Heating | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.11 |
| PTAC w/ Gas Heating | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.11 |
| PTHP | Housekeeping Setback | 0.08 |
| No Housekeeping Setback | 0.11 |
| Central Hot Water Fan Coil w/ Electric Resistance Heating | Housekeeping Setback | 0.05 |
| No Housekeeping Setback | 0.08 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 0.05 |
| No Housekeeping Setback | 0.08 |

**Natural Gas Energy Savings**

For PTACs with gas heating:

|  |  |  |
| --- | --- | --- |
| **Motel Natural Gas Energy Savings** | | |
| **Climate Zone (City based upon)** | **Baseline** | **Gas Savings (Therms/Ton)** |
| 1 (Rockford) | Housekeeping Setback | 30 |
| No Housekeeping Setback | 71 |
| 2 (Chicago) | Housekeeping Setback | 20 |
| No Housekeeping Setback | 62 |
| 3 (Springfield) | Housekeeping Setback | 17 |
| No Housekeeping Setback | 52 |
| 4 (Belleville) | Housekeeping Setback | 21 |
| No Housekeeping Setback | 70 |
| 5 (Marion-Williamson) | Housekeeping Setback | 13 |
| No Housekeeping Setback | 47 |

| **Hotel Natural Gas Energy Savings** | | | |
| --- | --- | --- | --- |
| **Climate Zone (City based upon)** | **Heating Source** | **Baseline** | **Gas Savings (Therms/Ton)** |
| 1 (Rockford) | PTAC w/ Gas Heating | Housekeeping Setback | 3.6 |
| No Housekeeping Setback | 6.4 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 3.6 |
| No Housekeeping Setback | 6.4 |
| 2 (Chicago) | PTAC w/ Gas Heating | Housekeeping Setback | 3.0 |
| No Housekeeping Setback | 6.5 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 3.0 |
| No Housekeeping Setback | 6.5 |
| 3 (Springfield) | PTAC w/ Gas Heating | Housekeeping Setback | 2.6 |
| No Housekeeping Setback | 4.1 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 2.6 |
| No Housekeeping Setback | 4.1 |
| 4 (Belleville) | PTAC w/ Gas Heating | Housekeeping Setback | 2.5 |
| No Housekeeping Setback | 4.8 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 2.5 |
| No Housekeeping Setback | 4.8 |
| 5 (Marion-Williamson) | PTAC w/ Gas Heating | Housekeeping Setback | 2.1 |
| No Housekeeping Setback | 4.2 |
| Central Hot Water Fan Coil w/ Gas Heating | Housekeeping Setback | 2.1 |
| No Housekeeping Setback | 4.2 |

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

###### Measure Code: CI-HVC-GREM-V05-150601

### Heat Pump Systems

###### Description

This measure applies to the installation of high-efficiency air cooled, water source, ground water source, and ground source heat pump systems. This measure could apply to replacing an existing unit at the end of its useful life, or installation of a new unit in a new or existing building

This measure was developed to be applicable to the following program types: TOS NC., If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the efficient equipment is assumed to be a high-efficiency air cooled, water source, ground water source, or ground source heat pump system that exceeds the energy efficiency requirements of the International Energy Conservation Code (IECC) 2012,.

###### Definition of Baseline Equipment

In order for this characterization to apply, the baseline equipment is assumed to be a standard-efficiency air cooled, water source, ground water source, or ground source heat pump system that meets the energy efficiency requirements of the International Energy Conservation Code (IECC) 2012,. The rating conditions for the baseline and efficient equipment efficiencies must be equivalent

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 15 years.[[300]](#footnote-301)

###### Deemed Measure Cost

For analysis purposes, the incremental capital cost for this measure is assumed as $100 per ton for air-cooled units.[[301]](#footnote-302) The incremental cost for all other equipment types should be determined on a site-specific basis

###### Loadshape

Loadshape C05 - Commercial Electric Heating and Cooling

###### Coincidence Factor

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.  Both values provided are based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren.

CFSSP = Summer System Peak Coincidence Factor for Commercial cooling (during system peak hour)

= 91.3% [[302]](#footnote-303)

CFPJM = PJM Summer Peak Coincidence Factor for Commercial cooling (average during peak period)

= 47.8%[[303]](#footnote-304)

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

For units with cooling capacities less than 65 kBtu/hr:

ΔkWh= Annual kWh Savingscool + Annual kWh Savingsheat

Annual kWh Savingscool = (kBtu/hrcool) \* [(1/SEERbase) – (1/SEERee)] \* EFLHcool

Annual kWh Savingsheat = (kBtu/hrcool) \* [(1/HSPFbase) – (1/HSPFee)] \* EFLHheat

For units with cooling capacities equal to or greater than 65 kBtu/hr:

ΔkWh= Annual kWh Savingscool + Annual kWh Savingsheat

Annual kWh Savingscool = (kBtu/hrcool) \* [(1/EERbase) – (1/EERee)] \* EFLHcool

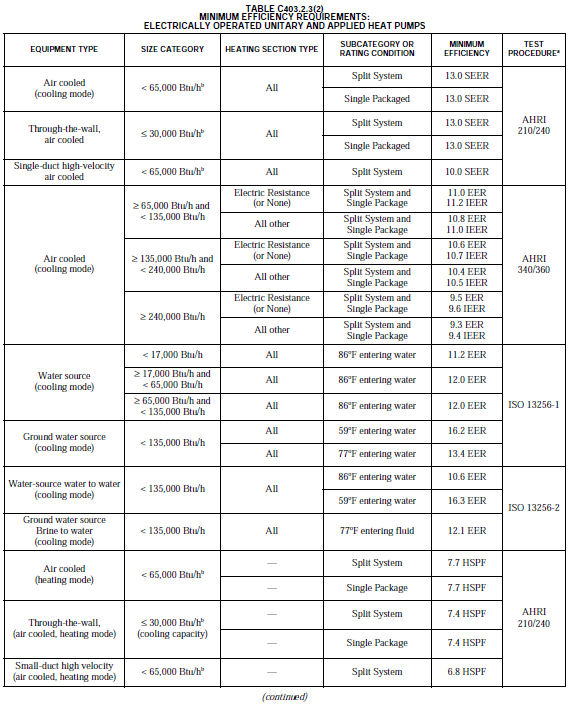
Annual kWh Savingsheat = (kBtu/hrheat)/3.412 \* [(1/COPbase) – (1/COPee)] \* EFLHheat

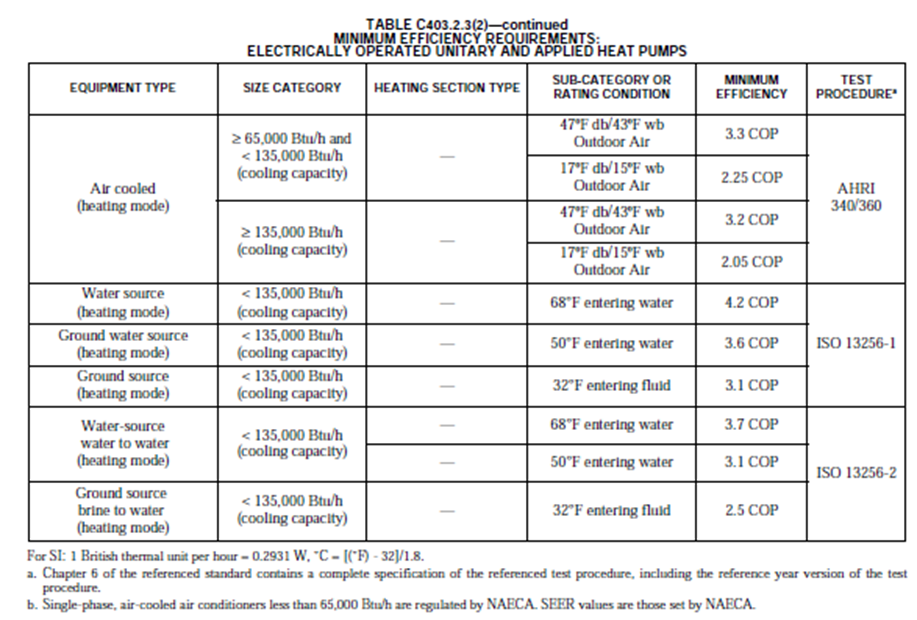
Where:

kBtu/hrcool = capacity of the cooling equipment in kBtu per hour (1 ton of cooling capacity equals 12 kBtu/hr).

= Actual installed

SEERbase =Seasonal Energy Efficiency Ratio of the baseline equipment; see table below for values. [[304]](#footnote-305)





SEERee = Seasonal Energy Efficiency Ratio of the energy efficient equipment.

= Actual installed

EFLHcool = Equivalent Full Load Hours for cooling are provided in section 4.4 HVAC End Use:

HSPFbase = Heating Seasonal Performance Factor of the baseline equipment; see table above for values.

HSPFee = Heating Seasonal Performance Factor of the energy efficient equipment.

= Actual installed

EFLHheat  = heating mode equivalent full load hours; see table above for default values.

EERbase = Energy Efficiency Ratio of the baseline equipment; see the table above for values. Since IECC 2012 does not provide EER requirements for air-cooled heat pumps < 65 kBtu/hr, assume the following conversion from SEER to EER: EER≈SEER/1.1.

EERee = Energy Efficiency Ratio of the energy efficient equipment. For air-cooled air conditioners < 65 kBtu/hr, if the actual EERee is unknown, assume the following conversion from SEER to EER: EER≈SEER/1.1.

= Actual installed

kBtu/hrheat = capacity of the heating equipment in kBtu per hour.

= Actual installed

3.412 = Btu per Wh.

COPbase = coefficient of performance of the baseline equipment; see table above for values.

COPee = coefficient of performance of the energy efficient equipment.

= Actual installed

Annual kWh Savingscool = (kBtu/hrcool) \* [(1/SEERbase) – (1/SEERee)] \* EFLHcool

Annual kWh Savingsheat = (kBtu/hrheat) \* [(1/HSPFbase) – (1/HSPFee)] \* EFLHheat

For example a 5 ton cooling unit at a restaurant in Chicago with 60 kbtu heating with an efficient EER of 14 and an efficient HSPF of 9 saves

= [(60) \* [(1/13) – (1/14)] \* 1134] + [(60) \* [(1/7.7) – (1/9)] \* 1354]

= 1650 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = (kBtu/hrcool) \* [(1/EERbase) – (1/EERee)] \*CF

Where CF value is chosen between:

CFSSP = Summer System Peak Coincidence Factor for Commercial cooling (during system peak hour)

= 91.3% [[305]](#footnote-306)

CFPJM = PJM Summer Peak Coincidence Factor for Commercial cooling (average during peak period)

= 47.8%[[306]](#footnote-307)

For example a 5 ton cooling unit with 60 kbtu heating with an efficient EER of 14 and an efficient HSPF of 9 saves

ΔkW = [(60) \* [(1/13) – (1/14)] \*.913

= 0.3

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-HVC-HPSY-V03-150601

### High Efficiency Boiler

###### Description

To qualify for this measure the installed equipment must be replacement of an existing boiler at the end of its service life, in a commercial or multifamily space with a high efficiency, gas-fired steam or hot water boiler. High efficiency boilers achieve gas savings through the utilization of a sealed combustion chamber and multiple heat exchangers that remove a significant portion of the waste heat from flue gasses. Because multiple heat exchangers are used to remove waste heat from the escaping flue gasses, some of the flue gasses condense and must be drained.

This measure was developed to be applicable to the following program types: TOS, RF. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a boiler used 80% or more for space heating, not process, and boiler AFUE, TE (thermal efficiency), or Ec (combustion efficiency) rating must be rated greater than or equal to 85% for hot water boilers and 81% for steam boilers.

###### Definition of Baseline Equipment

Dependent on when the unit is installed and whether the unit is hot water or steam. The baseline efficiency source is the Energy Independence and Security Act of 2007 with technical amendments from Federal Register, volume 73, Number 145, Monday, July 28, 2008 for boilers <300,000 Btu/hr and is Final Rule, Federal Register, volume 74, Number 139, Wednesday, July 22, 2009 for boiler ≥300,000 Btu/hr.

Hot water boiler baseline:

|  |  |
| --- | --- |
| Year | Efficiency |
| Hot Water <300,000 Btu/hr < June 1, 2013[[307]](#footnote-308) | 80% AFUE |
| Hot Water <300,000 Btu/hr ≥ June 1, 2013 | 82% AFUE |
| Hot Water ≥300,000 & ≤2,500,000 Btu/hr | 80% TE |
| Hot Water >2,500,000 Btu/hr | 82% Ec |

Steam boiler baseline:

|  |  |
| --- | --- |
| Year | Efficiency |
| Steam <300,000 Btu/hr < June 1, 2013[[308]](#footnote-309) | 75% AFUE |
| Steam <300,000 Btu/hr ≥June 1, 2013 | 80% AFUE |
| Steam - all except natural draft ≥300,000 & ≤2,500,000 Btu/hr | 79% TE |
| Steam - natural draft ≥300,000 & ≤2,500,000 Btu/hr | 77% TE |
| Steam - all except natural draft >2,500,000 Btu/hr | 79% TE |
| Steam - natural draft >2,500,000 Btu/hr | 77% TE |

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 20 years[[309]](#footnote-310)

###### Deemed Measure Cost

The incremental capital cost for this measure depends on efficiency as listed below[[310]](#footnote-311)

| Measure Tier | Incr. Cost, per unit |
| --- | --- |
| ENERGY STAR® Minimum | $1,470 |
| AFUE 90% | $2,400 |
| AFUE 95% | $3,370 |
| AFUE ≥ 96% | $4,340 |
| Boilers > 300,000 Btu/hr with TE (thermal efficiency) rating | Custom |

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Energy Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

ΔTherms = EFLH \* Capacity \* ((EfficiencyRating(actual) - EfficiencyRating(base)/ EfficiencyRating(base)) / 100,000

Where:

EFLH = Equivalent Full Load Hours for heating are provided in section 4.4 HVAC End Use

Capacity = Nominal Heating Input Capacity Boiler Size (Btu/hr) for efficient unit not existing unit

= custom Boiler input capacity in Btu/hr

EfficiencyRating(base) = Baseline Boiler Efficiency Rating, dependant on year and boiler type. Baseline efficiency values by boiler type and capacity are found in the Definition of Baseline Equipment Section

EfficiencyRating(actual) = Efficent Boiler Efficiency Rating use actual value

| Measure Type | Actual AFUE |
| --- | --- |
| ENERGY STAR® Minimum | 85% |
| AFUE 90% | 90% |
| AFUE 95% | 95% |
| AFUE ≥ 96% | ≥ 96% |
| Custom | Value to one significant digit i.e. 95.7% |

EXAMPLE

For example, a 150,000 btu/hr water boiler meeting AFUE 90% in Rockford at a high rise office building , in the year 2012

ΔTherms = 2,089\* 150,000 \* (0.90-0.80)/0.80) / 100,000 Btu/Therm

= 392 Therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-HVC-BOIL-V05-150601

### 

### 4.4.11 High Efficiency Furnace

**Description**

This measure covers the installation of a high efficiency gas furnace in lieu of a standard efficiency gas furnace in a commercial or industrial space. High efficiency gas furnaces achieve savings through the utilization of a sealed, super insulated combustion chamber, more efficient burners, and multiple heat exchangers that remove a significant portion of the waste heat from the flue gasses. Because multiple heat exchangers are used to remove waste heat from the escaping flue gasses, most of the flue gasses condense and must be drained. Furnaces equipped with ECM fan motors can save additional electric energy

This measure was developed to be applicable to the following program types: TOS RF and EREP. If applied to other program types, the measure savings should be verified.

Time of sale:

* 1. The installation of a new high efficiency, gas-fired condensing furnace in a commercial location. This could relate to the replacement of an existing unit at the end of its useful life, or the installation of a new system.

Early replacement:

1. The early removal of an existing functioning AFUE 75% or less furnace from service, prior to its natural end of life, and replacement with a new high efficiency unit. Savings are calculated between existing unit and efficient unit consumption during the remaining life of the existing unit, and between new baseline unit and efficient unit consumption for the remainder of the measure life. At time of writing, the DOE had rescinded the next Federal Standard change for furnaces, however it is likely that a new standard will be in effect after the assumed remaining useful life of the existing unit. For the purposes of this measure- the new baseline is assumed to be 90%.
2. The assumption of the existing unit efficiency in the Early Replacement section of this TRM is based upon the average efficiency of units that were classified in Ameren’s PY3-PY4 as functioning and AFUE <=75%. Therefore it is only appropriate to use these Early Replacement assumptions where those conditions are met. The TAC defined “functioning” as the unit is fully operational – providing sufficient space conditioning (i.e. heat exchanger, compressors, pumps work effectively) and/or the cost of repair is under 20% of the new baseline replacement cost. Therefore in order to apply early replacement assumptions the programs should apply the following eligibility criteria: AFUE <=75% and cost of any repairs <$528.

**Definition of Efficient Equipment**

To qualify for this measure the installed equipment must be a furnace with input energy less than 225,000 Btu/hr rated natural gas fired furnace with an Annual Fuel Utilization Efficiency (AFUE) rating and fan electrical efficiency exceeding the program requirements:

**Definition of Baseline Equipment**

Time of Sale: Although the current Federal Standard for gas furnaces is an AFUE rating of 78%, based upon review of available product in the AHRI database, the baseline efficiency for this characterization is assumed to be 80%. The baseline will be adjusted when the Federal Standard is updated.

Early replacement: The baseline for this measure is the efficiency of the existing equipment for the assumed remaining useful life of the unit and a new baseline unit for the remainder of the measure life. As discussed above we estimate that the new baseline unit that could be purchased in the year the existing unit would have needed replacing is 90%

**Definition of Measure Life**

The expected measure life is assumed to be 16.5 years[[311]](#footnote-312)

Remaining life of existing equipment is assumed to be 5.5 years[[312]](#footnote-313).

**Deemed Measure Cost**

Time of Sale: The incremental capital cost for this measure depends on efficiency as listed below[[313]](#footnote-314):

|  |  |  |
| --- | --- | --- |
| **AFUE** | **Installation Cost** | **Incremental Install Cost** |
| 80% | $2011 | n/a |
| 90% | $2641 | $630 |
| 91% | $2727 | $716 |
| 92% | $2813 | $802 |
| 93% | $3049 | $1,038 |
| 94% | $3286 | $1,275 |
| 95% | $3522 | $1,511 |
| 96% | $3758 | $1,747 |

Early Replacement: The full installation cost is provided in the table above. The assumed deferred cost (after 5.5 years) of replacing existing equipment with a new baseline unit is assumed to be $2641. This cost should be discounted to present value using the utilities discount rate.

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

ΔkWh = Heating Savings + Cooling Savings + Shoulder Season Savings

Where:

Heating Savings = Brushless DC motor or Electronically commutated motor (ECM) = 418 kWh[[314]](#footnote-315)

Cooling Savings = Brushless DC motor or electronically commutated motor (ECM) savings during cooling season

If air conditioning = 263 kWh

If no air conditioning = 175 kWh

If unknown (weighted average)= 241 kWh[[315]](#footnote-316)

Shoulder Season Savings = Brushless DC motor or electronically commutated motor (ECM) savings during shoulder seasons

= 51 kWh

EXAMPLE

For example, a blower motor in an office building where air conditioning presence is unknown:

ΔkWh = Heating Savings + Cooling Savings + Shoulder Season Savings

= 418 +251 + 51

= 721 kWh

**Summer Coincident Peak Demand Savings**

For units that have evaporator coils and condensing units and are cooling in the summer in addition to heating in the winter the summer coincident peak demand savings should be calculated. If the unit is not equipment with coils or condensing units, the summer peak demand savings will not apply.

ΔkW = (ΔkWh/HOURSyear) \* CF

Where:

HOURSyear = Actual hours per year if known, otherwise use hours from Table below for building type[[316]](#footnote-317).

| **Building Type** | **Pumps and fans (h/yr)** |
| --- | --- |
| College/University | 4216 |
| Grocery | 5840 |
| Heavy Industry | 3585 |
| Hotel/Motel | 6872 |
| Light Industry | 2465 |
| Medical | 6871 |
| Office | 2301 |
| Restaurant | 4654 |
| Retail/Service | 3438 |
| School(K-12) | 2203 |
| Warehouse | 3222 |
| Average=Miscellaneous | 4103 |

CF =Summer Peak Coincidence Factor for measure is provided below for different building types[[317]](#footnote-318):

|  |  |
| --- | --- |
| **Location** | **CF** |
| Restaurant | 0.80 |
| Office | 0.66 |
| School (K-12) | 0.22 |
| College/University | 0.56 |
| Medical | 0.75 |

EXAMPLE

For example, a blower motor in an office building where air conditioning presence is unknown:

ΔkW = (721 kWh/1766) \* 0.66 = 0.27 kW

**Natural Gas Energy Savings**

Time of Sale:

ΔTherms = EFLH \* Capacity \* ((AFUE(eff) – AFUE(base)/AFUE(base))/ 100,000 Btu/Therm

Early replacement[[318]](#footnote-319):

ΔTherms for remaining life of existing unit (1st 5.5 years):

ΔTherms = EFLH \* Capacity \* (AFUE(eff) – AFUE(exist)/ AFUE(exist)) / 100,000 Btu/Therm

ΔTherms for remaining measure life (next 11 years):

ΔTherms = EFLH \* Capacity \* (AFUE(eff) - AFUE(base)/AFUE(base)) / 100,000 Btu/Therm

Where:

EFLH = Equivalent Full Load Hours for heating are provided in section 4.4 HVAC End Use

Capacity = Nominal Heating Input Capacity Furnace Size (Btu/hr) for efficient unit not existing unit

= custom Furnace input capacity in Btu/hr

AFUE(exist) = Existing Furnace Annual Fuel Utilization Efficiency Rating

= Use actual AFUE rating where it is possible to measure or reasonably estimate.

If unknown, assume 64.4 AFUE% **[[319]](#footnote-320)**.

AFUE(base) = Baseline Furnace Annual Fuel Utilization Efficiency Rating, dependant on year as listed below:

Dependent on program type as listed below[[320]](#footnote-321):

|  |  |
| --- | --- |
| **Program Year** | **AFUE(base)** |
| Time of Sale | 80% |
| Early Replacement | 90% |

AFUE(eff) = Efficent Furnace Annual Fuel Utilization Efficiency Rating.

= Actual. If Unknown, assume 95%[[321]](#footnote-322)

EXAMPLE

For example, a 150,000 btu/hr 92% efficient furnace at a low rise office building in Rockford, in the year 2012

ΔTherms = 1497\* 150,000 \* ((0.92-0.80)/0.80)/ 100,000 Btu/Therm

= 337 Therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

###### Measure Code: CI-HVC-FRNC-V04-150601

### Infrared Heaters (all sizes), Low Intensity

###### Description

This measure applies to natural gas fired low-intensity infrared heaters with an electric ignition that use non-conditioned air for combustion

This measure was developed to be applicable to the following program types: TOS, NC. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a natural gas heater with an electric ignition that uses non-conditioned air for combustion

###### Definition of Baseline Equipment

The baseline equipment is a standard natural gas fired heater warm air heater.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 12 years[[322]](#footnote-323)

###### Deemed Measure Cost

The incremental capital cost for this measure is $1716[[323]](#footnote-324)

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

The annual natural gas energy savings from this measure is a deemed value equaling 451 Therms[[324]](#footnote-325)

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-HVC-IRHT-V01-120601

### Package Terminal Air Conditioner (PTAC) and Package Terminal Heat Pump (PTHP)

###### Description

A PTAC is a packaged terminal air conditioner that cools and sometimes provides heat through an electric resistance heater (heat strip). A PTHP is a packaged terminal heat pump. A PTHP uses its compressor year round to heat or cool. In warm weather, it efficiently captures heat from inside your building and pumps it outside for cooling. In cool weather, it captures heat from outdoor air and pumps it into your home, adding heat from electric heat strips as necessary to provide heat.

This measure characterizes:

1. Time of Sale: the purchase and installation of a new efficient PTAC or PTHP.
2. Early Replacement: the early removal of an existing PTAC or PTHP from service, prior to its natural end of life, and replacement with a new efficient PTAC or PTHP unit. Savings are calculated between existing unit and efficient unit consumption during the remaining life of the existing unit, and between new baseline unit and efficient unit consumption for the remainder of the measure life. The measure is only valid for non-fuel switching installations – for example replacing a cooling only PTAC with a PTHP can currently not use the TRM.

This measure was developed to be applicable to the following program types: TOS NC, EREP. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the efficient equipment is assumed to be PTACs or PTHPs that exceed baseline efficiencies.

###### Definition of Baseline Equipment

Time of Sale: the baseline conditions is provided in the Federal Baseline reference table provided below.

Early Replacement: the baseline is the existing PTAC or PTHP for the assumed remaining useful life of the unit and the new baseline as defined above for the remainder of the measure life.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 15 years. [[325]](#footnote-326)

Remaining life of existing equipment is assumed to be 5 years[[326]](#footnote-327)

###### Deemed Measure Cost

Time of Sale: The incremental capital cost for this equipment is estimated to be $84/ton.[[327]](#footnote-328)

Early Replacement: The measure cost is the full cost of removing the existing unit and installing a new one. The actual program cost should be used. If unknown assume $1,047 per ton[[328]](#footnote-329).

The assumed deferred cost (after 5 years) of replacing existing equipment with new baseline unit is assumed to be $963 per ton[[329]](#footnote-330). This cost should be discounted to present value using the utilities discount rate.

###### Loadshape

Loadshape C03 - Commercial Cooling

###### Coincidence Factor

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.  Both values provided are based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren.

CFSSP = Summer System Peak Coincidence Factor for Commercial cooling (during system peak hour)

= 91.3% [[330]](#footnote-331)

CFPJM = PJM Summer Peak Coincidence Factor for Commercial cooling (average during peak period)

= 47.8%[[331]](#footnote-332)

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

Electric savings for PTACs and PTHPs should be calculated using the following algorithms

###### Energy Savings

Time of Sale:

PTAC ΔkWh[[332]](#footnote-333)= Annual kWh Savingscool

PTHP ΔkWh= Annual kWh Savingscool + Annual kWh Savingsheat

Annual kWh Savingscool = (kBtu/hrcool) \* [(1/EERbase) – (1/EERee)] \* EFLHcool

Annual kWh Savingsheat = (kBtu/hrheat)/3.412 \* [(1/COPbase) – (1/COPee)] \* EFLHheat

Early Replacement:

ΔkWh for remaining life of existing unit (1st 5years) = Annual kWh Savingscool + Annual kWh Savingsheat

Annual kWh Savingscool = (kBtu/hrcool) \* [(1/EERexist) – (1/EERee)] \* EFLHcool

Annual kWh Savingsheat = (kBtu/hrheat)/3.412 \* [(1/COPexist) – (1/COPee)] \* EFLHheat

ΔkWh for remaining measure life (next 10 years) = Annual kWh Savingscool + Annual kWh Savingsheat

Annual kWh Savingscool = (kBtu/hrcool) \* [(1/EERbase) – (1/EERee)] \* EFLHcool

Annual kWh Savingsheat = (kBtu/hrheat)/3.412 \* [(1/COPbase) – (1/COPee)] \* EFLHheat

Where:

kBtu/hrcool = capacity of the cooling equipment in kBtu per hour (1 ton of cooling capacity equals 12 kBtu/hr).

= Actual installed

EFLHcool = Equivalent Full Load Hours for cooling are provided in section 4.4 HVAC End Use:

EFLHheat  = Equivalent Full Load Hours for heating are provided in section 4.4 HVAC End Use

EERexist = Energy Efficiency Ratio of the existing equipment

= Actual. If unknown assume 8.1 EER[[333]](#footnote-334)

EERbase = Energy Efficiency Ratio of the baseline equipment; see the table below for values.

Copy of Table C403.2.3(3), IECC 2012:

Minimum Efficiency Reguirements: Electrically operated packaged terminal air conditioners, packaged terminal heat pumps

|  |  |
| --- | --- |
| **Equipment Type** | **Minimum Efficiency as of 10/08/2012** |
| PTAC (Cooling mode)  New Construction | 13.8 – (0.300 x Cap/1000) EER |
| PTAC (Cooling mode)  Replacements | 10.9 – (0.213 x Cap/1000) EER |
| PTHP (Cooling mode)  New Construction | 14.0 – (0.300 x Cap/1000) EER |
| PTHP (Cooling mode)  Replacements | 10.8 – (0.213 x Cap/1000) EER |
| PTHP (Heating mode)  New Construction | 3.2 – (0.026 x Cap/1000) COP |
| PTHP (Heating mode)  Replacements | 2.9 – (0.026 x Cap/1000) COP |

“Cap” = The rated cooling capacity of the project in Btu/hr. If the units capacity is less than 7000 Btu/hr, use 7,000 Btu/hr in the calculation. If the unit’s capacity is greater than 15,000 Btu/hr, use 15,000 Btu/hr in the calculations.

Replacement unit shall be factory labeled as follows “MANUFACTURED FOR REPLACEMENT APPLICATIONS ONLY; NOT TO BE INSTALLED IN NEW CONSTRUCTION PROJECTS”, Replacement efficiencies apply only to units with existing sleeves less than 16 inches (406mm) in height and less than 42 inches (1067 mm) in width.

EERee = Energy Efficiency Ratio of the energy efficient equipment. For air-cooled air conditioners < 65 kBtu/hr, if the actual EERee is unknown, assume the following conversion from SEER to EER: EER≈SEER/1.1.

= Actual installed

kBtu/hrheat = capacity of the heating equipment in kBtu per hour.

= Actual installed

3.412 = Btu per Wh.

COPexist = coefficient of performance of the existing equipment

= Actual. If unknown assume 1.0 COP for PTAC units and 2.6 COP[[334]](#footnote-335) for PTHPs.

COPbase = coefficient of performance of the baseline equipment; see table above for values.

COPee = coefficient of performance of the energy efficient equipment.

= Actual installed

Time of Sale (assuming new construction baseline):

For example a 1 ton PTAC with an efficient EER of 12 at a hotel in Rockford saves:

= [(12) \* [(1/10.2) – (1/12)] \* 1,042

= 184 kWh

Early Replacement (assuming replacement baseline for deferred replacement in 5 years):

For example a 1 ton PTHP with an efficient EER of 12, COP of 3.0 in Rockford replaces a PTAC unit (with electric resistance heat) with unknown efficiency.

ΔkWh for remaining life of existing unit (1st 5years)

= (12 \* (1/8.1 – 1/12) \* 1,042) + (12/3.412 \* (1/1.0 – 1/3.0) \* 1,758)

= 502 + 4,122

= 4,624 kWh

ΔkWh for remaining measure life (next 10 years)

= (12 \* (1/8.3 – 1/12) \* 1,042) + (12/3.412 \* (1/1.0 – 1/3.0) \* 1,758)

= 465 + 4,122

= 34,587 kWh

**Summer Coincident Peak Demand Savings**

Time of Sale:

ΔkW = (kBtu/hrcool) \* [(1/EERbase) – (1/EERee)] \*CF

Early Replacement:

ΔkW for remaining life of existing unit (1st 5years) = (kBtu/hrcool) \* [(1/EERexist) – (1/EERee)] \*CF

ΔkWh for remaining measure life (next 10 years) = (kBtu/hrcool) \* [(1/EERbase) – (1/EERee)] \*CF

Where:

CFSSP = Summer System Peak Coincidence Factor for Commercial cooling (during system peak hour)

= 91.3% [[335]](#footnote-336)

CFPJM = PJM Summer Peak Coincidence Factor for Commercial cooling (average during peak period)

= 47.8% [[336]](#footnote-337)

Time of Sale:

For example a 1 ton replacement cooling unit with no heating with an efficient EER of 12 at a hotel in Rockford saves

ΔkWSSP = (12 \* (1/10.2 – 1/12) \*0.913

= 0.16 kW

For example a 1 ton PTHP with an efficient EER of 12, COP of 3.0 in Rockford replaces a PTAC unit with unknown efficiency.

ΔkW for remaining life of existing unit (1st 5years):

ΔkWSSP = 12 \* (1/8.1 – 1/12) \* 0.913

= 0.44 kW

ΔkW for remaining measure life (next 10 years):

ΔkWSSP = 12 \* (1/8.3 – 1/12) \* 0.913

= 0.41 kW

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-HVC-PTAC-V05-150601

### Pipe Insulation

###### Description

This measure provides rebates for installation of ≥1” or ≥2” fiberglass, foam, calcium silicate or other types of insulation with similar insulating properties to existing bare pipe on straight piping as well as other pipe components such as elbows, tees, valves, and flanges for all non-residential installations.

Default per linear foot savings estimates are provided for the both exposed indoor or above ground outdoor piping distributing fluid in the following system types (natural gas fired systems only):

* Hydronic heating systems (with or without outdoor reset controls), including:
  + boiler systems that do not circulate water around a central loop and operate upon demand from a thermostat (“non-recirculation”)
  + systems that recirculate during heating season only (“Recirculation – heating season only”)
  + systems recirculating year round (“Recirculation – year round”)
* Domestic hot water
* Low and high-pressure steam systems
  + non-recirculation
  + recirculation - heating season only
  + recirculation - year round

Process piping can also use the algorithms provided but requires custom entry of hours.

Minimum qualifying nominal pipe diameter is 1.” Indoor piping must have at least 1” of insulation and outdoor piping must have at least 2” of insulation and include an all-weather protective jacket. New advanced insulating materials may be thinner and savings can be calculated with 3E Plus.

This measure was developed to be applicable to the following program types:  RF, DI

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The efficient case is installing pipe wrap insulation to a length of pipe. Indoor piping must have at least 1” of insulation (or equivalent R-value) and outdoor piping must have at least 2” of insulation (or equivalent R-value) and include an all-weather protective jacket. Minimum qualifying pipe diameter is 1.” Insulation must be continuous and contiguous over fittings that directly connect to straight pipe, including elbows and tees.[[337]](#footnote-338)

###### Definition of Baseline Equipment

The base case for savings estimates is a bare pipe. Pipes are required by new construction code to be insulated but are still commonly found uninsulated in older commercial buildings.

###### Deemed Lifetime of Efficient Equipment

The measure life is assumed to be 15 years.[[338]](#footnote-339)

###### Deemed Measure Cost

Actual costs should be used if known. Otherwise the deemed measure costs below based on RS Means[[339]](#footnote-340) pricing reference materials may be used.[[340]](#footnote-341) The following table summarizes the estimated costs for this measure per foot of insulation added and include installation costs:

|  |  |  |
| --- | --- | --- |
|  | **INSULATION THICKNESS** | |
| **1 INCH (INDOOR)** | **2 INCHES (OUTDOOR)** |
| Pipe- RS Means # | 220719.10.5170 | 220719.10.5530 |
| Jacket- RS Means # | 220719.10.0156 | 220719.10.0320 |
| Jacket Type | PVC | Aluminum |
| Insulation Cost per foot | $9.40 | $13.90 |
| Jacket Cost per foot | $4.57 | $7.30 |
| **Total Cost per foot** | **$13.97** | **$21.20** |

###### Loadshape

N/A

###### Coincidence Factor

N/A

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Savings

Δtherms per foot[[341]](#footnote-342) = [((Qbase – Qeff) \* EFLH) / (100,000 \* ηBoiler)] \* TRF

= [Provided by tables below] \* TRF

Δtherms = (Lsp + Loc,i) \* Δtherms per foot

Where:

EFLH = Equivalent Full Load Hours for Heating

= Actual or defaults by building type provided in Section 4.4, HVAC end use

For year round recirculation or domestic hot water:

= 8760

For heating season recirculation, hours with the outside air temperature below 55°F:

| **Zone** | **Hours** |
| --- | --- |
| Zone 1 (Rockford) | 5,039 |
| Zone 2 (Chicago) | 4,963 |
| Zone 3 (Springfield) | 4,495 |
| Zone 4 (Belleville/ | 4,021 |
| Zone 5 (Marion) | 4,150 |
| Zone 1 (Rockford) | 5,039 |

Qbase = Heat Loss from Bare Pipe (Btu/hr/ft)

= See table below

Qeff = Heat Loss from Insulated Pipe (Btu/hr/ft)

= See table below

100,000 = conversion factor (1 therm = 100,000 Btu)

ηBoiler = Efficiency of the boiler being used to generate the hot water or steam in the pipe

= 81.9% for water boilers [[342]](#footnote-343)

= 80.7% for steam boilers, except multifamily low-pressure [[343]](#footnote-344)

= 64.8% for multifamily low-pressure steam boilers [[344]](#footnote-345)

TRF = Thermal Regain Factor for space type, applied only to space heating energy and is applied to values resulting from Δtherms/ft tables below [[345]](#footnote-346)

= See table below for base TRF values by pipe location

May vary seasonally such as: TRF[summer] \* summer hours + TRF[winter] \* winter hours where TRF values reflecting summer and winter conditions are apportioned by the hours for those conditions. TRF may also be adjusted by building specific balance temperature and operating hours above and below that balance temperature.[[346]](#footnote-347)

|  |  |  |
| --- | --- | --- |
| **Pipe Location** | **Assumed Regain** | **TRF, Thermal Regain Factor** |
| Outdoor | 0% | 1.0 |
| Indoor, heated space | 85% | 0.15 |
| Indoor, semi- heated, (unconditioned space, with heat transfer to conditioned space. E.g.: boiler room, ceiling plenum, basement, crawlspace, wall) | 30% | 0.70 |
| Indoor, unheated, (no heat transfer to conditioned space) | 0% | 1.0 |
| Location not specified | 85% | 0.15 |
| Custom | Custom | 1 – assumed regain |

Lsp = Length of straight pipe to be insulated (linear foot)

= actual installed ((linear foot)

Loc,I = Total equivalent length of the other components (valves and tees) of pipe to be insulated

= Actual installed (linear foot). See table “Equivalent Length of Other Components – Elbows and Tees” for equivalent lengths.

The heat loss estimates (Qbase and Qeff) were developed using the 3E Plus v4.0 software program.[[347]](#footnote-348) The energy savings analysis is based on adding 1-inch (indoor) or 2-inch (outdoor) thick insulation around bare pipe. The thermal conductivity of pipe insulation varies by material and temperature rating; to obtain a typical value, a range of materials allowed for this measure were averaged. For insulation materials not in the table below, use 3E Plusv4.0 software to calculate Qbase and Qeff.

|  |  |  |
| --- | --- | --- |
| **Insulation Type** | **Conductivity  (Btu.in / hr.ft2.ºF @ 75F)** | **Max temp (ºF)** |
| Polyethylene foam | 0.25 | 200 |
| Flexible polyurethane-based foam | 0.27 | 200 |
| Fiberglass | 0.31 | 250 |
| Melamine foam | 0.26 | 350 |
| Flexible silicon foam | 0.40 | 392 |
| Calcium silicate | 0.40 | 1200 |
| Cellular glass | 0.31 | 400 |
| Average conductivity of all these materials  (Btu.in / hr.ft2.ºF @ 75ºF) | 0.31 |  |

The pipe fluid temperature assumption used depends upon both the system type and whether there is outdoor reset controls:

|  |  |
| --- | --- |
| **System Type** | **Fluid temperature assumption**  **(**°**F)** |
| Hot Water space heating with outdoor reset - Non recirculation | 145 |
| Hot Water space heating without outdoor reset - Non recirculation | 170 |
| Hot Water space heating with outdoor reset – Recirculation heating season only | 145 |
| Hot Water space heating without outdoor reset – Recirculation heating season only | 170 |
| Hot Water space heating with outdoor reset – Recirculation year round | 130 |
| Hot Water space heating without outdoor reset – Recirculation year round | 170 |
| Domestic Hot Water | 125 |
| Low Pressure Steam | 225 |
| High Pressure Steam | 312 |

|  | **Indoor Insulation, Hot Water** | **Indoor Insulation, Low Pressure Steam** | **Indoor Insulation, High Pressure Steam** | **Domestic Hot Water** | **Outdoor Insulation, Hot Water** | **Outdoor Insulation, Low Pressure Steam** | **Outdoor Insulation, High Pressure Steam** |
| --- | --- | --- | --- | --- | --- | --- | --- |
| Insulation thickness (inch) | 1 | 1 | 1 | 1 | 2 | 2 | 2 |
| Temperature, Fluid in Pipe (ºF) | 170 (w/o reset)  145 (w/ reset heat)  130 (w/reset year) | 225 | 312 | 125 | 170 (w/o reset)  145 (w/ reset heat)  130 (w/reset year) | 225 | 312 |
| Av. steam pressure (psig) | n/a | 10.9 | 82.8 | n/a | n/a | 10.9 | 82.8 |
| Operating Time (hrs/yr) | 2,746 (non-recirc)  5,039 (recirc heating season)  8,760 (recirc year round) | | | | | | |
| Ambient Temperature (ºF)[[348]](#footnote-349) | 75 | 75 | 75 | 75 | 48.6 | 48.6 | 48.6 |
| Wind speed (mph)[[349]](#footnote-350) | 0 | 0 | 0 | 0 | 9.4 | 9.4 | 9.4 |
| **Pipe parameters** | | | | | | | |
| Pipe material | Copper | Steel | Steel | Copper | Copper | Steel | Steel |
| Pipe size for Heat Loss Calc | 2” | 2” | 2” | 2” | 2” | 2” | 2” |
| Outer Diameter, Pipe, actual | 2.38” | 2.38” | 2.38” | 2.38” | 2.38” | 2.38” | 2.38” |
| Heat Loss, Bare Pipe (from 3EPlus) (Btu/hr.ft) | 114 (w/o reset)  78 (w/ reset heat)  58 (w/reset year) | 232 | 432 | 52 | 460 (w/o reset)  363 (w/ reset heat)  306 (w/reset year) | 710 | 1101 |
| **Insulation parameters** | | | | | | | |
| Outer diameter, insulation | 4.38” | 4.38” | 4.38” | 4.38” | 4.38” | 4.38” | 4.38” |
| Average Heat Loss, Insulation (from 3EPlus) (Btu/hr.ft) | 24 (w/o reset)  17 (w/ reset heat)  13 (w/reset year) | 40 | 70 | 13.25 | 21 (w/o reset)  16 (w/ reset heat)  13 (w/reset year) | 32 | 52 |
| **Annual Energy Savings** | | | | | | | |
| Boiler / Water Heater efficiency | 81.9% | 80.7% (64.8% for MF) | 80.7% | 67% | 81.9% | 80.7% (64.8% for MF) | 80.7% |
| Annual Gas Use, Base Case (therms/yr/ft) | 3.8 (w/o reset)  4.8 (w/ reset heat)  6.2 (w/reset year) | 7.9 (non recirc)  14.5 (recirc heat)  25.2 (recirc year) | 14.7 (non recirc)  27.0 (recirc heat)  46.9 (recirc year) | 6.76 | 15.4 (w/o reset)  22.5 (w/ reset heat)  32.7 (w/reset year) | 24.1 (non recirc)  44.3 (recirc heat)  77.0 (recirc year) | 37.5 (non recirc)  68.7 (recirc heat)  119.5 (recirc year) |
| Annual Gas Use, Measure case (therms/yr/ft) | 0.8 (w/o reset)  1.1 (w/ reset heat)  1.4 (w/reset year) | 1.4 (non recirc)  2.5 (recirc heat)  4.4 (recirc year) | 2.4 (non recirc)  4.4 (recirc heat)  7.6 (recirc year) | 1.73 | 0.7 (w/o reset)  1.0 (w/ reset heat)  1.4 (w/reset year) | 1.1 (non recirc)  2.0 (recirc heat)  3.4 (recirc year) | 1.8 (non recirc)  3.2 (recirc heat)  5.6 (recirc year) |
| Annual Gas Savings (therms/yr/ft) | 3.0 (w/o reset)  3.7 (w/ reset heat)  4.8 (w/reset year) | 6.5 (non recirc)  12.0 (recirc heat)  20.8 (recirc year) | 12.3 (non recirc)  22.6 (recirc heat)  39.3 (recirc year) | 5.0 | 14.7 (w/o reset)  21.4 (w/ reset heat)  31.3 (w/reset year) | 23.1 (non recirc)  42.3 (recirc heat)  73.6 (recirc year) | 35.7 (non recirc)  65.5 (recirc heat)  113.9 (recirc year) |

Heat = heating season only, year = year round

Values below must be multiplied by the appropriate Thermal Regain Factor (TRF). All variables were the same except for hours of operation in the calculation of the default savings per foot for the various building types and applications as presented in the table below:

Savings Summary for Indoor pipe insulation by System Type and Building Type (Δtherms per foot) (continues for 3.5 pages)

|  |  |  | **Annual therm Savings per linear foot (therm /ft)**  **(2" pipe / 1" insulation for hot water, 2" insulation for steam)** | | | | |
| --- | --- | --- | --- | --- | --- | --- | --- |
| **Location** | **System Type** | **Building Type** | **Zone 1 (Rockford)** | **Zone 2 (Chicago)** | **Zone 3 (Springfield)** | **Zone 4 (Belleville)** | **Zone 5**  **(Marion)** |
| Indoor | Hot Water Space Heating with outdoor reset – non-recirculation | Assembly | 1.32 | 1.36 | 1.21 | 0.81 | 1.24 |
| Assisted Living | 1.25 | 1.22 | 1.07 | 0.79 | 0.95 |
| College | 1.13 | 1.06 | 0.95 | 0.53 | 0.63 |
| Convenience Store | 1.10 | 1.01 | 0.90 | 0.65 | 0.72 |
| Elementary School | 1.32 | 1.29 | 1.13 | 0.78 | 0.95 |
| Garage | 0.73 | 0.72 | 0.63 | 0.50 | 0.56 |
| Grocery | 1.19 | 1.19 | 1.04 | 0.65 | 0.78 |
| Healthcare Clinic | 1.17 | 1.20 | 1.05 | 0.71 | 0.75 |
| High School | 1.37 | 1.38 | 1.23 | 0.88 | 1.03 |
| Hospital - CAV no econ | 1.31 | 1.35 | 1.15 | 0.99 | 1.12 |
| Hospital - CAV econ | 1.33 | 1.37 | 1.17 | 1.01 | 1.15 |
| Hospital - VAV econ | 0.54 | 0.51 | 0.39 | 0.23 | 0.25 |
| Hospital - FCU | 0.98 | 1.12 | 0.91 | 1.07 | 1.44 |
| Hotel/Motel | 1.31 | 1.27 | 1.14 | 0.78 | 0.96 |
| Hotel/Motel - Common | 1.19 | 1.21 | 1.15 | 0.93 | 0.98 |
| Hotel/Motel - Guest | 1.30 | 1.26 | 1.13 | 0.75 | 0.93 |
| Manufacturing Facility | 0.78 | 0.75 | 0.70 | 0.42 | 0.47 |
| MF - High Rise | 1.13 | 1.12 | 1.02 | 0.87 | 0.87 |
| MF - High Rise - Common | 1.35 | 1.31 | 1.17 | 0.81 | 1.04 |
| MF - High Rise - Residential | 1.09 | 1.08 | 0.99 | 0.85 | 0.83 |
| MF - Mid Rise | 1.23 | 1.25 | 1.07 | 0.79 | 0.90 |
| Movie Theater | 1.35 | 1.33 | 1.24 | 0.94 | 1.12 |
| Office - High Rise - CAV no econ | 1.50 | 1.52 | 1.38 | 0.93 | 1.01 |
| Office - High Rise - CAV econ | 1.55 | 1.58 | 1.45 | 1.00 | 1.10 |
| Office - High Rise - VAV econ | 1.13 | 1.15 | 0.95 | 0.56 | 0.63 |
| Office - High Rise - FCU | 0.83 | 0.82 | 0.71 | 0.37 | 0.39 |
| Office - Low Rise | 1.06 | 1.06 | 0.84 | 0.51 | 0.59 |
| Office - Mid Rise | 1.17 | 1.18 | 0.99 | 0.63 | 0.70 |
| Religious Building | 1.19 | 1.11 | 1.07 | 0.78 | 0.89 |
| Restaurant | 1.00 | 1.00 | 0.90 | 0.68 | 0.81 |
| Retail - Department Store | 1.03 | 0.95 | 0.89 | 0.58 | 0.66 |
| Retail - Strip Mall | 0.99 | 0.91 | 0.81 | 0.56 | 0.60 |
| Warehouse | 1.08 | 1.01 | 1.04 | 0.65 | 0.80 |
| Unknown | 1.15 | 1.14 | 1.01 | 0.73 | 0.84 |
| Hot Water Space Heating without outdoor reset – non-recirculation | Assembly | 1.96 | 2.00 | 1.79 | 1.19 | 1.83 |
| Assisted Living | 1.84 | 1.80 | 1.58 | 1.16 | 1.40 |
| College | 1.67 | 1.56 | 1.40 | 0.78 | 0.93 |
| Convenience Store | 1.62 | 1.50 | 1.33 | 0.95 | 1.06 |
| Elementary School | 1.95 | 1.90 | 1.68 | 1.16 | 1.40 |
| Garage | 1.08 | 1.06 | 0.93 | 0.74 | 0.82 |
| Grocery | 1.76 | 1.75 | 1.54 | 0.96 | 1.15 |
| Healthcare Clinic | 1.73 | 1.77 | 1.55 | 1.05 | 1.11 |
| High School | 2.02 | 2.03 | 1.82 | 1.30 | 1.52 |
| Hospital - CAV no econ | 1.93 | 1.99 | 1.69 | 1.46 | 1.65 |
| Hospital - CAV econ | 1.96 | 2.03 | 1.73 | 1.50 | 1.70 |
| Hospital - VAV econ | 0.80 | 0.76 | 0.57 | 0.34 | 0.37 |
| Hospital - FCU | 1.45 | 1.65 | 1.35 | 1.58 | 2.13 |
| Hotel/Motel | 1.93 | 1.87 | 1.69 | 1.16 | 1.41 |
| Hotel/Motel - Common | 1.75 | 1.78 | 1.69 | 1.38 | 1.45 |
| Hotel/Motel - Guest | 1.92 | 1.86 | 1.66 | 1.11 | 1.37 |
| Manufacturing Facility | 1.15 | 1.11 | 1.03 | 0.62 | 0.69 |
| MF - High Rise | 1.67 | 1.65 | 1.50 | 1.28 | 1.28 |
| MF - High Rise - Common | 1.99 | 1.93 | 1.73 | 1.19 | 1.54 |
| MF - High Rise - Residential | 1.61 | 1.60 | 1.46 | 1.26 | 1.23 |
| MF - Mid Rise | 1.82 | 1.84 | 1.59 | 1.17 | 1.33 |
| Movie Theater | 1.99 | 1.96 | 1.83 | 1.39 | 1.66 |
| Office - High Rise - CAV no econ | 2.21 | 2.24 | 2.04 | 1.37 | 1.49 |
| Office - High Rise - CAV econ | 2.29 | 2.33 | 2.14 | 1.48 | 1.63 |
| Office - High Rise - VAV econ | 1.67 | 1.70 | 1.40 | 0.83 | 0.93 |
| Office - High Rise - FCU | 1.22 | 1.21 | 1.04 | 0.55 | 0.58 |
| Office - Low Rise | 1.56 | 1.56 | 1.24 | 0.76 | 0.87 |
| Office - Mid Rise | 1.73 | 1.74 | 1.47 | 0.94 | 1.04 |
| Religious Building | 1.75 | 1.65 | 1.58 | 1.15 | 1.32 |
| Restaurant | 1.48 | 1.48 | 1.33 | 1.01 | 1.19 |
| Retail - Department Store | 1.52 | 1.40 | 1.31 | 0.85 | 0.97 |
| Retail - Strip Mall | 1.46 | 1.35 | 1.19 | 0.82 | 0.89 |
| Warehouse | 1.59 | 1.49 | 1.53 | 0.96 | 1.18 |
| Unknown | 1.70 | 1.68 | 1.50 | 1.07 | 1.25 |
| Hot Water with outdoor reset | All buildings, Recirculation heating season only (Hours below 55F) | 3.73 | 3.68 | 3.33 | 2.98 | 3.08 |
| Hot Water w/o outdoor reset | All buildings, Recirculation heating season only (Hours below 55F) | 5.51 | 5.43 | 4.92 | 4.40 | 4.54 |
| Hot Water with outdoor reset | All buildings, Recirculation year round (All hours) | 4.79 | 4.79 | 4.79 | 4.79 | 4.79 |
| Hot Water w/o outdoor reset | All buildings, Recirculation year round (All hours) | 9.58 | 9.58 | 9.58 | 9.58 | 9.58 |
| Domestic Hot Water | DHW circulation loop | 5.02 | 5.02 | 5.02 | 5.02 | 5.02 |
| LP Steam – non-recirculation | Assembly | 4.25 | 4.36 | 3.89 | 2.59 | 3.97 |
| Assisted Living | 4.01 | 3.92 | 3.44 | 2.53 | 3.04 |
| College | 3.64 | 3.40 | 3.04 | 1.69 | 2.02 |
| Convenience Store | 3.52 | 3.26 | 2.89 | 2.07 | 2.32 |
| Elementary School | 4.24 | 4.13 | 3.64 | 2.52 | 3.05 |
| Garage | 2.34 | 2.31 | 2.03 | 1.62 | 1.79 |
| Grocery | 3.83 | 3.81 | 3.34 | 2.08 | 2.49 |
| Healthcare Clinic | 3.76 | 3.85 | 3.36 | 2.29 | 2.42 |
| High School | 4.39 | 4.42 | 3.96 | 2.82 | 3.30 |
| Hospital - CAV no econ | 4.20 | 4.33 | 3.69 | 3.17 | 3.60 |
| Hospital - CAV econ | 4.25 | 4.41 | 3.76 | 3.26 | 3.70 |
| Hospital - VAV econ | 1.74 | 1.65 | 1.24 | 0.75 | 0.81 |
| Hospital - FCU | 3.15 | 3.60 | 2.93 | 3.44 | 4.63 |
| Hotel/Motel | 4.19 | 4.07 | 3.67 | 2.51 | 3.07 |
| Hotel/Motel - Common | 3.81 | 3.87 | 3.68 | 3.00 | 3.15 |
| Hotel/Motel - Guest | 4.18 | 4.05 | 3.62 | 2.42 | 2.98 |
| Manufacturing Facility | 2.49 | 2.41 | 2.23 | 1.35 | 1.51 |
| MF - High Rise | 4.52 | 4.46 | 4.07 | 3.46 | 3.47 |
| MF - High Rise - Common | 5.38 | 5.22 | 4.68 | 3.23 | 4.17 |
| MF - High Rise - Residential | 4.37 | 4.34 | 3.94 | 3.41 | 3.33 |
| MF - Mid Rise | 4.94 | 4.99 | 4.30 | 3.16 | 3.60 |
| Movie Theater | 4.33 | 4.26 | 3.98 | 3.03 | 3.61 |
| Office - High Rise - CAV no econ | 4.81 | 4.88 | 4.45 | 2.98 | 3.24 |
| Office - High Rise - CAV econ | 4.97 | 5.07 | 4.66 | 3.21 | 3.54 |
| Office - High Rise - VAV econ | 3.64 | 3.71 | 3.06 | 1.81 | 2.01 |
| Office - High Rise - FCU | 2.66 | 2.62 | 2.27 | 1.20 | 1.26 |
| Office - Low Rise | 3.40 | 3.39 | 2.69 | 1.65 | 1.89 |
| Office - Mid Rise | 3.77 | 3.78 | 3.19 | 2.03 | 2.26 |
| Religious Building | 3.82 | 3.58 | 3.43 | 2.51 | 2.87 |
| Restaurant | 3.21 | 3.22 | 2.89 | 2.19 | 2.60 |
| Retail - Department Store | 3.31 | 3.04 | 2.86 | 1.86 | 2.12 |
| Retail - Strip Mall | 3.17 | 2.94 | 2.59 | 1.79 | 1.93 |
| Warehouse | 3.46 | 3.23 | 3.33 | 2.08 | 2.56 |
| Unknown | 3.70 | 3.66 | 3.26 | 2.34 | 2.71 |
| LP Steam | All buildings, Recirculation heating season only (Hours below 55F) | 11.99 | 11.81 | 10.70 | 9.57 | 9.88 |
| LP Steam | All buildings, Recirculation year round (All hours) | 20.84 | 20.84 | 20.84 | 20.84 | 20.84 |
| HP Steam – non-recirculation | Assembly | 8.02 | 8.22 | 7.34 | 4.89 | 7.49 |
| Assisted Living | 7.56 | 7.39 | 6.49 | 4.77 | 5.73 |
| College | 6.87 | 6.42 | 5.73 | 3.18 | 3.81 |
| Convenience Store | 6.65 | 6.14 | 5.45 | 3.91 | 4.37 |
| Elementary School | 8.00 | 7.79 | 6.87 | 4.75 | 5.76 |
| Garage | 4.42 | 4.35 | 3.82 | 3.05 | 3.38 |
| Grocery | 7.22 | 7.19 | 6.30 | 3.93 | 4.70 |
| Healthcare Clinic | 7.09 | 7.27 | 6.35 | 4.32 | 4.57 |
| High School | 8.28 | 8.34 | 7.48 | 5.33 | 6.23 |
| Hospital - CAV no econ | 7.92 | 8.16 | 6.95 | 5.98 | 6.79 |
| Hospital - CAV econ | 8.03 | 8.32 | 7.09 | 6.14 | 6.98 |
| Hospital - VAV econ | 3.28 | 3.12 | 2.35 | 1.41 | 1.53 |
| Hospital - FCU | 5.95 | 6.79 | 5.53 | 6.50 | 8.73 |
| Hotel/Motel | 7.91 | 7.69 | 6.93 | 4.74 | 5.79 |
| Hotel/Motel - Common | 7.18 | 7.30 | 6.95 | 5.65 | 5.94 |
| Hotel/Motel - Guest | 7.89 | 7.64 | 6.83 | 4.57 | 5.62 |
| Manufacturing Facility | 4.70 | 4.55 | 4.22 | 2.55 | 2.84 |
| MF - High Rise | 6.85 | 6.76 | 6.16 | 5.25 | 5.26 |
| MF - High Rise - Common | 8.15 | 7.91 | 7.09 | 4.89 | 6.31 |
| MF - High Rise - Residential | 6.62 | 6.57 | 5.97 | 5.17 | 5.04 |
| MF - Mid Rise | 7.48 | 7.57 | 6.51 | 4.79 | 5.46 |
| Movie Theater | 8.16 | 8.04 | 7.52 | 5.71 | 6.80 |
| Office - High Rise - CAV no econ | 9.07 | 9.20 | 8.39 | 5.62 | 6.12 |
| Office - High Rise - CAV econ | 9.38 | 9.57 | 8.80 | 6.06 | 6.67 |
| Office - High Rise - VAV econ | 6.86 | 6.99 | 5.76 | 3.41 | 3.80 |
| Office - High Rise - FCU | 5.02 | 4.95 | 4.27 | 2.27 | 2.38 |
| Office - Low Rise | 6.41 | 6.40 | 5.08 | 3.11 | 3.56 |
| Office - Mid Rise | 7.12 | 7.12 | 6.03 | 3.84 | 4.27 |
| Religious Building | 7.20 | 6.75 | 6.46 | 4.73 | 5.41 |
| Restaurant | 6.06 | 6.08 | 5.46 | 4.13 | 4.90 |
| Retail - Department Store | 6.25 | 5.74 | 5.39 | 3.51 | 4.00 |
| Retail - Strip Mall | 5.98 | 5.54 | 4.89 | 3.37 | 3.63 |
| Warehouse | 6.53 | 6.09 | 6.29 | 3.93 | 4.84 |
| Unknown | 6.97 | 6.91 | 6.14 | 4.41 | 5.11 |
| HP Steam | All buildings, Recirculation heating season only (Hours below 55F) | 22.62 | 22.28 | 20.18 | 18.05 | 18.63 |
| HP Steam | All buildings, Recirculation year round (All hours) | 39.32 | 39.32 | 39.32 | 39.32 | 39.32 |

Savings Summary for Outdoor pipe insulation by System Type and Building Type (Δtherms per foot) (continues for 3.5 pages)

|  |  |  | **Annual therm Savings per linear foot (therm /ft)**  **(2" pipe / 1" insulation for hot water, 2" insulation for steam)** | | | | |
| --- | --- | --- | --- | --- | --- | --- | --- |
| **Location** | **System Type** | **Building Type** | **Zone 1 (Rockford)** | **Zone 2 (Chicago)** | **Zone 3 (Springfield)** | **Zone 4 (Belleville)** | **Zone 5**  **(Marion)** |
| Outdoor | Hot Water Space Heating with outdoor reset – non-recirculation | Assembly | 7.58 | 7.77 | 6.94 | 4.62 | 7.08 |
| Assisted Living | 7.14 | 6.98 | 6.13 | 4.51 | 5.42 |
| College | 6.49 | 6.07 | 5.41 | 3.01 | 3.60 |
| Convenience Store | 6.28 | 5.80 | 5.15 | 3.70 | 4.13 |
| Elementary School | 7.56 | 7.36 | 6.50 | 4.49 | 5.44 |
| Garage | 4.18 | 4.11 | 3.61 | 2.88 | 3.19 |
| Grocery | 6.82 | 6.80 | 5.96 | 3.72 | 4.44 |
| Healthcare Clinic | 6.70 | 6.87 | 6.00 | 4.09 | 4.32 |
| High School | 7.83 | 7.88 | 7.07 | 5.03 | 5.89 |
| Hospital - CAV no econ | 7.49 | 7.71 | 6.57 | 5.65 | 6.41 |
| Hospital - CAV econ | 7.59 | 7.86 | 6.70 | 5.81 | 6.60 |
| Hospital - VAV econ | 3.10 | 2.95 | 2.22 | 1.33 | 1.44 |
| Hospital - FCU | 5.62 | 6.42 | 5.23 | 6.14 | 8.26 |
| Hotel/Motel | 7.47 | 7.26 | 6.55 | 4.48 | 5.47 |
| Hotel/Motel - Common | 6.79 | 6.90 | 6.57 | 5.34 | 5.61 |
| Hotel/Motel - Guest | 7.46 | 7.22 | 6.45 | 4.32 | 5.31 |
| Manufacturing Facility | 4.45 | 4.30 | 3.98 | 2.41 | 2.69 |
| MF - High Rise | 6.48 | 6.39 | 5.83 | 4.96 | 4.97 |
| MF - High Rise - Common | 7.70 | 7.48 | 6.70 | 4.62 | 5.96 |
| MF - High Rise - Residential | 6.26 | 6.21 | 5.64 | 4.89 | 4.77 |
| MF - Mid Rise | 7.07 | 7.15 | 6.15 | 4.53 | 5.16 |
| Movie Theater | 7.71 | 7.60 | 7.10 | 5.40 | 6.43 |
| Office - High Rise - CAV no econ | 8.57 | 8.70 | 7.93 | 5.31 | 5.78 |
| Office - High Rise - CAV econ | 8.86 | 9.04 | 8.32 | 5.73 | 6.31 |
| Office - High Rise - VAV econ | 6.48 | 6.61 | 5.45 | 3.22 | 3.59 |
| Office - High Rise - FCU | 4.75 | 4.67 | 4.04 | 2.14 | 2.25 |
| Office - Low Rise | 6.06 | 6.05 | 4.80 | 2.94 | 3.36 |
| Office - Mid Rise | 6.73 | 6.73 | 5.70 | 3.63 | 4.03 |
| Religious Building | 6.80 | 6.38 | 6.11 | 4.47 | 5.11 |
| Restaurant | 5.73 | 5.75 | 5.16 | 3.90 | 4.63 |
| Retail - Department Store | 5.91 | 5.42 | 5.09 | 3.31 | 3.78 |
| Retail - Strip Mall | 5.65 | 5.23 | 4.62 | 3.19 | 3.44 |
| Warehouse | 6.18 | 5.76 | 5.94 | 3.71 | 4.57 |
| Unknown | 6.59 | 6.53 | 5.81 | 4.17 | 4.83 |
| Hot Water Space Heating without outdoor reset – non-recirculation | Assembly | 9.59 | 9.83 | 8.77 | 5.85 | 8.96 |
| Assisted Living | 9.04 | 8.83 | 7.76 | 5.70 | 6.86 |
| College | 8.21 | 7.68 | 6.85 | 3.80 | 4.56 |
| Convenience Store | 7.95 | 7.34 | 6.52 | 4.68 | 5.22 |
| Elementary School | 9.56 | 9.32 | 8.22 | 5.68 | 6.89 |
| Garage | 5.28 | 5.20 | 4.57 | 3.65 | 4.04 |
| Grocery | 8.63 | 8.60 | 7.54 | 4.70 | 5.62 |
| Healthcare Clinic | 8.47 | 8.70 | 7.59 | 5.17 | 5.47 |
| High School | 9.90 | 9.97 | 8.94 | 6.37 | 7.45 |
| Hospital - CAV no econ | 9.47 | 9.76 | 8.31 | 7.15 | 8.11 |
| Hospital - CAV econ | 9.60 | 9.95 | 8.48 | 7.35 | 8.34 |
| Hospital - VAV econ | 3.93 | 3.73 | 2.80 | 1.68 | 1.82 |
| Hospital - FCU | 7.11 | 8.12 | 6.61 | 7.77 | 10.45 |
| Hotel/Motel | 9.45 | 9.19 | 8.29 | 5.67 | 6.92 |
| Hotel/Motel - Common | 8.59 | 8.73 | 8.31 | 6.76 | 7.10 |
| Hotel/Motel - Guest | 9.44 | 9.13 | 8.16 | 5.47 | 6.72 |
| Manufacturing Facility | 5.63 | 5.44 | 5.04 | 3.05 | 3.40 |
| MF - High Rise | 8.19 | 8.08 | 7.37 | 6.27 | 6.29 |
| MF - High Rise - Common | 9.74 | 9.46 | 8.48 | 5.85 | 7.54 |
| MF - High Rise - Residential | 7.92 | 7.86 | 7.14 | 6.18 | 6.03 |
| MF - Mid Rise | 8.94 | 9.05 | 7.78 | 5.73 | 6.53 |
| Movie Theater | 9.76 | 9.61 | 8.99 | 6.83 | 8.14 |
| Office - High Rise - CAV no econ | 10.84 | 11.01 | 10.03 | 6.72 | 7.32 |
| Office - High Rise - CAV econ | 11.21 | 11.44 | 10.52 | 7.25 | 7.98 |
| Office - High Rise - VAV econ | 8.20 | 8.36 | 6.89 | 4.07 | 4.54 |
| Office - High Rise - FCU | 6.00 | 5.91 | 5.11 | 2.71 | 2.84 |
| Office - Low Rise | 7.67 | 7.65 | 6.08 | 3.72 | 4.25 |
| Office - Mid Rise | 8.51 | 8.52 | 7.21 | 4.59 | 5.10 |
| Religious Building | 8.61 | 8.07 | 7.73 | 5.66 | 6.47 |
| Restaurant | 7.25 | 7.27 | 6.53 | 4.94 | 5.85 |
| Retail - Department Store | 7.47 | 6.86 | 6.44 | 4.19 | 4.78 |
| Retail - Strip Mall | 7.15 | 6.62 | 5.85 | 4.03 | 4.35 |
| Warehouse | 7.81 | 7.29 | 7.52 | 4.69 | 5.78 |
| Unknown | 8.34 | 8.26 | 7.35 | 5.27 | 6.11 |
| Hot Water with outdoor reset | All buildings, Recirculation heating season only (Hours below 55F) | 21.38 | 21.06 | 19.07 | 17.06 | 17.61 |
| Hot Water without outdoor reset | All buildings, Recirculation heating season only (Hours below 55F) | 27.05 | 26.64 | 24.13 | 21.58 | 22.28 |
| Hot Water with outdoor reset | All buildings, Recirculation year round (All hours) | 31.30 | 31.30 | 31.30 | 31.30 | 31.30 |
| Hot Water without outdoor reset | All buildings, Recirculation year round (All hours) | 47.02 | 47.02 | 47.02 | 47.02 | 47.02 |
| LP Steam – non-recirculation | Assembly | 15.01 | 15.38 | 13.73 | 9.15 | 14.02 |
| Assisted Living | 14.14 | 13.82 | 12.15 | 8.93 | 10.73 |
| College | 12.85 | 12.01 | 10.72 | 5.95 | 7.13 |
| Convenience Store | 12.44 | 11.49 | 10.20 | 7.32 | 8.17 |
| Elementary School | 14.96 | 14.58 | 12.86 | 8.88 | 10.78 |
| Garage | 8.27 | 8.14 | 7.15 | 5.71 | 6.32 |
| Grocery | 13.51 | 13.46 | 11.80 | 7.36 | 8.79 |
| Healthcare Clinic | 13.26 | 13.61 | 11.88 | 8.09 | 8.56 |
| High School | 15.50 | 15.60 | 13.99 | 9.97 | 11.66 |
| Hospital - CAV no econ | 14.82 | 15.27 | 13.01 | 11.19 | 12.70 |
| Hospital - CAV econ | 15.02 | 15.57 | 13.27 | 11.50 | 13.06 |
| Hospital - VAV econ | 6.14 | 5.84 | 4.39 | 2.64 | 2.85 |
| Hospital - FCU | 11.13 | 12.71 | 10.35 | 12.16 | 16.35 |
| Hotel/Motel | 14.80 | 14.38 | 12.97 | 8.87 | 10.84 |
| Hotel/Motel - Common | 13.45 | 13.66 | 13.00 | 10.58 | 11.12 |
| Hotel/Motel - Guest | 14.77 | 14.29 | 12.78 | 8.56 | 10.52 |
| Manufacturing Facility | 8.80 | 8.51 | 7.89 | 4.77 | 5.32 |
| MF - High Rise | 15.97 | 15.76 | 14.37 | 12.23 | 12.26 |
| MF - High Rise - Common | 18.99 | 18.44 | 16.53 | 11.39 | 14.71 |
| MF - High Rise - Residential | 15.43 | 15.31 | 13.92 | 12.05 | 11.75 |
| MF - Mid Rise | 17.43 | 17.63 | 15.17 | 11.16 | 12.72 |
| Movie Theater | 15.27 | 15.05 | 14.07 | 10.69 | 12.73 |
| Office - High Rise - CAV no econ | 16.97 | 17.22 | 15.70 | 10.51 | 11.45 |
| Office - High Rise - CAV econ | 17.55 | 17.91 | 16.47 | 11.35 | 12.49 |
| Office - High Rise - VAV econ | 12.83 | 13.09 | 10.79 | 6.37 | 7.11 |
| Office - High Rise - FCU | 9.40 | 9.26 | 8.00 | 4.25 | 4.45 |
| Office - Low Rise | 12.00 | 11.97 | 9.51 | 5.82 | 6.66 |
| Office - Mid Rise | 13.32 | 13.33 | 11.28 | 7.18 | 7.98 |
| Religious Building | 13.47 | 12.64 | 12.10 | 8.86 | 10.13 |
| Restaurant | 11.34 | 11.38 | 10.21 | 7.73 | 9.16 |
| Retail - Department Store | 11.69 | 10.74 | 10.08 | 6.56 | 7.48 |
| Retail - Strip Mall | 11.19 | 10.36 | 9.15 | 6.31 | 6.80 |
| Warehouse | 12.23 | 11.40 | 11.77 | 7.35 | 9.05 |
| Unknown | 13.05 | 12.93 | 11.50 | 8.25 | 9.57 |
| LP Steam | All buildings, Recirculation heating season only (Hours below 55F) | 42.33 | 41.69 | 37.76 | 33.78 | 34.86 |
| LP Steam | All buildings, Recirculation year round (All hours) | 73.59 | 73.59 | 73.59 | 73.59 | 73.59 |
| HP Steam – non-recirculation | Assembly | 23.24 | 23.81 | 21.26 | 14.16 | 21.70 |
| Assisted Living | 21.89 | 21.40 | 18.80 | 13.82 | 16.61 |
| College | 19.90 | 18.60 | 16.60 | 9.22 | 11.04 |
| Convenience Store | 19.26 | 17.79 | 15.79 | 11.33 | 12.65 |
| Elementary School | 23.16 | 22.57 | 19.91 | 13.75 | 16.69 |
| Garage | 12.80 | 12.60 | 11.08 | 8.84 | 9.78 |
| Grocery | 20.91 | 20.83 | 18.26 | 11.39 | 13.61 |
| Healthcare Clinic | 20.53 | 21.07 | 18.39 | 12.53 | 13.25 |
| High School | 23.99 | 24.15 | 21.66 | 15.43 | 18.05 |
| Hospital - CAV no econ | 22.94 | 23.64 | 20.14 | 17.32 | 19.66 |
| Hospital - CAV econ | 23.25 | 24.10 | 20.54 | 17.80 | 20.22 |
| Hospital - VAV econ | 9.51 | 9.03 | 6.79 | 4.08 | 4.42 |
| Hospital - FCU | 17.24 | 19.67 | 16.02 | 18.82 | 25.31 |
| Hotel/Motel | 22.90 | 22.27 | 20.08 | 13.74 | 16.77 |
| Hotel/Motel - Common | 20.81 | 21.15 | 20.13 | 16.38 | 17.21 |
| Hotel/Motel - Guest | 22.87 | 22.13 | 19.78 | 13.24 | 16.28 |
| Manufacturing Facility | 13.63 | 13.18 | 12.21 | 7.38 | 8.24 |
| MF - High Rise | 19.85 | 19.59 | 17.86 | 15.20 | 15.24 |
| MF - High Rise - Common | 23.60 | 22.92 | 20.55 | 14.16 | 18.28 |
| MF - High Rise - Residential | 19.18 | 19.03 | 17.30 | 14.98 | 14.61 |
| MF - Mid Rise | 21.67 | 21.92 | 18.86 | 13.87 | 15.81 |
| Movie Theater | 23.64 | 23.29 | 21.78 | 16.55 | 19.71 |
| Office - High Rise - CAV no econ | 26.27 | 26.66 | 24.30 | 16.28 | 17.73 |
| Office - High Rise - CAV econ | 27.16 | 27.72 | 25.49 | 17.57 | 19.33 |
| Office - High Rise - VAV econ | 19.87 | 20.26 | 16.70 | 9.87 | 11.00 |
| Office - High Rise - FCU | 14.54 | 14.33 | 12.38 | 6.57 | 6.89 |
| Office - Low Rise | 18.58 | 18.53 | 14.72 | 9.00 | 10.31 |
| Office - Mid Rise | 20.61 | 20.64 | 17.46 | 11.12 | 12.36 |
| Religious Building | 20.85 | 19.56 | 18.72 | 13.71 | 15.67 |
| Restaurant | 17.55 | 17.61 | 15.81 | 11.96 | 14.18 |
| Retail - Department Store | 18.10 | 16.63 | 15.61 | 10.16 | 11.58 |
| Retail - Strip Mall | 17.32 | 16.04 | 14.17 | 9.77 | 10.53 |
| Warehouse | 18.93 | 17.65 | 18.21 | 11.37 | 14.02 |
| Unknown | 20.20 | 20.01 | 17.80 | 12.77 | 14.81 |
| HP Steam | All buildings, Recirculation heating season only (Hours below 55F) | 65.53 | 64.54 | 58.45 | 52.29 | 53.97 |
| HP Steam | All buildings, Recirculation year round (All hours) | 113.92 | 113.92 | 113.92 | 113.92 | 113.92 |

For insulation covering elbows and tees that connect straight pipe, a calculated surface area will be assumed based on the dimensions for fittings given by ANSI/ASME B36.19. The surface area is then converted to an equivalent length of pipe that must be added to the total length of straight pipe in order to calculate total savings. Equivalent pipe lengths are given in 1” increments in pipe diameter for simplicity. In the case of pipe diameters in between full inch diameters, the closest equivalent length should be used. The larger pipe sizes mostly apply to steam header piping, which has the most heat loss per foot.

**Calculated Surface Areas of Elbows and Tees**

|  |  |  |
| --- | --- | --- |
| **Nominal Pipe Diameter** | **Calculated Surface Area (ft)** | |
| **90 Degree Elbow[[350]](#footnote-351)** | **Straight Tee[[351]](#footnote-352)** |
| 1” | 0.10 | 0.13 |
| 2” | 0.41 | 0.39 |
| 3” | 0.93 | 0.77 |
| 4” | 1.64 | 1.21 |
| 5” | 2.57 | 1.77 |
| 6” | 3.70 | 2.44 |
| 8” | 6.58 | 3.95 |
| 10” | 10.28 | 5.98 |
| 12” | 14.80 | 8.34 |

**Equivalent Length of Other Components – Elbows and Tees (Loc)**

|  |  |  |
| --- | --- | --- |
| **Nominal Pipe Diameter** | **Equivalent Length of Other Components (ft)** | |
| **90 Degree Elbow** | **Straight Tee** |
| 1” | 0.30 | 0.38 |
| 2” | 0.66 | 0.63 |
| 3” | 1.01 | 0.84 |
| 4” | 1.40 | 1.03 |
| 5” | 1.76 | 1.22 |
| 6” | 2.13 | 1.41 |
| 8” | 2.91 | 1.75 |
| 10” | 3.65 | 2.13 |
| 12” | 4.44 | 2.50 |

For insulation around valves or flanges, a surface area from ASTM standard C1129-12 will be assumed for 2” pipes. For 1” pipes, which weren’t included in the standard, a linear-trended value will be used. The surface area is then converted to an equivalent length of either 1” or 2” straight pipe that must be added to the total length of straight pipe in order to calculate total savings.

**Calculated Surface Areas of Flanges and Valves**

| **Valves** | | | | |  | **Flanges** | | | | |
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| **Class (psi)** | **150** | **300** | **600** | **900** |  | **Class (psi)** | **150** | **300** | **600** | **900** |
| **NPS (in)** | **ft2** | **ft2** | **ft2** | **ft2** |  | **NPS (in)** | **ft2** | **ft2** | **ft2** | **ft2** |
| 1 | 0.69 | 1.8 | 1.8 | 2.4 |  | 1 | 0.36 | 0.36 | 0.4 | 1.23 |
| 2 | 2.21 | 2.94 | 2.94 | 5.2 |  | 2 | 0.71 | 0.84 | 0.88 | 1.54 |
| 2.5 | 2.97 | 3.51 | 3.91 | 6.6 |  |  |  |  |  |  |
| 3 | 3.37 | 4.39 | 4.69 | 6.5 |  | 3 | 1.06 | 1.32 | 1.36 | 1.85 |
| 4 | 4.68 | 6.06 | 7.64 | 9.37 |  | 4 | 1.44 | 1.83 | 2.23 | 2.64 |
| 6 | 7.03 | 9.71 | 13.03 | 15.8 |  | 6 | 2.04 | 2.72 | 3.6 | 4.37 |
| 8 | 10.3 | 13.5 | 18.4 | 23.8 |  | 8 | 2.92 | 3.74 | 4.89 | 6.4 |
| 10 | 13.8 | 18 | 26.5 | 32.1 |  | 10 | 3.68 | 4.8 | 6.93 | 8.47 |
| 12 | 16.1 | 24.1 | 31.9 | 41.9 |  | 12 | 5.01 | 6.34 | 7.97 | 10.43 |

**Equivalent Length of Other Components - Flanges and Valves (Loc)**

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
| **ANSI Class (psi)** | **Equivalent Length of Other Components (ft)** | | | |
| **1” Valve** | **1” Flange** | **2” Valve** | **2” Flange** |
| 150 | 3.56 | 1.05 | 3.56 | 1.14 |
| 300 | 4.73 | 1.05 | 4.73 | 1.35 |
| 600 | 4.73 | 1.16 | 4.73 | 1.42 |
| 900 | 8.37 | 3.57 | 8.37 | 2.48 |

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-HVC-PINS-V03-150601

### Single-Package and Split System Unitary Air Conditioners

###### Description

This measure promotes the installation of high-efficiency unitary air-, water-, and evaporatively cooled air conditioning equipment, both single-package and split systems. Air conditioning (AC) systems are a major consumer of electricity and systems that exceed baseline efficiencies can save considerable amounts of energy. This measure could apply to the replacing of an existing unit at the end of its useful life or the installation of a new unit in a new or existing building.

This measure was developed to be applicable to the following program types: TOS, NC. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the efficient equipment is assumed to be a high-efficiency air-, water-, or evaporatively cooled air conditioner that exceeds the energy efficiency requirements of the International Energy Conservation Code (IECC) 2012

###### Definition of Baseline Equipment

In order for this characterization to apply, the baseline equipment is assumed to be a standard-efficiency air-, water, or evaporatively cooled air conditioner that meets the energy efficiency requirements of the International Energy Conservation Code (IECC) 2012,. The rating conditions for the baseline and efficient equipment efficiencies must be equivalent.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 15 years.[[352]](#footnote-353)

###### Deemed Measure Cost

The incremental capital cost for this measure is assumed to be $100 per ton.[[353]](#footnote-354)

###### Loadshape

Loadshape C03 - Commercial Cooling

###### Coincidence Factor

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.  Both values provided are based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren.

CFSSP = Summer System Peak Coincidence Factor for Commercial cooling (during system peak hour)

= 91.3% [[354]](#footnote-355)

CFPJM = PJM Summer Peak Coincidence Factor for Commercial cooling (average during peak period)

= 47.8%[[355]](#footnote-356)

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

For units with cooling capacities less than 65 kBtu/hr:

ΔkWH = (kBtu/hr) \* [(1/SEERbase) – (1/SEERee)] \* EFLH

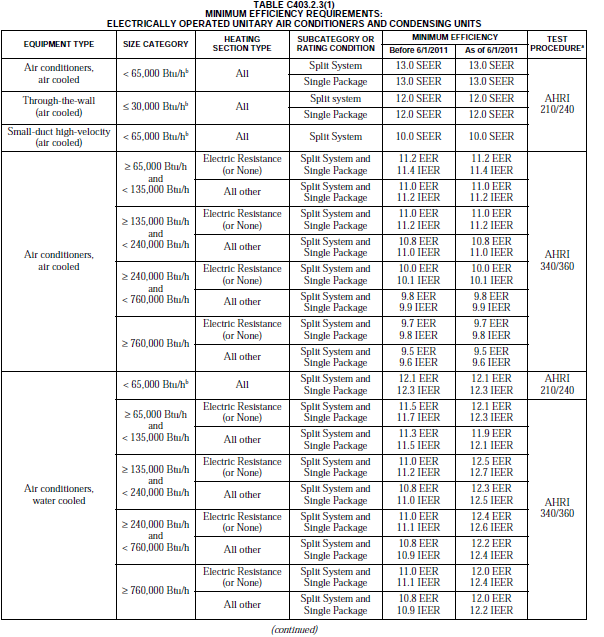
For units with cooling capacities equal to or greater than 65 kBtu/hr:

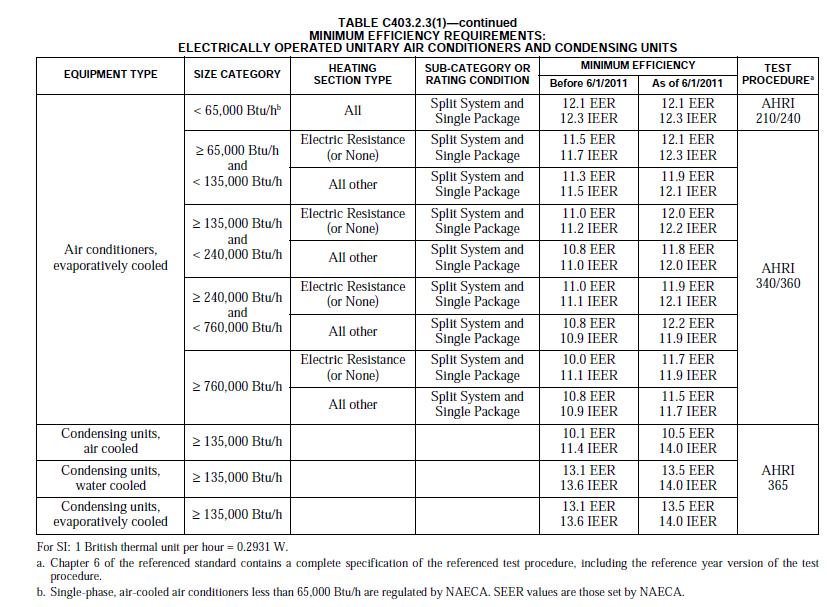
ΔkWH = (kBtu/hr) \* [(1/EERbase) – (1/EERee)] \* EFLH

Where:

kBtu/hr = capacity of the cooling equipment actually installed in kBtu per hour (1 ton of cooling capacity equals 12 kBtu/hr).

SEERbase = Seasonal Energy Efficiency Ratio of the baseline equipment; see table below for default values[[356]](#footnote-357)::





SEERee = Seasonal Energy Efficiency Ratio of the energy efficient equipment (actually installed).

EERbase = Energy Efficiency Ratio of the baseline equipment; see table above for default values. Since IECC 2012 does not provide EER requirements for air-cooled air conditioners < 65 kBtu/hr, assume the following conversion from SEER to EER: EER≈SEER/1.1

EERee = Energy Efficiency Ratio of the energy efficient equipment. For air-cooled air conditioners < 65 kBtu/hr, if the actual EERee is unknown, assume the following conversion from SEER to EER: EER≈SEER/1.1.

= Actual installed

EFLH = Equivalent Full Load Hours for cooling are provided in section 4.4 HVAC End Use:

For example a 5 ton air cooled split system with a SEER of 15 at a retail strip mall in Rockford would save

ΔkWH = (60) \* [(1/13) – (1/15)] \* 950

= 585 kWh

###### Summer Coincident Peak Demand Savings

ΔkWSSP = (kBtu/hr \* (1/EERbase - 1/EERee)) \* CFSSP

ΔkWPJM = (kBtu/hr \* (1/EERbase - 1/EERee)) \* CFPJM

Where:

CFSSP = Summer System Peak Coincidence Factor for Commercial cooling (during system peak hour)

= 91.3% [[357]](#footnote-358)

CFPJM = PJM Summer Peak Coincidence Factor for Commercial cooling (average during peak period)

= 47.8%[[358]](#footnote-359)

For example a 5 ton air cooled split system with a SEER of 15 in Rockford would save

ΔkWSSP = (60) \* [(1/13) – (1/15)] \* .913

= 0.562

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Measure Code: CI-HVC-SPUA-V03-150601

### Steam Trap Replacement or Repair [[359]](#footnote-360)

**Description**

The measure is for the repair or replacement of faulty steam traps that are allowing excess steam to escape and thereby increasing steam generation. The measure is applicable to commercial applications, commercial HVAC (low pressure steam) including multifamily buildings, low pressure industrial applications, medium pressure industrial applications, applications and high pressure industrial applications. Maximum pressure for this measure is 300 psig.

This measure was developed to be applicable to the following program types: TOS, RF. If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

Customers must have leaking traps to qualify for rebates. However, if a commercial customer opts to replace all traps without inspection, rebates and the savings are discounted to take into consideration the fact that some traps are being replaced that have not yet failed.

**Definition of Baseline Equipment**

The baseline criterion is a faulty steam trap in need of replacing. No minimum leak rate is required. Any leaking or blow through trap can be repaired or replaced. If a commercial customer chooses to repair or replace all the steam traps at the facility without verification, the savings are adjusted. Savings for commercial full replacement projects are reduced by the percentage of traps found to be leaking on average from the studies listed. If an audit is performed on a commercial site, then the leaking and blowdown can be adjusted.

**Deemed Lifetime of Efficient Equipment**

The life of this measure is 6 years[[360]](#footnote-361)

**Deemed Measure Cost**

|  |  |
| --- | --- |
| **Steam System** | **Cost per trap**[[361]](#footnote-362) **($)** |
| Commercial Dry Cleaners | 77 |
| Commercial Heating (including Multifamily), low pressure steam | 77 |
| Industrial Medium Pressure >15 psig psig < 30 psig | 180 |
| Steam Trap, Industrial Medium Pressure ≥30 <75 psig | 223 |
| Steam Trap, Industrial High Pressure ≥75 <125 psig | 276 |
| Steam Trap, Industrial High Pressure ≥125 <175 psig | 322 |
| Steam Trap, Industrial High Pressure ≥175 <250 psig | 370 |
| Steam Trap, Industrial High Pressure ≥250 psig | 418 |
| Steam Trap, Industrial Medium Pressure ≥30 <75 psig | 223 |
| Steam Trap, Industrial High Pressure ≥75 <125 psig | 276 |
| Steam Trap, Industrial High Pressure ≥125 <175 psig | 322 |
| Steam Trap, Industrial High Pressure ≥175 <250 psig | 370 |
| Steam Trap, Industrial High Pressure ≥250 psig | 418 |

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Savings**

**Energy Savings**

Δtherm = S \* (Hv/B) \* Hours \* A \* L / 100,000

Where:

S = Maximum theoretical steam loss per trap

|  |  |
| --- | --- |
| **Steam System** | **Avg Steam Loss[[362]](#footnote-363)**  **(lb/hr/trap)** |
| Commercial Dry Cleaners | 38.1 |
| Commercial Heating (including Multifamily)LPS | 13.8 |
| Industrial Low Pressure, <15 psig | 13.8 |
| Industrial Medium Pressure >15 psig < 30 psig | 12.7 |
| Steam Trap, Industrial Medium Pressure ≥30 <75 psig | 19.0 |
| Steam Trap, Industrial High Pressure ≥75 <125 psig | 67.9 |
| Steam Trap, Industrial High Pressure ≥125 <175 psig | 105.8 |
| Steam Trap, Industrial High Pressure ≥175 <250 psig | 143.7 |
| Steam Trap, Industrial High Pressure ≥250 psig | 200.5 |

Hv = Heat of vaporization of steam

|  |  |
| --- | --- |
| **Steam System** | **Heat of Vaporization**[[363]](#footnote-364) **(Btu/lb)** |
| Commercial Dry Cleaners | 890 |
| Commercial Heating (including Multifamily) LPS | 951 |
| Industrial Low Pressure ≤15 psig | 951 |
| Industrial Medium Pressure >15 psig < 30 psig | 945 |
| Steam Trap, Industrial Medium Pressure ≥30 <75 psig | 928 |
| Steam Trap, Industrial High Pressure ≥75 <125 psig | 894 |
| Steam Trap, Industrial High Pressure ≥125 <175 psig | 868 |
| Steam Trap, Industrial High Pressure ≥175 <250 psig | 846 |
| Steam Trap, Industrial High Pressure ≥250 psig | 820 |

B = Boiler efficiency

= custom, if unknown 0.8[[364]](#footnote-365)

Hours = Annual operating hours of steam plant

|  |  |  |
| --- | --- | --- |
| **Steam System** | **Hours/Yr**[[365]](#footnote-366) | **Zone** |
| Commercial Dry Cleaners | 2,425 |  |
| Industrial Low Pressure ≤15 psig | 7,752 |  |
| Industrial Medium Pressure >15 psig < 30 psig | 7,752 |  |
| Steam Trap, Industrial Medium Pressure ≥30 <75 psig | 7,752 |  |
| Steam Trap, Industrial High Pressure ≥75 <125 psig | 7,752 |  |
| Steam Trap, Industrial High Pressure ≥125 <175 psig | 7,752 |  |
| Steam Trap, Industrial High Pressure ≥175 <250 psig | 7,752 |  |
| Steam Trap, Industrial High Pressure ≥250 psig | 7,752 |  |
| Industrial Medium Pressure >15 psig < 30 psig | 7,752 |  |
| Steam Trap, Industrial Medium Pressure ≥30 <75 psig | 7,752 |  |
| Commercial Heating (including Multifamily)LPS[[366]](#footnote-367) | 4,272 | 1 (Rockford) |
| 4,029 | 2 (Chicago O'Hare) |
| 3,406 | 3 (Springfield) |
| 2,515 | 4 (Belleville) |
| 2,546 | 5 (Marion) |

A = Adjustment factor

= 50%[[367]](#footnote-368)

This factor is to account for reducing the maximum theortical steam flow (S) to the average steam flow (the Enbridge factor).

L = Leaking & blow-thru

L is 1.0 when applied to the replacment of an individual leaking trap. If a number of steam traps are replaced and the system has not been audited, the leaking and blow-thru is applied to reflect the assumed percentage of steam traps that were actually leaking and need to be replaced. A custom value can be utilized if a supported by an evaluation.

|  |  |
| --- | --- |
| **Steam System** | **%**[[368]](#footnote-369) |
| Custom | Custom |
| Commercial Dry Cleaners | 27% |
| Industrial Low Pressure ≤15 psig | 16% |
| Industrial Medium and High Pressure >15 psig | 16% |
| Commercial Heating (including Multifamily) LPS | 27% |

EXAMPLE

For example, a commercial dry cleaning facility with the default hours of operation and boiler efficiency;

ΔTherms = S \* (Hv/B) \* Hours \* A \* L

= 38.1 lbs/hr/trap \* (890 Btu/lb / 80%)/100,000 \* 2,425 \* 50% \* 27% =

138.8 therms per trap

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-HVC-STRE-V03-140601**

### Variable Speed Drives for HVAC Pumps and Cooling Tower Fans

###### Description

This measure is applied to variable speed drives (VSD) which are installed on the following HVAC system applications: chilled water pump, hot water pumps. There is a separate measure for HVAC supply and return fans. All other VSD applications require custom analysis by the program administrator. The VSD will modulate the speed of the motor when it does not need to run at full load. Since the power of the motor is proportional to the cube of the speed for these types of applications, significant energy savings will result.

This measure was developed to be applicable to the following program types: TOS, RF. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The VSD is applied to a motor which does not have a VSD. The application must have a variable load and installation is to include the necessary controls. Savings are based on application of VSDs to a range of baseline load conditions including no control, inlet guide vanes, outlet guide vanes and throttling valves.

###### Definition of Baseline Equipment

The time of sale baseline is a new motor installed without a VSD or other methods of control. Retrofit baseline is an existing motor operating as is. Retrofit baselines may or may not include guide vanes, throttling valves or other methods of control. This information shall be collected from the customer.

Installations of new equipment with VSDs which are required by IECC 2012 as adopted by the State of Illinois are not eligible for incentives.

###### Deemed Lifetime of Efficient Equipment

The expected measure life for HVAC application is 15 years;[[369]](#footnote-370) measure life for process is 10 years.[[370]](#footnote-371)

**Deemed Measure Cost**

Customer provided costs will be used when available. Default measure costs**[[371]](#footnote-372)** are noted below for up to 20 hp motors. Custom costs must be gathered from the customer for motor sizes not listed below.

| HP | Cost |
| --- | --- |
| 1 -5 HP | $ 1,330 |
| 7.5 HP | $ 1,622 |
| 10 HP | $ 1,898 |
| 15 HP | $ 2,518 |
| 20 HP | $ 3,059 |

###### Loadshape

|  |
| --- |
| Loadshape C42 - VFD - Boiler feedwater pumps <10 HP |
| Loadshape C43 - VFD - Chilled water pumps <10 HP |
| Loadshape C44 - VFD Boiler circulation pumps <10 HP |
| Loadshape C48 - VFD Boiler draft fans <10 HP |
| Loadshape C49 - VFD Cooling Tower Fans <10 HP |

###### Coincidence Factor

The demand savings factor (DSF) is already based upon coincident savings, and thus there is no additional coincidence factor for this characterization.

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = BHP /EFFi \* Hours \* ESF

Where:

BHP = System Brake Horsepower

(Nominal motor HP \* Motor load factor)

Motors are assumed to have a load factor of 65% for calculating kW if actual values cannot be determined[[372]](#footnote-373). Custom load factor may be applied if known.

EFFi = Motor efficiency, installed. Actual motor efficiency shall be used to calculate kW. If not known a default value of 93% shall be used.[[373]](#footnote-374)

Hours = Default hours are provided for HVAC applications which vary by HVAC application and building type[[374]](#footnote-375). When available, actual hours should be used.

| **Building Type** | **Pumps and fans** |
| --- | --- |
| College/University | 4216 |
| Grocery | 5840 |
| Heavy Industry | 3585 |
| Hotel/Motel | 6872 |
| Light Industry | 2465 |
| Medical | 6871 |
| Office | 2301 |
| Restaurant | 4654 |
| Retail/Service | 3438 |
| School(K-12) | 2203 |
| Warehouse | 3222 |
| Average=Miscellaneous | 4103 |

ESF = Energy savings factor varies by VFD application. Units are kW/HP.

| Application | ESF[[375]](#footnote-376) |
| --- | --- |
| Hot Water Pump | 0.424 |
| Chilled Water Pump | 0.411 |
| Air Foil/backward incline | 0.354 |
| Air Foil/ backward incline inlet Guide Vanes | 0.227 |
| Forward Curved Fan, with discharge dampers | 0.179 |
| Forward Curved Inlet Guide Vanes | 0.092 |

###### Summer Coincident Peak Demand Savings

ΔkW =BHP/EFFi \* DSF

Where:

DSF = Demand Savings Factor varies by VFD application.[[376]](#footnote-377) Units are kW/HP. Values listed below are based on typical peak load for the listed application.

| Application | DSF |
| --- | --- |
| Hot Water Pump | 0 |
| Chilled Water Pump | 0.299 |
| Air foil / backward incline | 0.260 |
| Air Foil / backward incline inlet Guide Vanes | 0.130 |
| Forward Curved Fan, with discharge dampers | 0.136 |
| Forward Curved Inlet Guide Vanes | 0.029 |

###### Fossil Fuel Impact Descriptions and Calculation

There are no expected fossil fuel impacts for this measure.

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-HVC-VSDHP-V02-150601

### Small Commercial Programmable Thermostats

**Description**

This measure characterizes the energy savings from the installation of a new Programmable Thermostat for reduced heating energy consumption through temperature set-back during unoccupied or reduced demand times. This measure is limited to small businesses, as they have smaller HVAC systems that are similar to residential HVAC systems and may be controlled by a simple manual adjustment thermostat. Mid to large sized businesses will typically have a building automation system or some other form of automated HVAC controls. Therefore, it is limited to select building types, including small office, retail – strip mall, restaurants (characterized as 1, 2 or 3 meal), small manufacturing, religious facilities, and convenience stores. This measure is only appropriate for single zone heating systems. Custom calculations are required for savings for programmable thermostats installed in multi-zone systems.

This measure was developed to be applicable to the following program types:  RF, DI.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

The criteria for this measure are established by replacement of a manual-only temperature control, with one that has the capability to adjust temperature setpoints according to a schedule without manual intervention.

**Definition of Baseline Equipment**

For new thermostats the baseline is a non-programmable thermostat requiring manual intervention to change temperature setpoint.

**Deemed Lifetime of Efficient Equipment**

The expected measure life of a programmable thermostat is assumed to be 8 years[[377]](#footnote-378) based upon equipment life only[[378]](#footnote-379). For the purposes of claiming savings for a new programmable thermostat, this is reduced by a 50% persistence factor to give a final measure life of 4 years.

**Deemed Measure Cost**

Actual material and labor costs should be used if the implementation method allows. If unknown the capital and labor cost for this measure is assumed to be $181 per thermostat[[379]](#footnote-380). For the purposes of screening and planning it should be assumed that one thermostat will serve 5 tons of Cooling Capacity at a cost of $36.20 / ton or 115kBtuh of Heating Capacity at a cost of $1.57 / kBtu.

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings[[380]](#footnote-381)**

The following equations are used to calculate baseline and proposed electric energy use. The savings is the difference between the proposed and baseline calculated usage. This approach allows the savings estimate to account for the operational attributes of the baseline as well as the proposed case, yielding a better estimate than an approach that assumes a particular baseline or proposed energy use to determine savings.

**Electric Energy Use Equations (kWh / ton)**

|  |  |  |
| --- | --- | --- |
| **Building Type** | **Fan Mode During Occupied Period (*Fo*)** | **Equation** |
| **Assembly** | Continuous | ***CZ***+***Fu***\*(0.83\****Tc***+0.83\****Th***+1.67\****Ws***-293.018)-0.0922\****Tc***\****Th***+1.291\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(1.911-0.12\****Tc***)+***Tc***\*(0.00311\****Ws***-0.229)+0.11\****Ws*** |
| **Convenience Store** | Continuous | ***CZ***+***Fu***\*(-28.629\****Tc***-11.69\****Th***+19.118\****Ws***-2935.12)+0.909\****Ws*** |
| Intermittent | ***CZ***+***Tc***\*(0.0863\****Ws***-12.688)+***Th***\*(0.043\****Ws***-6.38)+1.669\****Ws*** |
| **Office – Low Rise** | Continuous | ***CZ***+***Fu***\*(7.082\****Tc***-41.199\****Th***+18.734\****Ws***-3288.55)+***Tc***\*(0.205\****Ws***-34.929) |
| Intermittent | ***CZ***+***Tc***\*(0.0806\****Ws***-8.984)+***Th***\*(0.0864\****Ws***-9.558)+1.178\****Ws*** |
| **Religious** | Continuous | ***CZ***+***Fu***\*(-1.579\****Tc***-18.14\****Th***+15.01\****Ws***-2417.74)+***Tc***\*(0.177\****Ws***-26.412) |
| Intermittent | ***CZ***+***Fu***\*(0.266\****Tc***-2.067)+***Tc***\*(0.0295\****Ws***-4.502)+***Th***\*(0.0517\****Ws***-8.251)+0.735\****Ws*** |
| **Restaurant –**  **Fast Food** | Continuous | ***CZ***+***Fu***\*(0.678\****Tc***+0.257\****Th***+2.88\****Ws***-494.006)+***Tc***\*(0.0231\****Ws***-4.074)+***Th***\*(0.00936\****Ws***-1.655)+0.918\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.377\****Tc***+0.124\****Th***+0.13\****Ws***-24.893)+***Tc***\*(-0.0143\****Th***+0.0166\****Ws***-2.691)+0.898\****Ws*** |
| **Restaurant –**  **Sit Down** | Continuous | ***CZ***+***Fu***\*(-8.41\****Th***+11.766\****Ws***-1910.81)+***Tc***\*(0.282\****Ws***-43.851) |
| Intermittent | ***CZ***+0.123\****Fu***\****Tc***+***Tc***\*(0.0561\****Ws***-8.237)+***Th***\*(0.0219\****Ws***-3.284)+1.038\****Ws*** |
| **Retail – Large** | Continuous | ***CZ***+***Fu***\*(-1.475\****Th***+0.755\****Ws***-114.373)+***Th***\*(0.151\****Ws***-24.016)+1.612\****Ws*** |
| Intermittent | ***CZ***+***Tc***\*(0.0173\****Ws***-1.912)+***Th***\*(0.0249\****Ws***-3.29)+0.511\****Ws*** |
| **Retail – Strip Mall** | Continuous | ***CZ***+***Fu***\*(1.077\****Tc***-10.697\****Th***+6.91\****Ws***-1117.18)+***Tc***\*(0.0583\****Ws***-7.54)+1.231\****Ws*** |
| Intermittent | ***CZ***+0.0894\****Fu***\****Tc***+***Th***\*(-0.0142\****Tc***+0.04\****Ws***-5.278)+0.884\****Ws*** |

Where:

CZ = Climate Zone Coefficient

=Depends on Building Type and Fan Mode During Occupied Period (see table below)

Tc = Degrees of Cooling Setback °F

= Must be between 0-15°F

Th = Degrees of Heating Setback °F

=Must be between 0-15°F

Fo = Fan Mode During Occupied Period (**Note: Commercial mechanical code requires continuous fan operation during occupied periods to meet ventilation requirements**.)

= Continuous for occupied fan that runs continuously (e.g. Fan Mode Set to ‘On’)

= Intermittent for occupied fan that runs intermittently (e.g. Fan Mode Set to ‘Auto’)

Fu = Fan Mode During Unoccupied Period

= 0 for unoccupied fan that runs continuously (e.g. Fan Mode Set to ‘On’)

= 1 for unoccupied fan that runs intermittently (e.g. Fan Mode Set to ‘Auto’)

Ws = Weekly Hours thermostat is in Occupied mode

= Minimum values depends on Building Type (see table below), maximum value of 168 (24/7)

(e.g.: Weekly occupancy schedule of Mon-Sat 8AM-5PM, Sun 9AM-2PM, Ws = 59)

**Electric Energy Use Climate Zone Coefficients and Minimum Weekly Hours Occupied**

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
|  | **Fan Mode During Occupied Period (*Fo*)** | **Climate Zone Coefficient (*CZ*)**[[381]](#footnote-382) | | | | |  |
| **Building Type** | **1** | **2** | **3** | **4** | **5** | **Minimum *Ws*** |
| **Assembly** | Continuous | 911.366 | 928.924 | 1152.83 | 1208.999 | 1210.173 | 98 |
| Intermittent | 735.752 | 762.831 | 966.562 | 998.927 | 1028.906 |
| **Convenience Store** | Continuous | 4817.094 | 4832.784 | 5139.133 | 5182.161 | 5208.608 | 108 |
| Intermittent | 1478.133 | 1514.568 | 1784.384 | 1843.463 | 1930.47 |
| **Office - Low Rise** | Continuous | 5047.662 | 5039.592 | 5187.924 | 5217.672 | 5177.449 | 55 |
| Intermittent | 825.072 | 808.965 | 946.571 | 979.421 | 945.418 |
| **Religious Facility** | Continuous | 4197.117 | 4172.858 | 4380.025 | 4370.008 | 4356.054 | 133 |
| Intermittent | 632.404 | 603.395 | 678.294 | 664.717 | 616.853 |
| **Restaurant – Fast Food** | Continuous | 1342.988 | 1378.661 | 1664.018 | 1714.201 | 1727.841 | 108 |
| Intermittent | 993.764 | 1039.643 | 1307.8 | 1340.544 | 1389.791 |
| **Restaurant – Full Service** | Continuous | 4070.35 | 4094.742 | 4428.966 | 4501.829 | 4522.522 | 117 |
| Intermittent | 1472.014 | 1516.05 | 1856.108 | 1938.441 | 2056.45 |
| **Retail – Department Store** | Continuous | 1510.201 | 1496.47 | 1706.105 | 1716.128 | 1688.464 | 93 |
| Intermittent | 701.27 | 702.129 | 847.735 | 875.12 | 881.677 |
| **Retail – Strip Mall** | Continuous | 1926.294 | 1930.137 | 2156.856 | 2174.435 | 2165.03 | 93 |
| Intermittent | 656.479 | 673.257 | 835.906 | 850.322 | 869.921 |

A low rise office in Rockford (Climate Zone 1) is occupied Mon-Fri 7AM-6PM and has a 10 ton DX RTU controlled by a manual thermostat. The fan runs continuously during the occupied hours and building staff do not manually change the fan mode, cooling or heating setpoints during unoccupied periods.

A programmable thermostat is installed by a contractor who sets the occupied schedule to Mon-Fri 7AM-6PM with a 10°F cooling and heating unoccupied temperature setback. The contractor also programs the fan to operate continuously during the occupied periods and to intermittent “auto” during the unoccupied periods.

∆kWh = [Baseline Energy Use (kWh/Ton) – Proposed Energy Use(kWh/Ton)] \* Cooling Capacity (Tons)

Baseline Energy Use (kWh/Ton) = Equation for Office Low Rise, *Fo*=Continuous

= ***CZ***+***Fu***\*(7.082\****Tc***-41.199\****Th***+18.734\****Ws***-3288.55)+***Tc***\*(0.205\****Ws***-34.929)

= ***5047.662***+***0***\*(7.082\****0***-41.199\****0***+18.734\****168***-3288.55)+***0***\*(0.205\****168***-34.929)

= 5,047.662 kWh/Ton

Proposed Energy Use (kWh/Ton) = Equation for Office Low Rise, *Fo*=Continuous

= ***CZ***+***Fu***\*(7.082\****Tc***-41.199\****Th***+18.734\****Ws***-3288.55)+***Tc***\*(0.205\****Ws***-34.929)

= ***5047.662***+***1***\*(7.082\****10***-41.199\***10**+18.734\***55**-3288.55)+***10\*(***0.205\****55***-34.929)

= 2,211.722 kWh/Ton

∆kWh = [5,047.622 (kWh/Ton) – 2,211.722 (kWh/Ton)] \* 10 Tons

= 2,835.89 kWh/Ton \* 10 Tons

= 28,358.9 kWh

**Summer Coincident Peak Demand Savings**

N/A

**Natural Gas Energy Savings**

*The following equations are used to calculate baseline and proposed natural gas energy use. The savings is the difference between the proposed and baseline calculated usage. This approach allows the savings estimate to account for the operational attributes of the baseline as well as the proposed case, yielding a better estimate than an approach that assumes a particular baseline or proposed energy use to determine savings.*

**Natural Gas Energy Use Equations (therms / kbtu output)**

| **Building Type** | **Fan Mode During Occupied Period (*Fo*)** | **Equation** |
| --- | --- | --- |
| **Assembly** | Continuous | ***CZ***+***Fu***\*(0.232\****Th***+0.0984\****Ws***-18.79)+***Th***\*(0.00271\****Ws***-0.535)+0.0142\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.00405\****Th***+0.000519\****Ws***-0.11)+***Th***\*(0.0000689\****Ws***-0.0118)+0.0022\****Ws*** |
| **Convenience Store** | Continuous | ***CZ***+***Fu***\*(0.00545\****Th***-0.00251\****Ws***+0.416)+***Th***\*(0.000123\****Ws***-0.0204)+0.00183\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.00231\****Th***-0.0349)+***Th***\*(0.000309\****Ws***-0.0494)+0.00266\****Ws*** |
| **Office – Low Rise** | Continuous | ***CZ***+***Fu***\*(0.0205\****Th***+0.364)+***Th***\*(0.00046\****Ws***-0.0554)+0.00169\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.00745\****Th***-0.142)+***Th***\*(0.00077\****Ws***-0.111)+0.00199\****Ws*** |
| **Religious** | Continuous | ***CZ***+0.00791\****Fu***\****Th***+***Th***\*(0.00096\****Ws***-0.167)+0.00184\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.00143\****Th***-0.0309)+***Th***\*(0.0008\****Ws***-0.134)+0.00219\****Ws*** |
| **Restaurant – Fast Food** | Continuous | ***CZ***+***Fu***\*(0.0431\****Th***+0.0424\****Ws***-7.517)+***Th***\*(0.00113\****Ws***-0.213)+0.0119\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.0125\****Th***+0.0036\****Ws***-0.71)+***Th***\*(0.000329\****Ws***-0.0615)+0.00738\****Ws*** |
| **Restaurant –Sit Down** | Continuous | ***CZ***+***Fu***\*(0.00445\****Ws***-0.535)+***Th***\*(0.000679\****Ws***-0.1)+0.00218\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.00144\****Th***+0.000262\****Ws***-0.0553)+***Th***\*(0.00018\****Ws***-0.0299)+0.00166\****Ws*** |
| **Retail – Large** | Continuous | ***CZ***+0.00203\****Fu***\****Th***+***Th***\*(0.000591\****Ws***-0.0812)+0.00194\****Ws*** |
| Intermittent | ***CZ***+***Th***\*(0.000406\****Ws***-0.0611)+0.00228\****Ws*** |
| **Retail – Strip Mall** | Continuous | ***CZ***+***Fu***\*(0.00998\****Th***+0.00207\****Ws***-0.206)+***Th***\*(0.000665\****Ws***-0.101)+0.00292\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.00383\****Th***-0.0656)+***Th***\*(0.000575\****Ws***-0.0912)+0.00249\****Ws*** |

Where:

CZ = Climate Zone Coefficient

= Depends on Building Type and Fan Mode During Occupied Period (see table below)

Th = Degrees of Heating Setback °F

= Must be between 0-15°F

Fo = Fan Mode During Occupied Period (**Note: Commercial mechanical code requires continuous fan operation during occupied periods to meet ventilation requirements**.)

= Continuous for occupied fan that runs continuously (e.g. Fan Mode Set to ‘On’)

= Intermittent for occupied fan that runs intermittently (e.g. Fan Mode Set to ‘Auto’)

Fu = Fan Mode During Unoccupied Period

= 0 for unoccupied fan that runs continuously (e.g. Fan Mode Set to ‘On’)

= 1 for unoccupied fan that runs intermittently (e.g. Fan Mode Set to ‘Auto’)

Ws = Weekly Hours thermostat is in Occupied mode

= Minimum values depends on Building Type (see table below), maximum value of 168 (24/7)

(e.g.: Weekly occupancy schedule of Mon-Sat 8AM-5PM, Sun 9AM-2PM, Ws = 59)

**Natural Gas Energy Use Climate Zone Coefficients and Minimum Weekly Hours Occupied**

|  | **Fan Mode During Occupied Period (*Fo*)** | **Climate Zone Coefficient (*CZ*)** | | | | |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| **Building Type** | **1** | **2** | **3** | **4** | **5** | **Minimum *Ws*** |
| **Assembly** | Continuous | 19.872 | 17.83 | 15.828 | 15.282 | 13.482 | 98 |
| Intermittent | 0.237 | 0.0989 | 0.0267 | -0.0131 | -0.0871 |
| **Convenience Store** | Continuous | 1.493 | 1.081 | 0.782 | 0.544 | 0.114 | 108 |
| Intermittent | 1.128 | 0.854 | 0.619 | 0.437 | 0.0854 |
| **Office - Low Rise** | Continuous | 1.718 | 1.317 | 0.971 | 0.739 | 0.319 | 55 |
| Intermittent | 3.447 | 3.022 | 2.503 | 2.251 | 1.646 |
| **Religious Facility** | Continuous | 6.294 | 5.55 | 4.678 | 4.202 | 3.122 | 133 |
| Intermittent | 5.914 | 5.368 | 4.557 | 4.137 | 3.246 |
| **Restaurant – Fast Food** | Continuous | 8.383 | 7.211 | 6.034 | 5.767 | 4.71 | 108 |
| Intermittent | 1.227 | 0.636 | 0.302 | 0.102 | -0.262 |
| **Restaurant – Full Service** | Continuous | 5.247 | 4.484 | 3.753 | 3.465 | 2.627 | 117 |
| Intermittent | 0.951 | 0.704 | 0.51 | 0.381 | 0.0746 |
| **Retail – Department Store** | Continuous | 4.385 | 3.854 | 3.192 | 2.784 | 1.858 | 93 |
| Intermittent | 3.061 | 2.672 | 2.182 | 1.829 | 1.008 |
| **Retail – Strip Mall** | Continuous | 3.917 | 3.394 | 2.728 | 2.394 | 1.617 | 93 |
| Intermittent | 2.659 | 2.292 | 1.811 | 1.543 | 0.909 |

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-HVC-PROG-V02-150601**

### Demand Controlled Ventilation

**Description**

Demand control ventilation (DCV) adjusts outside ventilation air based on the number of occupants and the ventilation demands that those occupants create. DCV is part of a building's ventilation system control strategy. It may include hardware, software, and controls as an integral part of a building's ventilation design. Active control of the ventilation system provides the opportunity to reduce heating and cooling energy use.

The primary component is a control sensor to communicate either directly with the economizer or with a central computer. The component is most typically a carbon dioxide (CO2) sensor, occupancy sensor, or turnstile counter. This measure is applicable to multiple building types, and savings are classified by the specific building types defined in the Illinois TRM. . This measure is modeled to assume night time set backs are in operation and minimum outside air is being used when the building is unoccupied. Systems that have static louvers or that are open at night will likely have greater savings by using the custom program.

This measure was developed to be applicable to the following program types: RF. If applied to other program types, the measure savings should be verified

**Definition of Efficient Equipment**

The efficient equipment condition is defined by new CO2 sensors installed on return air systems where no other sensors were previously installed. For heating savings, this measure does not apply to any system with terminal reheat (constant volume or variable air volume). For terminal reheat system a custom savings calculation should be used.**Definition of Baseline Equipment**

The base case for this measure is a space with no demand control capability. The current code minimum for outside air (OA) is 17 CFM per occupant (ASHRAE 62.1) which is the value assumed in this measure.

**Deemed Lifetime of Efficient Equipment**

The deemed measure life is 10 years and based on CO2 sensor estimated life. [[382]](#footnote-383)

**Deemed Measure Cost**

The deemed measure cost is assumed to be the full cost of installation of a DCV retrofit including sensor cost ($500) and installation ($1000 labor) for a total of $1500[[383]](#footnote-384).

**Loadshape**

Commercial ventilation C23

**Coincidence Factor**

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

∆kWh = Condition Space/1000 \* Savings\_Factor

Where:

Conditioned Space = actual square footage of conditioned space controlled by sensor

Elec\_Savings\_Factor= value in table below based on building type and weather zone[[384]](#footnote-385)

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
| **Building Type** | **Elect\_Savings\_Factor (kWh/1000 sq ft)** | | | | |
| **Zone 1**  **(Rockford)** | **Zone 2**  **(Chicago)** | **Zone 3**  **(Springfield)** | **Zone 4**  **(Belleville)** | **Zone 5**  **(Marion)** |
| Office - Low-rise | 454 | 456 | 460 | 456 | 462 |
| Office - Mid-rise | 430 | 431 | 432 | 428 | 433 |
| Office- High-rise | 448 | 450 | 452 | 449 | 454 |
| Religious BuiIding | 493 | 509 | 573 | 584 | 605 |
| Restaurant | 505 | 515 | 553 | 569 | 581 |
| RetaiI - Department Store | 620 | 625 | 630 | 638 | 642 |
| Retail - Strip Mall | 380 | 376 | 356 | 406 | 407 |
| Convenience Store | 602 | 603 | 610 | 612 | 614 |
| Elementary School | 317 | 327 | 352 | 352 | 363 |
| High School | 305 | 316 | 340 | 340 | 352 |
| College/ University | 392 | 410 | 434 | 449 | 462 |
| Healthcare Clinic | 353 | 358 | 379 | 383 | 389 |
| Lodging | 576 | 578 | 586 | 588 | 591 |
| Manufacturing | 481 | 482 | 482 | 477 | 482 |
| Special Assembly Auditorium | 410 | 427 | 479 | 494 | 514 |
| De-fault | 451 | 458 | 475 | 482 | 490 |

For example: 7,500 SqFt of low-rise office space in Chicago.

ΔkWh= 7,500 SqFt /1000 SqFt \*456 kWh

= 3,420 kWh

**Summer Coincident Peak Demand Savings**

NA

**Natural Gas Savings**

∆therms = Condition Space/1000 \* Therm\_Savings\_Factor

Where:

Conditioned Space = actual square footage of conditioned space controlled by sensor

Therm \_Savings\_Factor= value in table below based on building type and weather zone[[385]](#footnote-386)

| **Building Type** | **Therm\_Savings\_Factor (Therm/1000 sq ft)** | | | | |
| --- | --- | --- | --- | --- | --- |
| **Zone 1**  **(Rockford)** | **Zone 2**  **(Chicago)** | **Zone 3**  **(Springfield)** | **Zone 4**  **(Belleville)** | **Zone 5**  **(Marion)** |
| Office - Low-rise | 30 | 26 | 23 | 22 | 19 |
| Office - Mid-rise | 20 | 17 | 15 | 15 | 13 |
| Office- High-rise | 27 | 23 | 21 | 20 | 17 |
| Religious BuiIding | 191 | 169 | 150 | 143 | 128 |
| Restaurant | 135 | 122 | 106 | 104 | 91 |
| RetaiI - Department Store | 47 | 42 | 37 | 36 | 32 |
| Retail - Strip Mall | 31 | 27 | 25 | 24 | 21 |
| Convenience Store | 23 | 21 | 18 | 17 | 15 |
| Elementary School | 83 | 73 | 64 | 60 | 53 |
| High School | 81 | 71 | 63 | 59 | 52 |
| College/ University | 161 | 141 | 124 | 120 | 101 |
| Healthcare Clinic | 57 | 50 | 44 | 42 | 38 |
| Lodging | 26 | 23 | 20 | 20 | 20 |
| Manufacturing | 21 | 19 | 16 | 15 | 14 |
| Special Assembly Auditorium | 225 | 198 | 179 | 175 | 154 |
| De-fault | 77 | 68 | 60 | 58 | 51 |

For example: 7500 SqFt of low-rise office space in Chicago.

ΔTherms = 7,500 SqFt \*26 Therm/1000 SqFt

= 195 Therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

###### Measure code: CI-HVC-DCV-V02-140601

### High Turndown Burner for Space Heating Boilers

**Description**

This measure is for a non-residential boilers equipped with linkageless controls providing space heating with burners having a turndown less than 6:1.[[386]](#footnote-387) Turndown is the ratio of the high firing rate to the low firing rate. When boilers are subjected to loads below the low firing rate, the boiler must cycle on/off to meet the load requirements. A higher turndown ratio reduces burner startups, provides better load control, saves wear-and-tear on the burner, and reduces purge-air requirements, all of these benefits result in better overall efficiency.

This measure was developed to be applicable to the following program types: NC, TOS, RF.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

To qualify the boiler linkageless burner must operate with a turndown greater than or equal to 10:1 and be subjected to loads less than or equal to 30%[[387]](#footnote-388) of the full fire input MBH for greater than 60%[[388]](#footnote-389) of the operating hours.

**Definition of Baseline Equipment**

The baseline boiler utilizes a linkageless burner with a turndown ration of 6:1 or less and is used primarily for space heating. Redundant boilers do not qualify.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 21 years.[[389]](#footnote-390)

**Deemed Measure Cost**

The deemed installed measure cost including labor is approximately $2.53/MBtu/hr.[[390]](#footnote-391)

**Deemed O&M Cost Adjustments**

N/A

###### Loadshape

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

N/A

**Summer Coincident Peak Demand Savings**

N/A

###### Natural Gas Savings

Δtherms= Ngi \* SF \* EFLH / 100

Where:

Ngi = Boiler gas input size (kBtu/hr) = custom

SF = Savings Factor = Percentage of energy loss per hour

= ( ∑ ((EL\_base – EL\_eff) \* H\_cycling)) / H)\*100

Where:

EL\_base = Base Boiler Percentage of energy loss due to cycling at % of Base Boiler Load where BL\_base ≤ TDR\_base

= 0.003 \* (Cycles\_base)2 – 0.001 \* Cycles\_base [[391]](#footnote-392)

Where:

Cycles\_base = Number of Cycles/hour of base boiler

= TDR\_base / BL

Where:

BL = % of full boiler load at bin hours being evaluated. This is assumed to be a straight line based on 0% load at the building balance point (assumed to be 55F), and full load corrected for the oversizing (OSF) at the lowest temperature bin of -10 to -5F.

OSF = Oversizing Factor = 1.3[[392]](#footnote-393) or custom

TDR\_base = Turndown ratio = 0.33[[393]](#footnote-394) or custom

EL\_eff = Efficient Boiler Percentage of energy loss due to cycling at % of Efficient Boiler Load

= 0.003 \* (Cycles\_eff)2 – 0.001 \* Cycles\_eff

Where:

Cycles\_eff = Number of Cycles/hour

= TDR\_eff / BL

Where:

TDR\_eff = Turndown ratio = 0.10[[394]](#footnote-395) or custom

H\_cycling = Hours base boiler is cycling at % of base boiler load

= see table below or custom

H = Total Number of Hours in Heating Season

=4,946 or custom

100 = convert to a percentage

SF = 69.1 / 4946 \*100 = 1.4% or custom (see table below for summary of values)

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
| Temp**erature** | H\_cycling | BL | EL\_base | EL\_eff | (EL\_base-EL\_eff)\* Hours |
| 50 to 55 | 601 | 6.0% | 8.5% | 0.7% | 47.2 |
| 45 to 50 | 603 | 12.0% | 2.0% | 0.0% | 12.0 |
| 40 to 45 | 455 | 18.0% | 0.8% | 0.0% | 3.8 |
| 35 to 40 | 925 | 24.0% | 0.4% | 0.0% | 4.0 |
| 30 to 35 | 814 | 30.0% | 0.3% | 0.0% | 2.1 |
| Total |  |  |  |  | 69.1 |

EFLH = Equivalent Full Load Hours for heating are provided in section 4.4 HVAC End Use.

100 = convert kBtu to therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

###### Measure Code: CI-HVAC-HTBC-V04-140601

### Linkageless Boiler Controls for Space Heating

**Description**

This measure is for a non-residential boiler providing space heating and currently having single point positioning combustion control. In single-point positioning control, the fuel valve is linked to the combustion air damper via a jackshaft mechanism to maintain correspondence between fuel and combustion air input. Most boilers with single point positioning control do not maintain low excess air levels over their entire firing range. Generally these boilers are calibrated at high fire, but due to the non-linearity required for efficient combustion, excess air levels tend to dramatically increase as the firing rate decreases. Boiler efficiency drops as the excess air levels are increased.

This measure was developed to be applicable to the following program types: TOS, RF.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

To qualify the boiler burner must have a linkageless control system allowing the combustion air damper position to be adjusted and set for optimal efficiency at several firing rates throughout the burner’s firing range. This requires the fuel valve and combustion air damper to each be powered by a separate actuator. An alternative to the combustion air damper is a Variable Speed Drive on the combustion air fan.

**Definition of Baseline Equipment**

The baseline boiler utilizes single point positioning for the burner combustion control.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 16 years.[[395]](#footnote-396)

**Deemed Measure Cost**

The deemed measure cost is estimated at $2.50/MBtu/hr burner input.[[396]](#footnote-397)

**Deemed O&M Cost Adjustments**

N/A

###### Loadshape

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

When a Variable Speed Drive is incorporated, electrical savings are calculated according to the Variable Speed Drive measure.

**Summer Coincident Peak Demand Savings**

N/A

###### Natural Gas Savings

Δtherms= Ngi \* SF \* EFLH / 100

Where:

Ngi = Boiler gas input size (kBtu/hr) = custom

SF = Savings factor

Note: Savings factor is the percentage increase in efficiency as a result of the addition of linkageless burner controls. At an average boiler load of 35%, single point controls are assumed to have excess air of 91%, while linkageless controls are assumed to have 34% excess air.[[397]](#footnote-398) The difference between controls types is 57% at this average operating condition. A 15% reduction in excess air is approximately a 1% increase in efficiency.[[398]](#footnote-399) Therefore the nominal combustion efficiency increase is 57 / 15 \* 1% = 3.8%.

= 3.8%

EFLH = Equivalent Full Load Hours for heating are provided in section 4.4 HVAC End Use

100 = convert kBtu to therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

###### Measure Code: CI-HVC-LBC-V04-140601

### Oxygen Trim Controls for Space Heating Boilers

###### Description

This measure is for a non-residential boiler providing space heating without oxygen trim combustion controls. Oxygen trim controls limit the amount of excess oxygen provided to the burner for combustion. This oxygen level is dependent upon the amount of air provided. Oxygen trim control converts parallel positioning, linkageless controls, into a closed-loop control configuration with the addition of an exhaust gas analyzer and PID controller. Boilers with oxygen trim controls can maintain a predetermined excess air rate (generally 15% to 30% excess air) over the entire burner firing rate. Boilers without these controls typically have excess air rates around 30% over the entire firing rate. Boiler efficiency drops as the excess air levels are increased.

This measure was developed to be applicable to the following program types: NC, TOS, RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify the boiler burner must have an oxygen control system allowing the combustion air to be adjusted to maintain a predetermined excess oxygen level in the flue exhaust at all firing rates throughout the burner’s firing range. This requires an oxygen sensor in the flue exhaust and linkageless fuel valve and combustion air controls.

###### Definition of Baseline Equipment

The baseline boiler utilizes single point positioning for the burner combustion control.

###### Deemed Lifetime of Efficient Equipment

The measure life for the O2 Trim controls is 18 years.[[399]](#footnote-400)

###### Deemed Measure Cost

The deemed measure cost is approximately $23,250.[[400]](#footnote-401)

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

Δtherms = Ngi \* SF \* EFLH / 100

Where:

Ngi = Boiler gas input size (kBtu/hr)

= Custom

SF = Savings factor

Note: Savings factor is the percentage reduction in gas consumption as a result of the addition of O2 trim controls. Linkageless controls have an excess air rate of 28% over the entire firing range.[[401]](#footnote-402) O2 trim controls have an excess air rate of 15%.[[402]](#footnote-403) The average difference is 13%. A 15% reduction in excess air is approximately a 1% increase in efficiency.[[403]](#footnote-404) Therefore the nominal combustion efficiency increase is 13 / 15 \* 1% = 0.87%.

= 0.87%

EFLH = Default Equivalent Full Load Hours for heating are provided in section 4.4 HVAC End Use. When available, actual hours should be used.

100 = convert kBtu to therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

The deemed annual Operations and Maintenance cost is $800.[[404]](#footnote-405)

###### Measure Code: CI-HVC-O2TC-V01-140601

### 

### Shut Off Damper for Space Heating Boilers or Furnaces

###### Description

This measure is for non-residential atmospheric boilers or furnaces providing space heating without a shut off damper. When appliances are on standby mode warm room air is drawn through the stack via the draft hood or dilution air inlet at a rate proportional to the stack height, diameter and outdoor temperature. More air is drawn through the vent immediately after the appliance shuts off and the flue is still hot. Installation of a new shut off damper can prevent heat from being drawn up the warm vent and reducing the amount of air that passes through the furnace or boiler heat exchanger. This reduction in air can slightly increase overall operating efficiency by reducing the time needed to achieve steady-state operating conditions.

This measure was developed to be applicable to the following program types: RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify the space heating boiler or furnace must have a new electrically or thermally activated shut off damper installed on either the exhaust flue or combustion air intake. Barometric dampers do not qualify. The damper actuation shall be interlocked with the firing controls.

###### Definition of Baseline Equipment

The baseline boiler or furnace incorporates no shut off damper on the combustion air intake or flue exhaust.

###### Deemed Lifetime of Efficient Equipment

The measure life for the shut off damper is 15 years.[[405]](#footnote-406)

###### Deemed Measure Cost

The deemed measure cost for this approximately $1,500.[[406]](#footnote-407)

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

Δtherms = Ngi \* SF \* EFLH / 100

Where:

Ngi = Boiler gas input size (kBtu/hr)

= Custom

SF = Savings factor

= 1%[[407]](#footnote-408)

Note: The savings factor assumes the boiler or furnace is located in an unconditioned space. The savings factor can be higher for those units located within conditioned space.

EFLH = Default Equivalent Full Load Hours for heating are provided in section 4.4 HVAC End Use. When available, actual hours should be used.

100 = convert kBtu to therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

The deemed annual Operations and Maintenance cost is $112.[[408]](#footnote-409)

###### Measure Code: CI-HVC-SODP-V01-140601

### Small Pipe Insulation

**Description**

This measure provides rebates for adding insulation to bare pipes with inner diameters of ½” and ¾”. Insulation must be at least one inch thick. Since new construction projects are required by code to have pipe insulation, this measure is only for retrofits of existing facilities. This covers bare straight pipe as well as all fittings.

Default savings are provided on a per linear foot basis. It is assumed that the majority of pipes less than one inch in commercial facilities are used for domestic hot water. However, this measure can cover hydronic heating systems as well as low and high pressure steam systems.

This measure was developed to be applicable to the following program types: RF.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

The efficient case is a ½“ or ¾“ diameter pipe with at least one inch of insulation. Insulation must be protected from damage which includes moisture, sunlight, equipment maintenance and wind. Outdoor pipes should have a weather protective jacket. Insulation must be continuous over straight pipe, elbows and tees.

**Definition of Baseline Equipment**

The base case for savings estimates is a bare hot water or steam pipe with a fluid temperature of 105 degrees Fahrenheit or greater. Current new construction code requires insulation amounts similar to this measure though this base case is commonly found in older existing buildings.

**Deemed Lifetime of Efficient Equipment**

The measure life is assumed to be 15 years.[[409]](#footnote-410)

**Deemed Measure Cost**

The incremental measure cost for insulation is the full cost of adding insulation to the pipe. Actual installation costs should be used for the measure cost. For planning purposes, the following costs can be used to estimate the full cost of materials and labor.[[410]](#footnote-411)

|  |  |  |
| --- | --- | --- |
| **Insulation Thickness** | **¾” pipe** | **½” pipe** |
| 1” | $4.45 | $4.15 |

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

N/A

**Summer Coincident Peak Demand Savings**

N/A

**Natural Gas Savings**

Δtherms per foot[[411]](#footnote-412) = [((Qbase – Qeff) \* EFLH) / (100,000 \* ηBoiler)] \* TRF

= [Provided by tables below] \* TRF

Δtherms = (Lsp + Loc,i) \* Δtherms per foot

Where:

EFLH = Equivalent Full Load Hours for Heating

= Actual or defaults by building type provided in Section 4.4, HVAC end use

For year round recirculation or domestic hot water:

= 8760

For heating season recirculation, hours with the outside air temperature below 55°F:

|  |  |
| --- | --- |
| **Zone** | **Hours** |
| Zone 1 (Rockford) | 5,039 |
| Zone 2 (Chicago) | 4,963 |
| Zone 3 (Springfield) | 4,495 |
| Zone 4 (Belleville/ | 4,021 |
| Zone 5 (Marion) | 4,150 |
| Zone 1 (Rockford) | 5,039 |

Qbase = Heat Loss from Bare Pipe (Btu/hr/ft)

= See table below

Qeff = Heat Loss from Insulated Pipe (Btu/hr/ft)

= See table below

100,000 = conversion factor (1 therm = 100,000 Btu)

ηBoiler = Efficiency of the boiler being used to generate the hot water or steam in the pipe

= 81.9% for water boilers [[412]](#footnote-413)

= 80.7% for steam boilers, except multifamily low-pressure [[413]](#footnote-414)

= 64.8% for multifamily low-pressure steam boilers [[414]](#footnote-415)

TRF = Thermal Regain Factor for space type, applied only to space heating energy and is applied to values resulting from Δtherms/ft tables below [[415]](#footnote-416)

= See table below for base TRF values by pipe location

May vary seasonally such as: TRF[summer] \* summer hours + TRF[winter] \* winter hours where TRF values reflecting summer and winter conditions are apportioned by the hours for those conditions. TRF may also be adjusted by building specific balance temperature and operating hours above and below that balance temperature.[[416]](#footnote-417)

|  |  |  |
| --- | --- | --- |
| **Pipe Location** | **Assumed Regain** | **TRF, Thermal Regain Factor** |
| Outdoor | 0% | 1.0 |
| Indoor, heated space | 85% | 0.15 |
| Indoor, semi- heated, (unconditioned space, with heat transfer to conditioned space. E.g.: boiler room, ceiling plenum, basement, crawlspace, wall) | 30% | 0.70 |
| Indoor, unheated, (no heat transfer to conditioned space) | 0% | 1.0 |
| Location not specified | 85% | 0.15 |
| Custom | Custom | 1 – assumed regain |

Lsp = Length of straight pipe to be insulated (linear foot)

Loc,i = Total equivalent length of (elbows and tees) of pipe to be insulated. Use table below to determine equivalent lengths.

|  |  |  |
| --- | --- | --- |
| **Nominal Pipe Diameter** | **Equivalent Length (ft)** | |
| **90 Degree Elbow** | **Straight Tee** |
|
| 1/2" | 0.04 | 0.03 |
| 3/4" | 0.06 | 0.05 |

Qbase = Heat Loss from Bare Pipe (Btu/hr/ft). Calculated with the 3E Plus software.

Qeff = Heat Loss from Insulated Pipe (Btu/hr/ft). Calculated with the 3E Plus software.

The table below shows the deemed therm savings by building type and region on a per linear foot basis for both ½” and ¾” copper pipe.

The following table provides deemed values for 1/2" copper pipe, temperatures are assumed by category below, and insulation is assumed to be one inch fiberglass.

| **Piping Use** | **Building Type** | **Annual Therms Saved / Linear Foot** | | | | |
| --- | --- | --- | --- | --- | --- | --- |
| **Zone 1 (Rockford)** | **Zone 2 (Chicago)** | **Zone 3 (Springfield)** | **Zone 4 (Belleville)** | **Zone 5 (Marion)** |
| Space Heating Non-recirculating | Assembly | 0.117 | 0.120 | 0.107 | 0.071 | 0.109 |
| Assisted Living | 0.110 | 0.107 | 0.094 | 0.069 | 0.083 |
| College | 0.100 | 0.093 | 0.083 | 0.046 | 0.055 |
| Convenience Store | 0.097 | 0.089 | 0.079 | 0.057 | 0.064 |
| Elementary School | 0.116 | 0.113 | 0.100 | 0.069 | 0.084 |
| Garage | 0.064 | 0.063 | 0.056 | 0.044 | 0.049 |
| Grocery | 0.105 | 0.105 | 0.092 | 0.057 | 0.068 |
| Healthcare Clinic | 0.103 | 0.106 | 0.092 | 0.063 | 0.066 |
| High School | 0.120 | 0.121 | 0.109 | 0.077 | 0.091 |
| Hospital - CAV no econ | 0.115 | 0.119 | 0.101 | 0.087 | 0.099 |
| Hospital - CAV econ | 0.117 | 0.121 | 0.103 | 0.089 | 0.101 |
| Hospital - VAV econ | 0.048 | 0.045 | 0.034 | 0.020 | 0.022 |
| Hospital - FCU | 0.087 | 0.099 | 0.080 | 0.094 | 0.127 |
| Hotel/Motel | 0.115 | 0.112 | 0.101 | 0.069 | 0.084 |
| Hotel/Motel - Common | 0.104 | 0.106 | 0.101 | 0.082 | 0.086 |
| Hotel/Motel - Guest | 0.115 | 0.111 | 0.099 | 0.066 | 0.082 |
| Manufacturing Facility | 0.068 | 0.066 | 0.061 | 0.037 | 0.041 |
| MF - High Rise | 0.100 | 0.098 | 0.090 | 0.076 | 0.076 |
| MF - High Rise - Common | 0.118 | 0.115 | 0.103 | 0.071 | 0.092 |
| MF - High Rise - Residential | 0.096 | 0.096 | 0.087 | 0.075 | 0.073 |
| MF - Mid Rise | 0.109 | 0.110 | 0.095 | 0.070 | 0.079 |
| Movie Theater | 0.119 | 0.117 | 0.109 | 0.083 | 0.099 |
| Office - High Rise - CAV no econ | 0.132 | 0.134 | 0.122 | 0.082 | 0.089 |
| Office - High Rise - CAV econ | 0.136 | 0.139 | 0.128 | 0.088 | 0.097 |
| Office - High Rise - VAV econ | 0.100 | 0.102 | 0.084 | 0.050 | 0.055 |
| Office - High Rise - FCU | 0.073 | 0.072 | 0.062 | 0.033 | 0.035 |
| Office - Low Rise | 0.093 | 0.093 | 0.074 | 0.045 | 0.052 |
| Office - Mid Rise | 0.103 | 0.104 | 0.088 | 0.056 | 0.062 |
| Religious Building | 0.105 | 0.098 | 0.094 | 0.069 | 0.079 |
| Restaurant | 0.088 | 0.088 | 0.079 | 0.060 | 0.071 |
| Retail - Department Store | 0.091 | 0.083 | 0.078 | 0.051 | 0.058 |
| Retail - Strip Mall | 0.087 | 0.081 | 0.071 | 0.049 | 0.053 |
| Warehouse | 0.095 | 0.089 | 0.091 | 0.057 | 0.070 |
| Unknown | 0.101 | 0.100 | 0.089 | 0.064 | 0.074 |
| Space Heating - recirculation heating season only | All buildings (Hours below 55°F) | 0.329 | 0.324 | 0.293 | 0.262 | 0.271 |
| Space Heating - recirculation year round | All buildings (All hours) | 0.572 | 0.572 | 0.572 | 0.572 | 0.572 |
| DHW | Recirculation loop | 0.572 | 0.572 | 0.572 | 0.572 | 0.572 |
| Process | Custom | Custom | | | | |

The following table provides deemed savings values for 3/4" copper pipe with temperatures assumed by category below, insulation is assumed to be one inch fiberglass.

| **Piping Use** | **Building Type** | **Annual Therms Saved / Linear Foot** | | | | |
| --- | --- | --- | --- | --- | --- | --- |
| **Zone 1 (Rockford)** | **Zone 2 (Chicago)** | **Zone 3 (Springfield)** | **Zone 4 (Belleville)** | **Zone 5 (Marion)** |
| Space Heating Non-recirculating | Assembly | 0.142 | 0.145 | 0.129 | 0.086 | 0.132 |
| Assisted Living | 0.133 | 0.130 | 0.115 | 0.084 | 0.101 |
| College | 0.121 | 0.113 | 0.101 | 0.056 | 0.067 |
| Convenience Store | 0.117 | 0.108 | 0.096 | 0.069 | 0.077 |
| Elementary School | 0.141 | 0.137 | 0.121 | 0.084 | 0.102 |
| Garage | 0.078 | 0.077 | 0.067 | 0.054 | 0.060 |
| Grocery | 0.127 | 0.127 | 0.111 | 0.069 | 0.083 |
| Healthcare Clinic | 0.125 | 0.128 | 0.112 | 0.076 | 0.081 |
| High School | 0.146 | 0.147 | 0.132 | 0.094 | 0.110 |
| Hospital - CAV no econ | 0.140 | 0.144 | 0.123 | 0.105 | 0.120 |
| Hospital - CAV econ | 0.142 | 0.147 | 0.125 | 0.108 | 0.123 |
| Hospital - VAV econ | 0.058 | 0.055 | 0.041 | 0.025 | 0.027 |
| Hospital - FCU | 0.105 | 0.120 | 0.098 | 0.115 | 0.154 |
| Hotel/Motel | 0.140 | 0.136 | 0.122 | 0.084 | 0.102 |
| Hotel/Motel - Common | 0.127 | 0.129 | 0.123 | 0.100 | 0.105 |
| Hotel/Motel - Guest | 0.139 | 0.135 | 0.120 | 0.081 | 0.099 |
| Manufacturing Facility | 0.083 | 0.080 | 0.074 | 0.045 | 0.050 |
| MF - High Rise | 0.121 | 0.119 | 0.109 | 0.093 | 0.093 |
| MF - High Rise - Common | 0.144 | 0.140 | 0.125 | 0.086 | 0.111 |
| MF - High Rise - Residential | 0.117 | 0.116 | 0.105 | 0.091 | 0.089 |
| MF - Mid Rise | 0.132 | 0.134 | 0.115 | 0.085 | 0.096 |
| Movie Theater | 0.144 | 0.142 | 0.133 | 0.101 | 0.120 |
| Office - High Rise - CAV no econ | 0.160 | 0.162 | 0.148 | 0.099 | 0.108 |
| Office - High Rise - CAV econ | 0.165 | 0.169 | 0.155 | 0.107 | 0.118 |
| Office - High Rise - VAV econ | 0.121 | 0.123 | 0.102 | 0.060 | 0.067 |
| Office - High Rise - FCU | 0.089 | 0.087 | 0.075 | 0.040 | 0.042 |
| Office - Low Rise | 0.113 | 0.113 | 0.090 | 0.055 | 0.063 |
| Office - Mid Rise | 0.126 | 0.126 | 0.106 | 0.068 | 0.075 |
| Religious Building | 0.127 | 0.119 | 0.114 | 0.084 | 0.095 |
| Restaurant | 0.107 | 0.107 | 0.096 | 0.073 | 0.086 |
| Retail - Department Store | 0.110 | 0.101 | 0.095 | 0.062 | 0.071 |
| Retail - Strip Mall | 0.106 | 0.098 | 0.086 | 0.059 | 0.064 |
| Warehouse | 0.115 | 0.108 | 0.111 | 0.069 | 0.085 |
| Unknown | 0.123 | 0.122 | 0.108 | 0.078 | 0.090 |
| Space Heating - recirculation heating season only | All buildings (Hours below 55°F) | 0.399 | 0.393 | 0.356 | 0.319 | 0.329 |
| Space Heating - recirculation year round | All buildings (All hours) | 0.694 | 0.694 | 0.694 | 0.694 | 0.694 |
| DHW | Recirculation loop | 0.694 | 0.694 | 0.694 | 0.694 | 0.694 |
| Process | Custom | Custom | | | | |

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-HVC-SPIN-V01-150601**

### Small Commercial Programmable Thermostat Adjustments

**Description**

This measure involves reprogramming existing commercial programmable thermostats or building automation systems for reduced energy consumption through adjustments of unoccupied heating/cooling setpoints and/or fan control. This measure is limited to packaged HVAC units that are controlled by a commercial thermostat or building automation system. The measure is limited to select building types presented below.

**Eligible Small Commercial Building Types**

|  |
| --- |
| **Building Type** |
| Assembly |
| Convenience Store |
| Office - Low Rise |
| Restaurant - Fast Food |
| Religious Facility |
| Restaurant - Full Service |
| Retail - Strip Mall |
| Retail - Department Store |

This measure was developed to be applicable to the following program types:  RF, DI.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

The criteria for this measure is established by optimizing heating/cooling temperature setbacks and fan operation with a commercial programmable thermostat or building automation system, which reprogrammed to match actual facility occupancy.

**Definition of Baseline Equipment**

The baseline for this measure is a commercial programmable thermostat or building automation system that is currently operating packaged HVAC units with heating/cooling temperature setbacks and fan operation that do not align with a facilities actual occupancy.

**Deemed Lifetime of Efficient Equipment**

The expected measure life of a programmable thermostat is assumed to be 8 years[[417]](#footnote-418) based upon equipment life only[[418]](#footnote-419). For the purposes of claiming savings for a adjustment of an existing programmable thermostat, this is reduced to a 25% persistence factor to give a final measure life of 2 years. It is recommended that this assumption be evaluated by future energy measurement and verification activities.

**Deemed Measure Cost**

Actual labor costs should be used if the implementation method allows. If unknown the labor cost for this measure is assumed to be $70.34[[419]](#footnote-420) per thermostat, as summarized in the table below.

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| **Measure** | **Units** | **Materials** | **Labor** | **Total Cost (including O&P)** | **City Cost Index (Install Only)\*** | **Total** | **Source** |
| Adjust Temperature Set Points | 4 | $0.00 | $5.95 | $6.55 | 134.5% | $35.24 | RS Means 2010 (pg 255, Section 23-09-8100) |
| Adjust Fan Schedule | 2 | $0.00 | $11.86 | $13.05 | 134.5% | $35.10 | RS Means 2010 (pg 255, Section 23-09-8120) |
| **Totals** |  |  |  |  |  | **$70.34** |  |
| \* Chicago, IL - Division 23 | |  |  |  |  |  |  |

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings[[420]](#footnote-421)**

The following equations are used to calculate baseline and proposed electric energy use. The savings is the difference between the proposed and baseline calculated usage. This approach allows the savings estimate to account for the operational attributes of the baseline as well as the proposed case, yielding a better estimate than an approach that assumes a particular baseline or proposed energy use to determine savings.

**Electric Energy Use Equations (kWh / ton)**

|  |  |  |
| --- | --- | --- |
| **Building Type** | **Fan Mode During Occupied Period (*Fo*)** | **Equation** |
| **Assembly** | Continuous | ***CZ***+***Fu***\*(0.83\****Tc***+0.83\****Th***+1.67\****Ws***-293.018)-0.0922\****Tc***\****Th***+1.291\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(1.911-0.12\****Tc***)+***Tc***\*(0.00311\****Ws***-0.229)+0.11\****Ws*** |
| **Convenience Store** | Continuous | ***CZ***+***Fu***\*(-28.629\****Tc***-11.69\****Th***+19.118\****Ws***-2935.12)+0.909\****Ws*** |
| Intermittent | ***CZ***+***Tc***\*(0.0863\****Ws***-12.688)+***Th***\*(0.043\****Ws***-6.38)+1.669\****Ws*** |
| **Office – Low Rise** | Continuous | ***CZ***+***Fu***\*(7.082\****Tc***-41.199\****Th***+18.734\****Ws***-3288.55)+***Tc***\*(0.205\****Ws***-34.929) |
| Intermittent | ***CZ***+***Tc***\*(0.0806\****Ws***-8.984)+***Th***\*(0.0864\****Ws***-9.558)+1.178\****Ws*** |
| **Religious** | Continuous | ***CZ***+***Fu***\*(-1.579\****Tc***-18.14\****Th***+15.01\****Ws***-2417.74)+***Tc***\*(0.177\****Ws***-26.412) |
| Intermittent | ***CZ***+***Fu***\*(0.266\****Tc***-2.067)+***Tc***\*(0.0295\****Ws***-4.502)+***Th***\*(0.0517\****Ws***-8.251)+0.735\****Ws*** |
| **Restaurant –**  **Fast Food** | Continuous | ***CZ***+***Fu***\*(0.678\****Tc***+0.257\****Th***+2.88\****Ws***-494.006)+***Tc***\*(0.0231\****Ws***-4.074)+***Th***\*(0.00936\****Ws***-1.655)+0.918\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.377\****Tc***+0.124\****Th***+0.13\****Ws***-24.893)+***Tc***\*(-0.0143\****Th***+0.0166\****Ws***-2.691)+0.898\****Ws*** |
| **Restaurant –**  **Sit Down** | Continuous | ***CZ***+***Fu***\*(-8.41\****Th***+11.766\****Ws***-1910.81)+***Tc***\*(0.282\****Ws***-43.851) |
| Intermittent | ***CZ***+0.123\****Fu***\****Tc***+***Tc***\*(0.0561\****Ws***-8.237)+***Th***\*(0.0219\****Ws***-3.284)+1.038\****Ws*** |
| **Retail – Large** | Continuous | ***CZ***+***Fu***\*(-1.475\****Th***+0.755\****Ws***-114.373)+***Th***\*(0.151\****Ws***-24.016)+1.612\****Ws*** |
| Intermittent | ***CZ***+***Tc***\*(0.0173\****Ws***-1.912)+***Th***\*(0.0249\****Ws***-3.29)+0.511\****Ws*** |
| **Retail – Strip Mall** | Continuous | ***CZ***+***Fu***\*(1.077\****Tc***-10.697\****Th***+6.91\****Ws***-1117.18)+***Tc***\*(0.0583\****Ws***-7.54)+1.231\****Ws*** |
| Intermittent | ***CZ***+0.0894\****Fu***\****Tc***+***Th***\*(-0.0142\****Tc***+0.04\****Ws***-5.278)+0.884\****Ws*** |

Where:

CZ = Climate Zone Coefficient

=Depends on Building Type and Fan Mode During Occupied Period (see table below)

Tc = Degrees of Cooling Setback °F

= Must be between 0-15°F

Th = Degrees of Heating Setback °F

=Must be between 0-15°F

Fo = Fan Mode During Occupied Period (**Note: Commercial mechanical code requires continuous fan operation during occupied periods to meet ventilation requirements**.)

= Continuous for occupied fan that runs continuously (e.g. Fan Mode Set to ‘On’)

= Intermittent for occupied fan that runs intermittently (e.g. Fan Mode Set to ‘Auto’)

Fu = Fan Mode during Unoccupied Period

= 0 for unoccupied fan that runs continuously (e.g. Fan Mode Set to ‘On’)

= 1 for unoccupied fan that runs intermittently (e.g. Fan Mode Set to ‘Auto’)

Ws = Weekly Hours thermostat is in Occupied mode,

= Minimum values depend on Building Type (see table below), maximum value of 168 (24/7)  
 ex: Weekly occupancy schedule of Mon-Sat 8AM-5PM, Sun 9AM-2PM, Ws = 59

**Electric Energy Use Climate Zone Coefficients and Minimum Weekly Hours Occupied**

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
|  | **Fan Mode During Occupied Period (*Fo*)** | **Climate Zone Coefficient (*CZ*)** | | | | |  |
| **Building Type** | **1** | **2** | **3** | **4** | **5** | **Minimum *Ws*** |
| **Assembly** | Continuous | 19.872 | 17.83 | 15.828 | 15.282 | 13.482 | 98 |
| Intermittent | 0.237 | 0.0989 | 0.0267 | -0.0131 | -0.0871 |
| **Convenience Store** | Continuous | 1.493 | 1.081 | 0.782 | 0.544 | 0.114 | 108 |
| Intermittent | 1.128 | 0.854 | 0.619 | 0.437 | 0.0854 |
| **Office - Low Rise** | Continuous | 1.718 | 1.317 | 0.971 | 0.739 | 0.319 | 55 |
| Intermittent | 3.447 | 3.022 | 2.503 | 2.251 | 1.646 |
| **Religious Facility** | Continuous | 6.294 | 5.55 | 4.678 | 4.202 | 3.122 | 133 |
| Intermittent | 5.914 | 5.368 | 4.557 | 4.137 | 3.246 |
| **Restaurant – Fast Food** | Continuous | 8.383 | 7.211 | 6.034 | 5.767 | 4.71 | 108 |
| Intermittent | 1.227 | 0.636 | 0.302 | 0.102 | -0.262 |
| **Restaurant – Full Service** | Continuous | 5.247 | 4.484 | 3.753 | 3.465 | 2.627 | 117 |
| Intermittent | 0.951 | 0.704 | 0.51 | 0.381 | 0.0746 |
| **Retail – Department Store** | Continuous | 4.385 | 3.854 | 3.192 | 2.784 | 1.858 | 93 |
| Intermittent | 3.061 | 2.672 | 2.182 | 1.829 | 1.008 |
| **Retail – Strip Mall** | Continuous | 3.917 | 3.394 | 2.728 | 2.394 | 1.617 | 93 |
| Intermittent | 2.659 | 2.292 | 1.811 | 1.543 | 0.909 |

**EXAMPLE**

A low rise office building in Rockford (Climate Zone 1) is occupied Mon-Fri 7AM-6PM and is heated and cooled with a packaged Gas (150 kBtu output) / DX (10 Ton) RTU which is controlled by a programmable thermostat. When the technician reviews the thermostat schedule they find the unoccupied schedule is programmed incorrectly. During the unoccupied periods the fan is programmed correctly, and runs in intermittent “auto” mode, although the heating and cooling temperature setpoints are not setback.

The technician adjusts the unoccupied schedule to include a 10°F cooling and heating temperature setback during the unoccupied periods.

∆kWh = [Baseline Energy Use (kWh/Ton) – Proposed Energy Use (kWh/Ton)] \* Cooling Capacity (Tons)

Baseline Energy Use (kWh/Ton) = Equation for Office Low Rise, *Fo*=Continuous

= ***CZ***+***Fu***\*(7.082\****Tc***-41.199\****Th***+18.734\****Ws***-3288.55)+***Tc***\*(0.205\****Ws***-34.929)

= ***5047.662***+1\*(7.082\****0***-41.199\****0***+18.734\****55***-3288.55)+***0***\*(0.205\****55***-34.929)

= 2,789.482 kWh/Ton

Proposed Energy Use (kWh/Ton) = Equation for Office Low Rise, *Fo*=Continuous

= ***CZ***+***Fu***\*(7.082\****Tc***-41.199\****Th***+18.734\****Ws***-3288.55)+***Tc***\*(0.205\****Ws***-34.929)

= ***5047.662***+***1***\*(7.082\****10***-41.199\***10**+18.734\***55**-3288.55)+***10\*(***0.205\****55***-34.929)

= 2,211.722 kWh/Ton

∆kWh = [2,789.482 (kWh/Ton) – 2,211.722 (kWh/Ton)] \* 10 Tons

= 577.71 kWh/Ton \* 10 Tons

= 5777.1 kWh

**Summer Coincident Peak Demand Savings**

N/A

**Natural Gas Energy Savings**

The following equations are used to calculate baseline and proposed natural gas energy use. The savings is the difference between the proposed and baseline calculated usage. This approach allows the savings estimate to account for the operational attributes of the baseline as well as the proposed case, yielding a better estimate than an approach that assumes a particular baseline or proposed energy use to determine savings.

**Natural Gas Energy Use Equations (therms / kbtu)**

|  |  |  |
| --- | --- | --- |
| **Building Type** | **Fan Mode During Occupied Period (*Fo*)** | **Equation** |
| **Assembly** | Continuous | ***CZ***+***Fu***\*(0.232\****Th***+0.0984\****Ws***-18.79)+***Th***\*(0.00271\****Ws***-0.535)+0.0142\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.00405\****Th***+0.000519\****Ws***-0.11)+***Th***\*(0.0000689\****Ws***-0.0118)+0.0022\****Ws*** |
| **Convenience Store** | Continuous | ***CZ***+***Fu***\*(0.00545\****Th***-0.00251\****Ws***+0.416)+***Th***\*(0.000123\****Ws***-0.0204)+0.00183\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.00231\****Th***-0.0349)+***Th***\*(0.000309\****Ws***-0.0494)+0.00266\****Ws*** |
| **Office – Low Rise** | Continuous | ***CZ***+***Fu***\*(0.0205\****Th***+0.364)+***Th***\*(0.00046\****Ws***-0.0554)+0.00169\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.00745\****Th***-0.142)+***Th***\*(0.00077\****Ws***-0.111)+0.00199\****Ws*** |
| **Religious** | Continuous | ***CZ***+0.00791\****Fu***\****Th***+***Th***\*(0.00096\****Ws***-0.167)+0.00184\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.00143\****Th***-0.0309)+***Th***\*(0.0008\****Ws***-0.134)+0.00219\****Ws*** |
| **Restaurant – Fast Food** | Continuous | ***CZ***+***Fu***\*(0.0431\****Th***+0.0424\****Ws***-7.517)+***Th***\*(0.00113\****Ws***-0.213)+0.0119\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.0125\****Th***+0.0036\****Ws***-0.71)+***Th***\*(0.000329\****Ws***-0.0615)+0.00738\****Ws*** |
| **Restaurant –Sit Down** | Continuous | ***CZ***+***Fu***\*(0.00445\****Ws***-0.535)+***Th***\*(0.000679\****Ws***-0.1)+0.00218\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.00144\****Th***+0.000262\****Ws***-0.0553)+***Th***\*(0.00018\****Ws***-0.0299)+0.00166\****Ws*** |
| **Retail – Large** | Continuous | ***CZ***+0.00203\****Fu***\****Th***+***Th***\*(0.000591\****Ws***-0.0812)+0.00194\****Ws*** |
| Intermittent | ***CZ***+***Th***\*(0.000406\****Ws***-0.0611)+0.00228\****Ws*** |
| **Retail – Strip Mall** | Continuous | ***CZ***+***Fu***\*(0.00998\****Th***+0.00207\****Ws***-0.206)+***Th***\*(0.000665\****Ws***-0.101)+0.00292\****Ws*** |
| Intermittent | ***CZ***+***Fu***\*(0.00383\****Th***-0.0656)+***Th***\*(0.000575\****Ws***-0.0912)+0.00249\****Ws*** |

Where:

CZ = Climate Zone Coefficient

= Depends on Building Type and Fan Mode During Occupied Period (see table below)

Th = Degrees of Heating Setback °F

= Must be between 0-15°F

Fo = Fan Mode During Occupied Period (**Note: Commercial mechanical code requires continuous fan operation during occupied periods to meet ventilation requirements**.)

= Continuous for occupied fan that runs continuously (e.g. Fan Mode Set to ‘On’)

= Intermittent for occupied fan that runs intermittently (e.g. Fan Mode Set to ‘Auto’)

Fu = Fan Mode during Unoccupied Period

= 0 for unoccupied fan that runs continuously (e.g. Fan Mode Set to ‘On’)

= 1 for unoccupied fan that runs intermittently (e.g. Fan Mode Set to ‘Auto’)

Ws = Weekly Hours thermostat is in Occupied mode,

= Minimum values depends on Building Type (see table below), maximum value of 168 (24/7)  
 ex: Weekly occupancy schedule of Mon-Sat 8AM-5PM, Sun 9AM-2PM, Ws = 59.

**Natural Gas Energy Use Climate Zone Coefficients and Minimum Weekly Hours Occupied**

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
|  | **Fan Mode During Occupied Period (*Fo*)** | **Climate Zone Coefficient (*CZ*)** | | | | |  |
| **Building Type** | **1** | **2** | **3** | **4** | **5** | **Minimum *Ws*** |
| **Assembly** | Continuous | 19.872 | 17.83 | 15.828 | 15.282 | 13.482 | 98 |
| Intermittent | 0.237 | 0.0989 | 0.0267 | -0.0131 | -0.0871 |
| **Convenience Store** | Continuous | 1.493 | 1.081 | 0.782 | 0.544 | 0.114 | 108 |
| Intermittent | 1.128 | 0.854 | 0.619 | 0.437 | 0.0854 |
| **Office - Low Rise** | Continuous | 1.718 | 1.317 | 0.971 | 0.739 | 0.319 | 55 |
| Intermittent | 3.447 | 3.022 | 2.503 | 2.251 | 1.646 |
| **Religious Facility** | Continuous | 6.294 | 5.55 | 4.678 | 4.202 | 3.122 | 133 |
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| **Restaurant – Fast Food** | Continuous | 8.383 | 7.211 | 6.034 | 5.767 | 4.71 | 108 |
| Intermittent | 1.227 | 0.636 | 0.302 | 0.102 | -0.262 |
| **Restaurant – Full Service** | Continuous | 5.247 | 4.484 | 3.753 | 3.465 | 2.627 | 117 |
| Intermittent | 0.951 | 0.704 | 0.51 | 0.381 | 0.0746 |
| **Retail – Department Store** | Continuous | 4.385 | 3.854 | 3.192 | 2.784 | 1.858 | 93 |
| Intermittent | 3.061 | 2.672 | 2.182 | 1.829 | 1.008 |
| **Retail – Strip Mall** | Continuous | 3.917 | 3.394 | 2.728 | 2.394 | 1.617 | 93 |
| Intermittent | 2.659 | 2.292 | 1.811 | 1.543 | 0.909 |

**EXAMPLE**

A low rise office building in Rockford (Climate Zone 1) is occupied Mon-Fri 7AM-6PM and is heated and cooled with a packaged Gas (150 kBtu output) / DX (10 Ton) RTU which is controlled by a programmable thermostat. When the technician reviews the thermostat schedule they find the unoccupied schedule is programmed incorrectly. During the unoccupied periods the fan is programmed correctly, and runs in intermittent “auto” mode, although the heating and cooling temperature setpoints are not setback.

The technician adjusts the unoccupied schedule to include a 10°F cooling and heating temperature setback during the unoccupied periods.

∆Therms = [Baseline Energy Use (Therms/kBtuh) – Proposed Energy Use(Therms/kBtuh)] \* Output Heating Capacity (kBtuh)

Baseline Energy Use (Therms/kBtuh) = Equation for Office Low Rise, *Fo*=Continuous

= ***CZ***+***Fu***\*(0.0205\****Th***+0.364)+***Th***\*(0.00046\****Ws***-0.0554)+0.00169\****Ws***

= ***1.718***+***1***\*(0.0205\****0***+0.364)+***0***\*(0.00046\****55***-0.0554)+0.00169\****55***

= 2.17495 Therms/kBtuh output

Proposed Energy Use (Therms/kBtuh) = Equation for Office Low Rise, *Fo*=Continuous

= ***CZ***+***Fu***\*(0.0205\****Th***+0.364)+***Th***\*(0.00046\****Ws***-0.0554)+0.00169\****Ws***

= ***1.718***+***1***\*(0.0205\****10***+0.364)+***10***\*(0.00046\****55***-0.0554)+0.00169\****55***

= 2.07895 Therms/kBtuh output

∆Therms = [2.17495 (Therms/kBtuh output) – 2.07895 (Therms/kBtuh output)] \* 150kBtuh output

= 0.096 (Therms/kBtuh output) \* 150kBtuh output

= 14.4 Therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-HVC- PRGA -V01-150601**

### Variable Speed Drives for HVAC Supply and Return Fans

**Description**

This measure is applied to variable speed drives (VSD) which are installed on HVAC supply fans and return fans. There is a separate measure for HVAC pumps and cooling tower fans. All other VSD applications require custom analysis by the program administrator. The VSD will modulate the speed of the motor when it does not need to run at full load. Since the power of the motor is proportional to the cube of the speed for these types of applications, significant energy savings will result.

This measure was developed to be applicable to the following program types: TOS, RF. If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

The VSD is applied to a motor which does not have a VSD. The application must have a variable load and installation is to include the necessary controls. Savings are based on application of VSDs to a range of baseline load conditions including no control, inlet guide vanes, outlet guide vanes and throttling valves.

**Definition of Baseline Equipment**

The time of sale baseline is a new motor installed without a VSD or other methods of control. Retrofit baseline is an existing motor operating as is. Retrofit baselines may or may not include guide vanes, throttling valves or other methods of control. This information shall be collected from the customer.

Installations of new equipment with VSDs which are required by IECC 2012 as adopted by the State of Illinois are not eligible for incentives.

**Deemed Lifetime of Efficient Equipment**

The expected measure life for HVAC application is 15 years;[[421]](#footnote-422) measure life for process is 10 years.[[422]](#footnote-423)

**Deemed Measure Cost**

Customer provided costs will be used when available. Default measure costs**[[423]](#footnote-424)** are noted below for up to 20 hp motors. Custom costs must be gathered from the customer for motor sizes not listed below.

| **HP** | **Cost** |
| --- | --- |
| 1 -5 HP | $ 1,330 |
| 7.5 HP | $ 1,622 |
| 10 HP | $ 1,898 |
| 15 HP | $ 2,518 |
| 20 HP | $ 3,059 |

**Loadshape**

|  |
| --- |
| Loadshape C39 - VFD - Supply fans <10 HP |
| Loadshape C40 - VFD - Return fans <10 HP |
| Loadshape C41 - VFD - Exhaust fans <10 HP |

**Coincidence Factor**

The demand savings factor (DSF) is already based upon coincident savings, and thus there is no additional coincidence factor for this characterization.

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings[[424]](#footnote-425)**

|  |  |
| --- | --- |
| kWhBase = |  |
| kWhRetrofit = |  |
| ∆kWhfan = |  |
| ∆kWhtotal = |  |

Where:

= Baseline annual energy consumption (kWh/yr)

= Retrofit annual energy consumption (kWh/yr)

= Fan-only annual energy savings

= Total project annual energy savings

= Conversion factor for HP to kWh

= Nominal horsepower of controlled motor

= Load Factor; Motor Load at Fan Design CFM (Default = 65%)[[425]](#footnote-426)

= Installed nominal/nameplate motor efficiency

Default motor is a NEMA Premium Efficiency, ODP, 4-pole/1800 RPM fan motor

**NEMA Premium Efficiency Motors Default Efficiencies[[426]](#footnote-427)**

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
| Size HP | Open Drip Proof (ODP) | | | Totally Enclosed Fan-Cooled (TEFC) | | |
| # of Poles | | | # of Poles | | |
| 6 | 4 | 2 | 6 | 4 | 2 |
| Speed (RPM) | | | Speed (RPM) | | |
| 1200 | 1800  Default | 3600 | 1200 | 1800 | 3600 |
| 1 | 0.825 | 0.855 | 0.770 | 0.825 | 0.855 | 0.770 |
| 1.5 | 0.865 | 0.865 | 0.840 | 0.875 | 0.865 | 0.840 |
| 2 | 0.875 | 0.865 | 0.855 | 0.885 | 0.865 | 0.855 |
| 3 | 0.885 | 0.895 | 0.855 | 0.895 | 0.895 | 0.865 |
| 5 | 0.895 | 0.895 | 0.865 | 0.895 | 0.895 | 0.885 |
| 7.5 | 0.902 | 0.910 | 0.885 | 0.910 | 0.917 | 0.895 |
| 10 | 0.917 | 0.917 | 0.895 | 0.910 | 0.917 | 0.902 |
| 15 | 0.917 | 0.930 | 0.902 | 0.917 | 0.924 | 0.910 |
| 20 | 0.924 | 0.930 | 0.910 | 0.917 | 0.930 | 0.910 |
| 25 | 0.930 | 0.936 | 0.917 | 0.930 | 0.936 | 0.917 |
| 30 | 0.936 | 0.941 | 0.917 | 0.930 | 0.936 | 0.917 |
| 40 | 0.941 | 0.941 | 0.924 | 0.941 | 0.941 | 0.924 |
| 50 | 0.941 | 0.945 | 0.930 | 0.941 | 0.945 | 0.930 |
| 60 | 0.945 | 0.950 | 0.936 | 0.945 | 0.950 | 0.936 |
| 75 | 0.945 | 0.950 | 0.936 | 0.945 | 0.954 | 0.936 |
| 100 | 0.950 | 0.954 | 0.936 | 0.950 | 0.954 | 0.941 |
| 125 | 0.950 | 0.954 | 0.941 | 0.950 | 0.954 | 0.950 |
| 150 | 0.954 | 0.958 | 0.941 | 0.958 | 0.958 | 0.950 |
| 200 | 0.954 | 0.958 | 0.950 | 0.958 | 0.962 | 0.954 |
| 250 | 0.954 | 0.958 | 0.950 | 0.958 | 0.962 | 0.958 |
| 300 | 0.954 | 0.958 | 0.954 | 0.958 | 0.962 | 0.958 |
| 350 | 0.954 | 0.958 | 0.954 | 0.958 | 0.962 | 0.958 |
| 400 | 0.958 | 0.958 | 0.958 | 0.958 | 0.962 | 0.958 |
| 450 | 0.962 | 0.962 | 0.958 | 0.958 | 0.962 | 0.958 |
| 500 | 0.962 | 0.962 | 0.958 | 0.958 | 0.962 | 0.958 |

= Annual operating hours for fan motor based on building type

Default hours are provided for HVAC applications which vary by HVAC application and building type[[427]](#footnote-428). When available, actual hours should be used.

| **Building Type** | **Pumps and fans** |
| --- | --- |
| College/University | 4216 |
| Grocery | 5840 |
| Heavy Industry | 3585 |
| Hotel/Motel | 6872 |
| Light Industry | 2465 |
| Medical | 6871 |
| Office | 2301 |
| Restaurant | 4654 |
| Retail/Service | 3438 |
| School(K-12) | 2203 |
| Warehouse | 3222 |
| Average=Miscellaneous | 4103 |

= Percentage of run-time spent within a given flow fraction range

Default Fan Duty Cycle Based on 2012 ASHRAE Handbook; HVAC Systems and Equipment, page 45.11, Figure 12.

|  |  |
| --- | --- |
| **Flow Fraction  (% of design cfm)** | **Percent of Time at Flow Fraction** |
| 0% to 10% | 0.0% |
| 10% to 20% | 1.0% |
| 20% to 30% | 5.5% |
| 30% to 40% | 15.5% |
| 40% to 50% | 22.0% |
| 50% to 60% | 25.0% |
| 60% to 70% | 19.0% |
| 70% to 80% | 8.5% |
| 80% to 90% | 3.0% |
| 90% to 100% | 0.5% |

= Part load ratio for a given flow fraction range based on the baseline flow control type

= Part load ratio for a given flow fraction range based on the retrofit flow control type

|  |  |  |  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| **Control Type** | **Flow Fraction** | | | | | | | | | |
| **10%** | **20%** | **30%** | **40%** | **50%** | **60%** | **70%** | **80%** | **90%** | **100%** |
| No Control or Bypass Damper | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Discharge Dampers | 0.46 | 0.55 | 0.63 | 0.70 | 0.77 | 0.83 | 0.88 | 0.93 | 0.97 | 1.00 |
| Outlet Damper, BI & Airfoil Fans | 0.53 | 0.53 | 0.57 | 0.64 | 0.72 | 0.80 | 0.89 | 0.96 | 1.02 | 1.05 |
| Inlet Damper Box | 0.56 | 0.60 | 0.62 | 0.64 | 0.66 | 0.69 | 0.74 | 0.81 | 0.92 | 1.07 |
| Inlet Guide Vane, BI & Airfoil Fans | 0.53 | 0.56 | 0.57 | 0.59 | 0.60 | 0.62 | 0.67 | 0.74 | 0.85 | 1.00 |
| Inlet Vane Dampers | 0.38 | 0.40 | 0.42 | 0.44 | 0.48 | 0.53 | 0.60 | 0.70 | 0.83 | 0.99 |
| Outlet Damper, FC Fans | 0.22 | 0.26 | 0.30 | 0.37 | 0.45 | 0.54 | 0.65 | 0.77 | 0.91 | 1.06 |
| Eddy Current Drives | 0.17 | 0.20 | 0.25 | 0.32 | 0.41 | 0.51 | 0.63 | 0.76 | 0.90 | 1.04 |
| Inlet Guide Vane, FC Fans | 0.21 | 0.22 | 0.23 | 0.26 | 0.31 | 0.39 | 0.49 | 0.63 | 0.81 | 1.04 |
| VFD with duct static pressure controls | 0.09 | 0.10 | 0.11 | 0.15 | 0.20 | 0.29 | 0.41 | 0.57 | 0.76 | 1.01 |
| VFD with low/no duct static pressure | 0.05 | 0.06 | 0.09 | 0.12 | 0.18 | 0.27 | 0.39 | 0.55 | 0.75 | 1.00 |

= HVAC interactive effects factor for energy (default = 15.7%)

**Summer Coincident Peak Demand Savings**

|  |  |
| --- | --- |
| kWBase = |  |
| kWRetrofit = |  |
| ∆kWfan = |  |
| ∆kWtotal = |  |

Where:

= Baseline summer coincident peak demand (kW)

= Retrofit summer coincident peak demand (kW)

= Fan-only summer coincident peak demand impact

= Total project summer coincident peak demand impact

= The part load ratio for the average flow fraction between the peak daytime hours during the weekday peak time period based on the baseline flow control type (default average flow fraction during peak period = 90%)

= The part load ratio for the average flow fraction between the peak daytime hours during the weekday peak time period based on the retrofit flow control type (default average flow fraction during peak period = 90%)

= HVAC interactive effects factor for summer coincident peak demand  
 (default = 15.7%)

**Fossil Fuel Impact Descriptions and Calculation**

There are no expected fossil fuel impacts for this measure.

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-HVC-VSDF-V01-150601**

### Energy Recovery Ventilator

**Description**

This measure includes the addition of energy recovery equipment on existing or new unitary equipment, where energy recovery is not required by the IECC 2012. This measure analyzes the heating savings potential from recovering energy from exhaust or relief building air. This measure assumes during unoccupied hours of the building no exhaust or relief air is available for energy recovery.

This measure was developed to be applicable to the following program types: TOS, NC, RF.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

Efficient equipment is unitary equipment that incorporates energy recovery not required by the IECC 2012.

**Definition of Baseline Equipment**

The baseline is unitary equipment not require by IECC 2012 to incorporate energy recovery.

**Deemed Lifetime of Efficient Equipment**

The measure life for the domestic energy recovery equipment is 15 years.[[428]](#footnote-429)

**Deemed Measure Cost**

The incremental cost for this measure assumes cost of cabinet and controls incorporated into packaged and built up air handler units. Additionally it assumes 1 to 1 ratio of fresh and exhausted air.

|  |  |
| --- | --- |
| **Energy Recovery Equipment Type** | **Incremental Cost $/CFM[[429]](#footnote-430)** |
| Fixed Plate | $6 |
| Rotary Wheel | $6 |
| Heat Pipe | $6 |

**Deemed O&M Cost Adjustments**

There are no expected O&M savings associated with this measure.

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

**Summer Coincident Peak Demand Savings**

There are no anticipated electrical savings from this measure as it is assumed that the additional fan energy due to the increased static pressure drop offsets cooling energy savings. Where this is not expected to be the case, a custom calculation should be used to determine the savings.

**Natural Gas Savings**

Gas savings algorithm is derived from the following:

ΔTherms = (Design Heating Load \* TE\_ERV \* EFLH \* OccHours/24) / (100,000 \* µHeat)

Where:

Design Heating Load = (1.08 \* CFM \* ΔT)

1.08 = A constant for sensible heat equations (BTU/h/CFM.°F)

CFM = Cubic Feet per Minute of Energy Recovery Ventilator

ΔT = T\_RA – T\_DD

T\_RA = Temperature of the Return Air = 70°F or custom

T\_DD = Temperature on design day of outside air[[430]](#footnote-431)

= (see Table below) or custom

|  |  |  |
| --- | --- | --- |
| **Zone** | **Weather Station** | **T\_DD, Temperature, °F** |
| 1 | Greater Rockford | -5.8 |
| 2 | Chicago/O’Hare ARPT. | -1.5 |
| 3 | Springfield/Capital | 0.4 |
| 4 | Scott AFB MidAmerica | 9.0 |
| 5 | Cape Girardeau Regional | 9.7 |
| Average | - | 2.4 |

TE\_ERV = Thermal Effectiveness of Energy Recovery Equipment[[431]](#footnote-432)

= (see Table below) or custom

|  |  |
| --- | --- |
| **Heat Recovery Equipment Type** | **TE\_ERV (%)** |
| Fixed Plate | 0.65 |
| Rotary Equipment | 0.68 |
| Heat Pipe | 0.55 |

EFLH = Equivalent Full Load Hours for heating are provided in section 4.4 HVAC End Use

OccHour = Average Hours per day facility is occupied

= (see Table 4.4.1 EQuest Modeling Inputs by Building Type) or custom

µHeat = Efficiency of heating system

= Actual

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-HVC-ERVE-V01-150601**

### Stack Economizer for Boilers Serving HVAC Loads

**Measure Description**

Stack economizers are designed to recover heat from hot boiler flue gasses. Recovered heat is used to preheat boiler feed water. This measure describes the retrofit of HVAC boilers with stack economizers. HVAC boilers are defined as those used for space heating applications. There is another, similar measure for boilers that serve process loads.

This measure was developed to be applicable to the following program types: NC, TOS, RF.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

To qualify the economizer must be installed on a boiler exhaust stack. Heat captured by the economizer is to be used to pre-heat boiler feed water.

**Definition of Baseline Equipment**

The baseline boiler does not have an economizer installed.

**Deemed Lifetime of Efficient Equipment**

The measure life for the boiler stack economizer is 15 years.[[432]](#footnote-433)

**Deemed Measure Cost**

The incremental and full measure cost for this measure is custom.

**Deemed O&M Cost Adjustments**

The O&M cost for this measure is custom.

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

N/A

**Summer Coincident Peak Demand Savings**

N/A

**Natural Gas Savings**

Δtherms = SF \* MBH\_In \* EFLH / 100

Where:

SF = (T\_existing – T\_eff) / 40°F \* TRE

= see default Savings Factor table below

Where:

T\_existing = Existing Full Fire Boiler Flue Gas Temperature as it exits the Stack

= 425F[[433]](#footnote-434) (water, 81.9% eff) or custom

= 480F3 (steam, 80.7% eff) or custom

T\_eff = Efficient Full Fire Boiler Flue Gas Temperature as it exits the Stack

= 338°F (conventional economizer – Water Boiler)[[434]](#footnote-435) or custom

= 365°F (conventional economizer – Steam Boiler)[[435]](#footnote-436) or custom

= 280°F (condensing economizer – Water Boiler)[[436]](#footnote-437) or custom

= 308°F (condensing economizer – Water Boiler)[[437]](#footnote-438) or custom

TRE = % efficiency increase for 40°F of stack temperature reduction

= 1%[[438]](#footnote-439) or custom

Based on defaults provided above:

|  |  |  |
| --- | --- | --- |
| **Boiler Type** | **SF[[439]](#footnote-440)** | |
| **Conventional Economizer** | **Condensing Economizer** |
| Hot Water Boiler | 2.19% average SF or custom | 3.63% average SF or custom |
| Steam Boiler | 2.88% average SF or custom | 4.31% average SF or custom |

MBH\_In = Rated boiler input capacity, in MBH

= Actual

EFLH = Equivalent Full Load Hours for heating are provided in Section 4.4 HVAC End Use

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-HVC-BECO-V01-150601**

### Stack Economizer for Boilers Serving Process Loads

**Measure Description**

Stack economizers are designed to recover heat from hot boiler flue gasses. Recovered heat is used to preheat boiler feed water. This measure describes the retrofit of process boilers with stack economizers. Process boilers are defined as those used for industrial, manufacturing, or other non-HVAC applications. There is another, similar measure for boilers that serve HVAC loads.  
  
This measure was developed to be applicable to the following program types: NC, TOS, RF.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

To qualify the economizer must be installed on a boiler exhaust stack. Heat captured by the economizer is to be used to pre-heat boiler feed water.

**Definition of Baseline Equipment**

The baseline boiler does not have an economizer installed.

**Deemed Lifetime of Efficient Equipment**

The measure life for the boiler stack economizer is 15 years.[[440]](#footnote-441)

**Deemed Measure Cost**

The incremental and full measure cost for this measure is custom.

**Deemed O&M Cost Adjustments**

The O&M cost for this measure is custom.

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

N/A

**Summer Coincident Peak Demand Savings**

N/A

**Natural Gas Savings**

Δtherms = SF \* MBH\_In \* 8766 \* UF / 100

Where:

SF = (T\_existing – T\_eff)/40°F \* TRE

= see default Savings Factor table below

T\_existing = Existing Full Fire Boiler Flue Gas Temperature as it exits the Stack

= 425F[[441]](#footnote-442) (water, 81.9% eff per IL TRM) or custom

= 480F3 (steam, 80.7% eff per IL TRM) or custom

T\_eff = Efficient Full Fire Boiler Flue Gas Temperature as it exits the Stack

= 338°F (conventional economizer – Water Boiler)[[442]](#footnote-443) or custom

= 365°F (conventional economizer – Steam Boiler)[[443]](#footnote-444) or custom

= 280°F (condensing economizer – Water Boiler)[[444]](#footnote-445) or custom

= 308°F (condensing economizer – Water Boiler)[[445]](#footnote-446) or custom

TRE = % efficiency increase for 40°F of stack temperature reduction

= 1%[[446]](#footnote-447) or custom

Based on defaults provided above:

|  |  |  |
| --- | --- | --- |
| **Boiler Type** | **SF[[447]](#footnote-448)** | |
| **Conventional Economizer** | **Condensing Economizer** |
| Hot Water Boiler | 2.19% average SF or custom | 3.63% average SF or custom |
| Steam Boiler | 2.88% average SF or custom | 4.31% average SF or custom |

MBH\_In = Rated boiler input capacity, in MBH

= Actual

8766 = Hours a year

UF = Utilization Factor

= 41.9%[[448]](#footnote-449) or custom

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-HVC-PECO-V01-150601**

### Notched V Belts for HVAC Systems

**Measure Description**

This measure is for replacement of smooth v-belts in non-residential package and split HVAC systems with notched v-belts. Typically there is a v-belt between the motor and the supply air fan and/or return air fan in larger package and split HVAC systems (RTU).

In general there are two styles of grooved v-belts, notched and synchronous. The DOE defines each as follows;

**Notched V-Belts** - A notched belt has grooves or notches that run perpendicular to the belt’s length, which reduces the bending resistance of the belt. Notched belts can use the same pulleys as cross-section standard V-belts. They run cooler, last longer, and are about 2% more efficient than standard V-belts.

**Synchronous Belts** - Synchronous belts (also called cogged, timing, positive-drive, or high-torque drive belts) are toothed and require the installation of mating grooved sprockets. These belts operate with a consistent efficiency of 98% and maintain their efficiency over a wide load range.

Smooth v-belts are usually referred to in five basic groups:

* “L” belts are low end belts that are for small, fractional horsepower motors and these are not used in RTUs.
* “A” and “B” belts are the two types typically used in RTUs. The “A” belt is a ½ inch width by 5/16 inch thickness and the “B” belt is larger, 21/32 inch wide and 12/32 inch thick so it can carry more power. V-belts come in a wide variety of lengths where 20 to 100 inches is typical.
* “C” and “D” belts are primarily for industrial applications with high power transmission requirements.
* V-belts are provided by various vendors. The notched version of these belts typically have an “X” added to the designation. For this HVAC fans notched v-belt Replacement measure, only the “A” and “B” v-belts are considered. A typical “A” v-belt is replaced by a notched “AX” v-belt and a “B” is replaced by a “BX.” In general, smooth v-belts have an efficiency of 90% to 98% while notched v-belts have an efficiency of 95% to 98%. Because notched v-belts are more flexible they work with smaller diameter pulleys and they have less resistance to bending. Lower bending resistance increases the power transmission efficiency, lowers the waste heat, and allows the belt to last longer than a smooth belt.

Three research papers[[449]](#footnote-450) [[450]](#footnote-451) [[451]](#footnote-452) show that the notched v-belt efficiency is 2% to 5% better than a typical smooth v-belt. A fourth paper by USDOE’s Energy Efficiency and Renewable Energy[[452]](#footnote-453) group reviewed most of the earlier literature and recommended using a conservative 2% efficiency improvement for energy savings for calculations.

For this measure it is assumed that upgrading a standard smooth v-belt with a new notched v-belt will result in a fan energy reduction of 2%.

**Definition of Efficient Equipment**

The Efficient Equipment is HVAC RTUs that have notched v-belts installed on the supply and/or return air fans.

**Definition of Baseline Equipment**

The Baseline Equipment is HVAC RTUs that have smooth v-belts installed on the supply and/or return air fans (i.e. RTU does not already have a notched v-belt installed).

**Deemed Lifetime of Efficient Equipment**

A v-belt has a life based on fan run hours which varies by building type based primarily on occupancy schedule because the fans are required by code to operate continuously during occupied hours. The supply and return fans will also run a few hours during unoccupied hours for heating and cooling as needed. For the notched v-belt EUL calculation, the default hours[[453]](#footnote-454) in the following table are used for a variety of building types and HVAC applications.

EUL = Belt Life / Occupancy Hours per year

Where:

Belt Life = 24,000 hours[[454]](#footnote-455)

Occupancy Hours per year = values from Table below

The notched v-belt measure EUL is summarized by building type in the following table.

**Notched v-belt Effective Useful Life (EUL)**

|  |  |  |
| --- | --- | --- |
| **Building Type** | **Pumps & Fans (annual Hours of operation)** | **EUL (Years)** |
| College/University | 4216 | 5.7 |
| Grocery | 5840 | 4.1 |
| Heavy Industry | 3585 | 6.7 |
| Hotel/Motel | 6872 | 3.5 |
| Light Industry | 2465 | 9.7 |
| Medical | 6871 | 3.5 |
| Office | 2301 | 10.4 |
| Restaurant | 4654 | 5.2 |
| Retail/Service | 3438 | 7.0 |
| School(K-12) | 2203 | 10.9 |
| Warehouse | 3222 | 7.4 |
| Average=Miscellaneous | 4103 | 5.8 |

**Deemed Measure Cost**

A review of the Grainger online[[455]](#footnote-456) pricing for “A,” “B,” “AX,” and “BX” v-belts showed the incremental cost to upgrade to notched v-belts would result in a 28% price increase. The notched v-belt incremental cost is summarized in the table below:

**Notched V-belt Incremental Cost Summary**

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
| **Smooth V-Belt Industry Number** | **Outside Length (Inches)** | **Dayton Smooth V-Belt\*** | **Notched V-belt Industry Number** | **Dayton Notched v-belt\*** | **Price Increase** | **% Increase** |
| A30 (Item # 1A095) | 32 | $12.70 | AX29 (Item # 3GWU4) | $17.65 | $4.95 | 28% |
| B29 (Item # 6L208) | 32 | $16.75 | BX29 (Item # 5TXL4) | $23.23 | $6.48 | 28% |
| \* Pricing based on Dayton Belts as found on Grainger Website 10/30/14 | | | | | | |

**Deemed O&M Cost Adjustments**

N/A

**Loadshape**

Loadshape C05 - Commercial Electric Heating and Cooling

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

ΔkWh = kWconnected\* Hours \* ESF

Where:

kWConnected =kW of equipment is calculated using motor efficiency.

= (HP \* 0.746 kW/HP\* Load Factor)/Motor Efficiency

Load Factor =Motors are assumed to have a load factor of 80% for calculating KW if actual values cannot be determined[[456]](#footnote-457). Custom load factor may be applied if known.

Motor Efficiency = Actual motor efficiency shall be used to calculate KW. If not known a value from the motor efficiency refrence tables below should be used**[[457]](#footnote-458)**

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
| **Baseline Motor Efficiencies (EPACT)** | | | |  |  |  |
|  | **Open Drip Proof (ODP)** | | | **Totally Enclosed Fan-Cooled (TEFC)** | | |
|  | **# of Poles** | | |
| **Size HP** | ***6*** | ***4*** | ***2*** | ***6*** | ***4*** | ***2*** |
|  | **Speed (RPM)** | | | **Speed (RPM)** | | |
|  | ***1200*** | ***1800*** | ***3600*** | ***1200*** | ***1800*** | ***3600*** |
| 1/8 | - | 44.00% | - | - | - | - |
| 1/6 | 57.50% | 62.00% | - | - | - | - |
| 1/4 | 68.00% | 68.00% | - | 68.00% | 64.00% | - |
| 1/3 | 70.00% | 70.00% | 72.00% | 70.00% | 68.00% | 72.00% |
| 1/2 | 78.50% | 80.00% | 68.00% | 72.00% | 74.00% | 68.00% |
| 3/4 | 77.00% | 78.50% | 74.00% | 77.00% | 75.50% | 74.00% |
| 1 | 80.00% | 82.50% | 75.50% | 80.00% | 82.50% | 75.50% |
| 1.5 | 84.00% | 84.00% | 82.50% | 85.50% | 84.00% | 82.50% |
| 2 | 85.50% | 84.00% | 84.00% | 86.50% | 84.00% | 84.00% |
| 3 | 86.50% | 86.50% | 84.00% | 87.50% | 87.50% | 85.50% |
| 5 | 87.50% | 87.50% | 85.50% | 87.50% | 87.50% | 87.50% |
| 7.5 | 88.50% | 88.50% | 87.50% | 89.50% | 89.50% | 88.50% |
| 10 | 90.20% | 89.50% | 88.50% | 89.50% | 89.50% | 89.50% |
| 15 | 90.20% | 91.00% | 89.50% | 90.20% | 91.00% | 90.20% |
| 20 | 91.00% | 91.00% | 90.20% | 90.20% | 91.00% | 90.20% |
| 25 | 91.70% | 91.70% | 91.00% | 91.70% | 92.40% | 91.00% |

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
| **Efficient Motor Efficiencies (NEMA Premium)** | | | | |  |  |
|  | **Open Drip Proof (ODP)** | | | **Totally Enclosed Fan-Cooled (TEFC)** | | |
|  | **# of Poles** | | | **# of Poles** | | |
|  | **2** | **4** | **6** | **2** | **4** | **6** |
| **Size HP** | **Speed (RPM)** | | | **Speed (RPM)** | | |
|  | **1200** | **1800** | **3600** | **1200** | **1800** | **3600** |
| 0.125 \* | - | 44.00% | - | - | - | - |
| 1/6 | 57.50% | 62.00% | - | - | - | - |
| 1/4 | 68.00% | 68.00% | - | 68.00% | 64.00% | - |
| 1/3 | 70.00% | 70.00% | 72.00% | 70.00% | 68.00% | 72.00% |
| 1/2 | 78.50% | 80.00% | 68.00% | 72.00% | 74.00% | 68.00% |
| 3/4 | 77.00% | 78.50% | 74.00% | 77.00% | 75.50% | 74.00% |
| 1 | 82.50% | 85.50% | 77.00% | 82.50% | 85.50% | 77.00% |
| 1.5 | 86.50% | 86.50% | 84.00% | 87.50% | 86.50% | 84.00% |
| 2 | 87.50% | 86.50% | 85.50% | 88.50% | 86.50% | 85.50% |
| 3 | 88.50% | 89.50% | 85.50% | 89.50% | 89.50% | 86.50% |
| 5 | 89.50% | 89.50% | 86.50% | 89.50% | 89.50% | 88.50% |
| 7.5 | 90.20% | 91.00% | 88.50% | 91.00% | 91.70% | 89.50% |
| 10 | 91.70% | 91.70% | 89.50% | 91.00% | 91.70% | 90.20% |
| 15 | 91.70% | 93.00% | 90.20% | 91.70% | 92.40% | 91.00% |
| 20 | 92.40% | 93.00% | 91.00% | 91.70% | 93.00% | 91.00% |
| 25 | 93.00% | 93.60% | 91.70% | 93.00% | 93.60% | 91.70% |

Hours = When available, actual hours should be used. If actual hours are not available default hours[[458]](#footnote-459) are provided in table below for HVAC fan operation which varies by building type:

|  |  |
| --- | --- |
| **Building Type** | **Pumps & Fans (annual Hours of operation)** |
| College/University | 4216 |
| Grocery | 5840 |
| Heavy Industry | 3585 |
| Hotel/Motel | 6872 |
| Light Industry | 2465 |
| Medical | 6871 |
| Office | 2301 |
| Restaurant | 4654 |
| Retail/Service | 3438 |
| School(K-12) | 2203 |
| Warehouse | 3222 |
| Average=Miscellaneous | 4103 |

ESF = Energy Savings Factor, the ESF for notched v-belt Installation is assumed to be 2%

**Summer Coincident Peak Demand Savings**

**EXAMPLE**

For example, an office building RTU with a 5 HP NEMA premium efficiency motor using the default hours of operation, motor load and 89.5% motor efficiency;

ΔkWh = kWconnected\* Hours \* ESF

= ((HP \* 0.746 kW/HP\* Load Factor)/Motor Efficiency) \* Hours \* ESF

= ((5 HP \* 0.746 kW/HP\* 80%) / 89.5%) \* 1766 Hours \* 2%

= 117.8 kWh Savings

ΔkW = kWconnected\* ESF

Where:

kWConnected = kW of equipment is calculated using motor efficiency.

= (HP \*0 .746 kW/HP\* Load Factor)/Motor Efficiency

Variables as provided above

**EXAMPLE**

For example, an office building RTU with a 5 HP NEMA premium efficiency motor using the default motor load and 89.5% motor efficiency;

ΔkW = kWconnected\* ESF

= ((HP \* 0.746 kW/HP\* Load Factor)/Motor Efficiency) \* ESF

= ((5 HP \* 0.746 kW/HP\* 80%) / 89.5%) \* 2%

= 0.0667 kW Savings

**Natural Gas Savings**

N/A

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-MSC-NVBE-V01-150601**

### Small Business Furnace Tune-Up

**Description**

This measure is for a natural gas Small Business furnace that provides space heating. The tune-up will improve furnace performance by inspecting, cleaning and adjusting the furnace and appurtenances for correct and efficient operation. Additional savings maybe realized through a complete system tune-up.

This measure was developed to be applicable to the following program types: Small business.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

To qualify for this measure an approved technician must complete the tune-up requirements[[459]](#footnote-460) listed below:

* Measure combustion efficiency using an electronic flue gas analyzer
* Check and clean blower assembly and components per manufacturer’s recommendations
* Where applicable Lubricate motor and inspect and replace fan belt if required
* Inspect for gas leaks
* Clean burner per manufacturer’s recommendations and adjust as needed
* Check ignition system and safety systems and clean and adjust as needed
* Check and clean heat exchanger per manufacturer’s recommendations
* Inspect exhaust/flue for proper attachment and operation
* Inspect control box, wiring and controls for proper connections and performance
* Check air filter and clean or replace per manufacturer’s
* Inspect duct work connected to furnace for leaks or blockages
* Measure temperature rise and adjust flow as needed
* Check for correct line and load volts/amps
* Check thermostat operation is per manufacturer’s recommendations (if adjustments made, refer to ‘Small Commercial Programmable Thermostat Adjustment’ measure for savings estimate)
* Perform Carbon Monoxide test and adjust heating system until results are within standard industry acceptable limits

**Definition of Baseline Equipment**

The baseline is furnace assumed not to have had a tune-up in the past 2 years.

**Deemed Lifetime of Efficient Equipment**

The measure life for the tune up is 2 years.[[460]](#footnote-461)

**Deemed Measure Cost**

The incremental cost for this measure should be the actual cost of tune up.

**Deemed O&M Cost Adjustments**

There are no expected O&M savings associated with this measure.

**Loadshape**

Loadshape C04 - Commercial Electric Heating

**Coincidence Factor**

N/A

**Algorithms**

**Calculation of Energy Savings**

**Electric Energy Savings**

ΔkWh = ΔTherms \* Fe \* 29.3

Where:

ΔTherms = as calculated below

Fe = Furnace Fan energy consumption as a percentage of annual fuel consumption

= 3.14%[[461]](#footnote-462)

29.3 = kWh per therm

**Summer Coincident Peak Demand Savings**

N/A

**Natural Gas Savings**

Δtherms = (Capacity \* EFLH \* (((Effbefore + Ei)/ Effbefore) – 1)) / 100,000

Where:

Capacity = Furnace gas input size (Btu/hr)

= Actual

EFLH       = Equivalent Full Load Hours for heating are provided in section 4.4 HVAC End Use

Effbefore = Efficiency of the furnace before the tune-up

= Actual

EI             = Efficiency Improvement of the furnace tune-up measure

= Actual

100,000 = Converts Btu to therms

**Example**

A 200 kBtu furnace in a Rockford low rise office records an efficiency prior to tune up of 82% AFUE and a 1.8% improvement in efficiency are tune up:

Δtherms = (200,000 \* 1497 \* (((0.82 + 0.018)/ 0.82) – 1)) /100,000

= 65.72 therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-HVC-FTUN-V01-150601**

## 

## Lighting End Use

The commercial lighting measures use a standard set of variables for hours or use, waste heat factors, coincident factors and HVAC interaction effects. This table has been developed based on information provided by the various stakeholders. For ease of review, the table is included here and referenced in each measure.

| **Building Type** | **Fixture Annual Operating Hours**[[462]](#footnote-463) | **[Screw based bulb Annual Operating hours](file:///O:\\Consulting\\Illinois_TRM\\Lighting%20Models\\Waste%20Heat%20Calculations1.xlsx" \l "RANGE!#REF!)**[[463]](#footnote-464) | **Waste Heat Cooling Energy WHFe**[[464]](#footnote-465) | **Waste Heat Cooling Demand**  **[WHFd](file:///O:\\Consulting\\Illinois_TRM\\Lighting%20Models\\Waste%20Heat%20Calculations1.xlsx" \l "RANGE!#REF!)**[[465]](#footnote-466) | **Coincid-ence Factor**  **[CF](file:///O:\\Consulting\\Illinois_TRM\\Lighting%20Models\\Waste%20Heat%20Calculations1.xlsx" \l "RANGE!#REF!)**[[466]](#footnote-467) | **Waste Heat Gas Heating**  **[IFTherms](file:///O:\\Consulting\\Illinois_TRM\\Lighting%20Models\\Waste%20Heat%20Calculations1.xlsx" \l "RANGE!#REF!)**[[467]](#footnote-468) | **Waste Heat Electric Resistance Heating**  **[IFkWh](file:///O:\\Consulting\\Illinois_TRM\\Lighting%20Models\\Waste%20Heat%20Calculations1.xlsx" \l "RANGE!#REF!)**[[468]](#footnote-469) | **Waste Heat Electric Heat Pump Heating**  **IFkWh** |
| --- | --- | --- | --- | --- | --- | --- | --- | --- |
| Assisted Living | 5,950 | 5,950 | 1.25 | 1.50 | 0.75 | 0.022 | 0.497 | 0.248 |
| College | 3,540 | 2,588 | 1.32 | 1.46 | 0.56 | 0.096 | 2.194 | 1.097 |
| Convenience Store | 5,802 | 3,650 | 1.34 | 1.53 | 0.69 | 0.022 | 0.504 | 0.252 |
| Elementary School | 2,422 | 2,118 | 1.31 | 1.40 | 0.22 | 0.028 | 0.634 | 0.317 |
| Garage | 3,540 | 3,540 | 1.00 | 1.00 | 1.00 | 0.000 | 0.000 | 0.000 |
| Garage, 24/7 lighting | 8,766 | 8,766 | 1.00 | 1.00 | 1.00 | 0.000 | 0.000 | 0.000 |
| Grocery | 5,802 | 3,650 | 1.14 | 1.35 | 0.69 | 0.024 | 0.553 | 0.276 |
| Healthcare Clinic | 5,095 | 4,207 | 1.34 | 1.47 | 0.75 | 0.010 | 0.218 | 0.109 |
| High School | 4,311 | 2,327 | 1.25 | 1.44 | 0.22 | 0.025 | 0.571 | 0.285 |
| Hospital - CAV no econ | 6,038 | 4,207 | 1.55 | 1.80 | 0.75 | 0.014 | 0.317 | 0.158 |
| Hospital - CAV econ | 6,038 | 4,207 | 1.37 | 1.80 | 0.75 | 0.014 | 0.318 | 0.159 |
| Hospital - VAV econ | 6,038 | 4,207 | 1.47 | 1.06 | 0.75 | 0.008 | 0.173 | 0.086 |
| Hospital - FCU | 6,038 | 4,207 | 1.50 | 1.37 | 0.75 | 0.001 | 0.028 | 0.014 |
| Manufacturing Facility | 5,041 | 2,629 | 1.03 | 1.38 | 0.89 | 0.011 | 0.257 | 0.128 |
| MF - High Rise - Common | 5,950 | 5,950 | 1.37 | 1.42 | 0.75 | 0.050 | 1.153 | 0.577 |
| MF - Mid Rise | 5,950 | 5,950 | 1.15 | 1.50 | 0.75 | 0.022 | 0.505 | 0.253 |
| Hotel/Motel - Guest | 777 | 777 | 1.17 | 1.55 | 0.21 | 0.024 | 0.539 | 0.269 |
| Hotel/Motel - Common | 5,311 | 4,542 | 1.20 | 1.56 | 0.21 | 0.007 | 0.164 | 0.082 |
| Movie Theater | 5,475 | 5,475 | 1.22 | 1.59 | 0.75 | 0.033 | 0.762 | 0.381 |
| Office - High Rise - CAV no econ | 4,439 | 3,088 | 1.52 | 1.42 | 0.66 | 0.019 | 0.440 | 0.220 |
| Office - High Rise - CAV econ | 4,439 | 3,088 | 1.48 | 1.52 | 0.66 | 0.019 | 0.433 | 0.216 |
| Office - High Rise - VAV econ | 4,439 | 3,088 | 1.35 | 1.58 | 0.66 | 0.020 | 0.453 | 0.227 |
| Office - High Rise - FCU | 4,439 | 3,088 | 1.31 | 2.19 | 0.66 | 0.011 | 0.252 | 0.126 |
| Office - Low Rise | 4,439 | 3,088 | 1.46 | 1.59 | 0.66 | 0.022 | 0.494 | 0.247 |
| Office - Mid Rise | 4,439 | 3,088 | 1.34 | 1.41 | 0.66 | 0.021 | 0.489 | 0.244 |
| Religious Building | 1,664 | 1,664 | 1.48 | 1.44 | 0.66 | 0.017 | 0.396 | 0.198 |
| Restaurant | 3,673 | 4,784 | 1.36 | 1.33 | 0.80 | 0.025 | 0.567 | 0.284 |
| Retail - Department Store | 4,719 | 2,935 | 1.24 | 1.49 | 0.83 | 0.022 | 0.502 | 0.251 |
| Retail - Strip Mall | 4,719 | 2,935 | 1.24 | 1.50 | 0.83 | 0.020 | 0.463 | 0.232 |
| Warehouse | 4,746 | 4,293 | 1.09 | 1.46 | 0.70 | 0.023 | 0.535 | 0.267 |
| Unknown | 4,683 | 3,612 | 1.31 | 1.53 | 0.66 | 0.023 | 0.524 | 0.262 |
| Exterior | 4,903 | 4,903 | 1.00 | 1.00 | 0.00 | 0.000 | 0.000 | 0.000 |
| Low-Use Small Business | 2,954 | 2,954 | 1.31 | 1.53 | 0.66 | 0.023 | 0.524 | 0.262 |
| Uncooled Building | Varies | varies | 1.00 | 1.00 | 0.66 | 0.014 | 0.320 | 0.160 |
| Refrigerated Cases | 5,802 | n/a | 1.29 | 1.29 | 0.69 | 0.000 | 0.000 | 0.000 |
| Freezer Cases | 5,802 | n/a | 1.50 | 1.5 | 0.69 | 0.000 | 0.000 | 0.000 |

### Commercial ENERGY STAR Compact Fluorescent Lamp (CFL)

###### Description

A low wattage ENERGY STAR qualified compact fluorescent screw-in bulb (CFL) is installed in place of a baseline screw-in bulb. This characterization assumes that the CFL is installed in a commercial location. If the implementation strategy does not allow for the installation location to be known a deemed split should be used. For Residential targeted programs (e.g. an upstream retail program), a deemed split of 96% Residential and 4% Commercial assumptions should be used[[469]](#footnote-470), and for Commercial targeted programs a deemed split of 4% Residential and 96% Commercial should be used[[470]](#footnote-471).

Federal legislation stemming from the Energy Independence and Security Act of 2007 (EISA) required all general-purpose light bulbs between 40W and 100W to be approximately 30% more energy efficient than current incandescent bulbs. Production of 100W, standard efficacy incandescent lamps ended in 2012 followed by restrictions on 75W in 2013 and 60W and 40W in 2014. The baseline for this measure has therefore become bulbs (improved incandescent or halogen) that meet the new standard.

Finally, a provision in the EISA regulations requires that by January 1, 2020, all lamps meet efficiency criteria of at least 45 lumens per watt, in essence making the baseline equivalent to a current day CFL. Therefore the measure life (number of years that savings should be claimed) should be reduced once the assumed lifetime of the bulb exceeds 2020. Due to expected delay in clearing retail inventory and to account for the operating life of a halogen incandescent potentially spanning over 2020, this shift is assumed not to occur until mid-2020.

This measure was developed to be applicable to the following program types: TOS, NC, RF. If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the high-efficiency equipment must be a standard ENERGY STAR qualified compact fluorescent lamp.

###### Definition of Baseline Equipment

The baseline equipment is assumed to be an EISA qualified incandescent or halogen as provided in the table provided in the Electric Energy Savings section.

###### Deemed Lifetime of Efficient Equipment

The expected measure life (number of years that savings should be claimed) should be calculated by dividing the rated life of the bulb (10,000 hours[[471]](#footnote-472)) by the run hours. For example using Miscellaneous at 4,589 hours would give 2.2 years. When the number of years exceeds June 2020, the number of years to that date should be used.

###### Deemed Measure Cost

The incremental capital cost assumption for all bulbs under 2600 lumens is $1.25, from June 2014 – May 2015, $1.6 from June 2015 to May 2016 and $1.70 from June 2017 to May 2018[[472]](#footnote-473).

For bulbs over 2600 lumens the assumed incremental capital cost is $5.

###### Loadshape

|  |
| --- |
| Loadshape C06 - Commercial Indoor Lighting |
| Loadshape C07 - Grocery/Conv. Store Indoor Lighting |
| Loadshape C08 - Hospital Indoor Lighting |
| Loadshape C09 - Office Indoor Lighting |
| Loadshape C10 - Restaurant Indoor Lighting |
| Loadshape C11 - Retail Indoor Lighting |
| Loadshape C12 - Warehouse Indoor Lighting |
| Loadshape C13 - K-12 School Indoor Lighting |
| Loadshape C14 - Indust. 1-shift (8/5) (e.g., comp. air, lights) |
| Loadshape C15 - Indust. 2-shift (16/5) (e.g., comp. air, lights) |
| Loadshape C16 - Indust. 3-shift (24/5) (e.g., comp. air, lights) |
| Loadshape C17 - Indust. 4-shift (24/7) (e.g., comp. air, lights) |
| Loadshape C18 - Industrial Indoor Lighting |
| Loadshape C19 - Industrial Outdoor Lighting |
| Loadshape C20 - Commercial Outdoor Lighting |

###### Coincidence Factor

The summer peak coincidence factor for this measure is dependent on the location type. Values are provided for each building type in section 4.5.

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh =((WattsBase-WattsEE)/1000) \* ISR \* Hours \* WHFe

Where:

WattsBase = Actual (if retrofit measure) or based on lumens of CFL bulb and program year installed:

|  |  |  |
| --- | --- | --- |
| Minimum Lumens | Maximum Lumens | Incandescent Equivalent  Post-EISA 2007  (WattsBase) |
| 5280 | 6209 | 300 |
| 3000 | 5279 | 200 |
| 2601 | 2999 | 150 |
| 1490 | 2600 | 72 |
| 1050 | 1489 | 53 |
| 750 | 1049 | 43 |
| 310 | 749 | 29 |
| 250 | 309 | 25 |

WattsEE = Actual wattage of CFL purchased or installed

ISR = In Service Rate or the percentage of units rebated that get installed.

=100%[[473]](#footnote-474) if application form completed with sign off that equipment is not placed into storage

If sign off form not completed assume the following 3 year ISR assumptions:

|  |  |  |  |
| --- | --- | --- | --- |
| **Weighted Average 1st year In Service Rate (ISR)** | **2nd year Installations** | **3rd year Installations** | **Final Lifetime In Service Rate** |
| 71%[[474]](#footnote-475) | 14.5% | 12.3% | 98.0%[[475]](#footnote-476) |

Hours = Average hours of use per year are provided in Reference Table in Section 4.5,Screw based bulb annual operating hours, for each building type[[476]](#footnote-477). If unknown use the Miscellaneous value.

WHFe = Waste heat factor for energy to account for cooling energy savings from efficient lighting are provided below for each building type in Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

For example, a 14W standard CFL is installed in an office in 2014 and sign off form provided:

ΔkWh = (((43 - 14)/1000)\* 1.0 \* 3088 \* 1.25

= 111.9 kWh

###### Heating Penalty

If electrically heated building:

ΔkWhheatpenalty[[477]](#footnote-478) = (((WattsBase-WattsEE)/1000) \* ISR \* Hours \* -IFkWh

Where:

IFkWh = Lighting-HVAC Interation Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficent lighting. Values are provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

For example, a 14W standard CFL is installed in a heat pump heated office in 2014 and sign off form provided:

ΔkWhheatpenalty = (((43 - 14)/1000)\* 1.0\*3088\*-0.183

= - 16.4 kWh

###### Deferred Installs

As presented above, if a sign off form is not completed the characterization assumes that a percentage of bulbs purchased are not installed until Year 2 and Year 3 (see ISR assumption above). The Illinois Technical Advisory Committee has determined the following methodology for calculating the savings of these future installs.

Year 1 (Purchase Year) installs: Characterized using assumptions provided above or evaluated assumptions if available.

Year 2 and 3 installs: Characterized using delta watts assumption and hours of use from the Install Year i.e. the actual deemed (or evaluated if available) assumptions active in Year 2 and 3 should be applied.

The NTG factor for the Purchase Year should be applied.

For example, for a 14W CFL (60W standard incandescent and 43W EISA qualified incandescent/halogen) purchased in 2014 and using miscellaneous hours assumption.

ΔkWH1st year installs = ((43 - 14) / 1000) \* 0.755 \* 3198 \* 1.06

= 74.2 kWh

ΔkWH2nd year installs = ((43 - 14) / 1000) \* 0.121 \* 3198 \* 1.06

= 11.9 kWh

Note: Here we assume no change in hours assumption. NTG value from Purchase year applied.

ΔkWH3rd year installs = ((43 - 14) / 1000) \* 0.103 \* 3198 \* 1.06

= 10.1 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = ((WattsBase-WattsEE)/1000) \* ISR \* WHFd \* CF

Where:

WHFd = Waste heat factor for demand to account for cooling savings from efficient lighting in cooled buildings is provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value..

CF = Summer Peak Coincidence Factor for measure is provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value..

Other factors as defined above

For example, a 14W standard CFLis installed in an office in 2014 and sign off form provided:

ΔkW = ((43 - 14)/1000)\*1.0\*1.3\*0.66

= 0.025kW

###### Natural Gas Energy Savings

Heating Penalty if fossil fuel heated building (or if heating fuel is unknown):

ΔTherms[[478]](#footnote-479) = (((WattsBase-WattsEE)/1000) \* ISR \* Hours \*- IFTherms

Where:

IFTherms = Lighting-HVAC Interation Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficent lighting. Values are provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

Other factors as defined above

For example, a 14W standard CFL is installed in an office in 2014 and sign off form provided:

ΔTherms = (((43 - 14)/1000)\* 1.0\*3088\*-0.016

= - 1.4 Therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

Bulb replacement costs assumed in the O&M calculations are provided below[[479]](#footnote-480).

|  |  |  |
| --- | --- | --- |
|  | **Std Inc.** | **EISA Compliant Halogen** |
| 2014 | $0.34 | $1.25 |
| 2015 | $0.34 | $0.90 |
| 2016 | $0.34 | $0.80 |
| 2017 | $0.34 | $0.70 |
| 2018 | $0.34 | $0.60 |
| 2019 | $0.34 | $0.60 |
| 2020 & after | $0.34 | N/A |

In order to account for the falling EISA Qualified bulb replacement cost provided above, an equivalent annual levelized baseline replacement cost over the lifetime of the CFL bulb is calculated. Note that the measure life for these measures is capped to the number of years remaining until 2020.

The NPV for replacement lamps and annual levelized replacement costs using the statewide real discount rate of 5.23% are presented below:

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| **Location** | **Lumen Level** | **NPV of replacement costs for period** | | | **Levelized annual replacement cost savings** | | |
| **June 2014 - May 2015** | **June 2015 - May 2016** | **June 2016 - May 2017** | **June 2014 - May 2015** | **June 2015 - May 2016** | **June 2016 - May 2017** |
| Commercial | Lumens <310 or >2600 (EISA exempt) | $2.83 | $2.83 | $2.83 | $1.40 | $1.40 | $1.40 |
| Lumens ≥ 310 and ≤ 2600 (EISA compliant) | $8.60 | $6.91 | $6.08 | $4.26 | $3.43 | $3.02 |
| Multi Family Common Areas | Lumens <310 or >2600 (EISA exempt) | $2.88 | $2.88 | $2.88 | $1.81 | $1.81 | $1.81 |
| Lumens ≥ 310 and ≤ 2600 (EISA compliant) | $9.27 | $7.24 | $6.40 | $5.84 | $4.56 | $4.03 |

For halogen bulbs, we assume the same replacement cycle as incandescent bulbs.[[480]](#footnote-481) The replacement cycle is based on the miscellaneous hours of use. Both incandescent and halogen lamps are assumed to last for 1,000 hours before needing replacement.

###### Measure Code: CI-LTG-CCFL-V05-150601

### Fluorescent Delamping

###### Description

This measure addresses the permanent removal of existing 8’, 4’, 3’ and 2’ fluorescent lamps. Unused lamps, lamp holders, and ballasts must be permanently removed from the fixture. This measure is applicable when retrofitting from T12 lamps to T8 lamps or simply removing lamps from a T8 fixture. Removing lamps from a T12 fixture that is not being retrofitted with T8 lamps are not eligible for this incentive.

Customers are responsible for determining whether or not to use reflectors in combination with lamp removal in order to maintain adequate lighting levels. Lighting levels are expected to meet the Illuminating Engineering Society of North America (IESNA) recommended light levels. Unused lamps, lamp holders, and ballasts must be permanently removed from the fixture and disposed of in accordance with local regulations. A pre-approval application is required for lamp removal projects.

This measure was developed to be applicable to the following program types: RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

Savings are defined on a per removed lamp basis. The retrofit wattage (efficient conditioned) is therefore assumed to be zero. The savings numbers provided below are for the straight lamp removal measures, as well as the lamp removal and install reflector measures. The lamp installed/retrofit is captured in another measure.

###### Definition of Baseline Equipment

The baseline condition is either a T12 or a T8 lamp with default wattages provided below. Note, if the program does not allow for the lamp type to be known, then a T12:T8 weighting of 80%:20% can be applied[[481]](#footnote-482).

###### Deemed Lifetime of Efficient Equipment

The measure life is assumed to be 11 years per DEER 2005.

###### Deemed Measure Cost

The incremental capital cost is provided in the table below:

|  |  |  |
| --- | --- | --- |
| **Measure Category** | **Value** | **Source** |
| 8-Foot Lamp Removal | $16.00 | ComEd/KEMA regression[[482]](#footnote-483) |
| 4-Foot Lamp Removal | $12.00 | ICF Portfolio Plan |
| 8-Foot Lamp Removal with reflector | $30.00 | KEMA Assumption |
| 4-Foot Lamp Removal with reflector | $25.00 | KEMA Assumption |
| 2-Foot or 3-Foot Removal | $12.35 | KEMA Assumption |
| 2-Foot or 3-Foot Removal with reflector | $25.70 | KEMA Assumption |

###### Loadshape

|  |
| --- |
| Loadshape C06 - Commercial Indoor Lighting |
| Loadshape C07 - Grocery/Conv. Store Indoor Lighting |
| Loadshape C08 - Hospital Indoor Lighting |
| Loadshape C09 - Office Indoor Lighting |
| Loadshape C10 - Restaurant Indoor Lighting |
| Loadshape C11 - Retail Indoor Lighting |
| Loadshape C12 - Warehouse Indoor Lighting |
| Loadshape C13 - K-12 School Indoor Lighting |
| Loadshape C14 - Indust. 1-shift (8/5) (e.g., comp. air, lights) |
| Loadshape C15 - Indust. 2-shift (16/5) (e.g., comp. air, lights) |
| Loadshape C16 - Indust. 3-shift (24/5) (e.g., comp. air, lights) |
| Loadshape C17 - Indust. 4-shift (24/7) (e.g., comp. air, lights) |
| Loadshape C18 - Industrial Indoor Lighting |
| Loadshape C19 - Industrial Outdoor Lighting |
| Loadshape C20 - Commercial Outdoor Lighting |

###### Coincidence Factor

The summer peak coincidence factor for this measure is dependent on the location type. Values are provided for each building type in the reference section below.

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh =((WattsBase-WattsEE)/1000) \* ISR \* Hours \* WHFe

Where:

WattsBase = Assume wattage reduction of lamp removed

|  |  |  |  |
| --- | --- | --- | --- |
|  | **Wattage of lamp removed**[[483]](#footnote-484) | | **Weighted average** |
|  | **T8** | **T12** | **80% T12, 20% T8** |
| 8-ft T8 | 38.6 | 60.3 | 56.0 |
| 4-ft T8 | 19.4 | 33.7 | 30.8 |
| 3-ft T8 | 14.6 | 40.0 | 34.9 |
| 2-ft T8 | 9.8 | 28.0 | 24.4 |

WattsEE = 0

ISR = In Service Rate or the percentage of units rebated that get installed.

=100% if application form completed with sign off that equipment permanently removed and disposed of.

Hours = Average hours of use per year are provided in Reference Table in Section 4.5. If unknown use the Miscellaneous value.

WHFe = Waste heat factor for energy to account for cooling energy savings from efficient lighting are provided below for each building type in Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

For example, delamping a 4 ft T8 fixture in an office building:

ΔkWh =((19.4 - 0)/1000) \* 1.0 \* 4439 \* 1.25

= 107.6 kWh

###### Heating Penalty

If electrically heated building:

ΔkWhheatpenalty[[484]](#footnote-485) = (((WattsBase-WattsEE)/1000) \* ISR \* Hours \* -IFkWh

Where:

IFkWh = Lighting-HVAC Interation Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficent lighting. Values are provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

For example, delamping a 4 ft T8 fixture in a heat pump heated office building:

ΔkWhheatpenalty =((19.4 - 0)/1000) \* 1.0 \* 4439 \* -0.151

=-13.0 kWh

###### Summer Coincident Peak Demand Savings

ΔkW= ((WattsBase-WattsEE)/1000) \* ISR \* WHFd \* CF

Where:

WHFd = Waste heat factor for demand to account for cooling savings from efficient lighting in cooled buildings is provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value..

CF = Summer Peak Coincidence Factor for measure is provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value..

Other factors as defined above

For example, delamping a 4 ft T8 fixture in an office building:

ΔkWh =((19.4 - 0)/1000) \* 1.0 \* 1.3 \* 0.66

= 0.017 kW

###### Natural Gas Energy Savings

Heating Penalty if fossil fuel heated building (or if heating fuel is unknown):

ΔTherms[[485]](#footnote-486) = (((WattsBase-WattsEE)/1000) \* ISR \* Hours \*- IFTherms

Where:

IFTherms = Lighting-HVAC Interation Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficent lighting. Values are provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

Other factors as defined above

For example, delamping a 4 ft T8 fixture in an office building:

ΔTherms =((19.4 - 0)/1000) \* 1.0 \* 4439 \* -0.016

=-1.4 therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-LTG-DLMP-V02-140601

### High Performance and Reduced Wattage T8 Fixtures and Lamps

**Description**

This measure applies to “High Performance T8” (HPT8) lamp/ballast systems that have higher lumens per watt than standard T8 systems. This measure applies to the installation of new equipment with efficiencies that exceed that of the equipment that would have been installed following standard market practices and is applicable to time of sale as well as retrofit measures. Retrofit measures may include new fixtures or relamp/reballast measures. In addition, options have been provided to allow for the “Reduced Wattage T8 lamps” or RWT8 lamps that result in re-lamping opportunities that produce equal or greater light levels than standard T8 lamps while using fewer watts.

If the implementation strategy does not allow for the installation location to be known, a deemed split of 99% Commercial and 1% Residential should be used[[486]](#footnote-487).

This measure was developed to be applicable to the following program types: TOS, RF, DI.

If applied to other program types, the measure savings should be verified.

The measure applies to all commercial HPT8 installations excluding new construction and major renovation or change of use measures (see lighting power density measure). Lookup tables have been provided to account for the different types of installations. Whenever possible, actual costs and hours of use should be utilized for savings calculations. Default new and baseline assumptions have been provided in the reference tables. Default component costs and lifetimes have been provided for Operating and Maintenance Calculations. Please see the Definition Table to determine applicability for each program. HPT8 configurations not included in the TRM may be included in custom program design using the provided algorithms as long as energy savings is achieved. The following table defines the applicability for different programs

| **Time of Sale (TOS)** | **Retrofit (RF) and Direct Install (DI)** |
| --- | --- |
| This measure relates to the installation of new equipment with efficiency that exceeds that of equipment that would have been installed following standard market practices. In general, the measure will include qualifying high efficiency low ballast factor ballasts paired with high efficiency long life lamps as detailed in the attached tables. High-bay applications use this system paired with qualifying high ballast factor ballasts and high performance 32 w lamps. Custom lighting designs can use qualifying low, normal or high ballast factor ballasts and qualifying lamps in lumen equivalent applications where total system wattage is reduced when calculated using the Calculation of Savings Algorithms. | This measure relates to the replacement of existing equipment with new equipment with efficiency that exceeds that of the existing equipment. In general, the retrofit will include qualifying high efficiency low ballast factor ballasts paired with high efficiency long life lamps as detailed in the attached tables. Custom lighting designs can use qualifying low, normal or high ballast factor ballasts and qualifying lamps in lumen equivalent applications where total system wattage is reduced when calculated using the Calculation of Savings Algorithms.  High efficiency troffers (new/or retrofit) utilizing HPT8 technology can provide even greater savings. When used in a high-bay application, high-performance T8 fixtures can provide equal light to HID high-bay fixtures, while using fewer watts; these systems typically utilize high ballast factor ballasts, but qualifying low and normal ballast factor ballasts may be used when appropriate light levels are provided and overall wattage is reduced. |

**Definition of Efficient Equipment**

The definition of efficient equipment varies based on the program and is defined below:

|  |  |
| --- | --- |
| **Time of Sale (TOS)** | **Retrofit (RF) and Direct Install (DI)** |
| In order for this characterization to apply, new lamps and ballasts must be listed on the CEE website on the qualifying High Performance T8 lamps and ballasts list (<http://www.cee1.org/com/com-lt/com-lt-main.php3>).    High efficiency troffers combined with high efficiency lamps and ballasts allow for fewer lamps to be used to provide a given lumen output. High efficiency troffers must have a fixture efficiency of 80% or greater to qualify. Default values are given for a 2 lamp HPT8 fixture replacing a 3 lamp standard efficiency T8 fixture, but other configurations may qualify and the Calculation of savings algorithm used to account for base watts being replaced with EE watts.  High bay fixtures must have fixture efficiencies of 85% or greater.  RWT8 lamps: In order for this characterization to apply, new 4' and U-tube lamps must be listed on the CEE website on the qualifying Reduced Wattage High Performance T8 lamps list. (http://library.cee1.org/content/commercial-lighting-qualifying-products-lists). 2', 3' and 8' lamps must meet the wattage requirements specified in the RWT8 new and baseline assumptions table. This measure assumes a lamp only purchase. | In order for this characterization to apply, new lamps and ballasts must be listed on the CEE website on the qualifying High Performance T8 lamps and ballasts list ([http://www.cee1.org/com/com-lt/com-lt-main.php3](http://www.ilsag.org/questions)).  High efficiency troffers (new or retrofit kits) combined with high efficiency lamps and ballasts allow for fewer lamps to be used to provide a given lumen output. High efficiency troffers must have a fixture efficiency of 80% or greater to qualify. Default values are given for a 2 lamp HPT8 fixture replacing a 3 lamp standard efficiency T8 fixture, but other configurations may qualify and the Calculation of savings algorithm used to account for base watts being replaced with EE watts.  High bay fixtures will have fixture efficiencies of 85% or greater.  RWT8: in order for this characterization to apply, new 4' and U-tube lamps must be listed on the CEE website on the qualifying Reduced Wattage High Performance T8 lamps list.  (http://library.cee1.org/content/commercial-lighting-qualifying-products-lists). 2', 3' and 8' lamps must meet the wattage requirements specified in the RWT8 new and baseline assumptions table. |

**Definition of Baseline Equipment**

The definition of baseline equipment varies based on the program and is defined below:

|  |  |
| --- | --- |
| **Time of Sale (TOS)** | **Retrofit (RF) and Direct Install (DI)** |
| The baseline is standard efficiency T8 systems that would have been installed. The baseline for high-bay fixtures is pulse start metal halide fixtures, the baseline for a 2 lamp high efficiency troffer is a 3 lamp standard efficency troffer. | The baseline is the existing system.  Due to new federal standards for linear fluorescent lamps, manufacturers of T12 lamps will not be permitted to manufacture most varieties of T12 lamps for sale in the United States after July 2012. All remaining stock and previously manufactured product may be sold after the July 2012 effective date. If a customer relamps an existing T12 fixture the day the standard takes effect, an assumption can be made that they would likely need to upgrade to, at a minimum, 800-series T8s in less than 5 years’ time. This assumes the T12s installed have a typical rated life of 20,000 hours and are operated for 4500 hours annually (average miscellaneous hours 4576/year). Certainly, it is not realistic that everyone would wait until the final moment to relamp with T12s. Also, the exempted T12 lamps greater than 87 CRI will continue to be available to purchase, although they will be expensive. Therefore the more likely scenario would be a gradual shift to T8s over the 4 year timeframe. In other words, we can expect that for each year between 2012 and 2016, ~20% of the existing T12 lighting will change over to T8 lamps that comply with the federal standard. To simplify this assumption, we recommend assuming that standard T8s become the baseline for all T12 linear fluorescent retrofit January 1, 2016. There will be a baseline shift applied to all measures installed before 2016. See table C-1. |

**Deemed Lifetime of Efficient Equipment**

The deemed lifetime of efficient equipment varies based on the program and is defined below:

|  |  |
| --- | --- |
| **Time of Sale (TOS)** | **Retrofit (RF) and Direct Install (DI)** |
| Fixture lifetime is 15 years[[487]](#footnote-488).  Fixture retrofits which utilize RWT8 lamps have a lifetime equivalent to the life of the lamp, capped at 15 years. There is no guarantee that a reduced wattage lamp will be installed at time of burnout, but if one is, savings will be captured in the RWT8 measure below.  RWT8 lifetime is the life of the product, at the reported operating hours (lamp life in hours divided by operating hours per year – see reference table "RWT8 Component Costs and Lifetime"), capped at 15 years.[[488]](#footnote-489) | Fixture lifetime is 15 years.  As per explanation above, for existing T12 fixtures, a mid life baseline shift should be applied in Jan 2016 as described in table C-1.  Note, since the fixture lifetime is deemed at 15 years, the replacement cost of both the lamp and ballast should be incorporated in to the O&M calculation. |

**Loadshape**

|  |
| --- |
| Loadshape C06 - Commercial Indoor Lighting |
| Loadshape C07 - Grocery/Conv. Store Indoor Lighting |
| Loadshape C08 - Hospital Indoor Lighting |
| Loadshape C09 - Office Indoor Lighting |
| Loadshape C10 - Restaurant Indoor Lighting |
| Loadshape C11 - Retail Indoor Lighting |
| Loadshape C12 - Warehouse Indoor Lighting |
| Loadshape C13 - K-12 School Indoor Lighting |
| Loadshape C14 - Indust. 1-shift (8/5) (e.g., comp. air, lights) |
| Loadshape C15 - Indust. 2-shift (16/5) (e.g., comp. air, lights) |
| Loadshape C16 - Indust. 3-shift (24/5) (e.g., comp. air, lights) |
| Loadshape C17 - Indust. 4-shift (24/7) (e.g., comp. air, lights) |
| Loadshape C18 - Industrial Indoor Lighting |
| Loadshape C19 - Industrial Outdoor Lighting |
| Loadshape C20 - Commercial Outdoor Lighting |

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

ΔkWh =( (Wattsbase-WattsEE)/1000) \* Hours \*WHFe\*ISR

Where:

Wattsbase = Input wattage of the existing system which depends on the baseline fixture configuration (number and type of lamp) and number of fixtures. Value can be selected from the appropriate reference table as shown below, of a custom value can be entered if the configurations in the tables is not representative of the exisitng system.

|  |  |
| --- | --- |
| **Program** | **Reference Table** |
| Time of Sale | A-1: HPT8 New and Baseline Assumptions |
| Retrofit | A-2: HPT8 New and Baseline Assumptions |
| Reduced Wattage T8, time of sale or retrofit | A-3: RWT8 New and Baseline Assumptions |

WattsEE = New Input wattage of EE fixture which depends on new fixture configuration (number of lamps) and ballast factor and number of fixtures. Value can be selected from the appropriate reference table as shown below, of a custom value can be entered if the configurations in the tables is not representative of the exisitng system.

|  |  |
| --- | --- |
| **Program** | **Reference Table** |
| Time of Sale | A-1: HPT8 New and Baseline Assumptions |
| Retrofit | A-2: HPT8 New and Baseline Assumptions |
| Reduced Wattage T8, time of sale or retrofit | A-3: RWT8 New and Baseline Assumptions |

Hours = Average hours of use per year as provided by the customer or selected from the Reference Table in Section 4.5,Fixture annual operating hours. If hours or building type are unknown, use the Miscellaneous value.

WHFe = Waste heat factor for energy to account for cooling energy savings from efficient lighting is selected from the Reference Table in Section 4.5 for each building type. If building is un-cooled, the value is 1.0.

ISR = In Service Rate or the percentage of units rebated that get installed.

=100%[[489]](#footnote-490) if application form completed with sign off that equipment is not placed into storage

If sign off form not completed assume the following 3 year ISR assumptions:

|  |  |  |  |
| --- | --- | --- | --- |
| **Weighted Average 1st year In Service Rate (ISR)** | **2nd year Installations** | **3rd year Installations** | **Final Lifetime In Service Rate** |
| 9698%[[490]](#footnote-491) | 1.0% | 0.90% | 98.0%[[491]](#footnote-492) |

**Heating Penalty**

If electrically heated building:

ΔkWhheatpenalty[[492]](#footnote-493) = (((WattsBase-WattsEE)/1000) \* ISR \* Hours \* -IFkWh

Where:

IFkWh = Lighting-HVAC Interation Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficent lighting. Values are provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

**Summer Coincident Demand Savings**

ΔkW =( (Wattsbase-WattsEE)/1000) \* WHFd\*CF\*ISR

Where:

WHFd = Waste Heat Factor for Demand to account for cooling savings from efficient lighting in cooled buildings is selected from the Reference Table in Section 4.5 for each building type. If the building is not cooled WHFd is 1.

CF = Summer Peak Coincidence Factor for measure is selected from the Reference Table in Section 4.5 for each building type. If the building type is unknown, use the Miscellaneous value of 0.66.

Other factors as defined above

**Natural Gas Savings**

ΔTherms[[493]](#footnote-494) = (((WattsBase-WattsEE)/1000) \* ISR \* Hours \*- IFTherms

Where:

IFTherms = Lighting-HVAC Integration Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Please select from the Reference Table in Section 4.5 for each building type.

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

See Reference tables for Operating and Maintenance Values

|  |  |
| --- | --- |
| **Program** | **Reference Table** |
| Time of Sale | B-1: HPT8 Component Costs and Lifetime |
| Retrofit | B-2: HPT8 Component Costs and Lifetime |
| Reduced Wattage T8, time of sale or retrofit | B-3: HPT8 Component Costs and Lifetime |

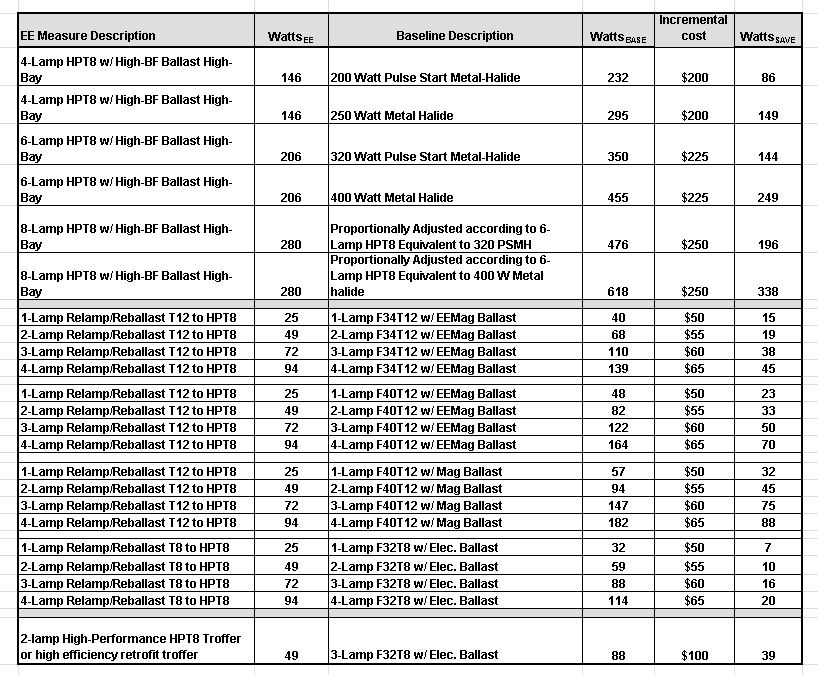
**Reference Tables**

See following page

A-1: Time of Sale: HPT8 New and Baseline Assumptions[[494]](#footnote-495)

| **EE Measure Description** | **WattsEE** | **Baseline Description** | **WattsBASE** | **Measure Cost** | **WattsSAVE** |
| --- | --- | --- | --- | --- | --- |
| 4-Lamp HPT8 w/ High-BF Ballast High-Bay | 146 | 200 Watt Pulse Start Metal-Halide | 232 | $75 | 86 |
| 6-Lamp HPT8 w/ High-BF Ballast High-Bay | 221 | 320 Watt Pulse Start Metal-Halide | 350 | $75 | 129 |
| 8-Lamp HPT8 w/ High-BF Ballast High-Bay | 280 | Proportionally Adjusted according to 6-Lamp HPT8 Equivalent to 320 PSMH | 455 | $75 | 175 |
|  |  |  |  |  |  |
| 1-Lamp HPT8-high performance 32 w lamp | 25 | 1-Lamp Standard F32T8 w/ Elec. Ballast | 32 | $15 | 7 |
| 1-Lamp HPT8-high performance 28 w lamp | 22 | 1-Lamp Standard F32T8 w/ Elec. Ballast | 32 | $15 | 10 |
| 1-Lamp HPT8-high performance 25 w lamp | 19 | 1-Lamp Standard F32T8 w/ Elec. Ballast | 32 | $15 | 13 |
| 2-Lamp HPT8 -high performance 32 w lamp | 49 | 2-Lamp Standard F32T8 w/ Elec. Ballast | 59 | $18 | 10 |
| 2-Lamp HPT8-high performance 28 w lamp | 43 | 2-Lamp Standard F32T8 w/ Elec. Ballast | 59 | $18 | 16 |
| 2-Lamp HPT8-high performance 25 w lamp | 35 | 2-Lamp Standard F32T8 w/ Elec. Ballast | 59 | $18 | 24 |
| 3-Lamp HPT8-high performance 32 w lamp | 72 | 3-Lamp Standard F32T8 w/ Elec. Ballast | 88 | $20 | 16 |
| 3-Lamp HPT8-high performance 28 w lamp | 65 | 3-Lamp Standard F32T8 w/ Elec. Ballast | 88 | $20 | 23 |
| 3-Lamp HPT8-high performance 25 w lamp | 58 | 3-Lamp Standard F32T8 w/ Elec. Ballast | 88 | $20 | 30 |
| 4-Lamp HPT8 -high performance 32 w lamp | 94 | 4-Lamp Standard F32T8 w/ Elec. Ballast | 114 | $23 | 20 |
| 4-Lamp HPT8-high performance 28 w lamp | 86 | 4-Lamp Standard F32T8 w/ Elec. Ballast | 114 | $23 | 28 |
| 4-Lamp HPT8-high performance 25 w lamp | 77 | 4-Lamp Standard F32T8 w/ Elec. Ballast | 114 | $23 | 37 |
|  |  |  |  |  |  |
| 2-lamp High-Performance HPT8 Troffer | 49 | 3-Lamp F32T8 w/ Elec. Ballast | 88 | $100 | 39 |
|  |  |  |  |  |  |
| Table developed using a constant ballast factor of .77. Input wattages are an average of manufacturer inputs that account for ballast efficacy | |  |  |  |  |

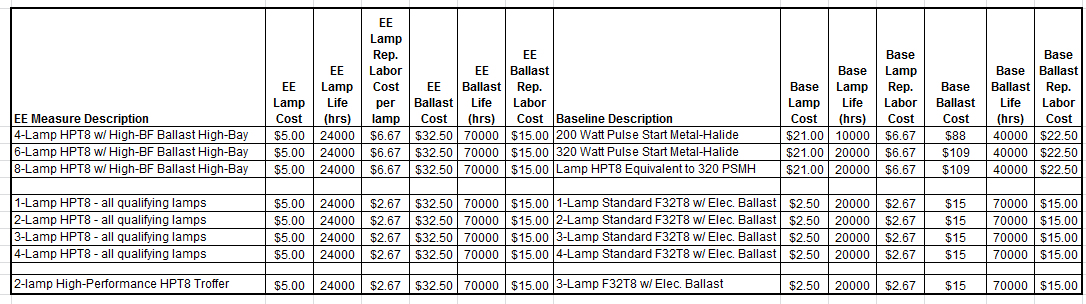
A-2: Retrofit HPT8 New and Baseline Assumptions[[495]](#footnote-496) (Note see definiton for validity after 2016)



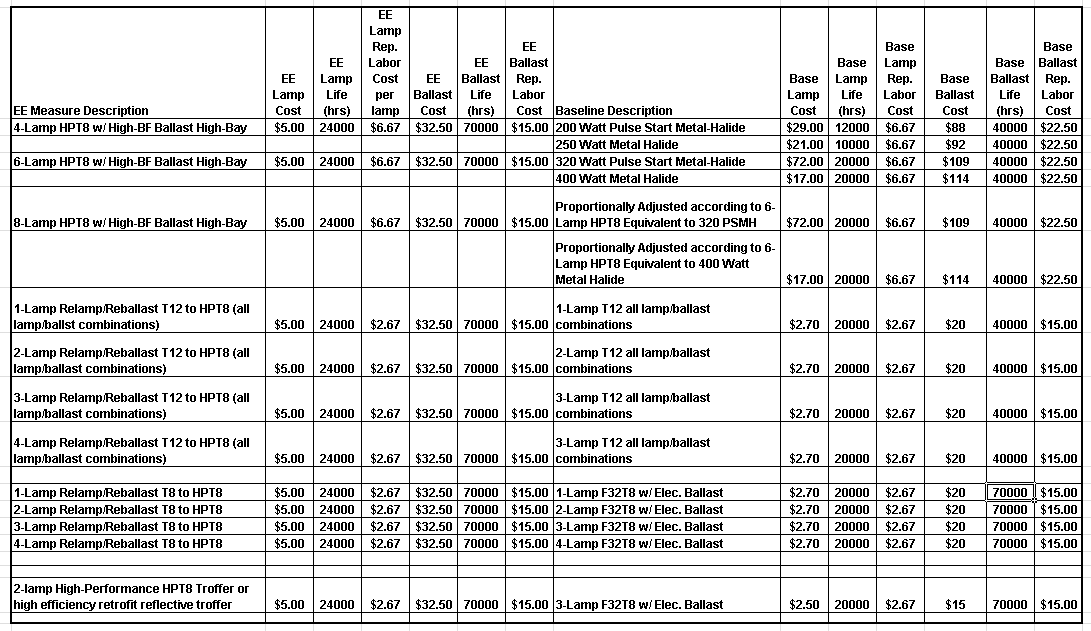
A– 3: RWT8 New and Baseline Assumptions



B-1: Time of Sale T8 Component Costs and Lifetime[[496]](#footnote-497)



B-2: T8 Retrofit Component Costs and Lifetime[[497]](#footnote-498)



B-3: Reduced Wattage T8 Component Costs and Lifetime[[498]](#footnote-499)



C-1: T12 Baseline Adjustment:

For measures installed in 2012 through 2015, the full savings (as calculated above in the Algorithm section) will be claimed through 2015.  A savings adjustment will be applied to the annual savings for the remainder of the measure life.  The adjustment to be applied for each measure is listed in the reference table below.

|  |  |  |  |
| --- | --- | --- | --- |
| Savings Adjustment Factors |  |  |  |
| **EE Measure Description** | **Savings Adjustment T12 EEmag ballast and 34 w lamps to HPT8** | **Savings Adjustment T12 EEmag ballast and 40 w lamps to HPT8** | **Savings Adjustment T12 mag ballast and 40 w lamps to HPT8** |
| 1-Lamp Relamp/Reballast T12 to HPT8 | 47% | 30% | 20% |
| 2-Lamp Relamp/Reballast T12 to HPT8 | 53% | 30% | 22% |
| 3-Lamp Relamp/Reballast T12 to HPT8 | 42% | 38% | 21% |
| 4-Lamp Relamp/Reballast T12 to HPT8 | 44% | 29% | 23% |

Measures installed in 2012 will claim full savings for four years, 2013 for three years, 2014 two years and 2015 one year.  Savings adjustment factors will be applied to the full savings for savings starting in 2016 and for the remainder of the measure life.  The savings adjustment is equal to the ratio between wattage reduction from T8 baseline to HPT8 and wattage reduction from T12 EE ballast with 40 w lamp baseline from the table ‘T8 New and Baseline Assumptions’.[[499]](#footnote-500)

Example: 2 lamp T8 to 2 lamp HPT8 retrofit saves 10 watts, while the T12 EE with 40 w lamp to HPT8 saves 33 watts. Thus the ratio of wattage reduced is 30%. Thus the ratio of wattage reduced is 30%.

**Measure Code: CI-LTG-T8FX-V04-150601**

### LED Bulbs and Fixtures

###### Description

This characterization provides savings assumptions for a variety of LED lamps including Omnidirectional (e.g. A-Type lamps), Decorative (e.g. Globes and Torpedoes) and Directional (PAR Lamps, Reflectors, MR16), and fixtures including refrigerated case, recessed and outdoor/garage fixtures.

If the implementation strategy does not allow for the installation location to be known, a deemed split of 96% Commercial and 4% Residential should be used[[500]](#footnote-501).

This measure was developed to be applicable to the following program types:  TOS, NC, RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, new lamps must be Energy Star labeled. Lamps and fixtures should be found in the reference tables below. Fixtures must be Energy Star labeled or on the Design Lights Consortium qualifying fixture list.

###### Definition of Baseline Equipment

Refer to the baseline tables. In 2012, Federal legislation stemming from the Energy Independence and Security Act of 2007 (EIAS) required all general-purpose light bulbs between 40 watts and 100 watts to have ~30% increased efficiency, essentially phasing out standard incandescent technology. In 2012, the 100 w lamp standards apply; in 2013 the 75 w lamp standards will apply, followed by restrictions on the 60 w and 40 w lamps in 2014.

###### Deemed Lifetime of Efficient Equipment

Lifetime is the life of the product, at the reported operating hours (lamp life in hours divided by operating hours per year – see reference table "LED component Costs and Lifetime." The analysis period is the same as the lifetime, capped at 15 years. (15 years from GDS Measure Life Report, June 2007).

###### Deemed Measure Cost

Wherever possible, actual incremental costs should be used. Refer to reference table “LED component Cost & Lifetime” for defaults.

###### Loadshape

|  |
| --- |
| Loadshape C06 - Commercial Indoor Lighting |
| Loadshape C07 - Grocery/Conv. Store Indoor Lighting |
| Loadshape C08 - Hospital Indoor Lighting |
| Loadshape C09 - Office Indoor Lighting |
| Loadshape C10 - Restaurant Indoor Lighting |
| Loadshape C11 - Retail Indoor Lighting |
| Loadshape C12 - Warehouse Indoor Lighting |
| Loadshape C13 - K-12 School Indoor Lighting |
| Loadshape C14 - Indust. 1-shift (8/5) (e.g., comp. air, lights) |
| Loadshape C15 - Indust. 2-shift (16/5) (e.g., comp. air, lights) |
| Loadshape C16 - Indust. 3-shift (24/5) (e.g., comp. air, lights) |
| Loadshape C17 - Indust. 4-shift (24/7) (e.g., comp. air, lights) |
| Loadshape C18 - Industrial Indoor Lighting |
| Loadshape C19 - Industrial Outdoor Lighting |
| Loadshape C20 - Commercial Outdoor Lighting |

###### Coincidence Factor

The summer peak coincidence factor for this measure is dependent on the location type. Values are provided for each building type in the reference section below.

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = ((Wattsbase-WattsEE)/1000) \* Hours \*WHFe\*ISR

Where:

Wattsbase = Input wattage of the existing system. Reference the “LED New and Baseline Assumptions” table for default values.

WattsEE = New Input wattage of EE fixture. See the “LED New and Baseline Assumptions” table.

For ENERGY STAR rated lamps the following lumen equivalence tables should be used:

**Omnidirectional Lamps - ENERGY STAR Minimum Luminous Efficacy = 50Lm/W for <10W lamps and 55Lm/W for >=10W lamps.**

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| **Minimum Lumens** | **Maximum Lumens** | **Lumens used to calculate LED Wattage (midpoint)** | **LED Wattage[[501]](#footnote-502) (WattsEE)** | **Baseline 2014-2019 (WattsBase)** | **Delta Watts 2014-2019 (WattsEE)** | **Baseline Post EISA 2020 requirement[[502]](#footnote-503)  (WattsBase)** | **Delta Watts Post 2020 (WattsEE)** |
|
|
| 5280 | 6209 | 5745 | 104.4 | 300.0 | 195.6 | 300.0 | 195.6 |
| 3000 | 5279 | 4140 | 75.3 | 200.0 | 124.7 | 200.0 | 124.7 |
| 2601 | 2999 | 2800 | 50.9 | 150.0 | 99.1 | 150.0 | 99.1 |
| 1490 | 2600 | 2045 | 37.2 | 72.0 | 34.8 | 45.4 | 8.3 |
| 1050 | 1489 | 1270 | 23.1 | 53.0 | 29.9 | 28.2 | 5.1 |
| 750 | 1049 | 900 | 16.4 | 43.0 | 26.6 | 20.0 | 3.6 |
| 310 | 749 | 530 | 9.6 | 29.0 | 19.4 | 11.8 | 2.1 |
| 250 | 309 | 280 | 5.6 | 25.0 | 19.4 | 25.0 | 19.4 |

**Decorative Lamps - ENERGY STAR Minimum Luminous Efficacy = 40Lm/W for all lamps**

|  |  |  |  |
| --- | --- | --- | --- |
| Nominal wattage of lamp to be replaced  (Wattsbase) | Minimum initial light output of LED lamp (lumens) | LED Wattage  (WattsEE) | Delta Watts |
| 10 | 70 | 1.75 | 8.25 |
| 15 | 90 | 2.25 | 12.75 |
| 25 | 150 | 3.75 | 21.25 |
| 40 | 300 | 7.5 | 32.5 |
| 60 | 500 | 12.5 | 47.5 |

Decorative lamps are exempt from EISA regulations.

**Directional Lamps - ENERGY STAR Minimum Luminous Efficacy = 40Lm/W for lamp diameter <= 20/8 inch (PAR 20 and smaller) and 45 Lm/W for lamp diameter > 20/8 inch (greater than PAR20).**

| **Bulb Type** | **Lower Lumen Range** | **Upper Lumen Range** | **Lumens used to calculate LED Wattage (midpoint)** | LED Wattage  **(WattsEE)** | **WattsBase** | **Delta Watts** |
| --- | --- | --- | --- | --- | --- | --- |
| **Reflector with medium screw bases w/ diameter <=2.25"** | 400 | 449 | 425 | 10.6 | 40 | 29.4 |
| 450 | 499 | 475 | 11.9 | 45 | 33.1 |
| 500 | 649 | 575 | 14.4 | 50 | 35.6 |
| 650 | 1199 | 925 | 23.1 | 65 | 41.9 |
| **R, PAR, ER, BR, BPAR or similar bulb shapes with medium screw bases w/ diameter >2.5" (\*see exceptions below)** | 640 | 739 | 690 | 15.3 | 40 | 24.7 |
| 740 | 849 | 795 | 17.7 | 45 | 27.3 |
| 850 | 1179 | 1015 | 22.5 | 50 | 27.5 |
| 1180 | 1419 | 1300 | 28.9 | 65 | 36.1 |
| 1420 | 1789 | 1605 | 35.7 | 75 | 39.3 |
| 1790 | 2049 | 1920 | 42.7 | 90 | 47.3 |
| 2050 | 2579 | 2315 | 51.4 | 100 | 48.6 |
| 2580 | 3429 | 3005 | 66.8 | 120 | 53.2 |
| 3430 | 4270 | 3850 | 85.6 | 150 | 64.4 |
| **R, PAR, ER, BR, BPAR or similar bulb shapes with medium screw bases w/ diameter > 2.26'' and ≤ 2.5" (\*see exceptions below)** | 540 | 629 | 585 | 14.6 | 40 | 25.4 |
| 630 | 719 | 675 | 16.9 | 45 | 28.1 |
| 720 | 999 | 860 | 21.5 | 50 | 28.5 |
| 1000 | 1199 | 1100 | 27.5 | 65 | 37.5 |
| 1200 | 1519 | 1360 | 34.0 | 75 | 41.0 |
| 1520 | 1729 | 1625 | 40.6 | 90 | 49.4 |
| 1730 | 2189 | 1960 | 49.0 | 100 | 51.0 |
| 2190 | 2899 | 2545 | 63.6 | 120 | 56.4 |
| 2900 | 3850 | 3375 | 84.4 | 150 | 65.6 |
| **\*ER30, BR30, BR40, or ER40** | 400 | 449 | 425 | 10.6 | 40 | 29.4 |
| 450 | 499 | 475 | 11.9 | 45 | 33.1 |
| 500 | 649 | 575 | 14.4 | 50 | 35.6 |
| **\*BR30, BR40, or ER40** | 650 | 1419 | 1035 | 23.0 | 65 | 42.0 |
| **\*R20** | 400 | 449 | 425 | 10.6 | 40 | 29.4 |
| 450 | 719 | 585 | 14.6 | 45 | 30.4 |
| **\*All reflector lamps below lumen ranges specified above** | 200 | 299 | 250 | 6.2 | 20 | 13.8 |
| 300 | [[503]](#footnote-504)399-639[[504]](#footnote-505) | 350 | 8.7 | 30 | 21.3 |

Directional lamps are exempt from EISA regulations.

Hours = Average hours of use per year are provided in the Reference Table in Section 4.5,Screw based bulb annual operating hours, for each building type. If unknown, use the Miscellaneous value.

WHFe = Waste heat factor for energy to account for cooling energy savings from efficient lighting are provided below for each building type in the Referecne Table in Section 4.5. If unknown, use the Miscellaneous value.

ISR = In service Rate -the percentage of units rebated that actually get installed.

=100%[[505]](#footnote-506) if application form completed with sign off that equipment is not placed into storage

If sign off form not completed assume 96%[[506]](#footnote-507)

###### Heating Penalty

If electrically heated building:

ΔkWhheatpenalty[[507]](#footnote-508) = (((WattsBase-WattsEE)/1000) \* ISR \* Hours \* -IFkWh

Where:

IFkWh = Lighting-HVAC Interation Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficent lighting. Values are provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

For example, For example, a 9W LED lamp, 450 lumens, is installed in a heat pump heated office in 2014 and sign off form provided:

ΔkWhheatpenalty = ((29-9/1000)\*1.0\*3088\* -0.151

= - 9.3 kWh

###### Summer Coincident Peak Demand Savings

ΔkW =( (Wattsbase-WattsEE)/1000) \* ISR \* WHFd \* CF

Where:

WHFd = Waste Heat Factor for Demand to account for cooling savings from efficient lighting in cooled buildings is provided in Referecne Table in Section 4.5. If unknown, use the Miscellaneous value.

CF = Summer Peak Coincidence Factor for measure is provided in the Referecne Table in Section 4.5. If unknown, use the Miscellaneous value.

For example, For example, a 9W LED lamp, 450 lumens, is installed in an office in 2014 and sign off form provided:

ΔkW = ((29-9/1000)\* 1.0\*1.3\*0.66

= 0.002 kW

###### Natural Gas Energy Savings

Heating Penalty if fossil fuel heated building (or if heating fuel is unknown):

ΔTherms = (((WattsBase-WattsEE)/1000) \* ISR \* Hours \* - IFTherms

Where:

IFTherms = Lighting-HVAC Integration Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Referecne Table in Section 4.5. If unknown, use the Miscellaneous value.

For example, For example, a 9W LED lamp, 450 lumens, is installed in an office in 2014 and sign off form provided:

ΔTherms = ((29-9/1000)\*1.0\*3088\* -0.016

= - 0.99 therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

For all measures except Standard Omnidirectional lamps (which have an EISA baseline shift) the individual component lifetimes and costs are provided in the reference table section below[[508]](#footnote-509).

In order to account for the falling EISA Qualified bulb replacement cost provided above, an equivalent annual levelized baseline replacement cost over the lifetime of the LED bulb (assumed to be 25,000/4576 =5.5 years) is calculated (see “C&I OmniDirectional LED O&M Calc.xls”). The key assumptions used in this calculation are documented below[[509]](#footnote-510):

|  | **Std Inc.** | **EISA Compliant Halogen** | **CFL** |
| --- | --- | --- | --- |
| 2014 | $0.34 | $1.25 | N/A |
| 2015 | $0.34 | $0.90 | N/A |
| 2016 | $0.34 | $0.80 | N/A |
| 2017 | $0.34 | $0.70 | N/A |
| 2018 | $0.34 | $0.60 | N/A |
| 2019 | $0.34 | $0.60 | N/A |
| 2020 & after | $0.34 | N/A | $2.50 |

The NPV for replacement lamps and annual levelized replacement costs using the statewide real discount rate of 5.23% are presented below:

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| **Location** | **Lumen Level** | **NPV of replacement costs for period** | | | **Levelized annual replacement cost savings** | | |
| **June 2014 - May 2015** | **June 2015 - May 2016** | **June 2016 - May 2017** | **June 2014 - May 2015** | **June 2015 - May 2016** | **June 2016 - May 2017** |
| Commercial | Lumens <310 or >2600 (EISA exempt) | $6.94 | $6.94 | $6.94 | $1.49 | $1.49 | $1.49 |
| Lumens ≥ 310 and ≤ 2600 (EISA compliant) | $16.86 | $13.90 | $11.51 | $3.63 | $2.99 | $2.48 |
| Multi Family Common Areas | Lumens <310 or >2600 (non-EISA compliant) | $7.13 | $7.13 | $7.13 | $1.93 | $1.93 | $1.93 |
| Lumens ≥ 310 and ≤ 2600 (EISA compliant) | $18.75 | $15.57 | $13.79 | $5.09 | $4.22 | $3.74 |

For halogen bulbs, we assume the same replacement cycle as incandescent bulbs.[[510]](#footnote-511) The replacement cycle is based on the miscellaneous hours of use. Both incandescent and halogen lamps are assumed to last for 1,000 hours before needing replacement and CFLs after 10,000 hours.

LED New and Baseline Assumptions[[511]](#footnote-512)

| LED Measure Description | WattsEE | Baseline Description | WattsBASE | Basis for Watt Assumptions | LED Lamp Cost | Baseline Cost (EISA 2012-2014, EISA 2020) | Incremental Cost (EISA 2012-2014, EISA 2020) | LED Minimum Lamp Life (hrs) |
| --- | --- | --- | --- | --- | --- | --- | --- | --- |
| LED Screw and Pin-based Bulbs, Omnidirectional, < 10W | See tables above | | | | $30.00 | $0.34 ($1.25, $2.50) | $29.66 ($28.75, $27.50) | 25,000 |
| LED Screw and Pin-based Bulbs, Omnidirectional, >= 10W | $40.00 | $0.34 ($1.25, $2.50) | $39.66 ($38.75, $37.50) | 25,000 |
| LED Screw and Pin-based Bulbs, Decorative | $30.00 | $1.00 | $29.00 | 25,000 |
| LED Screw-based Bulbs, Directional, < 15W | $45.00 | $5.00 | $40.00 | 35,000 |
| LED Screw-based Bulbs, Directional, >= 15W | $55.00 | $5.00 | $50.00 | 35,000 |
| LED Recessed, Surface, Pendant Downlights | 17.6 | Baseline LED Recessed, Surface, Pendant Downlights | 54.3 | 2008-2010 EVT Historical Data of 947 Measures | 50,000 |  | $50.00 |  |
| LED Track Lighting | 12.2 | Baseline LED Track Lighting | 60.4 | 2008-2010 EVT Historical Data of 242 Measures | 50,000 |  | $100.00 |  |
| LED Wall-Wash Fixtures | 8.3 | Baseline LED Wall-Wash Fixtures | 17.7 | 2008-2010 EVT Historical Data of 220 Measures | 50,000 |  | $80.00 |  |
| LED Portable Desk/Task Light Fixtures | 7.1 | Baseline LED Portable Desk/Task Light Fixtures | 36.2 | 2008-2010 EVT Historical Data of 21 Measures | 50,000 |  | $50.00 |  |
| LED Undercabinet Shelf-Mounted Task Light Fixtures (per foot) | 7.1 | Baseline LED Undercabinet Shelf-Mounted Task Light Fixtures | 36.2 | 2008-2010 EVT Historical Data of 21 Measures | 50,000 |  | $25.00 |  |
| LED Refrigerated Case Light, Horizontal or Vertical (per foot of light bar) | 7.6 | Baseline LED Refrigerated Case Light, Horizontal or Vertical (per foot of light bar) | 15.2 | PG&E Refrigerated Case Study[[512]](#footnote-513) normalized to per foot of light bar. | 50,000 |  | $50.00 |  |
| LED Freezer Case Light, Horizontal or Vertical (per foot) | 7.7 | Baseline LED Freezer Case Light, Horizontal or Vertical (per foot) | 18.7 | PG&E Refrigerated Case Study normalized to per foot. | 50,000 |  | $50.00 |  |
| LED Display Case Light Fixture (per foot) | 7.1 | Baseline LED Display Case Light Fixture | 36.2 | Modeled after LED Undercabinet Shelf-Mounted Task Light Fixtures (per foot) | 35,000 |  | $25.00 |  |
| LED 2x2 Recessed Light Fixture | 44.9 | T8 U-Tube 2L-FB32 w/ Elec - 2' | 61.0 | Based on average watts of DLC qualified products as of 11/21/11 | 35,000 |  | $75.00 |  |
| LED 2x4 Recessed Light Fixture | 53.6 | T8 3L-F32 w/ Elec - 4' | 88.0 | Based on average watts of DLC qualified products as of 11/21/11 | 35,000 |  | $125.00 |  |
| LED 1x4 Recessed Light Fixture | 32.2 | T8 2L-F32 w/ Elec - 4' | 59.0 | Based on average watts of DLC qualified products as of 11/21/11 | 35,000 |  | $100.00 |  |
| LED High- and Low-Bay Fixtures | 160.2 | MH 250 W CWA Pulse Start | 295.0 | Based on average watts of DLC qualified products as of 11/21/11 | 35,000 |  | $200.00 |  |
| LED Outdoor Pole/Arm Mounted Parking/Roadway, < 30W | 18.6 | Baseline LED Outdoor Pole/Arm Mounted Parking/Roadway, < 30W | 124.3 | 2008-2010 EVT Historical Data of 2,813 Measures | 50,000 |  | $125.00 |  |
| LED Outdoor Pole/Arm Mounted Parking/Roadway, 30W - 75W | 52.5 | Baseline LED Outdoor Pole/Arm Mounted Parking/Roadway, 30W - 75W | 182.9 | 2008-2010 EVT Historical Data of 1,081 Measures | 50,000 |  | $250.00 |  |
| LED Outdoor Pole/Arm Mounted Parking/Roadway, >= 75W | 116.8 | Baseline LED Outdoor Pole/Arm Mounted Parking/Roadway, >= 75W | 361.4 | 2008-2010 EVT Historical Data of 806 Measures | 50,000 |  | $375.00 |  |
| LED Outdoor Pole/Arm Mounted Decorative Parking/Roadway, < 30W | 18.6 | Baseline LED Outdoor Pole/Arm Mounted Decorative Parking/Roadway, < 30W | 124.3 | 2008-2010 EVT Historical Data of 2,813 Measures | 50,000 |  | $125.00 |  |
| LED Outdoor Pole/Arm Mounted Decorative Parking/Roadway, 30W - 75W | 52.5 | Baseline LED Outdoor Pole/Arm Mounted Decorative Parking/Roadway, 30W - 75W | 182.9 | 2008-2010 EVT Historical Data of 1,081 Measures | 50,000 |  | $250.00 |  |
| LED Outdoor Pole/Arm Mounted Decorative Parking/Roadway, >= 75W | 116.8 | Baseline LED Outdoor Pole/Arm Mounted Decorative Parking/Roadway, >= 75W | 361.4 | 2008-2010 EVT Historical Data of 806 Measures | 50,000 |  | $375.00 |  |
| LED Parking Garage/Canopy, < 30W | 18.6 | Baseline LED Parking Garage/Canopy, < 30W | 124.3 | 2008-2010 EVT Historical Data of 2,813 Measures | 50,000 |  | $125.00 |  |
| LED Parking Garage/Canopy, 30W - 75W | 52.5 | Baseline LED Parking Garage/Canopy, 30W - 75W | 182.9 | 2008-2010 EVT Historical Data of 1,081 Measures | 50,000 |  | $250.00 |  |
| LED Parking Garage/Canopy, >= 75W | 116.8 | Baseline LED Parking Garage/Canopy, >= 75W | 361.4 | 2008-2010 EVT Historical Data of 806 Measures | 50,000 |  | $375.00 |  |
| LED Wall-Mounted Area Lights, < 30W | 18.6 | Baseline LED Wall-Mounted Area Lights, < 30W | 124.3 | 2008-2010 EVT Historical Data of 2,813 Measures | 50,000 |  | $125.00 |  |
| LED Wall-Mounted Area Lights, 30W - 75W | 52.5 | Baseline LED Wall-Mounted Area Lights, 30W - 75W | 182.9 | 2008-2010 EVT Historical Data of 1,081 Measures | 50,000 |  | $250.00 |  |
| LED Wall-Mounted Area Lights, >= 75W | 116.8 | Baseline LED Wall-Mounted Area Lights, >= 75W | 361.4 | 2008-2010 EVT Historical Data of 806 Measures | 50,000 |  | $375.00 |  |
| LED Bollard, < 30W | 13.9 | Baseline LED Bollard, < 30W | 54.3 | 2008-2010 EVT Historical Data of 33 Measures | 50,000 |  | $150.00 |  |
| LED Bollard, >= 30W | 41.0 | Baseline LED Bollard, >= 30W | 78.0 | 2008-2010 EVT Historical Data of 15 Measures | 50,000 |  | $250.00 |  |
| LED Flood Light, < 15W | 8.7 | Baseline LED Flood Light, < 15W | 51.7 | Consistent with LED Screw-base Directional | 50,000 |  | $35.00 |  |
| LED Flood Light, >= 15W | 16.2 | Baseline LED Flood Light, >= 15W | 64.4 | Consistent with LED Screw-base Directional | 50,000 |  | $45.00 |  |

LED Component Costs & Lifetime[[513]](#footnote-514)

LED Component Costs and Lifetimes

| **LED Measure Description** | **LED Minimum Lamp Life (hrs)** | **LED Lamp Cost Total** | **LED Driver Life (hrs)** | **LED Driver Cost Total** | **Baseline Technology (1)** | **Lamp (1) Life (hrs)** | **Lamp (1) Total Cost** | **Ballast (1) Life (hrs)** | **Ballast (1) Total Cost** | **Baseline Technology (2)** | **Lamp (2) Life (hrs)** | **Lamp (2) Total Cost** |
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| LED Screw and Pin-based Bulbs, Decorative | 25,000 | N/A | N/A | N/A | 53W EISA Halogen | 2,000 | $4.67 | N/A | N/A | N/A | N/A | N/A |
| LED Screw-based Bulbs, Directional, < 15W | 35,000 | N/A | N/A | N/A | 15% CFL 18W Pin Base | 10,000 | $11.62 | 40,000 | $36.00 | 85% Halogen PAR20 | 2,500 | $12.67 |
| LED Screw-based Bulbs, Directional, >= 15W | 35,000 | N/A | N/A | N/A | 15% CFL 26W Pin Base | 10,000 | $12.62 | 40,000 | $36.00 | 85% Halogen PAR30/38 | 2,500 | $12.67 |
| LED Recessed, Surface, Pendant Downlights | 50,000 | $47.50 | 70,000 | $47.50 | 40% CFL 26W Pin Base | 10,000 | $12.62 | 40,000 | $36.00 | 60% Halogen PAR30/38 | 2,500 | $12.67 |
| LED Track Lighting | 50,000 | $47.50 | 70,000 | $47.50 | 10% CMH PAR38 | 12,000 | $62.92 | 40,000 | $110.00 | 90% Halogen PAR38 | 2,500 | $12.67 |
| LED Wall-Wash Fixtures | 50,000 | $47.50 | 70,000 | $47.50 | 40% CFL 42W Pin Base | 10,000 | $15.72 | 40,000 | $67.50 | 60% Halogen PAR38 | 2,500 | $12.67 |
| LED Portable Desk/Task Light Fixtures | 50,000 | $47.50 | 70,000 | $47.50 | 50% 13W CFL Pin Base | 10,000 | $5.52 | 40,000 | $25.00 | 50% 50W Halogen | 2,500 | $12.67 |
| LED Undercabinet Shelf-Mounted Task Light Fixtures (per foot) | 50,000 | $47.50 | 70,000 | $47.50 | 50% 2' T5 Linear | 7,500 | $9.92 | 40,000 | $45.00 | 50% 50W Halogen | 2,500 | $12.67 |
| LED Refrigerated Case Light, Horizontal or Vertical (per foot) | 50,000 | $9.50 | 70,000 | $9.50 | 5' T8 | 15,000 | $2.77 | 40,000 | $9.50 | N/A | N/A | N/A |
| LED Freezer Case Light, Horizontal or Vertical (per foot) | 50,000 | $8.75 | 70,000 | $7.92 | 6' T12HO | 12,000 | $11.03 | 40,000 | $59.58 | N/A | N/A | N/A |
| LED Display Case Light Fixture (per foot) | 35,000 | $47.50 | 70,000 | $28.75 | 50% 2' T5 Linear | 7,500 | $9.92 | 40,000 | $45.00 | 50% 50W Halogen | 2,500 | $12.67 |
| LED 2x2 Recessed Light Fixture | 35,000 | $47.50 | 70,000 | $47.50 | T8 U-Tube 2L-FB32 w/ Elec - 2' | 15,000 | $24.95 | 40,000 | $52.00 | N/A | N/A | N/A |
| LED 2x4 Recessed Light Fixture | 35,000 | $72.50 | 70,000 | $47.50 | T8 3L-F32 w/ Elec - 4' | 15,000 | $17.00 | 40,000 | $35.00 | N/A | N/A | N/A |
| LED 1x4 Recessed Light Fixture | 35,000 | $47.50 | 70,000 | $47.50 | T8 2L-F32 w/ Elec - 4' | 15,000 | $11.33 | 40,000 | $35.00 | N/A | N/A | N/A |
| LED High- and Low-Bay Fixtures | 35,000 | $112.50 | 70,000 | $62.50 | 250W MH | 10,000 | $41.25 | 40,000 | $130.25 | N/A | N/A | N/A |
| LED Outdoor Pole/Arm Mounted Parking/Roadway, < 30W | 50,000 | $62.50 | 70,000 | $62.50 | 100W MH | 10,000 | $54.25 | 40,000 | $166.70 | N/A | N/A | N/A |
| LED Outdoor Pole/Arm Mounted Parking/Roadway, 30W - 75W | 50,000 | $87.50 | 70,000 | $62.50 | 175W MH | 10,000 | $48.25 | 40,000 | $110.00 | N/A | N/A | N/A |
| LED Outdoor Pole/Arm Mounted Parking/Roadway, >= 75W | 50,000 | $112.50 | 70,000 | $62.50 | 250W MH | 10,000 | $41.25 | 40,000 | $130.25 | N/A | N/A | N/A |
| LED Outdoor Pole/Arm Mounted Decorative Parking/Roadway, < 30W | 50,000 | $62.50 | 70,000 | $62.50 | 100W MH | 10,000 | $54.25 | 40,000 | $166.70 | N/A | N/A | N/A |
| LED Outdoor Pole/Arm Mounted Decorative Parking/Roadway, 30W - 75W | 50,000 | $87.50 | 70,000 | $62.50 | 175W MH | 10,000 | $48.25 | 40,000 | $110.00 | N/A | N/A | N/A |
| LED Outdoor Pole/Arm Mounted Decorative Parking/Roadway, >= 75W | 50,000 | $112.50 | 70,000 | $62.50 | 250W MH | 10,000 | $41.25 | 40,000 | $130.25 | N/A | N/A | N/A |
| LED Parking Garage/Canopy, < 30W | 50,000 | $47.50 | 70,000 | $47.50 | 100W MH | 10,000 | $36.92 | 40,000 | $151.70 | N/A | N/A | N/A |
| LED Parking Garage/Canopy, 30W - 75W | 50,000 | $72.50 | 70,000 | $47.50 | 175W MH | 10,000 | $30.92 | 40,000 | $95.00 | N/A | N/A | N/A |
| LED Parking Garage/Canopy, >= 75W | 50,000 | $97.50 | 70,000 | $47.50 | 250W MH | 10,000 | $23.92 | 40,000 | $115.25 | N/A | N/A | N/A |
| LED Wall-Mounted Area Lights, < 30W | 50,000 | $47.50 | 70,000 | $47.50 | 100W MH | 10,000 | $36.92 | 40,000 | $151.70 | N/A | N/A | N/A |
| LED Wall-Mounted Area Lights, 30W - 75W | 50,000 | $72.50 | 70,000 | $47.50 | 175W MH | 10,000 | $30.92 | 40,000 | $95.00 | N/A | N/A | N/A |
| LED Wall-Mounted Area Lights, >= 75W | 50,000 | $97.50 | 70,000 | $47.50 | 250W MH | 10,000 | $23.92 | 40,000 | $115.25 | N/A | N/A | N/A |
| LED Bollard, < 30W | 50,000 | $47.50 | 70,000 | $47.50 | 50W MH | 10,000 | $36.92 | 40,000 | $135.50 | N/A | N/A | N/A |
| LED Bollard, >= 30W | 50,000 | $72.50 | 70,000 | $47.50 | 70W MH | 10,000 | $36.92 | 40,000 | $142.50 | N/A | N/A | N/A |
| LED Flood Light, < 15W | 50,000 | $47.50 | 70,000 | $47.50 | 25% 50W MH | 10,000 | $36.92 | 40,000 | $135.50 | 75% Halogen PAR20 | 2,500 | $12.67 |
| LED Flood Light, >= 15W | 50,000 | $47.50 | 70,000 | $47.50 | 50% 50W MH | 10,000 | $36.92 | 40,000 | $135.50 | 50% Halogen PAR30/38 | 2,500 | $12.67 |

###### Measure Code: CI-LTG-LEDB-V04-150601

### Commercial LED Exit Signs

###### Description

This measure characterizes the savings associated with installing a Light Emitting Diode (LED) exit sign in place of a fluorescent or incandescent exit sign in a Commercial building. Light Emitting Diode exit signs have a string of very small, typically red or green, glowing LEDs arranged in a circle or oval. The LEDs may also be arranged in a line on the side, top or bottom of the exit sign. LED exit signs provide the best balance of safety, low maintenance, and very low energy usage compared to other exit sign technologies.

This measure was developed to be applicable to the following program types:  RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The efficient equipment is assumed to be an exit sign illuminated by LEDs.

###### Definition of Baseline Equipment

The baseline equipment is assumed to be a fluorescent or incandescent model.

###### Deemed Lifetime of Efficient Equipment

The measure life is assumed to be 16 years[[514]](#footnote-515).

###### Deemed Measure Cost

The incremental cost for this measure is assumed to be $30[[515]](#footnote-516).

###### Loadshape

Loadshape C53 - Flat

###### Coincidence Factor

The summer peak coincidence factor for this measure is assumed to be 100%[[516]](#footnote-517).

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = ((WattsBase - WattsEE) / 1000) \* HOURS \* WHFe

Where:

WattsBase = Actual wattage if known, if unknown assume the following:

|  |  |
| --- | --- |
| **Baseline Type** | **WattsBase** |
| Incandescent | 35W[[517]](#footnote-518) |
| Fluorescent | 11W[[518]](#footnote-519) |
| Unknown (e.g. time of sale) | 23W[[519]](#footnote-520) |

WattsEE = Actual wattage if known, if unknown assume 2W[[520]](#footnote-521)

HOURS = Annual operating hours

= 8766

WHFe = Waste heat factor for energy to account for cooling energy savings from efficient lighting are provided for each building type in the Referecne Table in Section 4.5. If unknown, use the Miscellaneous value.

For example, replacing incandescent fixture in an office

ΔkWH = (35 – 2)/1000 \* 8766 \* 1.25

= 362 kWh

For example, replacing fluorescent fixture in a hospital

ΔkWH = (11 – 2)/1000 \* 8766 \* 1.35

= 106.5 kWh

###### Heating Penalty

If electrically heated building:

ΔkWhheatpenalty[[521]](#footnote-522) = (((WattsBase-WattsEE)/1000) \* Hours \* -IFkWh

Where:

IFkWh = Lighting-HVAC Interation Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficent lighting. Values are provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

For example, replacing incandescent fixture in a heat pump heated office

ΔkWhheatpenalty = (35 – 2)/1000 \* 8760 \* -0.151

= -43.7 kWh

For example, replacing fluorescent fixture in a heat pump heated hospital

ΔkWhheatpenalty = (11 – 2)/1000 \* 8760 \* -0.104

= 8.2 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = ((WattsBase - WattsEE) / 1000) \* WHFd \* CF

Where:

WHFd = Waste heat factor for demand to account for cooling savings from efficient lighting in cooled buildings is provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value..

CF = Summer Peak Coincidence Factor for measure

= 1.0

For example, replacing incandescent fixture in an office

ΔkW = (35 – 2)/1000 \* 1.3 \* 1.0

= 0.043 kW

For example, replacing fluorescent fixture in a hospital

ΔkW = (11 – 2)/1000 \* 1.69 \* 1.0

= 0.015 kW

###### Natural Gas Savings

Heating Penalty if natural gas heated building (or if heating fuel is unknown):

Δtherms = (((WattsBase-WattsEE)/1000) \* Hours \*- IFTherms

Where:

IFTherms = Lighting-HVAC Integration Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Referecne Table in Section 4.5. If unknown, use the Miscellaneous value.

For example, replacing incandescent fixture in an office

ΔTherms = (35 – 2)/1000 \* 8760 \* -0.016

= -4.63 Therms

For example, replacing fluorescent fixture in a hospital

ΔTherms = (11 – 2)/1000 \* 8760 \* -0.011

= 0.87 Therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

The annual O&M Cost Adjustment savings should be calculated using the following component costs and lifetimes.

|  |  |  |
| --- | --- | --- |
|  | **Baseline Measures** | |
| Component | Cost | Life (yrs) |
| Lamp | $7.00[[522]](#footnote-523) | 1.37 years[[523]](#footnote-524) |

###### Measure Code: CI-LTG-LEDE-V02-140601

### LED Traffic and Pedestrian Signals

###### Description

Traffic and pedestrian signals are retrofitted to be illuminated with light emitting diodes (LED) instead of incandescent lamps. Incentive applies for the replacement or retrofit of existing incandescent traffic signals with new LED traffic and pedestrian signal lamps.  Each lamp can have no more than a maximum LED module wattage of 25. Incentives are not available for spare lights. Lights must be hardwired and single lamp replacements are not eligible, with the exception of pedestrian hand signals. Eligible lamps must meet the Energy Star Traffic Signal Specification and the Institute for Transportation Engineers specification for traffic signals.

This measure was developed to be applicable to the following program types: RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

Refer to the Table titled ‘Traffic Signals Technology Equivalencies’ for efficient technology wattage and savings assumptions.

###### Definition of Baseline Equipment

Refer to the Table titled ‘Traffic Signals Technology Equivalencies’ for baseline efficiencies and savings assumptions.

###### Deemed Lifetime of Efficient Equipment

The assumed lifetime of an LED traffic signal is 100,000 hours (manufacturer’s estimate), capped at 10 years.[[524]](#footnote-525) The life in years is calculated by dividing 100,000 hrs by the annual operating hours for the particular signal type.

###### Deemed Measure Cost

The actual measure installation cost should be used (including material and labor).

###### Loadshape

|  |
| --- |
| Loadshape C24 - Traffic Signal - Red Balls, always changing or flashing |
| Loadshape C25 - Traffic Signal - Red Balls, changing day, off night |
| Loadshape C26 - Traffic Signal - Green Balls, always changing |
| Loadshape C27 - Traffic Signal - Green Balls, changing day, off night |
| Loadshape C28 - Traffic Signal - Red Arrows |
| Loadshape C29 - Traffic Signal - Green Arrows |
| Loadshape C30 - Traffic Signal - Flashing Yellows |
| Loadshape C31 - Traffic Signal - “Hand” Don’t Walk Signal |
| Loadshape C32 - Traffic Signal - “Man” Walk Signal |
| Loadshape C33 - Traffic Signal - Bi-Modal Walk/Don’t Walk |

###### Coincidence Factor[[525]](#footnote-526)

The summer peak coincidence factor (CF) for this measure is dependent on lamp type as below:

| Lamp Type | CF |
| --- | --- |
| Red Round, always changing or flashing | 0.55 |
| Red Arrows | 0.90 |
| Green Arrows | 0.10 |
| Yellow Arrows | 0.03 |
| Green Round, always changing or flashing | 0.43 |
| Flashing Yellow | 0.50 |
| Yellow Round, always changing | 0.02 |
| “Hand” Don’t Walk Signal | 0.75 |
| “Man” Walk Signal | 0.21 |

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = (Wbase - Weff) x HOURS / 1000

Where:

Wbase =The connected load of the baseline equipment

= see Table ‘Traffic Signals Technology Equivalencies’

Weff=The connected load of the baseline equipment

= see Table ‘Traffic Signals Technology Equivalencies’

EFLH = annual operating hours of the lamp

= see Table ‘Traffic Signals Technology Equivalencies’

1000 = conversion factor (W/kW)

EXAMPLE

For example, an 8 inch red, round signal:

ΔkWh = ((69 - 7) x 4818) / 1000

= 299 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = (Wbase– Weff) x CF / 1000

Where:

Wbase =The connected load of the baseline equipment

= see Table ‘Traffic Signals Technology Equivalencies’

Weff =The connected load of the efficient equipment

= see Table ‘Traffic Signals Technology Equivalencies’

CF = Summer Peak Coincidence Factor for measure

EXAMPLE

For example, an 8 inch red, round signal:

ΔkW = ((69 – 7) x 0.55) / 1000

= 0.0341 kW

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Reference Tables

Traffic Signals Technology Equivalencies[[526]](#footnote-527)

| **Traffic Fixture Type** | **Fixture Size and Color** | **Efficient Lamps** | **Baseline Lamps** | **HOURS** | **Efficient Fixture Wattage** | **Baseline Fixture Wattage** | **Energy Savings**  **(in kWh)** |
| --- | --- | --- | --- | --- | --- | --- | --- |
| Round Signals | 8” Red | LED | Incandescent | 4818 | 7 | 69 | 299 |
| Round Signals | 12” Red | LED | Incandescent | 4818 | 6 | 150 | 694 |
| Flashing Signal[[527]](#footnote-528) | 8” Red | LED | Incandescent | 4380 | 7 | 69 | 272 |
| Flashing Signal | 12” Red | LED | Incandescent | 4380 | 6 | 150 | 631 |
| Flashing Signal | 8” Yellow | LED | Incandescent | 4380 | 10 | 69 | 258 |
| Flashing Signal | 12” Yellow | LED | Incandescent | 4380 | 13 | 150 | 600 |
| Round Signals | 8” Yellow | LED | Incandescent | 175 | 10 | 69 | 10 |
| Round Signals | 12” Yellow | LED | Incandescent | 175 | 13 | 150 | 24 |
| Round Signals | 8” Green | LED | Incandescent | 3767 | 9 | 69 | 266 |
| Round Signals | 12” Green | LED | Incandescent | 3767 | 12 | 150 | 520 |
| Turn Arrows | 8” Yellow | LED | Incandescent | 701 | 7 | 116 | 76 |
| Turn Arrows | 12” Yellow | LED | Incandescent | 701 | 9 | 116 | 75 |
| Turn Arrows | 8” Green | LED | Incandescent | 701 | 7 | 116 | 76 |
| Turn Arrows | 12” Green | LED | Incandescent | 701 | 7 | 116 | 76 |
| Pedestrian Sign | 12” Hand/Man | LED | Incandescent | 8760 | 8 | 116 | 946 |

Reference specifications for above traffic signal wattages are from the following manufacturers:

1. 8” Incandescent traffic signal bulb: General Electric Traffic Signal Model 17325-69A21/TS
2. 12” Incandescent traffic signal bulb: General Electric Signal Model 35327-150PAR46/TS
3. Incandescent Arrows & Hand/Man Pedestrian Signs: General Electric Traffic Signal Model 19010-116A21/TS
4. 8” and 12” LED traffic signals: Leotek Models TSL-ES08 and TSL-ES12
5. 8” LED Yellow Arrow: General Electric Model DR4-YTA2-01A
6. 8” LED Green Arrow: General Electric Model DR4-GCA2-01A
7. 12” LED Yellow Arrow: Dialight Model 431-3334-001X
8. 12: LED Green Arrow: Dialight Model 432-2324-001X
9. LED Hand/Man Pedestrian Sign: Dialight 430-6450-001X

###### Measure Code: CI-LTG-LEDT-V01-120601

### Lighting Power Density

###### Description

This measure relates to installation of efficient lighting systems in new construction or substantial renovation of commercial buildings excluding low rise (three stories or less) residential buildings. Substantial renovation is when two or more building systems are renovated, such as shell and heating, heating and lighting, etc. State Energy Code specifies a lighting power density level by building type for both the interior and the exterior. Either the Building Area Method or Space by Space method as defined in IECC 2012 can be used for calculating the Interior Lighting Power Density[[528]](#footnote-529). The measure consists of a design that is more efficient (has a lower lighting power density in watts/square foot) than code requires. The IECC 2012, which is adopted in Illinois, applies to both new construction and renovation.

This measure was developed to be applicable to the following program types: NC.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the lighting system must be more efficient than the baseline Energy Code lighting power density in watts/square foot for either the interior space or exterior space.

###### Definition of Baseline Equipment

The baseline is assumed to be a lighting power density that meets IECC 2012, the State of Illinois Energy Code requirements.

###### Deemed Calculation for this Measure

Annual kWh Savings = ΔkWh = (WSFbase-WSFeffic )/1000\* SF\* Hours \* WHFe

Summer Coincident Peak kW Savings = ΔkW = (WSFbase-WSFeffic )/1000\* SF\* CF \* WHFd

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 15 years[[529]](#footnote-530)

###### Deemed Measure Cost

The actual incremental cost over a baseline system will be collected from the customer if possible or developed on a fixture by fixture basis.

###### Loadshape

|  |
| --- |
| Loadshape C06 - Commercial Indoor Lighting |
| Loadshape C07 - Grocery/Conv. Store Indoor Lighting |
| Loadshape C08 - Hospital Indoor Lighting |
| Loadshape C09 - Office Indoor Lighting |
| Loadshape C10 - Restaurant Indoor Lighting |
| Loadshape C11 - Retail Indoor Lighting |
| Loadshape C12 - Warehouse Indoor Lighting |
| Loadshape C13 - K-12 School Indoor Lighting |
| Loadshape C14 - Indust. 1-shift (8/5) (e.g., comp. air, lights) |
| Loadshape C15 - Indust. 2-shift (16/5) (e.g., comp. air, lights) |
| Loadshape C16 - Indust. 3-shift (24/5) (e.g., comp. air, lights) |
| Loadshape C17 - Indust. 4-shift (24/7) (e.g., comp. air, lights) |
| Loadshape C18 - Industrial Indoor Lighting |
| Loadshape C19 - Industrial Outdoor Lighting |
| Loadshape C20 - Commercial Outdoor Lighting |

###### Coincidence Factor

The summer peak coincidence factor for this measure is dependent on the building type.

**Algorithm**

###### Calculation of Savings

###### Energy Savings

ΔkWh = (WSFbase-WSFeffic )/1000\* SF\* Hours \* WHFe

Where:

WSFbase = Baseline lighting watts per square foot or linear foot as determined by building or space type. Whole building analysis values are presented in the Reference Tables below.[[530]](#footnote-531)

WSFeffic = The actual installed lighting watts per square foot or linear foot.

SF = Provided by customer based on square footage of the building area applicable to the lighting design for new building.

Hours = Annual site-specific hours of operation of the lighting equipment collected from the customer. If not available, use building area type as provided in the Reference Table in Section 4.5, Fixture annual operating hours.

WHFe  = Waste Heat Factor for Energy to account for cooling savings from efficient lighting is as provided in the Reference Table in Section 4.5 by buidling type. If building is not cooled WHFe is 1.

###### Heating Penalty

If electrically heated building:

ΔkWhheatpenalty[[531]](#footnote-532) = (WSFbase-WSFeffic )/1000\* SF\* Hours \* -IFkWh

Where:

IFkWh = Lighting-HVAC Interation Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficent lighting. Values are provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

###### Summer Coincident Peak Demand Savings

ΔkW = (WSFbase-WSFeffic )/1000\* SF\* CF \* WHFd

Where:

WHFd = Waste Heat Factor for Demand to account for cooling savings from efficient lighting in cooled buildings is as provided in the Reference Table in Section 4.5 by buidling type. If building is not cooled WHFd is 1.

CF = Summer Peak Coincidence Factor for measure is as provided in the Reference Table in Section 4.5 by buidling type. If the building type is unknown, use the Miscellaneous value of 0.66.

Other factors as defined above

**Natural Gas Energy Savings**

ΔTherms = (WSFbase-WSFeffic )/1000\* SF\* Hours \* - IFTherms

Where:

IFTherms = Lighting-HVAC Integration Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. This value is provided in the Reference Table in Section 4.5 by buidling type.

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

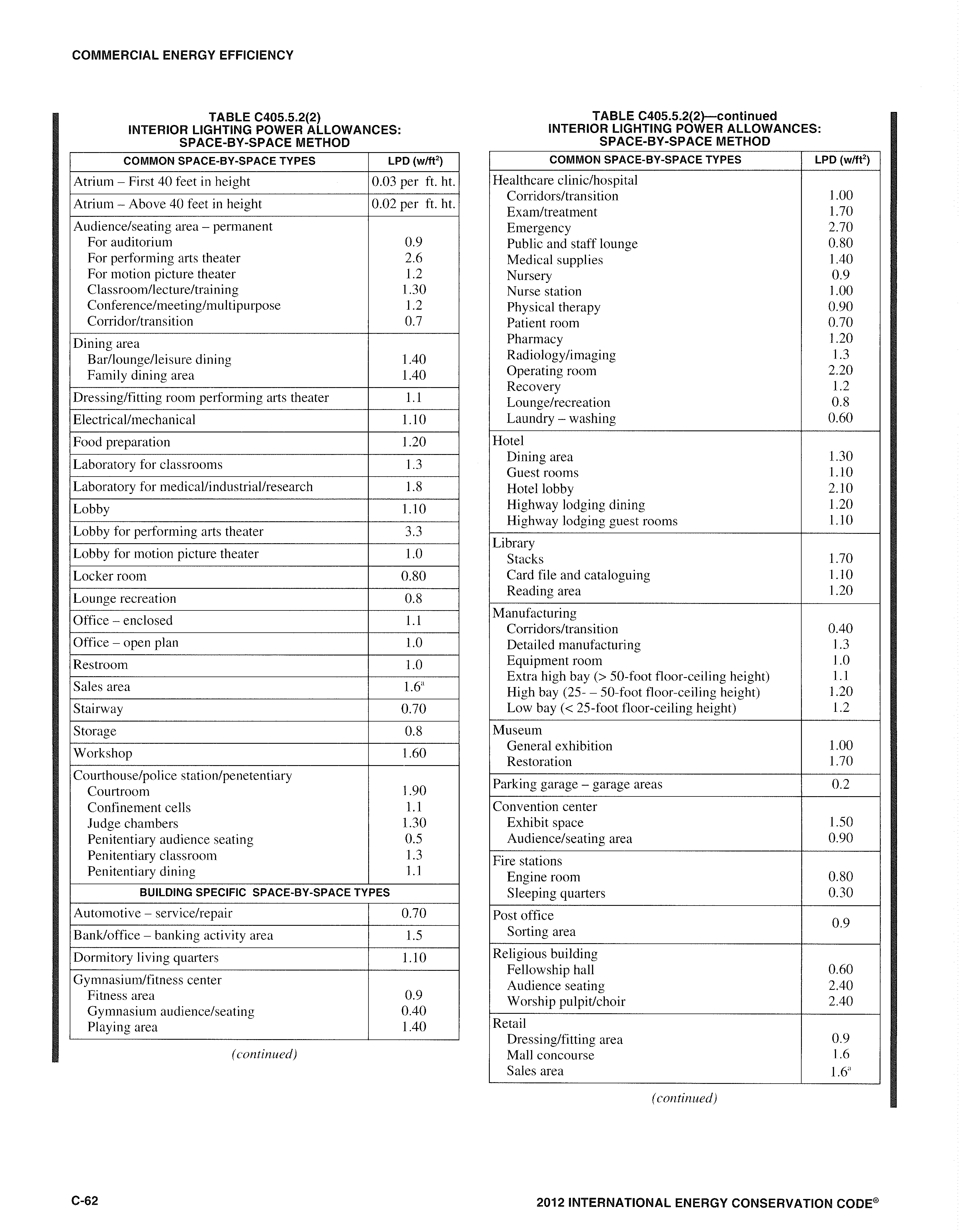
N/A

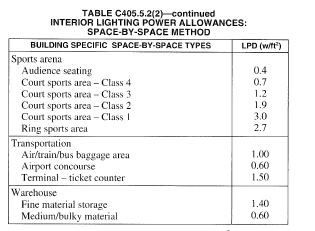
Reference Tables

Lighting Power Density Values from IECC 2012 for Interior Commercial New Construction and Substantial Renovation Building Area Method:

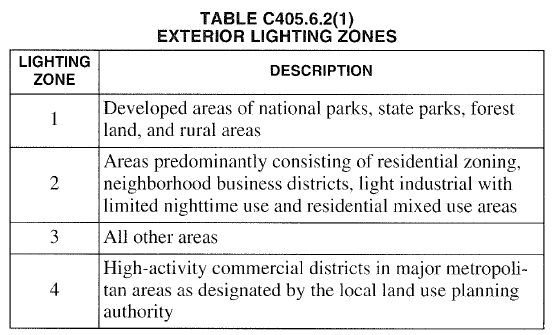
| Building Area Type [[532]](#footnote-533) | Lighting Power Density (w/ft2) |
| --- | --- |
| Automotive Facility | 0.9 |
| Convention Center | 1.2 |
| Court House | 1.2 |
| Dining: Bar Lounge/Leisure | 1.3 |
| Dining: Cafeteria/Fast Food | 1.4 |
| Dining: Family | 1.6 |
| Dormitory | 1.0 |
| Exercise Center | 1.0 |
| Fire station | 0.8 |
| Gymnasium | 1.1 |
| Healthcare – clinic | 1.0 |
| Hospital | 1.2 |
| Hotel | 1.0 |
| Library | 1.3 |
| Manufacturing Facility | 1.3 |
| Motel | 1.0 |
| Motion Picture Theater | 1.2 |
| Multifamily | 0.7 |
| Museum | 1.1 |
| Office | 0.9 |
| Parking Garage | 0.3 |
| Penitentiary | 1.0 |
| Performing Arts Theater | 1.6 |
| Police Station | 1.0 |
| Post Office | 1.1 |
| Religious Building | 1.3 |
| Retail[[533]](#footnote-534) | 1.4 |
| School/University | 1.2 |
| Sports Arena | 1.1 |
| Town Hall | 1.1 |
| Transportation | 1.0 |
| Warehouse | 0.6 |
| Workshop | 1.4 |

Lighting Power Density Values from IECC 2012 for Interior Commercial New Construction and Substantial Renovation Space by Space Method:

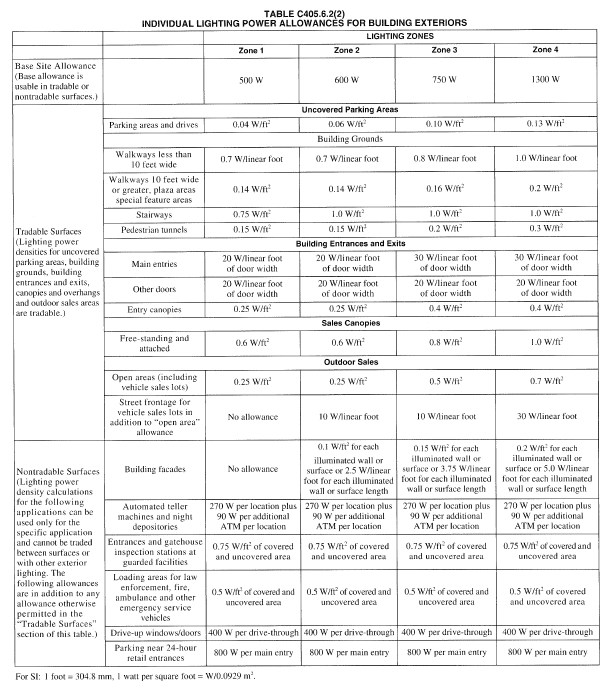




The exterior lighting design will be based on the building location and the applicable “Lighting Zone” as defined in IECC 2012 Table C405.6.2(1) which follows.



The lighting power density savings will be based on reductions below the allowable design levels as specified in IECC 2012 Table 405.6.2(2) which follows.



###### Measure Code: CI-LTG-LPDE-V02-1406

### Miscellaneous Commercial/Industrial Lighting

###### Description

This measure is designed to calculate savings from energy efficient lighting upgrades that are not captured in other measures within the TRM. If a lighting project fits the measure description in sections 4.5.1-4.5.4, then those criteria, definitions, and calculations should be used.

Unlike other lighting measures this one applies only to RF applications (because there is no defined baseline for TOS or NC applications).

###### Definition of Efficient Equipment

A lighting fixture that replaces an existing fixture to provide the same or greater lumen output at a lower kW consumption.

###### Definition of Baseline Equipment

The definition of baseline equipment is the existing lighting fixture.

###### Deemed Lifetime of Efficient Equipment

The deemed lifetime of the efficient equipment fixture, regardless of program type is 15 years[[534]](#footnote-535).

###### Deemed Measure Cost

The actual cost of the efficient light fixture should be used.

###### Loadshape

|  |
| --- |
| Loadshape C06 - Commercial Indoor Lighting |
| Loadshape C07 - Grocery/Conv. Store Indoor Lighting |
| Loadshape C08 - Hospital Indoor Lighting |
| Loadshape C09 - Office Indoor Lighting |
| Loadshape C10 - Restaurant Indoor Lighting |
| Loadshape C11 - Retail Indoor Lighting |
| Loadshape C12 - Warehouse Indoor Lighting |
| Loadshape C13 - K-12 School Indoor Lighting |
| Loadshape C14 - Indust. 1-shift (8/5) (e.g., comp. air, lights) |
| Loadshape C15 - Indust. 2-shift (16/5) (e.g., comp. air, lights) |
| Loadshape C16 - Indust. 3-shift (24/5) (e.g., comp. air, lights) |
| Loadshape C17 - Indust. 4-shift (24/7) (e.g., comp. air, lights) |
| Loadshape C18 - Industrial Indoor Lighting |
| Loadshape C19 - Industrial Outdoor Lighting |
| Loadshape C20 - Commercial Outdoor Lighting |

###### Coincidence Factor

The summer peak coincidence factor for this measure is dependent on the location type. Values are provided for each building type in section 4.5.

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = ((Wattsbase-WattsEE)/1000) \* Hours \* WHFe \* ISR

Where:

Wattsbase = Input wattage of the existing system which depends on the baseline fixture configuration (number and type of lamp) and ballast factor (if applicable) and number of fixtures.

=Actual

WattsEE = New Input wattage of EE fixture which depends on new fixture configuration (number of lamps) and ballast factor (if applicable) (if applicable) and number of fixtures.

= Actual

Hours = Average hours of use per year as provided by the customer or selected from the Reference Table in Section 4.5, Fixture annual operating hours, by building type. If hours or building type are unknown, use the Miscellaneous value.

WHFe = Waste heat factor for energy to account for cooling energy savings from efficient lighting is selected from the Reference Table in Section 4.5 for each building type. If building is un-cooled, the value is 1.0.

ISR = In Service Rate or the percentage of units rebated that get installed.

=100%[[535]](#footnote-536) if application form completed with sign off that equipment is not placed into storage

If sign off form not completed assume the following 3 year ISR assumptions:

|  |  |  |  |
| --- | --- | --- | --- |
| Weigted Average 1st year In Service Rate (ISR) | 2nd year Installations | 3rd year Installations | Final Lifetime In Service Rate |
| 75.5%[[536]](#footnote-537) | 12.1% | 10.3% | 98.0%[[537]](#footnote-538) |

###### Heating Penalty

If electrically heated building:

ΔkWhheatpenalty[[538]](#footnote-539) = (((WattsBase-WattsEE)/1000) \* ISR \* Hours \* -IFkWh

Where:

IFkWh = Lighting-HVAC Interation Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficent lighting. Values are provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

###### Deferred Installs

As presented above, if a sign off form is not completed the characterization assumes that a percentage of bulbs purchased are not installed until Year 2 and Year 3 (see ISR assumption above). The Illinois Technical Advisory Committee has determined the following methodology for calculating the savings of these future installs.

Year 1 (Purchase Year) installs: Characterized using assumptions provided above or evaluated assumptions if available.

Year 2 and 3 installs: Characterized using delta watts assumption and hours of use from the Install Year i.e. the actual deemed (or evaluated if available) assumptions active in Year 2 and 3 should be applied.

The NTG factor for the Purchase Year should be applied.

###### Summer Coincident Demand Savings

ΔkW = ((Wattsbase-WattsEE)/1000) \* WHFd \* CF \* ISR

Where:

WHFd = Waste Heat Factor for Demand to account for cooling savings from efficient lighting in cooled buildings is selected from the Reference Table in Section 4.5 for each building type. If the building is not cooled WHFd is 1.

CF = Summer Peak Coincidence Factor for measure is selected from the Reference able in Section 4.5 for each building type. If the building type is unknown, use the Miscellaneous value of 0.66.

Other factors as defined above

###### Natural Gas Energy Savings

ΔTherms[[539]](#footnote-540) = (((WattsBase-WattsEE)/1000) \* ISR \* Hours \* - IFTherms

Where:

IFTherms = Lighting-HVAC Integration Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. This value is selected from the Reference Table in Section 6.5 for each building type.

Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

If there are differences between the maintenance of the efficient and baseline lighting system then they should be evaluated on a project-by-project basis.

###### Measure Code: CI-LTG-MSCI-V02-140601

### Multi-Level Lighting Switch

###### Description

This measure relates to the installation new multi-level lighting switches on an existing lighting system.

This measure can only relate to the adding of a new control in an existing building, since multi-level switching is required in the Commercial new construction building energy code (IECC 2012).

This measure was developed to be applicable to the following program types: RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the efficient system is assumed to be a lighting system controlled by multi-level lighting controls.

###### Definition of Baseline Equipment

The baseline equipment is assumed to be an uncontrolled lighting system where all lights in a given area are on the same circuit or all circuits come on at the same time.

###### Deemed Lifetime of Efficient Equipment

The expected measure life for all lighting controls is assumed to be 8 years[[540]](#footnote-541).

###### Deemed Measure Cost

When available, the actual cost of the measure shall be used. When not available, the incremental capital cost for this measure is assumed to be $274[[541]](#footnote-542).

###### Loadshape

|  |
| --- |
| Loadshape C06 - Commercial Indoor Lighting |
| Loadshape C07 - Grocery/Conv. Store Indoor Lighting |
| Loadshape C08 - Hospital Indoor Lighting |
| Loadshape C09 - Office Indoor Lighting |
| Loadshape C10 - Restaurant Indoor Lighting |
| Loadshape C11 - Retail Indoor Lighting |
| Loadshape C12 - Warehouse Indoor Lighting |
| Loadshape C13 - K-12 School Indoor Lighting |
| Loadshape C14 - Indust. 1-shift (8/5) (e.g., comp. air, lights) |
| Loadshape C15 - Indust. 2-shift (16/5) (e.g., comp. air, lights) |
| Loadshape C16 - Indust. 3-shift (24/5) (e.g., comp. air, lights) |
| Loadshape C17 - Indust. 4-shift (24/7) (e.g., comp. air, lights) |
| Loadshape C18 - Industrial Indoor Lighting |
| Loadshape C19 - Industrial Outdoor Lighting |
| Loadshape C20 - Commercial Outdoor Lighting |

###### Coincidence Factor

The summer peak coincidence factor for this measure is dependent on the location type. Values are provided for each building type in the reference section below.

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = KWControlled\* Hours \* ESF \* WHFe

Where:

KWControlled = Total lighting load connected to the control in kilowatts.

= Actual

Hours = total operating hours of the controlled lighting circuit before the lighting controls are installed. This number should be collected from the customer. Average hours of use per year are provided in the Reference Table in Section 4.5, Fixture annual operating hours, for each building type if customer specific information is not collected. If unknown buidling type, use the Miscellaneous value.

ESF = Energy Savings factor (represents the percentage reduction to the KWcontrolled due to the use of multi-level switching).

= Dependent on building type[[542]](#footnote-543):

|  |  |
| --- | --- |
| **Building Type** | **Energy Savings Factor (ESF)** |
| Private Office | 21.6% |
| Open Office | 16.0% |
| Retail | 14.8% |
| Classrooms | 8.3% |
| Unknown, average | 15% |

WHFe = Waste heat factor for energy to account for cooling energy savings from efficient lighting is provided in the Reference Table in Section 4.5 for each building type. If building is un-cooled, the value is 1.0.

###### Heating Penalty

If electrically heated building:

ΔkWhheatpenalty[[543]](#footnote-544) = KWControlled\* Hours \* ESF \* -IFkWh

Where:

IFkWh = Lighting-HVAC Interation Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficent lighting. Values are provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

###### Summer Coincident Peak Demand Savings

ΔkW = KWcontrolled  \* ESF \* WHFd\* CF

Where:

WHFd = Waste Heat Factor for Demand to account for cooling savings from efficient lighting in cooled buildings is provided in the Reference Table in Section 4.5. If the building is un-cooled WHFd is 1.

CF = Summer Peak Coincidence Factor for measure is provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value of 0.66[[544]](#footnote-545).

###### Natural Gas Energy Savings

Δtherms = KWControlled\* Hours \* ESF \* - IFTherms

Where:

IFTherms = Lighting-HVAC Integration Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting and provided in the Reference Table in Section 4.5 by buidling type.

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-LTG-MLLC-V02-140601

### Occupancy Sensor Lighting Controls

###### Description

This measure relates to the installation of new occupancy sensors on a new or existing lighting system. Lighting control types covered by this measure include wall, ceiling or fixture mounted occupancy sensors. Passive infrared, ultrasonic detectors and fixture-mounted sensors or sensors with a combination thereof are eligible. Lighting controls required by state energy codes are not eligible. This must be a new installation and may not replace an existing lighting occupancy sensor control.

This measure was developed to be applicable to the following program types: RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the existing system is assumed to be manually controlled or an uncontrolled lighting system which is being controlled by one of the lighting controls systems listed above. All sensors must be hard wired and control interior lighting.

A subset of occupancy sensors are those that are programmed as “vacancy” sensors. To qualify as a vacancy sensor, the control must be configured such that manual input is required to turn on the controlled lighting and the control automatically turns the lighting off. Additional savings are achieved compared to standard occupancy sensors because lighting does not automatically turn on and occupants may decide to not turn it on. Note that vacancy sensors are not a viable option for many applications where standard occupancy sensors should be used instead.

###### Definition of Baseline Equipment

The baseline is assumed to be a lighting system uncontrolled by occupancy.

###### Deemed Lifetime of Efficient Equipment

The expected measure life for all lighting controls is assumed to be 8 years[[545]](#footnote-546).

###### Deemed Measure Cost

When available, the actual cost of the measure shall be used. When not available, the following default values are provided:

|  |  |
| --- | --- |
| Lighting control type | Cost |
| Full cost of wall mounted occupancy sensor | $42[[546]](#footnote-547) |
| Full cost mounted occupancy sensor | $66[[547]](#footnote-548) |
| Full cost of fixture-mounted occupancy sensor | $125[[548]](#footnote-549) |

###### Loadshape

|  |
| --- |
| Loadshape C06 - Commercial Indoor Lighting |
| Loadshape C07 - Grocery/Conv. Store Indoor Lighting |
| Loadshape C08 - Hospital Indoor Lighting |
| Loadshape C09 - Office Indoor Lighting |
| Loadshape C10 - Restaurant Indoor Lighting |
| Loadshape C11 - Retail Indoor Lighting |
| Loadshape C12 - Warehouse Indoor Lighting |
| Loadshape C13 - K-12 School Indoor Lighting |
| Loadshape C14 - Indust. 1-shift (8/5) (e.g., comp. air, lights) |
| Loadshape C15 - Indust. 2-shift (16/5) (e.g., comp. air, lights) |
| Loadshape C16 - Indust. 3-shift (24/5) (e.g., comp. air, lights) |
| Loadshape C17 - Indust. 4-shift (24/7) (e.g., comp. air, lights) |
| Loadshape C18 - Industrial Indoor Lighting |
| Loadshape C19 - Industrial Outdoor Lighting |
| Loadshape C20 - Commercial Outdoor Lighting |

###### Coincidence Factor

The summer peak coincidence factor for this measure is dependent on location.

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = KWControlled\* Hours \* ESF \* WHFe

Where:

KwControlled = Total lighting load connected to the control in kilowatts. Savings is per control. The total connected load per control should be collected from the customer or the default values presented below used;

|  |  |
| --- | --- |
| Lighting Control Type | Default kw controlled |
| Wall mounted occupancy sensor | 0.350[[549]](#footnote-550) |
| Remote mounted occupancy sensor | 0.587[[550]](#footnote-551) |
| Fixture mounted sensor | 0.073[[551]](#footnote-552) |

Hours = total operating hours of the controlled lighting circuit before the lighting controls are installed. This number should be collected from the customer. Average hours of use per year are provided in the Reference Table in Section 4.5, Fixture annual operating hours, for each building type if customer specific information is not collected. If unknown buidling type, use the Miscellaneous value.

ESF = Energy Savings factor (represents the percentage reduction to the operating Hours from the non-controlled baseline lighting system).

|  |  |
| --- | --- |
| Lighting Control Type | Energy Savings Factor[[552]](#footnote-553) |
| Wall or Ceiling-Mounted Occupancy Sensors | 41% or custom |
| Fixture Mounted Occupancy Sensors | 30% or custom |
| Wall-Mounted Occupancy Sensors Configured as “Vacancy Sensors” | 53% or custom[[553]](#footnote-554) |

WHFe = Waste heat factor for energy to account for cooling energy savings from efficient lighting is provided in the Reference Table in Section 4.5 for each building type. If building is un-cooled, the value is 1.0.

###### Heating Penalty

If electrically heated building:

ΔkWhheatpenalty[[554]](#footnote-555) = KWControlled\* Hours \* ESF \* -IFkWh

Where:

IFkWh = Lighting-HVAC Interation Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficent lighting. Values are provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

###### Summer Coincident Peak Demand Savings

ΔkW = KWcontrolled  \*WHFd\*(CFbaseline – CFos)

Where:

WHFd = Waste Heat Factor for Demand to account for cooling savings from efficient lighting in cooled buildings is provided in the Reference Table in Section 4.5. If the building is un-cooled WHFd is 1.

CFbaseline = Baseline Summer Peak Coincidence Factor for the lighting system without Occupancy Sensors installed selected from the Reference Table in Section 4.5 for each building type. If the building type is unknown, use the Miscellaneous value of 0.66

CFos = Retrofit Summer Peak Coincidence Factor the lighting system with Occupancy Sensors installed is 0.15 regardless of building type.[[555]](#footnote-556)

###### Natural Gas Energy Savings

Δtherms = KWControlled\* Hours \* ESF \* - IFTherms

Where:

IFTherms = Lighting-HVAC Integration Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting and provided in the Reference Table in Section 4.5 by buidling type.

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-LTG-OSLC-V02-140601

### Solar Light Tubes

###### Description

A tubular skylight which is 10” to 21” in diameter with a prismatic or translucent lens is installed on the roof of a commercial facility. The lens reflects light captured from the roof opening through a highly specular reflective tube down to the mounted fixture height. When in use, a light tube fixture resembles a metal halide fixture. Uses include grocery, school, retail and other single story commercial buildings.

In order that the savings characterized below apply, the electric illumination in the space must be automatically controlled to turn off or down when the tube is providing enough light.

This measure was developed to be applicable to the following program types:  TOS, NC, RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The efficient equipment is assumed to be a tubular skylight that concentrates and directs light from the roof to an area inside the facility.

###### Definition of Baseline Equipment

The baseline equipment for this measure is a fixture with comparable luminosity. The specifications for the baseline lamp depend on the size of the Light Tube being installed.

###### Deemed Lifetime of Efficient Equipment

The estimated useful life for a light tube commercial skylight is 10 years[[556]](#footnote-557).

###### Deemed Measure Cost

If available, the actual incremental cost should be used. For analysis purposes, assume an incremental cost for a light tube commercial skylight is $5002.

###### Loadshape

|  |
| --- |
| Loadshape C14 - Indust. 1-shift (8/5) (e.g., comp. air, lights)[[557]](#footnote-558) |

###### Coincidence Factor

The summer peak coincidence factor for this measure is dependent on location.

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = kWf\* HOURS \* WHFe

Where:

kWf *=* Connected load of the fixture the solar tube replaces

|  |  |  |  |
| --- | --- | --- | --- |
| **Size of Tube** | **Average Lumen output for Chicago Illinois (minimum)[[558]](#footnote-559)** | **Equivalent fixture** | **kW** |
| 21” | 9,775 (4,179) | 50% 3 x 2 32W lamp CFL (207W, 9915 lumens)  50% 4 lamp F32 w/Elec 4’ T8 (114W, 8895 lumens) | 0.161 |
| 14” | 4,392 (1,887) | 50% 2 42W lamp CFL (94W, 4406 lumens)  50% 2 lamp F32 w/Elec 4’ T8 (59W, 4448 lumens) | 0.077 |
| 10” | 2,157 (911) | 50% 1 42W lamp CFL (46W, 2203 lumens)  50% 1 lamp F32 w/Elec 4’ T8 (32W, 2224 lumens) | 0.039 |
|  |  | **AVERAGE** | **0.092** |

HOURS = Equivalent full load hours

= 2400 [[559]](#footnote-560)

WHFe = Waste heat factor for energy to account for cooling energy savings from efficient lighting is selected from the Reference Table in Section 4.5 for each building type. If building is un-cooled, the value is 1.0.

###### Heating Penalty

If electrically heated building:

ΔkWhheatpenalty[[560]](#footnote-561) = kWf\* HOURS \* -IFkWh

Where:

IFkWh = Lighting-HVAC Interation Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficent lighting. Values are provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

###### Summer Coincident Peak Demand Savings

∆kW*=* ∆kWf \* WHFd \*CF

Where:

WHFd = Waste Heat Factor for Demand to account for cooling savings from efficient lighting in cooled buildings is selected from the Reference Table in Section 4.5 for each building type. If the building is not cooled WHFd is 1.

CF = Summer Peak Coincidence Factor for measure is selected from the Reference Table in Section 4.5 for each building type. If the building type is unknown, use the Miscellaneous value of 0.66.

###### Natural Gas Savings

ΔTherms[[561]](#footnote-562) = ∆kWf \* HOURS \*- IFTherms

Where:

IFTherms = Lighting-HVAC Integration Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Please select from the Reference Table in Section 4.5 for each building type.

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-LTG-STUB-V02-140601

### T5 Fixtures and Lamps

###### Description

T5 Lamp/ballast systems have higher lumens per watt than a standard T8 or an existing T8 or T12 system. The smaller lamp diameter allows for better optical systems, and more precise control of lighting. These characteristics result in light fixtures that produce equal or greater light than standard T8 or T12 fixtures, while using fewer watts.

This measure applies to the installation of new equipment with efficiencies that exceed that of the equipment that would have been installed following standard market practices and is applicable to time of sale as well as retrofit measures.

If the implementation strategy does not allow for the installation location to be known, a deemed split of 98% Commercial and 2% Residential should be used[[562]](#footnote-563).

This measure was developed to be applicable to the following program types: TOS, RF.

If applied to other program types, the measure savings should be verified.

The measure applies to all commercial T5 installations excluding new construction and substantial renovation or change of use measures (see lighting power density measure). Lookup tables have been provided to account for various installations. Actual existing equipment wattages should be compared to new fixture wattages whenever possible while maintaining lumen equivalent designs. Default new and baseline assumptions are provided if existing equipment cannot be determined. Actual costs and hours of use should be utilized when available. Default component costs and lifetimes have been provided for Operating and Maintenance Calculations. Please see the Definition Table to determine applicability for each program. Configurations not included in the TRM may be included in custom program design using the provided algorithms as long as energy savings is achieved. The following table defines the applicability for different programs:

|  |  |
| --- | --- |
| Time of Sale (TOS) | Retrofit (RF) |
| This program applies to installations where customer and location of equipment is not known, or at time of burnout of existing equipment. T5 Lamp/ballast systems have higher lumens per watt than a standard T8 system. The smaller lamp diameter allows for better optical systems, and more precise control of lighting. These characteristics result in light fixtures that produce equal or greater light than standard T8 fixtures, while using fewer watts. | For installations that upgrade installations before the end of their useful life. T5 Lamp/ballast systems have higher lumens per watt than a standard T8 or T12 system. The smaller lamp diameter allows for better optical systems, and more precise control of lighting. These characteristics result in light fixtures that produce equal or greater light than standard T8 or T12 fixtures, while using fewer watts and having longer life. |

###### Definition of Efficient Equipment

The definition of efficient equipment varies based on the program and is defined below:

|  |  |
| --- | --- |
| Time of Sale (TOS) | Retrofit (RF) |
| 4' fixtures must use a T5 lamp and ballast configuration. 1' and 3' lamps are not eligible. High Performance Troffers must be 85% efficient or greater. T5 HO high bay fixtures must be 3, 4 or 6 lamps and 90% efficient or better. | 4' fixtures must use a T5 lamp and ballast configuration. 1' and 3' lamps are not eligible. High Performance Troffers must be 85% efficient or greater. T5 HO high bay fixtures must be 3, 4 or 6 lamps and 90% efficient or better. |

###### Definition of Baseline Equipment

The definition of baseline equipment varies based on the program and is defined below:

|  |  |
| --- | --- |
| Time of Sale (TOS) | Retrofit (RF) |
| The baseline is T8 with equivalent lumen output. In high-bay applications, the baseline is pulse start metal halide systems. | The baseline is the existing system. For T12 systems, the baseline becomes standard T8 in 2016.  Retrofits to T12 systems installed before 2016 have a baseline adjustment applied in 2016 for the remainder of the measure life.  Due to new federal standards for linear fluorescent lamps, manufacturers of T12 lamps will not be permitted to manufacture most varieties of T12 lamps for sale in the United States after July 2012. All remaining stock and previously manufactured product may be sold after the July 2012 effective date. If a customer relamps an existing T12 fixture the day the standard takes effect, an assumption can be made that they would likely need to upgrade to, at a minimum, 800-series T8s in less than 5 years’ time. This assumes the T12s installed have a typical rated life of 20,000 hours and are operated for 4500 hours annually (average miscellaneous hours 4576/year). Certainly, it is not realistic that everyone would wait until the final moment to relamp with T12s. Also, the exempted T12 lamps greater than 87 CRI will continue to be available to purchase, although they will be expensive. Therefore the more likely scenario would be a gradual shift to T8s over the 4 year timeframe. In other words, we can expect that for each year between 2012 and 2016, ~20% of the existing T12 lighting will change over to T8 lamps that comply with the federal standard. To simplify this assumption, we recommend assuming that standard T8s become the baseline for all T12 linear fluorescent retrofit January 1, 2016. There will be a baseline shift applied to all measures installed before 2016 in 2016 in years remaining in the measure life.. See table C-1. |

###### Deemed Lifetime of Efficient Equipment

The deemed lifetime of the efficient equipment fixture, regardless of program type is Fixture lifetime is 15 years[[563]](#footnote-564).

###### Loadshape

|  |
| --- |
| Loadshape C06 - Commercial Indoor Lighting |
| Loadshape C07 - Grocery/Conv. Store Indoor Lighting |
| Loadshape C08 - Hospital Indoor Lighting |
| Loadshape C09 - Office Indoor Lighting |
| Loadshape C10 - Restaurant Indoor Lighting |
| Loadshape C11 - Retail Indoor Lighting |
| Loadshape C12 - Warehouse Indoor Lighting |
| Loadshape C13 - K-12 School Indoor Lighting |
| Loadshape C14 - Indust. 1-shift (8/5) (e.g., comp. air, lights) |
| Loadshape C15 - Indust. 2-shift (16/5) (e.g., comp. air, lights) |
| Loadshape C16 - Indust. 3-shift (24/5) (e.g., comp. air, lights) |
| Loadshape C17 - Indust. 4-shift (24/7) (e.g., comp. air, lights) |
| Loadshape C18 - Industrial Indoor Lighting |
| Loadshape C19 - Industrial Outdoor Lighting |
| Loadshape C20 - Commercial Outdoor Lighting |

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh =( (Wattsbase-WattsEE)/1000) \* Hours \*WHFe\*ISR

Where:

|  |  |
| --- | --- |
| Program | Reference Table |
| Time of Sale | A-1: T5 New and Baseline Assumptions |
| Retrofit | A-2: T5 New and Baseline Assumptions |

Wattsbase = Input wattage of the existing system which depends on the baseline fixture configuration (number and type of lamp) and number of fixtures. Value can be selected from the appropriate reference table as shown below, of a custom value can be entered if the configurations in the tables is not representative of the exisitng system.

WattsEE = New Input wattage of EE fixture which depends on new fixture configuration (number of lamps) and ballast factor and number of fixtures. Value can be selected from the appropriate reference table as shown below, of a custom value can be entered if the configurations in the tables is not representative of the exisitng system.

|  |  |
| --- | --- |
| Program | Reference Table |
| Time of Sale | A-1: T5 New and Baseline Assumptions |
| Retrofit | A-2: T5 New and Baseline Assumptions |

Hours = Average hours of use per year as provided by the customer or selected from the Reference Table in Section 4.5, Fixture annual operating hours, by building type. If hours or building type are unknown, use the Miscellaneous value.

WHFe = Waste heat factor for energy to account for cooling energy savings from efficient lighting is selected from the Reference Table in Section 4.5 for each building type. If building is un-cooled, the value is 1.0.

ISR = In Service Rate or the percentage of units rebated that get installed.

=100%[[564]](#footnote-565) if application form completed with sign off that equipment is not placed into storage

If sign off form not completed assume the following 3 year ISR assumptions:

|  |  |  |  |
| --- | --- | --- | --- |
| Weigted Average 1st year In Service Rate (ISR) | 2nd year Installations | 3rd year Installations | Final Lifetime In Service Rate |
| 96%[[565]](#footnote-566) | 1.1% | 0.9% | 98.0%[[566]](#footnote-567) |

###### Heating Penalty

If electrically heated building:

ΔkWhheatpenalty[[567]](#footnote-568) = (((WattsBase-WattsEE)/1000) \* ISR \* Hours \* -IFkWh

Where:

IFkWh = Lighting-HVAC Interation Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficent lighting. Values are provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

###### Summer Coincident Demand Savings

ΔkW =((Wattsbase-WattsEE)/1000) \* WHFd\*CF\*ISR

Where:

WHFd = Waste Heat Factor for Demand to account for cooling savings from efficient lighting in cooled buildings is selected from the Reference Table in Section 4.5 for each building type. If the building is not cooled WHFd is 1.

CF = Summer Peak Coincidence Factor for measure is selected from the Reference Table in Section 4.5 for each building type. If the building type is unknown, use the Miscellaneous value of 0.66.

###### Natural Gas Energy Savings

ΔTherms[[568]](#footnote-569) = (((WattsBase-WattsEE)/1000) \* ISR \* Hours \*- IFTherms

Where:

IFTherms = Lighting-HVAC Integration Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. This value is selected from the Reference Table in Section 4.5 for each building type.

Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

See Reference tables for Operating and Maintenance Values

|  |  |
| --- | --- |
| Program | Reference Table |
| Time of Sale | B-1: T5 Component Costs and Lifetime |
| Retrofit | B-2: T5 Component Costs and Lifetime |

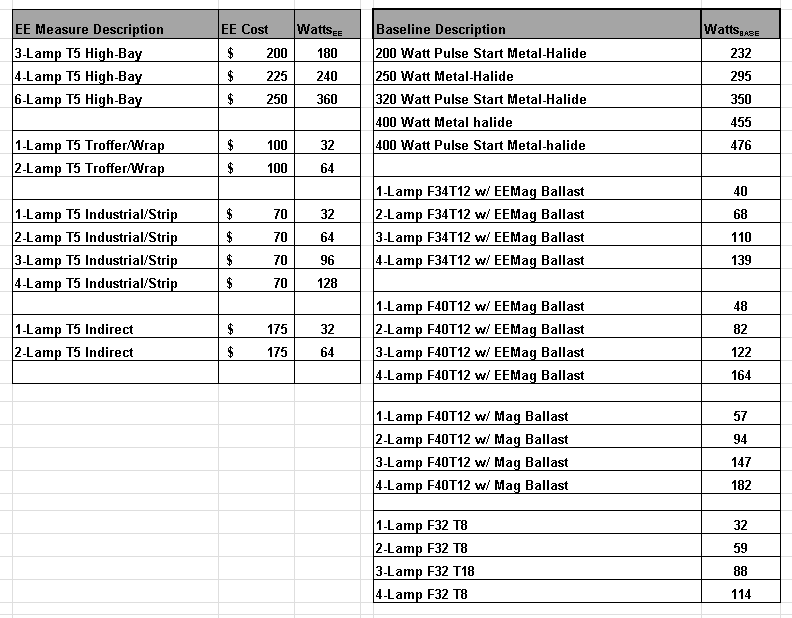
###### Reference Tables

See following page

A-1: Time of Sale: T5 New and Baseline Assumptions[[569]](#footnote-570)



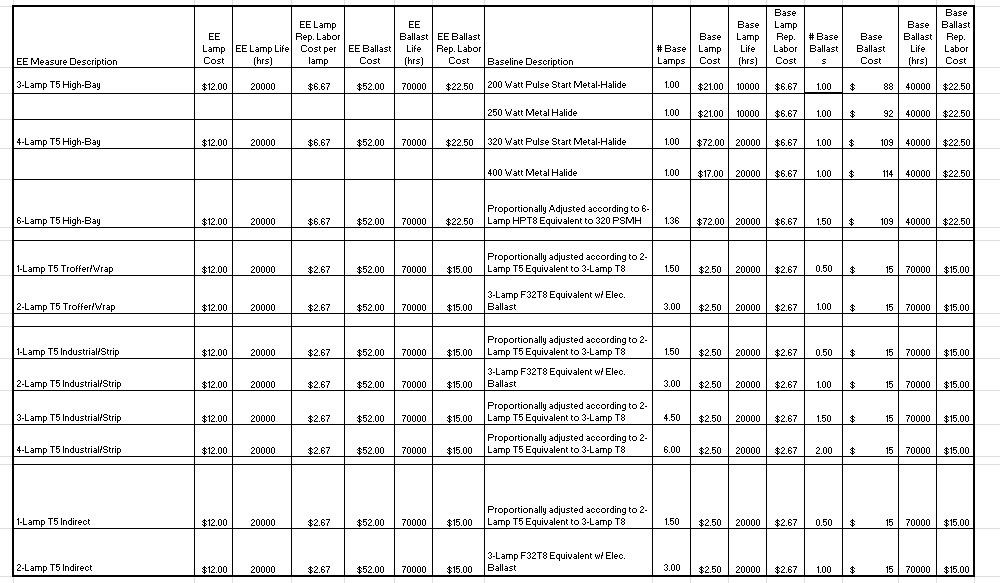
A-2: Retrofit T5 New and Baseline Assumptions[[570]](#footnote-571)



B-1: Time of Sale T5 Component Costs and Lifetime[[571]](#footnote-572)

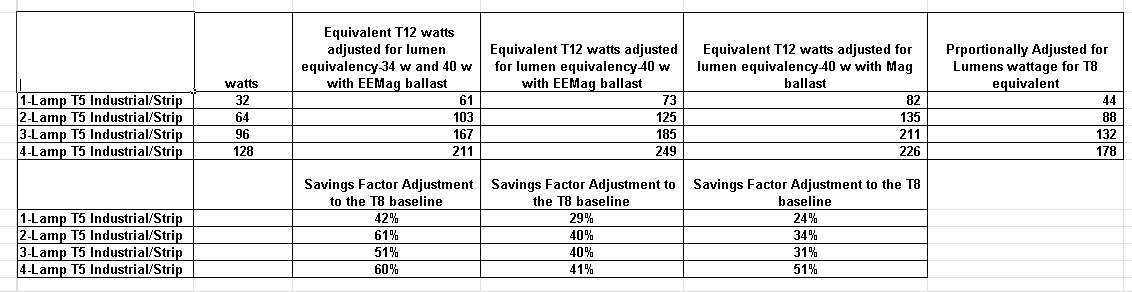


B-2: T5 Retrofit Component Costs and Lifetime[[572]](#footnote-573)



C-1: T12 Baseline Adjustment:

|  |  |  |  |
| --- | --- | --- | --- |
| Savings Adjustment Factors |  |  |  |



Measures installed in 2012 will claim full savings for four years, 2013 for three years, 2014 two years and 2015 one year.  Savings adjustment factors based on a T8 baseline will be applied to the full savings for savings starting in 2016 and for the remainder of the measure life. The adjustment to be applied for each measure is listed in the reference table above and is based on equivalent lumens.

###### Measure Code: CI-LTG-T5FX-V02-140601

### Occupancy Controlled Bi-Level Lighting Fixtures

###### Description

This measure relates to replacing existing uncontrolled continuous lighting fixtures with new bi-level lighting fixtures. This measure can only relate to replacement in an existing building, since multi-level switching is required in the Commercial new construction building energy code (IECC 2012).

This measure was developed to be applicable to the following program types: RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the efficient system is assumed to be an occupancy controlled lighting fixture that reduces light level during unoccupied periods.

###### Definition of Baseline Equipment

The baseline equipment is assumed to be an uncontrolled lighting system on continuously, e.g. in stairwells and corridors for health and safety reasons.

###### Deemed Lifetime of Efficient Equipment

The expected measure life for all lighting controls is assumed to be 8 years[[573]](#footnote-574).

###### Deemed Measure Cost

When available, the actual cost of the measure shall be used. When not available, the assumed measure cost is $274[[574]](#footnote-575).

###### Loadshape

|  |
| --- |
| Loadshape C06 - Commercial Indoor Lighting |
| Loadshape C07 - Grocery/Conv. Store Indoor Lighting |
| Loadshape C08 - Hospital Indoor Lighting |
| Loadshape C09 - Office Indoor Lighting |
| Loadshape C10 - Restaurant Indoor Lighting |
| Loadshape C11 - Retail Indoor Lighting |
| Loadshape C12 - Warehouse Indoor Lighting |
| Loadshape C13 - K-12 School Indoor Lighting |
| Loadshape C14 - Indust. 1-shift (8/5) (e.g., comp. air, lights) |
| Loadshape C15 - Indust. 2-shift (16/5) (e.g., comp. air, lights) |
| Loadshape C16 - Indust. 3-shift (24/5) (e.g., comp. air, lights) |
| Loadshape C17 - Indust. 4-shift (24/7) (e.g., comp. air, lights) |
| Loadshape C18 - Industrial Indoor Lighting |
| Loadshape C19 - Industrial Outdoor Lighting |
| Loadshape C20 - Commercial Outdoor Lighting |

###### Coincidence Factor

The summer peak coincidence factor for this measure is dependent on the location type. Values are provided for each building type in the reference section below.

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = (KWBaseline - (KWControlled \*(1 –ESF))) \* Hours \* WHFe

Where:

KWBaseline = Total baseline lighting load of the existing/baseline fixture

= Actual

Note that if the existing fixture is only being retrofit with bi-level occpuancy controls and not being replaced KWBaseline will equal KWControlled .

KWControlled = Total contolled lighting load at full light output of the new bi-level fixture

= Actual

Hours = Number of hours lighting is on. This measure is limited to 24/7 operation.

= 8,766

ESF = Energy Savings factor (represents the percentage reduction to the KWControlled due to the occupancy control).

= % Standby Mode \* (1 - % Full Light at Standby Mode)

% Standby Mode = Represents the percentage of the time the fixture is operating in standby (i.e. low-wattage) mode.

% Full Light at Standby Mode = Represents the assumed wattage consumption during standby mode relative to the full wattage consumption. Can be achieved either through dimming or a stepped control strategy.

= Dependent on application. If customer provided or metered data is available for both or either of these inputs a custom savings factor should be calculated. If not defaults are provided below:

|  |  |  |  |
| --- | --- | --- | --- |
| **Application** | **% Standby Mode** | **% Full Light at Standby Mode** | **Energy Savings Factor (ESF)** |
| Stairwells | 78.5%[[575]](#footnote-576) | 50% | 39.3% |
| 33% | 52.6% |
| 10% | 70.7% |
| 5% | 74.6% |
| Corridors | 50.0%[[576]](#footnote-577) | 50% | 25.0% |
| 33% | 33.5% |
| 10% | 45.0% |
| 5% | 47.5% |
| Other 24/7 Space Type | 50.0%[[577]](#footnote-578) | 50% | 25.0% |
| 33% | 33.5% |
| 10% | 45.0% |
| 5% | 47.5% |

WHFe = Waste heat factor for energy to account for cooling energy savings from efficient lighting is provided in the Reference Table in Section 4.5 for each building type. If building is un-cooled, the value is 1.0.

###### Heating Penalty

If electrically heated building:

ΔkWhheatpenalty[[578]](#footnote-579) = (KWBaseline - (KWControlled \*(1 –ESF))) \* Hours \* -IFkWh

Where:

IFkWh = Lighting-HVAC Interation Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficent lighting. Values are provided in the Reference Table in Section 4.5. If unknown, use the Miscellaneous value.

###### Summer Coincident Peak Demand Savings

ΔkW = (KWBaseline - (KWControlled \* (1 –ESF))) \* WHFd \* (CFbaseline - CFos)

Where:

WHFd = Waste Heat Factor for Demand to account for cooling savings from efficient lighting in cooled buildings is provided in the Reference Table in Section 4.5. If the building is un-cooled WHFd is 1.

CFbaseline = Baseline Summer Peak Coincidence Factor for the lighting system without Occupancy Sensors installed selected from the Reference Table in Section 4.5 for each building type. If the building type is unknown, use the Miscellaneous value of 0.66

CFos = Retrofit Summer Peak Coincidence Factor the lighting system with Occupancy Sensors installed is 0.15 regardless of building type.[[579]](#footnote-580)

###### Natural Gas Heating Penalty

If natural gas heating:

Δtherms = (KWBaseline - (KWControlled \*(1 –ESF))) \* Hours \* - IFTherms

Where:

IFTherms = Lighting-HVAC Integration Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting and provided in the Reference Table in Section 4.5 by buidling type.

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-LTG-OCBL-V01-140601

## Refrigeration End Use

### Automatic Door Closer for Walk-In Coolers and Freezers

###### Description

This measure is for installing an auto-closer to the main insulated opaque door(s) of a walk-in cooler or freezer. The auto-closer must firmly close the door when it is within 1 inch of full closure.

This measure was developed to be applicable to the following program types: RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

This measure consists of the installation of an automatic, hydraulic-type door closer on main walk-in cooler or freezer doors. These closers save energy by reducing the infiltration of warm outside air into the refrigeration itself.

###### Definition of Baseline Equipment

In order for this characterization to apply, the baseline condition is assumed to be a walk in cooler or freezer without an automatic closure.

###### Deemed Lifetime of Efficient Equipment

The deemed measure life is 8 years.[[580]](#footnote-581)

###### Deemed Measure Cost

The deem measure cost is $156.82 for a walk-in cooler or freezer.[[581]](#footnote-582)

###### Loadshape

Loadshape C22 - Commercial Refrigeration

###### Coincidence Factor

The measure has deemed kW savings therefore a coincidence factor does not apply

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

Savings calculations are based on values from through PG&E’s Workpaper PGECOREF110.1 – Auto-Closers for Main Cooler or Freezer Doors. Savings are averaged across all California climate zones and vintages[[582]](#footnote-583).

|  |  |
| --- | --- |
| Annual Savings | kWh |
| Walk in Cooler | 943 kWh |
| Walk in Freezer | 2307 kWh |

###### Summer Coincident Peak Demand Savings

|  |  |
| --- | --- |
| Annual Savings | kW |
| Walk in Cooler | 0.137 kW |
| Walk in Freezer | 0.309 kW |

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-RFG-ATDC-V01-120601

### Beverage and Snack Machine Controls

###### Description

This measure relates to the installation of new controls on refrigerated beverage vending machines, non-refrigerated snack vending machines, and glass front refrigerated coolers. Controls can significantly reduce the energy consumption of vending machine and refrigeration systems. Qualifying controls must power down these systems during periods of inactivity but, in the case of refrigerated machines, must always maintain a cool product that meets customer expectations. This measure relates to the installation of a new control on a new or existing unit. This measure should **not** be applied to ENERGY STAR qualified vending machines, as they already have built-in controls.

This measure was developed to be applicable to the following program types: RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the efficient equipment is assumed to be a standard efficiency refrigerated beverage vending machine, non-refrigerated snack vending machine, or glass front refrigerated cooler with a control system capable of powering down lighting and refrigeration systems during periods of inactivity.

###### Definition of Baseline Equipment

In order for this characterization to apply, the baseline equipment is assumed to be a standard efficiency refrigerated beverage vending machine, non-refrigerated snack vending machine, or glass front refrigerated cooler without a control system capable of powering down lighting and refrigeration systems during periods of inactivity

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 5 years [[583]](#footnote-584).

###### Deemed Measure Cost

The actual measure installation cost should be used (including material and labor), but the following can be assumed for analysis purposes[[584]](#footnote-585):

Refrigerated Vending Machine and Glass Front Cooler: $180.00

Non-Refrigerated Vending Machine: $80.00

###### Loadshape

Loadshape C52 - Beverage and Snack Machine Controls

###### Coincidence Factor

The summer peak coincidence factor for this measure is assumed to be 0[[585]](#footnote-586).

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = WATTSbase / 1000 \* HOURS \* ESF

Where:

WATTSbase = connected W of the controlled equipment; see table below for default values by connected equipment type:

|  |  |
| --- | --- |
| Equipment Type | WATTSbase[[586]](#footnote-587) |
| Refrigerated Beverage Vending Machines | 400 |
| Non-Refrigerated Snack Vending Machines | 85 |
| Glass Front Refrigerated Coolers | 460 |

1000 = conversion factor (W/kW)

HOURS = operating hours of the connected equipment; assumed that the equipment operates 24 hours per day, 365.25 days per year

= 8766

ESF = Energy Savings Factor; represents the percent reduction in annual kWh consumption of the equipment controlled; see table below for default values:

|  |  |
| --- | --- |
| Equipment Type | Energy Savings Factor (ESF)[[587]](#footnote-588) |
| Refrigerated Beverage Vending Machines | 46% |
| Non-Refrigerated Snack Vending Machines | 46% |
| Glass Front Refrigerated Coolers | 30% |

EXAMPLE

For example, adding controls to a refrigerated beverage vending machine:

ΔkWh = WATTSbase / 1000 \* HOURS \* ESF

=400/1000\* 8766\* .46 = 1.6 kWh

###### Summer Coincident Peak Demand Savings

N/A

###### NATURAL GAS ENERGY SAVINGS

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-RFG-BEVM-V01-120601

### Door Heater Controls for Cooler or Freezer

###### Description

By installing a control device to turn off door heaters when there is little or no risk of condensation, one can realize significant energy savings. There are two commercially available control strategies that achieve “on-off” control of door heaters based on either (1) the relative humidity of the air in the store or (2) the “conductivity” of the door (which drops when condensation appears). In the first strategy, the system activates your door heaters when the relative humidity in your store rises above a specific setpoint, and turns them off when the relative humidity falls below that setpoint. In the second strategy, the sensor activates the door heaters when the door conductivity falls below a certain setpoint, and turns them off when the conductivity rises above that setpoint.

This measure was developed to be applicable to the following program types: RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the efficient equipment is assumed to be a door heater control on a commercial glass door cooler or refrigerator utilizing humidity or conductivity control.

###### Definition of Baseline Equipment

In order for this characterization to apply, the baseline condition is assumed to be a commercial glass door cooler or refrigerator with a standard heated door with no controls installed.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 12 years [[588]](#footnote-589).

###### Deemed Measure Cost

The incremental capital cost for a humidity-based control is $300 per circuit regardless of the number of doors controlled. The incremental cost for conductivity-based controls is $200[[589]](#footnote-590).

###### Loadshape

Loadshape C51 - Door Heater Control

###### Coincidence Factor[[590]](#footnote-591)

The summer peak coincidence factor for this measure is assumed to be 0%[[591]](#footnote-592).

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWH = kWbase \* NUMdoors \* ESF \* BF \*8760

Where:

kWbase[[592]](#footnote-593) = connected load kW for typical reach-in refrigerator or freezer door and frame with a heater.

= If actual kWbase is unknown, assume 0.195 kW for freezers and 0.092 kW for coolers.

NUMdoors = number of reach-in refrigerator or freezer doors controlled by sensor

= Actual installed

ESF[[593]](#footnote-594) = Energy Savings Factor; represents the percentage of hours annually that the door heater is powered off due to the controls.

= assume 55% for humidity-based controls, 70% for conductivity-based controls

BF[[594]](#footnote-595) = Bonus Factor; represents the increased savings due to reduction in cooling load inside the cases, and the increase in cooling load in the building space to cool the additional heat generated by the door heaters.

|  |  |  |  |
| --- | --- | --- | --- |
| Definition | Representative Evaporator Temperature Range, °F[[595]](#footnote-596) | Typical Uses | BF |
| Low | -35 to 0 | Freezers for times such as frozen pizza, ice cream, etc. | 1.36 |
| Medium | 0 – 20 | Coolers for items such as meat, milk, dairy, etc | 1.22 |
| High | 20 – 45 | Coolers for items such as floral, produce and meat preperation rooms | 1.15 |

8760 = annual hours of operation

###### Summer Coincident Peak Demand Savings

N/A

###### NATURAL GAS ENERGY SAVINGS

N/A

###### Water Impact Descriptions and Calculation

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

###### Measure Code: CI-RFG-DHCT-V01-120601

### Electronically Commutated Motors (ECM) for Walk-in and Reach-in Coolers / Freezers

###### Description

This measure is applicable to the replacement of an existing standard-efficiency shaded-pole evaporator fan motor in refrigerated display cases or fan coil in walk-ins.

This measure was developed to be applicable to the following program types: RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

This measure applies to the replacement of an existing standard-efficiency shaded-pole evaporator fan motor in refrigerated display cases or fan coil in walk-ins. The replacement unit must be an electronically commutated motor (ECM). This measure cannot be used in conjunction with the evaporator fan controller measure

###### Definition of Baseline Equipment

In order for this characterization to apply, the baseline equipment is assumed to be a shaded pole motor

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 15 years[[596]](#footnote-597)

###### Deemed Measure Cost

The measure cost is assumed to be $50 for a walk in cooler and walk in freezer. [[597]](#footnote-598)

###### Loadshape

Loadshape C22 - Commercial Refrigeration

###### Coincidence Factor

The measure has deemed peak kW savings therefore a coincidence factor does not apply.

**Algorithm**

###### Calculation of Savings [[598]](#footnote-599)

Savings values are obtained from the SCE workpaper for efficient evaporator fan motors, which covers all 16 California climate zones. SCE savings values were determined using a set of assumed conditions for restaurants and grocery stores. We have used only PG&E climate zones in calculating our averages and have taken out the drier, warmer climates of southern California. SCE’s savings approach calculates refrigeration demand, by taking into consideration temperature, compressor efficiency, and various loads involved for both walk-in and reach-in refrigerators. Details on cooling load calculations, including refrigeration conditions, can be found in the SCE workpaper. The baseline for this measure assumes that the refrigeration unit has a shaded-pole motor. The following tables are values calculated within the SCE workpaper.

Table 156 SCE Restaurant Savings Walk-In

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
|  | Restaurant | | | |
| SCE Workpaper Values | Cooler | | Freezer | |
| Northern California Climate Zones | kWh Savings Per Motor | Peak kW Savings Per Motor | kWh Savings Per Motor | Peak kW Savings Per Motor |
| 1 | 318 | 0.0286 | 507 | 0.03 |
| 2 | 253 | 0.033 | 263 | 0.037 |
| 3 | 364 | 0.0315 | 649 | 0.034 |
| 4 | 365 | 0.0313 | 652 | 0.034 |
| 5 | 350 | 0.0305 | 605 | 0.033 |
| 11 | 410 | 0.0351 | 780 | 0.04 |
| 12 | 399 | 0.034 | 748 | 0.039 |
| 13 | 407 | 0.0342 | 771 | 0.039 |
| 16 | 354 | 0.0315 | 620 | 0.034 |
| Average | 358 | 0.0322 | 622 | 0.036 |

Table 157: SCE Grocery Savings Walk-In

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
|  | Grocery | | | |
| SCE Workpaper Values | Cooler | | Freezer | |
| Northern California Climate Zones | kWh Savings Per Motor | Peak kW Savings Per Motor | kWh Savings Per Motor | Peak kW Savings Per Motor |
| 1 | 318 | 0.0284 | 438 | 0.03 |
| 2 | 252 | 0.0534 | 263 | 0.064 |
| 3 | 364 | 0.0486 | 552 | 0.056 |
| 4 | 365 | 0.048 | 553 | 0.055 |
| 5 | 349 | 0.0452 | 516 | 0.051 |
| 11 | 410 | 0.0601 | 656 | 0.074 |
| 12 | 398 | 0.0566 | 631 | 0.069 |
| 13 | 406 | 0.0574 | 649 | 0.07 |
| 16 | 354 | 0.0486 | 528 | 0.056 |
| Average | 357 | 0.0496 | 532 | 0.058 |

Table 158: SCE Grocery Savings Reach-In

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
|  | Grocery |  |  |  |
| SCE Workpaper Values | Cooler | | Freezer | |
| Northern California Climate Zones | kWh Savings Per Motor | Peak kW Savings Per Motor | kWh Savings Per Motor | Peak kW Savings Per Motor |
| 1 | 306 | 0.031 | 362 | 0.031 |
| 2 | 269 | 0.033 | 273 | 0.035 |
| 3 | 331 | 0.032 | 421 | 0.034 |
| 4 | 332 | 0.032 | 422 | 0.034 |
| 5 | 323 | 0.032 | 402 | 0.033 |
| 11 | 357 | 0.034 | 476 | 0.037 |
| 12 | 350 | 0.034 | 462 | 0.036 |
| 13 | 355 | 0.034 | 472 | 0.037 |
| 16 | 325 | 0.032 | 409 | 0.034 |
| Average | 328 | 0.033 | 411 | 0.035 |

Savings values in the following table are an average of walk-in cooler (80 percent) and freezer (20 percent) applications. The workpapers for the 2006-2008 program years include this distribution of coolers and freezers in their refrigeration measure savings analyses.

###### Electric Energy Savings

The following table provides the kWh savings.

|  |  |
| --- | --- |
| Building type | kWh Savings/ft |
| Restaurant | 411 |
| Grocery | 392 |
| Average | 401 |

###### Summer Coincident Peak Demand Savings

The following table provides the kW savings

|  |  |
| --- | --- |
| Building Type | Peak kW Savings/motor |
| Restaurant | 0.033 |
| Grocery | 0.051 |
| Average | 0.042 |

###### NATURAL GAS ENERGY SAVINGS

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-RFG-ECMF-V01-120601

### ENERGY STAR Refrigerated Beverage Vending Machine

###### Description

ENERGY STAR qualified new and rebuilt vending machines incorporate more efficient compressors, fan motors, and lighting systems as well as low power mode option that allows the machine to be placed in low-energy lighting and/or low-energy refrigeration states during times of inactivity.

This measure was developed to be applicable to the following program types: TOS, NC .

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The refrigerated vending machine can be new or rebuilt but must meet the ENERGY STAR specifications which include low power mode.

###### Definition of Baseline Equipment

The baseline vending machine is a standard unit

###### Deemed Lifetime of Efficient Equipment

The deemed lifetime of this measure is 14 years[[599]](#footnote-600)

###### Deemed Measure Cost

The incremental cost of this measure is $500[[600]](#footnote-601)

###### Loadshape

Loadshape C22 - Commercial Refrigeration

###### Coincidence Factor

It is assumed that controls are only effective during off-peak hours and so have no peak-kW savings.

**Algorithm**

###### Calculation of Savings

Beverage machine savings are taken from the ENERGY STAR savings calculator and summarized in the following table. ENERGY STAR provides savings numbers for machines with and without control software. The average savings are calculated here.

###### Electric Energy Savings

ENERGY STAR Vending Machine Savings[[601]](#footnote-602)

|  |  |  |
| --- | --- | --- |
| Vending Machine Capacity (cans) | kWh Savings Per Machine w/o software | kWh Savings Per Machine w/ software |
| <500 | 1,099 | 1,659 |
| 500 | 1,754 | 2,231 |
| 699 | 1,242 | 1,751 |
| 799 | 1,741 | 2,283 |
| 800+ | 713 | 1,288 |
| Average | 1,310 | 1,842 |

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-RFG-ESVE-V01-120601

### Evaporator Fan Control

###### Description

This measure is for the installation of controls in existing medium temperature walk-in coolers. The controller reduces airflow of the evaporator fans when there is no refrigerant flow.

This measure was developed to be applicable to the following program types: RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The measure must control a minimum of 1/20 HP where fans operate continuously at full speed. The measure also must reduce fan motor power by at least 75% during the off cycle. This measure is not applicable if any of the following conditions apply:

* The compressor runs all the time with high duty cycle
* The evaporator fan does not run at full speed all the time
* The evaporator fan motor runs on poly-phase power
* Evaporator does not use off-cycle or time-off defrost.

###### Definition of Baseline Equipment

In order for this characterization to apply, the baseline measure is assumed to be a cooler with continuously running evaporator fan. An ECM can also be updated with controls.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 16 years[[602]](#footnote-603)

###### Deemed Measure Cost

The measure cost is assumed to be $291[[603]](#footnote-604)

###### Loadshape

Loadshape C46 - Evaporator Fan Control

###### Coincidence Factor

The measure has deemed kW savings therefore a coincidence factor does not apply.

**Algorithm**

###### Calculation of Savings

Savings for this measure were obtained from the DEER database. The baseline is assumed to be evaporator fans that run continuously with either a permanent split capacitor or shaded-pole motors. In the energy-efficient case the fan is still assumed to operate even with the evaporator inactive.[[604]](#footnote-605)

###### Electric Energy Savings

DEER provides savings numbers for building vintages and grocery only. The numbers are averages of these vintages. We are assuming that this measure will be applicable for all building types. The DEER savings vary by climate zone between 476 and 483 kWh/motor. Climate zone most closely remembling IL are 1, 3, and 16. The simple average of the savings in those zones is given below.[[605]](#footnote-606)

ΔkWh = Savings per motor \* motors

Where:

Savings per motor = 481 kWh

motors = number of fan motors controlled

###### Summer Coincident Peak Demand Savings

Using the same source and methodology as for ΔkWh:

ΔkW = 0.060 kW

###### NATURAL GAS ENERGY SAVINGS

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-RFG-EVPF-V02-140601

### Strip Curtain for Walk-in Coolers and Freezers

**Description**

This commercial measure pertains to the installation of infiltration barriers (strip curtains) on walk-in coolers or freezers. Strip curtains impede heat transfer from adjacent warm and humid spaces into walk-ins when the main door is opened, thereby reducing the cooling load. As a result, compressor run time and energy consumption are reduced. The engineering assumption is that the walk-in door is open 72 minutes per day every day, and the strip curtain covers the entire door frame.

This measure was developed to be applicable to the following program types: RF.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

The efficient equipment is a polyethylene strip curtain added to a walk-in cooler or freezer

**Definition of Baseline Equipment**

The baseline assumption is a walk-in cooler or freezer that previously had either no strip curtain installed or an old, ineffective strip curtain installed.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 6 years[[606]](#footnote-607).

**Deemed Measure Cost**

The incremental capital cost for this measure is $286.16 [[607]](#footnote-608)

**Loadshape**

Loadshape C22 - Commercial Refrigeration

**Coincidence Factor**

The summer peak coincidence factor for this measure is 100%[[608]](#footnote-609).

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings[[609]](#footnote-610)

ΔkWh = 2,974 per freezer with curtains installed

= 422 per cooler with curtains installed

###### Summer Coincident Peak Demand Savings

ΔkW = ΔkWh / 8760 \* CF

= 0.35 for freezers

= 0.05 for coolers

Where:

8766 = hours per year

CF = Summer Peak Coincidence Factor for the measure

= 1.0

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-RFG-CRTN-V02-130601

### Refrigeration Economizers

**Description**

This measure applies to commercial walk in refrigeration systems and includes two components, outside air economizers and evaporator fan controllers. Economizers save energy by bringing in outside air when weather conditions allow, rather than operating the compressor. Walk-in refrigeration systems evaporator fans run almost all the time; 24 hrs/day, 365 days/yr. This is because they must run constantly to provide cooling when the compressor is running, and to provide air circulation when the compressor is not running. However, evaporator fans are a very inefficient method of providing air circulation. Installing an evaporator fan control system will turn off evaporator fans while the compressor is not running, and instead turn on an energy-efficient 35 watt fan to provide air circulation, resulting in significant energy savings. This measures allows for economizer systems with evaporator fan controls plus a circulation fan and without a circulation fan.

**Definition of Efficient Equipment**

To qualify for this measure an economizer is installed on a walk in refrigeration system.

**Definition of Baseline Equipment**

The baseline condition is a walk-in refrigeration system without an economizer

**Deemed Lifetime of Efficient Equipment**

The estimated life of this measure is 15 years[[610]](#footnote-611).

**Deemed Measure Cost**

The installation cost for an economizer is $2,558.[[611]](#footnote-612)

**Loadshape**

Loadshape C22 - Commercial Refrigeration

**Coincidence Factor**

The summer peak coincidence factor for this measure is assumed to be 0%[[612]](#footnote-613).

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

Electric energy savings is calculated based on whether evaporator fans run all

With Fan Control Installed

ΔkWh = [HP x kWhCond] + [((kWEvap x nFans) – kWCirc) x Hours x DCComp x BF] – [kWEcon x DCEcon x Hours]

Without Fan Control Installed

ΔkWh = [HP x kWhCond] – [kWEcon x DCEcon x Hours]

Where:

HP = Horsepower of Compressor

= actual installed

kWhCond = Condensing unit savings, per hp. (value from savings table) [[613]](#footnote-614)

|  |  |  |  |
| --- | --- | --- | --- |
|  | **Hermetic / Semi-Hermetic** | **Scroll** | **Discus** |
| kWh/HP | 1,256 | 1,108 | 1,051 |

Hours = Number of annual hours that economizer operates [[614]](#footnote-615).

|  |  |
| --- | --- |
| **Region (city)** | **Hours** |
| 1 (Rockford) | 2,376 |
| 2 (Chicago/O’Hare) | 1,968 |
| 3 (Springfield) | 1,728 |
| 4 (Belleview) | 1,488 |
| 5 (Marion) | 1,224 |

DCComp = Duty cycle of the compressor

= 50% [[615]](#footnote-616)

kWEvap = Connected load kW of each evaporator fan,

= If known, actual installed. Otherwise assume 0.123 kW[[616]](#footnote-617)

kWCirc = Connected load kW of the circulating fan

= If known, actual installed. Otherwise assume 0.035 kW[[617]](#footnote-618)

nFans = Number of evaporator fans

= actual number of evaporator fans

DCEcon = Duty cycle of the economizer fan on days that are cool enough for the economizer to be working

= If known, actual installed. Otherwise assume 63%[[618]](#footnote-619)

BF = Bonus factor for reduced cooling load from running the evaporator fan less or (1.3)[[619]](#footnote-620)

kWEcon = Connected load kW of the economizer fan

= If known, actual installed. Otherwise assume 0.227 kW.[[620]](#footnote-621)

EXAMPLE

For example, adding an outdoor air economizer and fan controls in Rockford to a 5 hp walk in refrigeration unit with 3 evaporator fans would save:

ΔkWh = [HP \* kWhCond] + [((kWEvap ´\*nFans)) \* Hours ´\*DCComp \* BF] – [kWEcon \* DCEcon \* Hours]

= [5 \* 1256] + [((0.123 ´\*3)) \* 2376 ´\*0.5 \* 1.3] – [0.227 \* .63 \* 2376]

= 6510 kWh

**Summer Coincident Peak Demand Savings**

ΔkW= ΔkWh / Hours

**Natural Gas Savings**

N/A

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure code: CI-RFG-ECON-V04-140601**

### Night Covers for Open Refrigerated Display Cases

**Description**

This measure is the installation of fitted covers on existing open-type refrigerated and freezer display cases that are deployed during the facility unoccupied hours. Night covers are designed to reduce refrigeration energy consumption by reducing the work done by the compressor. Night covers reduce the heat and moisture entry into the refrigerated space through various heat transfer mechanisms. By fully or partially covering the case opening, night covers reduce the convective heat transfer into the case through reduced air infiltration. Additionally, they provide a measure of insulation, reducing conduction into the case, and also decrease radiation into the case by blocking radiated heat from entering the refrigerated space.

**Definition of Efficient Equipment**

Curtains or covers on top of open refrigerated or freezer display cases that are applied at least six hours (during off-hours) in a 24-hour period.

**Definition of Baseline Equipment**

Refrigerated and freezer, open-type display case in vertical, semi-vertical, and horizontal displays, with no night cover.

**Deemed Lifetime of Efficient Equipment**

The measure life is 5 years, based on DEER 2014.[[621]](#footnote-622)

**Deemed Measure Cost**

The incremental capital cost for this measure is $42 per linear foot of cover installed including material and labor.[[622]](#footnote-623)

**Loadshape**

Loadshape 22: Commercial Refrigeration

**Coincidence Factor**

N/A – savings occur at night only.

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

∆kWh = ES \* L

Where:

ES = the energy savings (∆kWh/ft) found in table below:

|  |  |  |  |
| --- | --- | --- | --- |
| **Display Case Description** | **Case Temperature Range (°F)** | **Annual Electricity Use**  **kWh/ft[[623]](#footnote-624)** | **ES**  **∆kWh/ft reduction**  **(= 9% reduction of electricity use**[[624]](#footnote-625),[[625]](#footnote-626)**)** |
| Vertical Open, Remote Condensing, Medium Temperature | 35°F to 55°F | 1453 | 131 |
| Vertical Open, Remote Condensing, Low Temperature | 0°F to 30°F | 3292 | 296 |
| Vertical Open, Self-Contained Medium Temperature | 35°F to 55°F | 2800 | 252 |
| Horizontal Open, Remote Condensing, Medium Temperature | 35°F to 55°F | 439 | 40 |
| Horizontal Open, Remote Condensing, Low Temperature | 0°F to 30°F | 1007 | 91 |
| Horizontal Open, Self-Contained, Medium Temperature | 35°F to 55°F | 1350 | 121 |
| Horizontal Open, Self-Contained, Low Temperature | 0°F to 30°F | 2749 | 247 |

L = the length of the refrigerated case in linear feet

= Actual

**Summer Coincident Peak Demand Savings**

Peak savings are null because savings occur at night only.

**Natural Gas Savings**

N/A

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-RFG-NCOV-V01-150601**

## Miscellaneous End Use

### VSD Air Compressor

###### Description

This measure relates to the installation of an air compressor with a variable frequency drive, load/no load controls or variable displacement control. The baseline compressors defined choke off the inlet air to modulate the compressor output, which is not efficient. Efficient compressors use a variable speed drive on the motor to match output to the load. Savings are calculated using representative baseline and efficient demand numbers for compressor capacities according to the facility’s load shape, and the number of hours the compressor runs at that capacity. Demand curves are as per DOE data for a Variable Speed compressor versus a Modulating compressor. This measure applies only to an individual compressor ≤ 40 hp

This measure was developed to be applicable to the following program types: TOS.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The high efficiency equipment is a compressor ≤ 40 hp with variable speed control.

###### Definition of Baseline Equipment

The baseline equipment is a modulating compressor with blow down ≤ 40 hp

###### Deemed Lifetime of Efficient Equipment

10 years.

###### Deemed Measure Cost

IncrementalCost ($) *=* (127 x hpcompressor) + 1446

Where:

127 and 1446[[626]](#footnote-627) = compressor motor nominal hp to incremental cost conversion factor and offset

hpcompressor = compressor motor nominal

###### Deemed O&M Cost Adjustments

N/A

###### Loadshape

Loadshape C35 - Industrial Process

###### Coincidence Factor

The coincidence factor equals 0.95

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh*=* 0.9 x hpcompressor x HOURS x (CFb – CFe)

Where:

ΔkWh= gross customer annual kWh savings for the measure

hpcompressor = compressor motor nominal hp

0.9[[627]](#footnote-628) = compressor motor nominal hp to full load kW conversion factor

HOURS = compressor total hours of operation below depending on shift

|  |  |
| --- | --- |
| **Shift** | **Hours** |
| Single shift (8/5) | 1976 hours  7 AM – 3 PM, weekdays, minus some holidays and scheduled down time |
| 2-shift (16/5) | 3952 hours  7AM – 11 PM, weekdays, minus some holidays and scheduled down time |
| 3-shift (24/5) | 5928 hours  24 hours per day, weekdays, minus some holidays and scheduled down time |
| 4-shift (24/7) | 8320 hours  24 hours per day, 7 days a week minus some holidays and scheduled down time |

CFb = baseline compressor factor[[628]](#footnote-629)

=0.890

CFe = efficient compressor [[629]](#footnote-630)

=0.705

EXAMPLE

For example a VFD compressor with 10 HP operating in a 1 shift facility would save

ΔkWh*=* 0.9 x 10 x 1976 x (0.890 – 0.705)

= 3290 kWh

###### Summer Coincident Peak Demand Savings

ΔkW*=* ΔkWh / HOURS \* CF

EXAMPLE

For example a VFD compressor with 10 HP operating in a 1 shift facility would save

ΔkW*=* 3290/1976\*.95

= 1.58 kW

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-MSC-VSDA-V01-120601

* + 1. Compressed Air Low Pressure Drop Filters

**Description**

Low pressure drop filters remove solids and aerosols from compressed air systems with a longer life and lower pressure drop than standard coalescing filters, resulting in better efficiencies.

This measure was developed to be applicable to the following program types: RF. If applied to other program types, the measure savings should be verified

**Definition of Efficient Equipment**

The efficient condition is a low pressure drop filter with pressure drop not exceeding 1 psid when new and 3 psid at element change.

**Definition of Baseline Equipment**

The baseline condition is a standard coalescing filter with a pressure drop of 3 psid when new and 5 or more at element change

**Deemed Lifetime of Efficient Equipment**

5 years

**Deemed Measure Cost**

The incremental cost for this measure is estimated to be $1000 Incremental cost per filter[[630]](#footnote-631)

**Loadshape**

Loadshape C35 - Industrial Process

**Coincidence Factor**

The coincidence factor equals 0.95

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

∆kWh = (kWtypical x ∆P x SF x Hours / HPtypical) x HPreal

Where:

kWtypical = Adjusted compressor power (kW) based on typical compressor loading and operating profile. Use Use actual compressor control type if known:

|  |  |
| --- | --- |
| Compressor kWtypical |  |
| **Control Type** | **kWtypical [[631]](#footnote-632)** |
| Reciprocating - On/off Control | 70.2 |
| Reciprocating - Load/Unload | 74.8 |
| Screw - Load/Unload | 82.3 |
| Screw - Inlet Modulation | 82.5 |
| Screw - Inlet Modulation w/ Unloading | 82.5 |
| Screw - Variable Displacement | 73.2 |
| Screw - VFD | 70.8 |

= If the actual compressor control type is not known, then use a weighted average based on the following market assumptions:

|  |  |  |
| --- | --- | --- |
| **Control Type** | **Share %** | **kWtypical[[632]](#footnote-633)** |
| Market share estimation for load/unload control compressors | 40% | 74.8 |
| Market share estimation for modulation w/unloading control compressors | 40% | 82.5 |
| Market share estimation for variable displacement control compressors | 20% | 73.2 |
| Weighted Average | | 77.6 |

∆P = Reduced filter loss (psi) =2 psi[[633]](#footnote-634)

SF =1% reduction in power per 2 psi reduction in system pressure is equal to 0.5% reduction per 1 psi, or a Savings Factor of 0.005[[634]](#footnote-635)

Hours = depending on shifts

Single shift (8/5) – 1976 hours (7 AM – 3 PM, weekdays, minus some holidays and scheduled down time) + 500 hrs maintenance = 2476 hrs

2-shift (16/5) – 3952 hours (7AM – 11 PM, weekdays, minus some holidays and scheduled down time) + 500 hrs maintenance = 4452 hrs

3-shift (24/5) – 5928 hours (24 hours per day, weekdays, minus some holidays and scheduled down time) + 500 hrs maintenance = 6428 hrs

4-shift (24/7) – 8320 hours (24 hours per day, 7 days a week minus some holidays and scheduled down time)

HPtypical = Nominal HP for typical compressor = 100 hp[[635]](#footnote-636)

HPreal = Total HP of real compressors distibuting air through filter. This should include the total horsepower of the compressors that normally run through the filter, but not backup compressors

**Summer Coincident Peak Demand Savings**

ΔkW*=* ΔkWh / HOURS \* CF

**Natural Gas Energy Savings**

N/A

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-MSC-CALPDF-V01-140601**

### Compressed Air No-Loss Condensate Drains

###### Description

No-loss condensate drains remove condensate as needed without venting compressed air, resulting in less air demand and consequently better efficiency. Replacement or upgrades of existing no-loss drains are not eligible for the incentive.

This measure was developed to be applicable to the following program types: RF. If applied to other program types, the measure savings should be verified

###### Definition of Efficient Equipment

The efficient condition is installation of no-loss condensate drains.

###### Definition of Baseline Equipment

The baseline condition is installation of standard condensate drains (open valve, timer, or both)

###### Deemed Lifetime of Efficient Equipment

10 years

###### Deemed Measure Cost

$700 per drain [[636]](#footnote-637)

###### Loadshape

Loadshape C35 - Industrial Process

###### Coincidence Factor

The coincidence factor equals 0.95

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

∆kWh = CFMreduced x kWCFM x Hours

Where:

CFMreduced = Reduced air consumption (CFM) per drain = 3 CFM*[[637]](#footnote-638)*

kWCFM= System power reduction per reduced air demand (kw/CFM) depending on the type of compressor control:

|  |  |
| --- | --- |
| System Power Reduction per Reduced Air Demand[[638]](#footnote-639) | |
| **Control Type** | **kW / CFM** |
| Reciprocating - On/off Control | 0.184 |
| Reciprocating - Load/Unload | 0.136 |
| Screw - Load/Unload | 0.152 |
| Screw - Inlet Modulation | 0.055 |
| Screw - Inlet Modulation w/ Unloading | 0.055 |
| Screw - Variable Displacement | 0.153 |
| Screw - VFD | 0.178 |

Or if compressor control type is unknow, then a weighted average based on market share can be used:

|  |  |  |
| --- | --- | --- |
| **Control Type** | **Share %** | ***kW / CFM*** |
| Market share estimation for load/unload control compressors | 40% | *0.136* |
| Market share estimation for modulation w/unloading control compressors | 40% | *0.055* |
| Market share estimation for variable displacement control compressors | 20% | *0.153* |
| Weighted Average | | *0.107* |

Hours = Compressed air system pressurized hours =6136 hours*[[639]](#footnote-640)*

###### Summer Coincident Peak Demand Savings

ΔkW*=* ΔkWh / HOURS \* CF

###### Natural Gas Energy Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: CI-MSC-CANLCD-V01-140601

### Pump Optimization

**Description**

Pump improvements can be done to optimize the design and control of centrifugal water pumping systems, including water solutions with freeze protection up to 15% concentration by volume. Other fluid and gas pumps cannot use this measure calculation. The measurement of energy and demand savings for commercial and industrial applications will vary with the type of pumping technology, operating hours, efficiency, and existing and proposed controls. Depending on the specific application slowing the pump, trimming or replacing the impeller may be suitable options for improving pumping efficiency. Pumps up to 40 HP are allowed to use this energy savings calculation. Larger motors should use a custom calculation (which may result in larger savings that this measure would claim).

**Definition of Efficient Equipment**

In order for this characterization to apply, the efficient equipment is proven to be an optimized centrifugal pumping system meeting the applicable program efficiency requirements:

* Pump balancing valves no more than 15% throttled
* Balancing valves on at least one load 100% open.

**Definition of Baseline Equipment**

In order for this characterization to apply, the baseline equipment is assumed to be the existing pumping system including existing controls and sequence of operations.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 10 years[[640]](#footnote-641)

**Deemed Measure Cost**

The incremental capital cost for this measure can vary considerably depending upon the strategy employed to achieve the required efficiency levels and should be determined on a site-specific basis.

**Deemed O&M Cost Adjustments**

N/A

**Coincidence Factor**

The summer peak coincidence factor for this measure is assumed to be 38%[[641]](#footnote-642)

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

ΔkWh = (HPmotor \* 0.746 \* LF / ηmotor) \* HOURS \* ESF

Where:

HPmotor = Installed nameplate motor horsepower

= Actual

0.746 = Conversion factor from horse-power to kW (kW/hp)

LF / ηmotor = Combined as a single factor since efficiency is a function of load

= 0.65 [[642]](#footnote-643)

Where:

LF = Load Factor; Ratio of the peak running load to the nameplate rating of the motor

ηmotor = Motor efficiency at pump operating conditions

HOURS = Annual operating hours of the pump

= Actual

ESF = Energy Savings Factor; assume a value of 15%[[643]](#footnote-644).

**Summer Coincident Peak Demand Savings**

ΔkW = (HPmotor \* 0.746 \*( LF / ηmotor)) \* (ESF) \* CF

Where:

CF = Summer Coincident Peak Factor for measure

= 0.38[[644]](#footnote-645)

**NATURAL GAS ENERGY SAVINGS**

N/A

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: CI-MSC-PMPO-V01-150601**

### Efficient Compressed Air Nozzles

**Description**

This measure is for the replacement of standard air nozzle with high-efficiency air nozzle used in a compressed air system. High-efficiency air nozzles reduce the amount of air required to blow off parts or for drying. These nozzles utilize the Coandă effect to pull in free air to accomplish tasks with significantly less compressed air. High-efficiency nozzles often replace simple copper tubes. These nozzles have the added benefits of noise reduction and improved safety in systems with greater than 30 psig.

**Definition of Efficient Equipment**

The high-efficiency air nozzle must meet the following specifications:

1. High-efficiency air nozzle must replace continuous open blow-offs
2. High-efficiency air nozzle must meet SCFM rating at 80psig less than or equal to: 1/8” 11 SCFM, 1/4" 29 SCFM, 5/16” 56 SCFM, 1/2" 140 SCFM.
3. Manufacturer’s specification sheet of the high-efficiency air nozzle must be provided along with the make and model

**Definition of Baseline Equipment**

The baseline condition is a standard air nozzle

**Deemed Lifetime of Efficient Equipment**

The measure life is 15 years[[645]](#footnote-646)

**Deemed Measure Cost**

The estimated incremental measure costs are presented in the following table[[646]](#footnote-647)

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
| **Nozzle Diameter** | **1/8”** | **1/4"** | **5/16”** | **1/2"** |
| Average IMC | $42 | $57 | $87 | $121 |

**Loadshape**

Loadshape C35 - Industrial Process

**Coincidence Factor**

The coincidence factor equals 0.95

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

ΔkWh = (SCFM \* SCFM%Reduced) \* kW/CFM \* HOURS

Where:

SCFM = Air flow through standard nozzle. Use actual rated flow at 80 psi if known. If unknown, the table below includes the CFM by orifice diameter**[[647]](#footnote-648)**, **[[648]](#footnote-649)**.

|  |  |
| --- | --- |
| **Orifice Diameter** | **SCFM** |
| 1/8” | 21 |
| 1/4” | 58 |
| 5/16” | 113 |
| 1/2" | 280 |

SCFM%Reduced = Percent in reduction of air loss per nozzle. Estimated at 50%[[649]](#footnote-650)

kW/CFM = System power reduction per air demand (kW/CFM) depending on the type of air compressor found in table below**[[650]](#footnote-651)**

|  |  |
| --- | --- |
| **Air Compressor Type** | **ΔkW/CFM** |
| Reciprocating – On/off Control | 0.18 |
| Reciprocating – Load/Unload | 0.14 |
| Screw – Load/Unload | 0.15 |
| Screw – Inlet Modulation | 0.06 |
| Screw – Inlet Modulation w/ Unloading | 0.06 |
| Screw – Variable Displacement | 0.15 |
| Screw - VFD | 0.18 |

Hours = Compressed air system pressurized hours.

= Use actual hours if known, otherwise assume values in table below:

|  |  |
| --- | --- |
| **Shift** | **Hours** |
| Single Shift | 1976 |
| Two Shifts | 3952 |
| Three Shifts | 5928 |
| Four Shifts or Continual Operation | 8320 |
| Unknown / Weighted average[[651]](#footnote-652) | 5702 |

**Summer Coincident Peak Demand Savings**

ΔkW = ΔkWh/HOURS \* CF

Where:

ΔkWh = As calculated above

CF = 0.95

**Natural Gas Savings**

N/A

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

###### Measure Code: CI-MSC-CNOZ-V01-150601

### Roof Insulation for C&I Facilities

**Description**

Energy and demand saving are realized through reductions in the building cooling and heating loads. This measure was developed to be applicable to the following program types: RF and NC.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

The efficient condition is defined by ASHRAE 90.1 – 2013 (see tables below):

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
|  | **IL TRM Zones 4 & 5 [ASHREA/IECC Climate Zone 4 (A, B, C)]** | | | | | |
| **Nonresidential** | | **Residential** | | **Semiheated** | |
| **Assembly Maximum** | **Insulation**  **Min. R-Value** | **Assembly Maximum** | **Insulation**  **Min. R-Value** | **Assembly Maximum** | **Insulation Min. R-Value** |
| **Insulation Entirely Above Deck** | 0.032 | R-30.0 c.i. | 0.032 | R-30.0 c.i. | 0.093 | R-10 c.i. |
| **Metal Building (Roof)** | 0.037 | R-19 + R-11 Ls or  R-25 + R-8 Ls | 0.037 | R-19 + R-11 Ls or  R-25 + R-8 Ls | 0.082 | R-19 |
| **Attic and Other** | 0.021 | R-49 | 0.021 | R-49 | 0.034 | R-30 |

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
|  | **IL TRM Zones 1, 2, & 3 [ASHREA/IECC Climate Zone 5 (A, B, C)]** | | | | | |
| **Nonresidential** | | **Nonresidential** | | **Nonresidential** | |
| **Assembly Maximum** | **Insulation**  **Min. R-Value** | **Assembly Maximum** | **Insulation**  **Min. R-Value** | **Assembly Maximum** | **Insulation Min. R-Value** |
| **Insulation Entirely Above Deck** | 0.032 | R-30.0 c.i. | 0.032 | R-30.0 c.i. | 0.063 | R-15 c.i. |
| **Metal Building (Roof)** | 0.037 | R-19 + R-11 Ls or  R-25 + R-8 Ls | 0.037 | R-19 + R-11 Ls or  R-25 + R-8 Ls | 0.082 | R-19 |
| **Attic and Other** | 0.021 | R-49 | 0.021 | R-49 | 0.034 | R-30 |

**Definition of Baseline Equipment**

The retrofit baseline condition is adopted from Ohio Energy Technical Reference Manual and expanded to cover all type of commercial buildings in the state of Illinois as follows.

For retrofits, the R-value for the entire assembly:

| **Building Type** | **Zone 1 (Rockford)Retrofit Assembly R-Value** |
| --- | --- |
| Assembly | 13.5 |
| Assisted Living | 13.5 |
| College | 13.5 |
| Convenience Store | 13.5 |
| Elementary School | 13.5 |
| Garage | 13.5 |
| Grocery | 13.5 |
| Healthcare Clinic | 13.5 |
| High School | 13.5 |
| Hospital | 13.5 |
| Hotel/Motel | 13.5 |
| Manufacturing Facility | 1,04812 |
| MF - High Rise | 13.5 |
| MF - Mid Rise | 13.5 |
| Movie Theater | 13.5 |
| Office - High Rise | 13.5 |
| Office - Low Rise | 13.5 |
| Office - Mid Rise | 13.5 |
| Religious Building | 13.5 |
| Restaurant | 13.5 |
| Retail - Department Store | 13.5 |
| Retail - Strip Mall | 13.5 |
| Warehouse | 12 |
| Unknown | 13.5 |

For new construction use IECC 2012 or ASHRAE – 90.1 – 2010 (listed below)

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
|  | **IL TRM Zones 4 & 5 [ASHREA/IECC Climate Zone 4 (A, B, C)]** | | | | | |
|  | **Nonresidential** | | **Residential** | | **Semiheated** | |
|  | **Assembly Maximum** | **Insulation Min. R-Value** | **Assembly Maximum** | **Insulation Min. R-Value** | **Assembly Maximum** | **Insulation Min. R-Value** |
| **Insulation Entirely Above Deck** | 0.048 | R-20.0 c.i. | 0.048 | R-20.0 c.i. | 0.173 | R-5.0 c.i. |
| **Metal Building (Roof)** | 0.055 | R-13.0 + R-13.0 | 0.055 | R-13.0 + R-13.0 | 0.097 | R-10.0 |
| **Attic and Other** | 0.027 | R-38.0 | 0.027 | R-38.0 | 0.053 | R-19.0 |

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
|  | **IL TRM Zones 1, 2, & 3 [ASHREA/IECC Climate Zone 5 (A, B, C)]** | | | | | |
|  | **Nonresidential** | | **Nonresidential** | | **Nonresidential** | |
|  | **Assembly Maximum** | **Assembly Maximum** | **Assembly Maximum** | **Assembly Maximum** | **Assembly Maximum** | **Assembly Maximum** |
| **Insulation Entirely Above Deck** | 0.048 | R-20 c.i. | U-0.048 | R-20 c.i. | U-0.119 | R-7.6 c.i. |
| **Metal Building (Roof)** | 0.055 | R-13.0 + R-13.0 | U-0.055 | R-13.0 + R-13.0 | U-0.083 | R-13.0 |
| **Attic and Other** | 0.027 | R-38.0 | U-0.027 | R-38.0 | U-0.053 | R-19.0 |

**Deemed Lifetime of Efficient Equipment**

The measure expected useful life (EUL) is assumed to be 20 years per DEER 2008. This is consistent with SDG&E’s 9th Year Measure Retrofit Study (1996 & 1997 Residential Weatherization Programs), CPUC’s Energy Efficiency Policy Manual v.2, and GDS’s Measure Life Report Residential and Commercial/Industrial Lighting and HVAC Measures (June 2007).

**Deemed Measure Cost**

Per the 2008 Database for Energy-Efficiency Resources (DEER), Version 2008.2.05, “Cost Values and Summary Documentation”, the material cost for R-30 insulation is $0.75 per square foot. The installation cost is $0.61 per square foot. The total measure cost, therefore, is $1.36 per square foot of insulation installed. However, the actual cost should be used when available.

**Loadshape**

Loadshape C03: Commercial Cooling

**Coincidence Factor**

CFSSP = Summer System Peak Coincidence Factor for Commercial cooling (during system peak hour)

= 91.3% [[652]](#footnote-653)

CFPJM = PJM Summer Peak Coincidence Factor for Commercial cooling (average during peak period)

= 47.8% [[653]](#footnote-654)

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

Electric energy savings is calculated as the sum of energy saved when cooling the building and energy saved when heating the building

∆kWh = ∆kWh\_cooling + ∆kWh\_heating

If central cooling, the electric energy saved in annual cooling due to the added insulation is

∆kWh\_cooling = ((1/R\_existing) - (1/R\_new)) \* Area \* EFLHcooling \* ΔTAVG,cooling / 1,000 / η\_cooling

Where:

R\_existing = Roof heat loss coefficient with existing insulation [(hr-⁰F-ft2)/Btu]

R\_new = Roof heat loss coefficienty with new insulation [(hr-⁰F-ft2)/Btu]

Area = Area of the roof surface in square feet. Assume 1000 sq ft for planning.

EFLHcooling = Equivalent Full Load Hours for Cooling [hr] are provided in Section 4.4, HVAC end use

ΔTAVG,cooling = Average temperature difference [⁰F] during cooling season between outdoor air temperature and assumed 75⁰F indoor air temperature

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **OAAVG,cooling [°F][[654]](#footnote-655)** | **ΔTAVG,cooling [°F]** |
| 1 (Rockford) | 81 | 6 |
| 2 (Chicago) | 81 | 6 |
| 3 (Springfield) | 81 | 6 |
| 4 (Belleville) | 82 | 7 |
| 5 (Marion) | 82 | 7 |

1,000 = Conversion from Btu to kBtu

η\_cooling = Seasonal energy efficiency ratio (SEER) of cooling system (kBtu/kWh). Use actual if possible, if unknown and for planning purposes assume the following:

|  |  |
| --- | --- |
| **Year Equipment was Installed** | **SEER estimate** |
| Before 2006 | 10 |
| After 2006 | 13 |

If the building is heated with electric heat (resistance or heat pump), the electric energy saved in annual heating due to the added insulation is

∆kWh\_heating = [(1/R\_existing) - (1/R\_new)] \* Area \* EFLHheating \* ΔTAVG,heating / 3,412 / η\_heating

Where:

EFLHheating = Equivalent Full Load Hours for Heating [hr] are provided in Section 4.4, HVAC end use

ΔTAVG,heating = Average temperature difference [⁰F] during heating season between outdoor air temperature and assumed 55⁰F heating base temperature

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **OAAVG,heating [°F][[655]](#footnote-656)** | **ΔTAVG,heating [°F]** |
| 1 (Rockford) | 32 | 23 |
| 2 (Chicago) | 34 | 21 |
| 3 (Springfield) | 35 | 20 |
| 4 (Belleville) | 36 | 19 |
| 5 (Marion) | 39 | 16 |

3,142 = Conversion from Btu to kWh.

η\_heating = Efficiency of heating system. Use actual efficiency. If not available refer to default table below.

|  |  |  |  |
| --- | --- | --- | --- |
| **System Type** | **Age of Equipment** | **HSPF Estimate** | **ηHeat (Effective COP Estimate) (HSPF/3.413)\*0.85** |
| Heat Pump | Before 2006 | 6.8 | 1.7 |
| After 2006 | 7.7 | 1.92 |
| Resistance | N/A | N/A | 1 |

If the building is heated with a gas furnace, there will be some electric savings in heating the building attributed to extra insulation since the furnace fans will run less.

∆kWh\_heating = ∆Therms \* Fe \* 29.3

Where:

∆Therms = Gas savings calculated with equation below.

Fe = Percentage of heating energy consumed by fans, assume 3.14%

29.3 = Conversion from therms to kWh

**Summer Coincident Peak Demand Savings**

∆kW = (∆kWh\_cooling / EFLH\_cooling) \* CF

Where:

EFLHcooling = Equivalent full load hours of air conditioning are provided in Section 4.4, HVAC end use

CFSSP = Summer System Peak Coincidence Factor for Commercial cooling (during system peak hour)

= 91.3% [[656]](#footnote-657)

CFPJM = PJM Summer Peak Coincidence Factor for Commercial cooling (average during peak period)

= 47.8% [[657]](#footnote-658)

**Natural Gas Savings**

If building uses a gas furnace, the savings resulting from the insulation is calculated with the following formula.

∆Therms = ((1/R\_existing) - (1/R\_new)) \* Area \* EFLHheating \* ΔTAVG,heating / 100,000 / η\_heat

Where:

R\_existing = Roof heat loss coefficient with existing insulation [(hr-⁰F-ft2)/Btu]

R\_new = Roof heat loss coefficienty with new insulation [(hr-⁰F-ft2)/Btu]

Area = Area of the roof surface in square feet. Assume 1000 sq ft for planning.

EFLHheating = Equvalent Full Load Hours for Heating are provided in Section 4.4, HVAC end use

ΔTAVG,heating = Average temperature difference [⁰F] during heating season (see above)

100,000 = Conversion from BTUs to Therms

η\_heat = Efficiency of existing furnace. Assume 0.78 for planning purposes.

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure code: CI-HVC-RINS-V01-150601**

### Computer Power Management Software

**Description**

Computer power management software is installed on a network of computers. This is software which monitors and records computer and monitor usage, as well as allows centralized control of computer power management settings.

**Definition of Efficient Equipment**

The efficient equipment is defined by the requirements listed below:

* Allow centralized control and override of computer power management settings of workstations which include both a computer monitor and CPU (i.e. a desktop or laptop computer on a distributed network)
* Be able to control on/off/sleep states on both the CPU and monitor according to the Network Administrator-defined schedules and apply power management policies to network groups
* Have capability to allow networked workstations to be remotely wakened from power-saving mode (e.g. for system maintenance or power/setting adjustments)
* Have capability to detect and monitor power management performance and generate energy savings reports
* Have capability to produce system reports to confirm the inventory and performance of equipment on which the software is installed.

This measure was developed to be applicable to the following program types: Retrofit. If applied to other program types, the measure savings should be verified.

**Definition of Baseline Equipment**

Baseline is defined as a computer network without software enforcing the power management capabilities in existing computers and monitors.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is five years.[[658]](#footnote-659)

**Deemed Measure Cost**

The deemed measure cost is $29 per networked computer, including labor.[[659]](#footnote-660)

**Loadshape**

Loadshape C21: Commercial Office Equipment.

**Coincidence Factor**

NA

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

ΔkWh = Wsavings \* W

Where:

Wsavings = annual energy savings per workstation

= 200 kWh[[660]](#footnote-661) for desktops, 50 kWh for laptops[[661]](#footnote-662)

= If unknown assume 161 kWh (based on 74% desktop and 26% laptop[[662]](#footnote-663))

W = number of desktop or laptop workstations controlled by the power management software

**Summer Coincident Peak Demand Savings**

NA

**Natural Gas Saving**

NA

**Water Impact Descriptions and Calculation**

NA

**Deemed O&M Cost Adjustment Calculation**

Assumed to be $1/unit [[663]](#footnote-664)

###### Measure code: CI-MSC-CPMS-V01-150601

# Residential Measures

## Appliances End Use

### ENERGY STAR Air Purifier/Cleaner

###### Description

An air purifier (cleaner) meeting the efficiency specifications of ENERGY STAR is purchased and installed in place of a model meeting the current federal standard.

This measure was developed to be applicable to the following program types:  TOS, NC.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The efficient equipment is defined as an air purifier meeting the efficiency specifications of ENERGY STAR as provided below.

* Must produce a minimum 50 Clean Air Delivery Rate (CADR) for Dust[[664]](#footnote-665) to be considered under this specification.
* Minimum Performance Requirement: = 2.0 CADR/Watt (Dust)
* Standby Power Requirement: = 2.0 Watts Qualifying models that perform secondary consumer functions (e.g. clock, remote control) must meet the standby power requirement.
* UL Safety Requirement: Models that emit ozone as a byproduct of air cleaning must meet UL Standard 867 (ozone production must not exceed 50ppb)

###### Definition of Baseline Equipment

The baseline equipment is assumed to be a conventional unit[[665]](#footnote-666).

###### Deemed Lifetime of Efficient Equipment

The measure life is assumed to be 9 years[[666]](#footnote-667).

###### Deemed Measure Cost

The incremental cost for this measure is $70.[[667]](#footnote-668)

###### Loadshape

Loadshape C53 - Flat

###### Coincidence Factor

The summer peak coincidence factor for this measure is assumed to be 100 % (the unit is assumed to be always on).

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = kWhBase- kWhESTAR

Where:

kWhBASE *=* Baseline kWh consumption per year[[668]](#footnote-669)

= see table below

kWhESTAR *=* ENERGY STAR kWh consumption per year[[669]](#footnote-670)

= see table below

|  |  |  |  |
| --- | --- | --- | --- |
| **Clean Air Delivery Rate** | **Baseline Unit Energy Consumption (kWh/year)** | **ENERGY STAR Unit Energy Consumption (kWh/year)** | **ΔkWH** |
| CADR 51-100 | 596 | 329 | 268 |
| CADR 101-150 | 1,072 | 548 | 525 |
| CADR 151-200 | 1,480 | 767 | 714 |
| CADR 201-250 | 1,887 | 986 | 902 |
| CADR Over 250 | 1,641 | 1205 | 437 |

###### Summer Coincident Peak Demand Savings

∆kW*=* ∆kWh/Hours \*CF

Where:

∆kWh = Gross customer annual kWh savings for the measure

Hours = Average hours of use per year

= 8766 hours[[670]](#footnote-671)

CF = Summer Peak Coincidence Factor for measure

= 1.0

|  |  |
| --- | --- |
| **Clean Air Delivery Rate** | **ΔkW** |
| CADR 51-100 | 0.031 |
| CADR 101-150 | 0.060 |
| CADR 151-200 | 0.081 |
| CADR 201-250 | 0.103 |
| CADR Over 250 | 0.050 |

###### Natural Gas Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

There are no operation and maintenance cost adjustments for this measure.[[671]](#footnote-672)

###### Measure Code: RS-APL-ESAP-V01-120601

### ENERGY STAR and ENERGY STAR Most Efficient Clothes Washers

**Description**

This measure relates to the installation of a clothes washer meeting the ENERGY STAR, or ENERGY STAR Most Efficient minimum qualifications. Note if the DHW and dryer fuels of the installations are unknown (for example through a retail program) savings should be based on a weighted blend using RECS data (the resultant values (kWh, therms and gallons of water) are provided). The algorithms can also be used to calculate site specific savings where DHW and dryer fuels are known.

This measure was developed to be applicable to the following program types:  TOS, NC.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

Clothes washer must meet the ENERGY STAR or ENERGY STAR Most Efficient minimum qualifications, as required by the program .

**Definition of Baseline Equipment**

The baseline condition is a clothes washer meeting the minimum federal baseline as of March 2015[[672]](#footnote-673).

|  |  |  |  |
| --- | --- | --- | --- |
| **Efficiency Level** | **Top loading >2.5 Cu ft** | **Top loading <2.5 cu ft** | **Front Loading** |
| Federal Standard | 1.29 IMEF,  8.4 IWF | | 1.84 IMEF, 4.7 IWF |
| ENERGY STAR | 2.06 IMEF, 4.3 IWF | 2.07 IMEF, 4.2 IWF | 2.38 IMEF, 3.7 IWF |
| ENERGY STAR Most Efficient | 2.76 IMEF, 3.5 IWF | N/A | 2.74 IMEF, 3.2IWF |

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 14 years[[673]](#footnote-674).

**Deemed Measure Cost**

The incremental cost for an ENERGY STAR unit is assumed to be $65 and for an ENERGY STAR Most Efficient unit it is $210[[674]](#footnote-675).

**Deemed O&M Cost Adjustments**

N/A

**Loadshape**

Loadshape R01 - Residential Clothes Washer

**Coincidence Factor**

The coincidence factor for this measure is 3.8%[[675]](#footnote-676).

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

1. Calculate clothes washer savings based on Modified Energy Factor (MEF).

The Modified Energy Factor (MEF) includes unit operation, water heating and drying energy use: *"MEF is the quotient of the capacity of the clothes container, C, divided by the total clothes washer energy consumption per cycle, with such energy consumption expressed as the sum of the machine electrical energy consumption, M, the hot water energy consumption, E, and the energy required for removal of the remaining moisture in the wash load, D"* [[676]](#footnote-677).

The hot water and dryer savings calculated here assumes electric DHW and Dryer (this will be separated in Step 2).

IMEFsavings[[677]](#footnote-678) = Capacity \* (1/IMEFbase - 1/IMEFeff) \* Ncycles

Where

Capacity = Clothes Washer capacity (cubic feet)

= Actual. If capacity is unknown assume 3.45 cubic feet [[678]](#footnote-679)

IMEFbase = Integrated Modified Energy Factor of baseline unit

= 1.66[[679]](#footnote-680)

IMEFeff = Integrated Modified Energy Factor of efficient unit

= Actual. If unknown assume average values provided below.

Ncycles = Number of Cycles per year

= 295[[680]](#footnote-681)

IMEFsavings is provided below based on deemed values[[681]](#footnote-682):

|  |  |  |
| --- | --- | --- |
| **Efficiency Level** | **IMEF** | **IMEFSavings (kWh)** |
| Federal Standard | 1.66 | 0.0 |
| Energy StarENERGY STAR | 2.26 | 251163 |
| ENERGY STAR Most Efficient | 2.74 | 242 |

1. Break out savings calculated in Step 1 for electric DHW and electric dryer

∆kWh = [(Capacity \* 1/IMEFbase \* Ncycles) \* (%CWbase + (%DHWbase \* %Electric\_DHW) + (%Dryerbase \* %Electric\_Dryer)] - [(Capacity \* 1/IMEFeff \* Ncycles) \* (%CWeff + (%DHWeff \* %Electric\_DHW) + (%Dryereff \* %Electric\_Dryer)]

Where:

%CW = Percentage of total energy consumption for Clothes Washer operation (different for baseline and efficient unit – see table below)

%DHW = Percentage of total energy consumption used for water heating (different for baseline and efficient unit – see table below)

%Dryer = Percentage of total energy consumption for dryer operation (different for baseline and efficient unit – see table below)

|  |  |  |  |
| --- | --- | --- | --- |
|  | **Percentage of Total Energy Consumption[[682]](#footnote-683)** | | |
|  | **%CW** | **%DHW** | **%Dryer** |
| Baseline | 8% | 31% | 61% |
| ENERGY STAR | 8% | 23% | 69% |
| ENERGY STAR Most Efficient | 14% | 10% | 76% |

%Electric\_DHW = Percentage of DHW savings assumed to be electric

| **DHW fuel** | **%Electric\_DHW** |
| --- | --- |
| Electric | 100% |
| Natural Gas | 0% |
| Unknown | 16%[[683]](#footnote-684) |

%Electric\_Dryer = Percentage of dryer savings assumed to be electric

|  |  |
| --- | --- |
| **Dryer fuel** | **%Electric\_DHW** |
| Electric | 100% |
| Natural Gas | 0% |
| Unknown | 27%[[684]](#footnote-685) |

Using the default assumptions provided above, the prescriptive savings for each configuration are presented below:

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
|  | **ΔkWH** | | | |
|  | **Electric DHW Electric Dryer** | **Gas DHW**  **Electric Dryer** | **Electric DHW**  **Gas Dryer** | **Gas DHW**  **Gas Dryer** |
| ENERGY STAR | 250.6163.4 | 77.4 | 96.0 | 10.3 |
| ENERGY STAR Most Efficient | 298.9242.1 | 88.1 | 149.6 | -4.0 |

If the DHW and dryer fuel is unknown the prescriptive kWH savings based on defaults provided above should be:

|  |  |
| --- | --- |
|  | **ΔkWH** |
| ENERGY STAR | 42.1 |
| ENERGY STAR Most Efficient | 45.4 |

**Summer Coincident Peak Demand Savings**

ΔkW = ΔkWh/Hours \* CF

Where:

ΔkWh = Energy Savings as calculated above

Hours = Assumed Run hours of Clothes Washer

= 295 hours[[685]](#footnote-686)

CF = Summer Peak Coincidence Factor for measure.

= 0.038[[686]](#footnote-687)

Using the default assumptions provided above, the prescriptive savings for each configuration are presented below:

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
|  | **ΔkW** | | | |
|  | **Electric DHW**  **Electric Dryer** | **Gas DHW**  **Electric Dryer** | **Electric DHW**  **Gas Dryer** | **Gas DHW**  **Gas Dryer** |
| ENERGY STAR | 0.021 | 0.010 | 0.012 | 0.0013 |
| ENERGY STAR Most Efficient | 0.031 | 0.011 | 0.019 | -0.001 |

If the DHW and dryer fuel is unknown the prescriptive kW savings should be:

|  | **ΔkW** |
| --- | --- |
| ENERGY STAR | 0.005 |
| ENERGY STAR Most Efficient | 0.006 |

**Natural Gas Savings**

Break out savings calculated in Step 1 of electric energy savings (MEF savings) and extract Natural Gas DHW and Natural Gas dryer savings from total savings:

∆Therm = [(Capacity \* 1/IMEFbase \* Ncycles) \* ((%DHWbase \* %Natural Gas\_DHW \* R\_eff) + (%Dryerbase \* %Gas \_Dryer)] - [(Capacity \* 1/IMEFeff \* Ncycles) \* ((%DHWeff \* %Natural Gas\_DHW \* R\_eff) + (%Dryereff \* %Gas\_Dryer)] \* Therm\_convert

Where:

Therm\_convert = Convertion factor from kWh to Therm

= 0.03413

R\_eff = Recovery efficiency factor

= 1.26[[687]](#footnote-688)

%Natural Gas\_DHW = Percentage of DHW savings assumed to be Natural Gas

|  |  |
| --- | --- |
| **DHW fuel** | **%Natural Gas\_DHW** |
| Electric | 0% |
| Natural Gas | 100% |
| Unknown | 84%[[688]](#footnote-689) |

%Gas\_Dryer = Percentage of dryer savings assumed to be Natural Gas

|  |  |
| --- | --- |
| **Dryer fuel** | **%Gas\_Dryer** |
| Electric | 100% |
| Natural Gas | 0% |
| Unknown | 44%[[689]](#footnote-690) |

Other factors as defined above

Using the default assumptions provided above, the prescriptive savings for each configuration are presented below:

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
|  | **ΔTherms** | | | |
|  | **Electric DHW**  **Electric Dryer** | **Gas DHW**  **Electric Dryer** | **Electric DHW**  **Gas Dryer** | **Gas DHW**  **Gas Dryer** |
| ENERGY STAR | 0.00 | 3.7 | 2.3 | 6.0 |
| ENERGY STAR Most Efficient | 0.00 | 6.6 | 3.1 | 9.7 |

If the DHW and dryer fuel is unknown the prescriptive Therm savings should be:

|  |  |
| --- | --- |
|  | **ΔTherms** |
| ENERGY STAR | 4.11 |
| ENERGY STAR Most Efficient | 6.93 |

**Water Impact Descriptions and Calculation**

∆Water (gallons) = (Capacity \* (IWFbase - IWFeff)) \* Ncycles

Where

IWFbase = Integrated Water Factor of baseline clothes washer

= 5.92[[690]](#footnote-691)

IWFeff = Water Factor of efficient clothes washer

= Actual. If unknown assume average values provided below.

Using the default assumptions provided above, the prescriptive water savings for each efficiency level are presented below:

|  |  |  |
| --- | --- | --- |
| **Efficiency Level** | **IWF[[691]](#footnote-692)** | **∆Water**  **(gallons per year)** |
| Federal Standard | 8.865.92 | 0.0 |
| ENERGY STAR | 5.423.93 | 2020 |
| ENERGY STAR Most Efficient | 4.073.21 | 2755 |

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: RS-APL-ESCL-V03-150601**

### ENERGY STAR Dehumidifier

###### Description

A dehumidifier meeting the minimum qualifying efficiency standard established by the current ENERGY STAR (Version 2.1 or 3.0)[[692]](#footnote-693) is purchased and installed in a residential setting in place of a unit that meets the minimum federal standard efficiency.

This measure was developed to be applicable to the following program types:  TOS, NC.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure, the new dehumidifier must meet the ENERGY STAR standards as defined below:

Until 9/30/2012:

|  |  |
| --- | --- |
| **Capacity**  **(pints/day)** | **ENERGY STAR Criteria**  **(L/kWh)** |
| ≤25 | ≥1.20 |
| > 25 to ≤35 | ≥1.40 |
| > 35 to ≤45 | ≥1.50 |
| > 45 to ≤ 54 | ≥1.60 |
| > 54 to ≤ 75 | ≥1.80 |
| > 75 to ≤ 185 | ≥2.50 |

After 10/1/2012[[693]](#footnote-694):

|  |  |
| --- | --- |
| **Capacity**  **(pints/day)** | **ENERGY STAR Criteria**  **(L/kWh)** |
| <75 | ≥1.85 |
| 75 to ≤185 | ≥2.80 |

Qualifying units shall be equipped with an adjustable humidistat control or shall require a remote humidistat control to operate.

###### Definition of Baseline Equipment

The baseline for this measure is defined as a new dehumidifier that meets the Federal Standard efficiency standards. The Federal Standard for Dehumidifiers changed as of October 2012 as defined below:

Until 9/30/2012:

|  |  |
| --- | --- |
| **Capacity**  **(pints/day)** | **Federal Standard Criteria**  **(L/kWh)** |
| ≤25 | ≥1.0 |
| > 25 to ≤35 | ≥1.20 |
| > 35 to ≤45 | ≥1.30 |
| > 45 to ≤ 54 | ≥1.30 |
| > 54 to ≤ 75 | ≥1.50 |
| > 75 to ≤ 185 | ≥2.25 |

Post 10/1/2013

|  |  |
| --- | --- |
| **Capacity**  **(pints/day)** | **Federal Standard Criteria**  **(L/kWh)** **[[694]](#footnote-695)** |
| Up to 35 | ≥1.35 |
| > 35 to ≤45 | ≥1.50 |
| > 45 to ≤ 54 | ≥1.60 |
| > 54 to ≤ 75 | ≥1.70 |
| > 75 to ≤ 185 | ≥2.50 |

###### Deemed Lifetime of Efficient Equipment

The assumed lifetime of the measure is 12 years[[695]](#footnote-696).

###### Deemed Measure Cost

The assumed incremental capital cost for this measure is $40 for units purchased prior to 10/1/2012 and $60 for units purchased after 10/1/2012[[696]](#footnote-697).

###### Loadshape

Loadshape R12 - Residential - Dehumidifier

###### Coincidence Factor

The coincidence factor is assumed to be 37% [[697]](#footnote-698).

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = (((Avg Capacity \* 0.473) / 24) \* Hours) \* (1 / (L/kWh\_Base)– 1 / (L/kWh\_Eff))

Where:

Avg Capacity = Average capacity of the unit (pints/day)

0.473 = Constant to convert Pints to Liters

24 = Constant to convert Liters/day to Liters/hour

Hours = Run hours per year

= 1620 [[698]](#footnote-699)

L/kWh = Liters of water per kWh consumed, as provided in tables above

Annual kWh results for each capacity class are presented below:

Until 9/30/2012 (V 2.1):

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
|  |  |  |  | **Annual kWh** | | |
| **Capacity** | **Capacity Used** | **Federal Standard Criteria** | **ENERGY STAR Criteria** | **Federal Standard** | **ENERGY STAR** | **Savings** |
| **(pints/day) Range** | **(≥ L/kWh)** | **(≥ L/kWh)** |
| ≤25 | 20 | 1.0 | 1.2 | 643 | 536 | 107 |
| > 25 to ≤35 | 30 | 1.2 | 1.4 | 804 | 689 | 115 |
| > 35 to ≤45 | 40 | 1.3 | 1.5 | 990 | 858 | 132 |
| > 45 to ≤ 54 | 50 | 1.3 | 1.6 | 1237 | 1005 | 232 |
| > 54 to ≤ 75 | 65 | 1.5 | 1.8 | 1394 | 1161 | 232 |
| > 75 to ≤ 185 | 130 | 2.25 | 2.5 | 1858 | 1673 | 186 |
| Average | 46 | 1.31 | 1.55 | 1129 | 953 | 176 |

After 10/1/2012 (V 3.0):

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
|  |  |  |  | **Annual kWh** | | |
| **Capacity** | **[[699]](#footnote-700)Capacity Used** | **Federal Standard Criteria** | **ENERGY STAR Criteria** | **Federal Standard** | **ENERGY STAR** | **Savings** |
| **(pints/day) Range** | **(≥ L/kWh)** | **(≥ L/kWh)** |
| ≤25 | 20 | 1.35 | 1.85 | 477 | 348 | 129 |
| > 25 to ≤35 | 30 | 1.35 | 1.85 | 715 | 522 | 193 |
| > 35 to ≤45 | 40 | 1.5 | 1.85 | 858 | 695 | 162 |
| > 45 to ≤ 54 | 50 | 1.6 | 1.85 | 1005 | 869 | 136 |
| > 54 to ≤ 75 | 65 | 1.7 | 1.85 | 1230 | 1130 | 100 |
| > 75 to ≤ 185 | 130 | 2.5 | 2.8 | 1673 | 1493 | 179 |
| Average | 46 | 1.51 | 1.85 | 983 | 800 | 183 |

**Summer Coincident Peak Demand Savings**

ΔkW = ΔkWh/Hours \* CF

Where:

Hours = Annual operating hours

= 1632 hours [[700]](#footnote-701)

CF = Summer Peak Coincidence Factor for measure

= 0.37 [[701]](#footnote-702)

Summer coincident peak demand results for each capacity class are presented below:

Until 9/30/2012 (V 2.1):

|  |  |
| --- | --- |
| **Capacity**  **(pints/day) Range** | **Annual Summer peak kW Savings** |
| ≤25 | 0.024 |
| > 25 to ≤35 | 0.026 |
| > 35 to ≤45 | 0.030 |
| > 45 to ≤ 54 | 0.053 |
| > 54 to ≤ 75 | 0.053 |
| > 75 to ≤ 185 | 0.042 |
| Average | 0.040 |

After 10/1/2012 (V 3.0):

|  |  |
| --- | --- |
| **Capacity**  **(pints/day) Range** | **Annual Summer peak kW Savings** |
| ≤25 | 0.029 |
| > 25 to ≤35 | 0.044 |
| > 35 to ≤45 | 0.037 |
| > 45 to ≤ 54 | 0.031 |
| > 54 to ≤ 75 | 0.023 |
| > 75 to ≤ 185 | 0.041 |
| Average | 0.042 |

###### Natural Gas Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-APL-ESDH-V02-130601

### ENERGY STAR Dishwasher

###### Description

A dishwasher meeting the efficiency specifications of ENERGY STAR is installed in place of a model meeting the federal standard. This measure is only for standard dishwashers, not compact dishwashers. A compact dishwasher is a unit that holds less than eight place settings with six serving pieces.

This measure was developed to be applicable to the following program types:  TOS, NC.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The efficient equipment is defined as a dishwasher meeting the efficiency specifications of ENERGY STAR (for standard dishwashers[[702]](#footnote-703)). The Energy Star standard is presented in the table below:

|  |  |  |
| --- | --- | --- |
| **Dishwasher Type** | **Maximum kWh/year** | **Maximum gallons/cycle** |
| Standard | 295 | 4.25 |

###### Definition of Baseline Equipment

The Baseline reflects the minimum federal efficiency standards for dishwashers effective May 30, 2013, as presented in the table below[[703]](#footnote-704).

|  |  |  |
| --- | --- | --- |
| **Dishwasher Type** | **Maximum kWh/year** | **Maximum gallons/cycle** |
| Standard | 307 | 5.0 |

###### Deemed Lifetime of Efficient Equipment

The assumed lifetime of the measure is 13 years[[704]](#footnote-705).

###### Deemed Measure Cost

The incremental cost for this measure is $50[[705]](#footnote-706).

###### Loadshape

Loadshape R02 - Residential Dish Washer

###### Coincidence Factor

The coincidence factor is assumed to be 2.6%[[706]](#footnote-707).

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh[[707]](#footnote-708) = ((kWhBase- kWhESTAR) \* (%kWh\_op + (%kWh\_heat \* %Electric\_DHW )))

Where:

kWhBASE *=* Baseline kWh consumption per year

= 307 kWh

kWhESTAR *=* ENERGY STAR kWh annual consumption

= 295 kWh

%kWh\_op = Percentage of dishwasher energy consumption used for unit operation

= 1 - 56%[[708]](#footnote-709)

= 44%

%kWh\_heat = Percentage of dishwasher energy consumption used for water heating

= 56%[[709]](#footnote-710)

%Electric\_DHW = Percentage of DHW savings assumed to be electric

|  |  |
| --- | --- |
| **DHW fuel** | **%Electric\_DHW** |
| Electric | 100% |
| Natural Gas | 0% |
| Unknown | 16%[[710]](#footnote-711) |

An Energy Star standard dishwasher installed in place of a baseline unit with unknown DHW fuel:

ΔkWh = ((307- 295) \* (0.44 + (0.56\*0.16)))

= 6.4 kWh

An Energy Star standard dishwasher installed in place of a baseline unit with electric DHW:

ΔkWh = ((307- 295) \* (0.44 + (0.56\*1.0)))

= 12 kWh

**Summer Coincident Peak Demand Savings**

ΔkW = ΔkWh/Hours \* CF

Where:

Hours = Annual operating hours[[711]](#footnote-712)

= 252 hours

CF = Summer Peak Coincidence Factor

= 2.6% [[712]](#footnote-713)

An Energy Star standard dishwasher installed in place of a baseline unit with unknown DHW fuel:

ΔkWh = 6.4/252 \* 0.026

= 0.0007 kW

An Energy Star standard dishwasher installed in place of a baseline unit with electric DHW:

ΔkWh = 12/252 \* 0.026

= 0.001 kWh

###### Natural Gas Savings

Δ Therm = (kWhBase- kWhESTAR) \* %kWh\_heat \* %Natural Gas\_DHW \* R\_eff \* 0.03413

Where

%kWh\_heat = % of dishwasher energy used for water heating

= 56%

%Natural Gas\_DHW = Percentage of DHW savings assumed to be Natural Gas

|  |  |
| --- | --- |
| **DHW fuel** | **%Natural Gas\_DHW** |
| Electric | 0% |
| Natural Gas | 100% |
| Unknown | 84%[[713]](#footnote-714) |

R\_eff = Recovery efficiency factor

= 1.26[[714]](#footnote-715)

0.03413 = factor to convert from kWh to Therm

An Energy Star standard dishwasher installed in place of a baseline unit with unknown DHW fuel:

Δ Therm = (307- 295) \* 0.56 \* 0.84\* 1.26 \* 0.03413

= 0.24 therm

An Energy Star standard dishwasher installed in place of a baseline unit with gas DHW:

Δ Therm = (307- 295) \* 0.56 \* 1.0\* 1.26 \* 0.03413

= 0.29 Therm

###### Water Impact Descriptions and Calculation

ΔWater = WaterBase- WaterEFF

Where

WaterBase = water consumption of conventional unit

= 840 gallons[[715]](#footnote-716)

WaterEFF = annualwater consumption of efficient unit:

= 714 gallons[[716]](#footnote-717)

Δ Water = 840– 714

= 126 gallons

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-APL-ESDI-V02-130601

### ENERGY STAR Freezer

###### Description

A freezer meeting the efficiency specifications of ENERGY STAR is installed in place of a model meeting the federal standard (NAECA). Energy usage specifications are defined in the table below (note, AV is the freezer Adjusted Volume and is calculated as 1.73\*Total Volume):

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
| **Product Category** | **Volume**  **(cubic feet)** | **Assumptions up to September 2014** | | **Assumptions after September 2014** | |
| **Federal Baseline Maximum Energy Usage in kWh/year[[717]](#footnote-718)** | **ENERGY STAR Maximum Energy Usage in kWh/year[[718]](#footnote-719)** | **Federal Baseline  Maximum Energy Usage in kWh/year[[719]](#footnote-720)** | **ENERGY STAR Maximum Energy Usage in kWh/year[[720]](#footnote-721)** |
| Upright Freezers with Manual Defrost | 7.75 or greater | 7.55\*AV+258.3 | 6.795\*AV+232.47 | 5.57\*AV + 193.7 | 5.01\*AV + 174.3 |
| Upright Freezers with Automatic Defrost | 7.75 or greater | 12.43\*AV+326.1 | 11.187\*AV+293.49 | 8.62\*AV + 228.3 | 7.76\*AV + 205.5 |
| Chest Freezers and all other Freezers except Compact Freezers | 7.75 or greater | 9.88\*AV+143.7 | 8.892\*AV+129.33 | 7.29\*AV + 107.8 | 6.56\*AV + 97.0 |
| Compact Upright Freezers with Manual Defrost | < 7.75 and 36 inches or less in height | 9.78\*AV+250.8 | 7.824\*AV+200.64 | 8.65\*AV + 225.7 | 7.79\*AV + 203.1 |
| Compact Upright Freezers with Automatic Defrost | < 7.75 and 36 inches or less in height | 11.40\*AV+391 | 9.12\*AV+312.8 | 10.17\*AV + 351.9 | 9.15\*AV + 316.7 |
| Compact Chest Freezers | <7.75 and 36 inches or less in height | 10.45\*AV+152 | 8.36\*AV+121.6 | 9.25\*AV + 136.8 | 8.33\*AV + 123.1 |

This measure was developed to be applicable to the following program types:  TOS, NC.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The efficient equipment is defined as a freezer meeting the efficiency specifications of ENERGY STAR, as defined below and calculated above:

|  |  |  |
| --- | --- | --- |
| **Equipment** | **Volume** | **Criteria** |
| Full Size Freezer | 7.75 cubic feet or greater | At least 10% more energy efficient than the minimum federal government standard (NAECA). |
| Compact Freezer | Less than 7.75 cubic feet and 36 inches or less in height | At least 20% more energy efficient than the minimum federal government standard (NAECA). |

###### Definition of Baseline Equipment

The baseline equipment is assumed to be a model that meets the federal minimum standard for energy efficiency. The standard varies depending on the size and configuration of the freezer (chest freezer or upright freezer, automatic or manual defrost) and is defined in the table above.

###### Deemed Lifetime of Efficient Equipment

The measure life is assumed to be 11 years[[721]](#footnote-722).

###### Deemed Measure Cost

The incremental cost for this measure is $35[[722]](#footnote-723).

###### Loadshape

Loadshape R04 - Residential Freezer

###### Coincidence Factor

The summer peak coincidence factor for this measure is assumed to be 95%[[723]](#footnote-724).

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings:

ΔkWh = kWhBase- kWhESTAR

Where:

kWhBASE *=* Baseline kWh consumption per year as calculated in algorithm provided in table above.

kWhESTAR *=* ENERGY STAR kWh consumption per year as calculated in algorithm provided in table above.

For example for a 7.75 cubic foot Upright Freezers with Manual Defrost purchased after September 2014:

ΔkWh*=*(5.57\*(7.75\* 1.73)+193.7) – (5.01\*(7.75\* 1.73)+174.3)

*=* 268.4 – 241.5

= 26.9 kWh

If volume is unknown, use the following default values:

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| **Product Category** | **Volume Used[[724]](#footnote-725)** | **Assumptions up to September 2014** | | | **Assumptions after September 2014** | | |
| **kWhBASE** | **kWhESTAR** | **kWh Savings** | **kWhBASE** | **kWhESTAR** | **kWh Savings** |
| Upright Freezers with Manual Defrost | 27.9 | 469.1 | 422.2 | 46.9 | 349.2 | 314.2 | 35.0 |
| Upright Freezers with Automatic Defrost | 27.9 | 673.2 | 605.9 | 67.3 | 469.0 | 422.2 | 46.8 |
| Chest Freezers and all other Freezers except Compact Freezers | 27.9 | 419.6 | 377.6 | 42.0 | 311.4 | 280.2 | 31.2 |
| Compact Upright Freezers with Manual Defrost | 10.4 | 352.3 | 281.9 | 70.5 | 467.2 | 420.6 | 46.6 |
| Compact Upright Freezers with Automatic Defrost | 10.4 | 509.3 | 407.5 | 101.9 | 635.9 | 572.2 | 63.7 |
| Compact Chest Freezers | 10.4 | 260.5 | 208.4 | 52.1 | 395.1 | 355.7 | 39.4 |

###### Summer Coincident Peak Demand Savings

∆kW*=* ∆kWh/ Hours \* CF

Where:

∆kWh = Gross customer annual kWh savings for the measure

Hours = Full Load hours per year

= 5890[[725]](#footnote-726)

CF = Summer Peak Coincident Factor

= 0.95 [[726]](#footnote-727).

For example for a 7.75 cubic foot Upright Freezers with Manual Defrost:

ΔkW *=* 26.9/5890 \* 0.95

= 0.0043 kW

If volume is unknown, use the following default values:

|  |  |  |
| --- | --- | --- |
| **Product Category** | **Assumptions up to September 2014** | **Assumptions after September 2014** |
| **kW Savings** | **kW Savings** |
| Upright Freezers with Manual Defrost | 0.0076 | 0.0057 |
| Upright Freezers with Automatic Defrost | 0.0109 | 0.0076 |
| Chest Freezers and all other Freezers except Compact Freezers | 0.0068 | 0.0050 |
| Compact Upright Freezers with Manual Defrost | 0.0114 | 0.0075 |
| Compact Upright Freezers with Automatic Defrost | 0.0164 | 0.0103 |
| Compact Chest Freezers | 0.0084 | 0.0064 |

###### Natural Gas Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-APL-ESFR-V02-140601

### ENERGY STAR and CEE Tier 2 Refrigerator

###### Description

This measure relates to:

1. Time of Sale: the purchase and installation of a new refrigerator meeting either ENERGY STAR or CEE TIER 2 specifications.
2. Early Replacement: the early removal of an existing residential inefficient Refrigerator from service, prior to its natural end of life, and replacement with a new ENERGY STAR or CEE Tier 2 qualifying unit. Savings are calculated between existing unit and efficient unit consumption during the remaining life of the existing unit, and between new baseline unit and efficient unit consumption for the remainder of the measure life.

Energy usage specifications are defined in the table below (note, Adjusted Volume is calculated as the fresh volume + (1.63 \* Freezer Volume):

| **Product Category** | **Existing Unit** | **Assumptions up to September 2014** | | **Assumptions after September 2014** | |
| --- | --- | --- | --- | --- | --- |
| **Based on Refrigerator Recycling algorithm** | **Federal Baseline  Maximum Energy Usage in kWh/year[[727]](#footnote-728)** | **ENERGY STAR Maximum Energy Usage in kWh/year**[[728]](#footnote-729) | **Federal Baseline  Maximum Energy Usage in kWh/year[[729]](#footnote-730)** | **ENERGY STAR Maximum Energy Usage in kWh/year[[730]](#footnote-731)** |
| 1. Refrigerators and Refrigerator-freezers with manual defrost | Use Algorithm in 5.1.8 Refrigerator and Freezer Recycling measure to estimate existing unit consumption | 8.82\*AV+248.4 | 7.056\*AV+198.72 | 6.79AV + 193.6 | 6.11 \* AV + 174.2 |
| 2. Refrigerator-Freezer--partial automatic defrost | 8.82\*AV+248.4 | 7.056\*AV+198.72 | 7.99AV + 225.0 | 7.19 \* AV + 202.5 |
| 3. Refrigerator-Freezers--automatic defrost with top-mounted freezer without through-the-door ice service and all-refrigerators--automatic defrost | 9.80\*AV+276 | 7.84\*AV+220.8 | 8.07AV + 233.7 | 7.26 \* AV + 210.3 |
| 4. Refrigerator-Freezers--automatic defrost with side-mounted freezer without through-the-door ice service | 4.91\*AV+507.5 | 3.928\*AV+406 | 8.51AV + 297.8 | 7.66 \* AV + 268.0 |
| 5. Refrigerator-Freezers--automatic defrost with bottom-mounted freezer without through-the-door ice service | 4.60\*AV+459 | 3.68\*AV+367.2 | 8.85AV + 317.0 | 7.97 \* AV + 285.3 |
| 5A Refrigerator-freezer—automatic defrost with bottom-mounted freezer with through-the-door ice service | N/A | N/A | 9.25AV + 475.4 | 8.33 \* AV \* 436.3 |
| 6. Refrigerator-Freezers--automatic defrost with top-mounted freezer with through-the-door ice service | 10.20\*AV+356 | 8.16\*AV+284.8 | 8.40AV + 385.4 | 7.56 \* AV + 355.3 |
| 7. Refrigerator-Freezers--automatic defrost with side-mounted freezer with through-the-door ice service | 10.10\*AV+406 | 8.08\*AV+324.8 | 8.54AV + 432.8 | 7.69 \* AV + 397.9 |

Note CEE Tier 2 standard criteria is 25% less consumption than a new baseline unit. It is assumed that after September 2014 when the Federal Standard and ENERGY STAR specifications change, the CEE Tier 2 will remain set at 25% less that the new baseline assumption.

This measure was developed to be applicable to the following program types:  TOS, NC, EREP.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The efficient equipment is defined as a refrigerator meeting the efficiency specifications of ENERGY STAR or CEE Tier 2 (defined as requiring >= 20% or >= 25% less energy consumption than an equivalent unit meeting federal standard requirements respectively). The ENERGY STAR standard varies according to the size and configuration of the unit, as shown in table above.

###### Definition of Baseline Equipment

Time of Sale: baseline is a new refrigerator meeting the minimum federal efficiency standard for refrigerator efficiency. The current federal minimum standard varies according to the size and configuration of the unit, as shown in table above.. Note also that this federal standard will be increased for units manufactured after September 1, 2014.

Early Replacement: the baseline is the existing refrigerator for the assumed remaining useful life of the unit and the new baseline as defined above for the remainder of the measure life.

###### Deemed Lifetime of Efficient Equipment

The measure life is assumed to be 12 years.[[731]](#footnote-732)

Remaining life of existing equipment is assumed to be 4 years[[732]](#footnote-733)

###### Deemed Measure Cost

Time of Sale: The incremental cost for this measure is assumed to be $40[[733]](#footnote-734) for an ENERGY STAR unit and $140[[734]](#footnote-735) for a CEE Tier 2 unit.

Early Replacement: The measure cost is the full cost of removing the existing unit and installing a new one. The actual program cost should be used. If unavailable assume $451 for ENERGY STAR unit and $551 for CEE Tier 2 unit[[735]](#footnote-736).

The avoided replacement cost (after 4 years) of a baseline replacement refrigerator is $390[[736]](#footnote-737).

###### Loadshape

Loadshape R05 - Residential Refrigerator

###### Coincidence Factor

A coincidence factor is not used to calculate peak demand savings for this measure, see below.

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings:

Time of Sale: ΔkWh = UECBASE – UECEE

Early Replacement:

ΔkWh for remaining life of existing unit (1st 4 years) = UECEXIST – UECEE

ΔkWh for remaining measure life (next 8 years) = UECBASE – UECEE

Where:

UECEXIST = Annual Unit Energy Consumption of existing unit as calculated in algorithm from 5.1.8 Refrigerator and Freezer Recycling measure.

UECBASE = Annual Unit Energy Consumption of baseline unit as calculated in algorithm provided in table above.

UECEE = Annual Unit Energy Consumption of ENERGY STAR unit as calculated in algorithm provided in table above.

For CEE Tier 2, unit consumption is calculated as 25% lower than baseline.

If volume is unknown, use the following defaults, based on an assumed Adjusted Volume of 25.8**[[737]](#footnote-738)**:

Assumptions prior to standard changes on September 1st, 2014:

| **Product Category** | **Existing Unit UECEXIST[[738]](#footnote-739)** | **New Baseline UECBASE** | **New Efficient**  **UECEE** | | **Early Replacement**  **(1st 4 years)**  **ΔkWh** | | **Time of Sale and**  **Early Replacement (last 8 years) ΔkWh** | |
| --- | --- | --- | --- | --- | --- | --- | --- | --- |
| **ENERGY STAR** | **CEE T2** | **ENERGY STAR** | **CEE T2** | **ENERGY STAR** | **CEE T2** |
| 1. Refrigerators and Refrigerator-freezers with manual defrost | 1027.7 | 475.7 | 380.5 | 356.8 | 647.2 | 671.0 | 95.1 | 118.9 |
| 2. Refrigerator-Freezer--partial automatic defrost | 1027.7 | 475.7 | 380.5 | 356.8 | 647.2 | 671.0 | 95.1 | 118.9 |
| 3. Refrigerator-Freezers--automatic defrost with top-mounted freezer without through-the-door ice service and all-refrigerators--automatic defrost | 814.5 | 528.5 | 422.8 | 396.4 | 391.7 | 418.1 | 105.7 | 132.1 |
| 4. Refrigerator-Freezers--automatic defrost with side-mounted freezer without through-the-door ice service | 1241.0 | 634.0 | 507.2 | 475.5 | 733.7 | 765.4 | 126.8 | 158.5 |
| 5. Refrigerator-Freezers--automatic defrost with bottom-mounted freezer without through-the-door ice service | 814.5 | 577.5 | 462.0 | 433.2 | 352.5 | 381.4 | 115.5 | 144.4 |
| 6. Refrigerator-Freezers--automatic defrost with top-mounted freezer with through-the-door ice service | 814.5 | 618.8 | 495.1 | 464.1 | 319.5 | 350.4 | 123.8 | 154.7 |
| 7. Refrigerator-Freezers--automatic defrost with side-mounted freezer with through-the-door ice service | 1241.0 | 666.3 | 533.0 | 499.7 | 707.9 | 741.3 | 133.3 | 166.6 |

Assumptions after standard changes on September 1st, 2014:

| **Product Category** | **Existing Unit UECEXIST[[739]](#footnote-740)** | **New Baseline UECBASE** | **New Efficient**  **UECEE** | | **Early Replacement**  **(1st 4 years)**  **ΔkWh** | | **Time of Sale and**  **Early Replacement (last 8 years) ΔkWh** | |
| --- | --- | --- | --- | --- | --- | --- | --- | --- |
| **ENERGY STAR** | **CEE T2** | **ENERGY STAR** | **CEE T2** | **ENERGY STAR** | **CEE T2** |
| 1. Refrigerators and Refrigerator-freezers with manual defrost | 1027.7 | 368.6 | 331.6 | 276.4 | 696.1 | 751.3 | 36.9 | 92.1 |
| 2. Refrigerator-Freezer--partial automatic defrost | 1027.7 | 430.9 | 387.8 | 323.2 | 640.0 | 704.6 | 43.1 | 107.7 |
| 3. Refrigerator-Freezers--automatic defrost with top-mounted freezer without through-the-door ice service and all-refrigerators--automatic defrost | 814.5 | 441.7 | 397.4 | 331.2 | 417.2 | 483.3 | 44.3 | 110.4 |
| 4. Refrigerator-Freezers--automatic defrost with side-mounted freezer without through-the-door ice service | 1241.0 | 517.1 | 465.4 | 387.8 | 775.6 | 853.1 | 51.7 | 129.3 |
| 5. Refrigerator-Freezers--automatic defrost with bottom-mounted freezer without through-the-door ice service | 814.5 | 545.1 | 490.7 | 408.8 | 323.9 | 405.8 | 54.4 | 136.3 |
| 5A Refrigerator-freezer—automatic defrost with bottom-mounted freezer with through-the-door ice service | 814.5 | 713.8 | 651.0 | 535.3 | 163.6 | 279.2 | 62.8 | 178.4 |
| 6. Refrigerator-Freezers--automatic defrost with top-mounted freezer with through-the-door ice service | 814.5 | 601.9 | 550.1 | 451.4 | 264.4 | 363.2 | 51.7 | 150.5 |
| 7. Refrigerator-Freezers--automatic defrost with side-mounted freezer with through-the-door ice service | 1241.0 | 652.9 | 596.1 | 489.6 | 644.9 | 751.3 | 56.8 | 163.2 |

###### Summer Coincident Peak Demand Savings

ΔkW = (ΔkWh/8766) \* TAF \* LSAF

Where:

TAF = Temperature Adjustment Factor

= 1.25[[740]](#footnote-741)

LSAF = Load Shape Adjustment Factor

= 1.057 [[741]](#footnote-742)

If volume is unknown, use the following defaults:

|  |  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- | --- |
| **Product Category** | **Assumptions prior to September 2014 standard change**  **ΔkW** | | | | **Assumptions after September 2014 standard change**  **ΔkW** | | | |
| **Early Replacement (1st 4 years)** | | **Time of Sale and Early Replacement (last 8 years)** | | **Early Replacement (1st 4 years)** | | **Time of Sale and Early Replacement (last 8 years)** | |
| **ENERGY STAR** | **CEE T2** | **ENERGY STAR** | **CEE T2** | **ENERGY STAR** | **CEE T2** | **ENERGY STAR** | **CEE T2** |
| 1. Refrigerators and Refrigerator-freezers with manual defrost | 0.098 | 0.101 | 0.014 | 0.018 | 0.105 | 0.113 | 0.006 | 0.014 |
| 2. Refrigerator-Freezer--partial automatic defrost | 0.098 | 0.101 | 0.014 | 0.018 | 0.096 | 0.106 | 0.006 | 0.016 |
| 3. Refrigerator-Freezers--automatic defrost with top-mounted freezer without through-the-door ice service and all-refrigerators--automatic defrost | 0.059 | 0.063 | 0.016 | 0.020 | 0.063 | 0.073 | 0.007 | 0.017 |
| 4. Refrigerator-Freezers--automatic defrost with side-mounted freezer without through-the-door ice service | 0.111 | 0.115 | 0.019 | 0.024 | 0.117 | 0.129 | 0.008 | 0.019 |
| 5. Refrigerator-Freezers--automatic defrost with bottom-mounted freezer without through-the-door ice service | 0.053 | 0.057 | 0.017 | 0.022 | 0.049 | 0.061 | 0.008 | 0.021 |
| 5A Refrigerator-freezer—automatic defrost with bottom-mounted freezer with through-the-door ice service | n/a | n/a | n/a | n/a | 0.025 | 0.042 | 0.009 | 0.027 |
| 6. Refrigerator-Freezers--automatic defrost with top-mounted freezer with through-the-door ice service | 0.048 | 0.053 | 0.019 | 0.023 | 0.040 | 0.055 | 0.008 | 0.023 |
| 7. Refrigerator-Freezers--automatic defrost with side-mounted freezer with through-the-door ice service | 0.107 | 0.112 | 0.020 | 0.025 | 0.097 | 0.113 | 0.009 | 0.025 |

###### Natural Gas Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-APL-ESRE-V02-140601

### ENERGY STAR and CEE Tier 1 Room Air Conditioner

###### Description

This measure relates to:

1. Time of Sale the purchase and installation of a room air conditioning unit that meets CEE TIER 1 (equivalent to ENERGY STAR version 3.0 which is effective October 1st 2013) or CEE Tier 2 minimum qualifying efficiency specifications, in place of a baseline unit. The baseline is equivalent to ENERGY STAR Version 2.0 efficiency ratings presented below since according to ENERGY STAR Shipment Data the estimated market penetration of ENERGY STAR Room AC went from 33%[[742]](#footnote-743) in 2010 to 62%[[743]](#footnote-744) in 2011 and a 2012 Illinois program evaluation found a net-to-gross ratio of just 1% for a Version 2.0 ENERGY STAR unit.

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
| **Product Type and Class (Btu/hr)** | | **ENERGY STAR v2.0 with louvered sides**  **(EER)[[744]](#footnote-745)** | **ENERGY STAR v2.0 without louvered sides**  **(EER)** | **ENERGY STAR v3.0 / CEE Tier 1 with louvered sides (EER)[[745]](#footnote-746)** | **ENERGY STAR v3.0 / CEE Tier 1 without louvered sides (EER)** | **CEE TIER 2 (EER)[[746]](#footnote-747)** |
| Without Reverse Cycle | < 8,000 | 10.7 | 9.9 | 11.2 | 10.4 | 11.6 |
| 8,000 to 10,999 | 10.8 | 9.9 | 11.3 | 9.8 | 11.8 |
| 11,000 to 13,999 | 10.8 | 9.4 | 11.3 | 9.8 | 11.8 |
| 14,000 to 19,999 | 10.7 | 9.4 | 11.2 | 9.8 | 11.6 |
| 20,000 to 24,999 | 9.4 | 9.4 | 9.8 | 9.8 | 10.2 |
| >=25,000 | 9.4 | 9.4 | 9.8 | 9.8 | 10.2 |
| With Reverse Cycle | <14,000 | 9.9 | 9.4 | 10.4 | 9.8 | 11.8 |
| 14,000 to 19,999 | 9.9 | 8.8 | 10.4 | 9.2 | 11.6 |
| >=20,000 | 9.4 | 8.8 | 9.8 | 9.2 | 10.2 |
| Casement only | | 9.6 | | 10.0 | |  |
| Casement-Slider | | 10.5 | | 10.9 | |  |

Side louvers extend from a room air conditioner model in order to position the unit in a window. A model without louvered sides is placed in a built-in wall sleeve and are commonly referred to as "through-the-wall" or "built-in" models.

Casement-only refers to a room air conditioner designed for mounting in a casement window of a specific size.

Casement-slider refers to a room air conditioner with an encased assembly designed for mounting in a sliding or casement window of a specific size.

Reverse cycle refers to the heating function found in certain room air conditioner models.

1. Early Replacement: the early removal of an existing residential inefficient Room AC unit from service, prior to its natural end of life, and replacement with a new ENERGY STAR or CEE Tier 1 qualifying unit. Savings are calculated between existing unit and efficient unit consumption during the remaining life of the existing unit, and between new baseline unit and efficient unit consumption for the remainder of the measure life.

This measure was developed to be applicable to the following program types:  TOS, NC, EREP.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the new room air conditioning unit must meet the CEE TIER 1 (equivalent to ENERGY STAR version 3.0 which is effective October 1st 2013) efficiency standards presented above.

###### Definition of Baseline Equipment

Time of Sale: the baseline assumption is a new room air conditioning unit that meets the ENERGY STAR Version 2.0 efficiency standards as presented above.

Early Replacement: the baseline is the existing Room AC for the assumed remaining useful life of the unit and the new baseline as defined above for the remainder of the measure life.

###### Deemed Lifetime of Efficient Equipment

The measure life is assumed to be 12 years[[747]](#footnote-748).

Remaining life of existing equipment is assumed to be 4 years[[748]](#footnote-749)

###### Deemed Measure Cost

Time of Sale: The incremental cost for this measure is assumed to be $40 for a CEE TIER 1 unit and $100 for a CEE Tier 2 unit[[749]](#footnote-750).

Early Replacement: The measure cost is the full cost of removing the existing unit and installing a new one. The actual program cost should be used. If unavailable assume $448 for CEE Tier 1 unit and $548 for CEE Tier 2 unit[[750]](#footnote-751).

The avoided replacement cost (after 4 years) of a baseline replacement refrigerator is $376.[[751]](#footnote-752)

###### Loadshape

Loadshape R08 - Residential Cooling

###### Coincidence Factor

The coincidence factor for this measure is assumed to be 0.3[[752]](#footnote-753).

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

Time of Sale: ΔkWh = (FLHRoomAC \* Btu/H \* (1/EERbase - 1/EERee))/1000

Early Replacment:

ΔkWh for remaining life of existing unit (1st 4 years) = (FLHRoomAC \* Btu/H \* (1/EERexist - 1/EERee))/1000

ΔkWh for remaining measure life (next 8 years) = (FLHRoomAC \* Btu/H \* (1/EERbase - 1/EERee))/1000

Where:

FLHRoomAC = Full Load Hours of room air conditioning unit

= dependent on location[[753]](#footnote-754):

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **FLHRoomAC** |
| 1 (Rockford) | 220 |
| 2 (Chicago) | 210 |
| 3 (Springfield) | 319 |
| 4 (Belleville) | 428 |
| 5 (Marion) | 374 |
| Weighted Average**[[754]](#footnote-755)** | 248 |

Btu/H = Size of rebated unit

= Actual. If unknown assume 8500 Btu/hr[[755]](#footnote-756)

EERexist = Efficiency of existing unit

= Actual. If unknown assume 7.7[[756]](#footnote-757)

EERbase = Efficiency of baseline unit

= As provided in tables above

EERee = Efficiency of CEE Tier 1 (or ENERGY STAR Version 3.0) unit

= Actual. If unknown assume minimum qualifying standard as provided in tables above

Time of Sale:

For example for an 8,500 Btu/H capacity unit, with louvered sides, in an unknown location:

ΔkWHCEE TIER 1 = (248 \* 8500 \* (1/10.8 – 1/11.3)) / 1000

= 8.6 kWh

Early Replacement:

A 7.7EER, 9000Btu/h unit is removed from a home in Springfield and replaced with a CEE T1 unit with louvered sides:

ΔkWh for remaining life of existing unit (1st 4 years) = (319 \* 9000 \* (1/7.7 - 1/11.3))/1000

= 118.8 kWh

ΔkWh for remaining measure life (next 8 years) = (319 \* 9000 \* (1/10.8 - 1/11.3))/1000

= 11.8 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = Btu/H \* ((1/EERbase - 1/EERee))/1000) \* CF

Where:

CF = Summer Peak Coincidence Factor for measure

= 0.3[[757]](#footnote-758)

Other variable as defined above

Time of Sale:

For example for an 8,500 Btu/H capacity unit, with louvered sides, for an unknown location:

ΔkWCEE TIER 1 = (8500 \* (1/10.8 – 1/11.3)) / 1000 \* 0.3

= 0.010 kW

Early Replacement:

A 7.7EER, 9000Btu/h unit is removed from a home in Springfield and replaced with a CEE T1 unit with louvered sides:

ΔkW for remaining life of existing unit (1st 4 years) = (9000 \* (1/7.7 - 1/11.3))/1000 \* 0.3

= 0.11 kW

ΔkW for remaining measure life (next 8 years) = (9000 \* (1/10.8 - 1/11.3))/1000 \* 0.3

= 0.011 kW

###### Natural Gas Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-APL-ESRA-V03-140601

### Refrigerator and Freezer Recycling

###### Description

This measure describes savings from the retirement and recycling of inefficient but operational refrigerators and freezers. Savings are provided based on a 2013 workpaper provided by Cadmus that used data from a 2012 ComEd metering study and metering data from a Michigan study, to develop a regression equation that uses key inputs describing the retired unit. The savings are equivalent to the Unit Energy Consumption of the retired unit and should be claimed for the assumed remaining useful life of that unit. A part use factor is applied to account for those secondary units that are not in use throughout the entire year. The reader should note that the regression algorithm is designed to provide an accurate portrayal of savings for the population as a whole and includes those parameters that have a significant effect on the consumption. The precision of savings for individual units will vary.

The Net to Gross factor applied to these units should incorporate adjustments that account for:

* Those participants who would have removed the unit from the grid anyway (e.g. customers replacing their refrigerator via a big box store and using the pick-up option, customers taking their unit to the landfill or recycling station);
* Those participants who decided, based on the incentive provided by the Appliance Recycling program alone, to replace their existing inefficient unit with a new unit. This segment of participants is expected to be very small and documentation of their intentions will be gathered via telephone surveys (i.e., primary data sources). For such customers, the consumption of the new unit should be subtracted from the retired unit consumption and savings claimed for the remaining life of the existing unit. Note that participants who were already planning to replace their unit, and the incentive just ensured that the retired unit was recycled and not placed on the secondary market, should not be included in this adjustment.

This measure was developed to be applicable to the following program types:  ERET.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

n/a

###### Definition of Baseline Equipment

The existing inefficient unit must be operational and have a capacity of between 10 and 30 cubic feet.

###### Deemed Lifetime of Efficient Equipment

The estimated remaining useful life of the recycling units is 8 years [[758]](#footnote-759).

###### Deemed Measure Cost

Measure cost includes the cost of pickup and recycling of the refrigerator and should be based on actual costs of running the program. If unknown assume $120[[759]](#footnote-760) per unit.

###### Loadshape

Loadshape R05 - Residential Refrigerator

###### Coincidence Factor

The coincidence factor is assumed to be 0.00012.

**Algorithm**

###### Calculation of Savings

###### Energy Savings[[760]](#footnote-761)

Refrigerators:

Energy savings for refrigerators are based upon a linear regression model using the following coefficients[[761]](#footnote-762):

|  |  |
| --- | --- |
| **Independent Variable Description** | **Estimate Coefficient** |
| Intercept | 83.324 |
| Age (years) | 3.678 |
| Pre-1990 (=1 if manufactured pre-1990) | 485.037 |
| Size (cubic feet) | 27.149 |
| Dummy: Side-by-Side (= 1 if side-by-side) | 406.779 |
| Dummy: Primary Usage Type (in absence of the program)  (= 1 if primary unit) | 161.857 |
| Interaction: Located in Unconditioned Space x CDD/365.25 | 15.366 |
| Interaction: Located in Unconditioned Space x HDD/365.25 | -11.067 |

ΔkWh = [83.32 + (Age \* 3.68) + (Pre-1990 \* 485.04) + (Size \* 27.15) + (Side-by-side \* 406.78) + (Proportion of Primary Appliances \* 161.86) + (CDD/365.25 \* unconditioned \* 15.37) + (HDD/365.25 \*unconditioned \*-11.07)] \* Part Use Factor

Where:

Age = Age of retired unit

Pre-1990 = Pre-1990 dummy (=1 if manufactured pre-1990, else 0)

Size = Capacity (cubic feet) of retired unit

Side-by-side = Side-by-side dummy (= 1 if side-by-side, else 0)

Single-Door = Single-Door dummy (= 1 if Single-Door, else 0)

Primary Usage = Primary Usage Type (in absence of the program) dummy

(= 1 if Primary, else 0)

Interaction: Located in Unconditioned Space x CDD/365.25

(=1 \* CDD/365.25 if in unconditioned space)

CDD = Cooling Degree Days

= Dependent on location[[762]](#footnote-763):

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **CDD 65** | **CDD/365.25** |
| 1 (Rockford) | 820 | 2.25 |
| 2 (Chicago) | 842 | 2.31 |
| 3 (Springfield) | 1,108 | 3.03 |
| 4 (Belleville) | 1,570 | 4.30 |
| 5 (Marion) | 1,370 | 3.75 |

Interaction: Located in Unconditioned Space x HDD/365.25

(=1 \* HDD/365.25 if in unconditioned space)

HDD = Heating Degree Days

= Dependent on location:[[763]](#footnote-764)

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **HDD 65** | **HDD/365.25** |
| 1 (Rockford) | 6,569 | 17.98 |
| 2 (Chicago) | 6,339 | 17.36 |
| 3 (Springfield) | 5,497 | 15.05 |
| 4 (Belleville) | 4,379 | 11.99 |
| 5 (Marion) | 4,476 | 12.25 |

Part Use Factor = To account for those units that are not running throughout the entire year. The most recent part-use factor participant survey results available at the start of the current program year shall be used[[764]](#footnote-765).  For illustration purposes, this example uses 0.93.[[765]](#footnote-766)

For example, the program averages for AIC’s ARP in PY4 produce the following equation:

ΔkWh = [83.32 + (22.81 \* 3.68) + (0.45 \* 485.04) + (18.82 \* 27.15) + (0.17 \* 406.78) + (0.34 \* 161.86) + (1.29 \* 15.37) + (6.49 \* -11.07)] \* 0.93

= 969 \* 0.93

= 900.9 kWh

Freezers:

Energy savings for freezers are based upon a linear regression model using the following coefficients[[766]](#footnote-767):

|  |  |
| --- | --- |
| **Independent Variable Description** | **Estimate Coefficient** |
| Intercept | 132.122 |
| Age (years) | 12.130 |
| Pre-1990 (=1 if manufactured pre-1990) | 156.181 |
| Size (cubic feet) | 31.839 |
| Chest Freezer Configuration (=1 if chest freezer) | -19.709 |
| Interaction: Located in Unconditioned Space x CDD/365.25 | 9.778 |
| Interaction: Located in Unconditioned Space x HDD/365.25 | -12.755 |

ΔkWh = [132.12 + (Age \* 12.13) + (Pre-1990 \* 156.18) + (Size \* 31.84) + (Chest Freezer \* -19.71) + (CDDs\* unconditioned \*9.78) + (HDDs\*unconditioned \*-12.75)] \* Part Use Factor

Where:

Age = Age of retired unit

Pre-1990 = Pre-1990 dummy (=1 if manufactured pre-1990, else 0)

Size = Capacity (cubic feet) of retired unit

Chest Freezer = Chest Freezer dummy (= 1 if chest freezer, else 0)

Interaction: Located in Unconditioned Space x CDD/365.25

(=1 \* CDD/365.25 if in unconditioned space)

CDD = Cooling Degree Days (see table above)

Interaction: Located in Unconditioned Space x HDD/365.25

(=1 \* HDD/365.25 if in unconditioned space)

HDD = Heating Degree Days (see table above)

Part Use Factor = To account for those units that are not running throughout the entire year. The most recent part-use factor participant survey results available at the start of the current program year shall be used[[767]](#footnote-768).  . For illustration purposes, the example uses 0.85.[[768]](#footnote-769)

The program averages for AIC’s ARP PY4 program are used as an example.

ΔkWh = [132.12 + (26.92 \* 12.13) + (0.6 \* 156.18) + (15.9 \* 31.84) + (0.48 \* -19.71) + (6.61 \* 9.78) + (1.3 \* -12.75)] \* 0.825

= 977 \* 0.825

= 905 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = kWh/8760 \* CF

Where:

kWh = Savings provided in algorithm above

CF = Coincident factor defined as summer kW/average kW

= 1.081 for Refrigerators

= 1.028 for Freezers[[769]](#footnote-770)

For example, the program averages for AIC’s ARP in PY4 produce the following equation:

ΔkW = 806/8760 \* 1.081

= 0.099 kW

###### Natural Gas Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-APL-RFRC-V05-150601

### Room Air Conditioner Recycling

###### Description

This measure describes the savings resulting from running a drop off service taking existing residential, inefficient Room Air Conditioner units from service, prior to their natural end of life. This measure assumes that though a percentage of these units will be replaced this is not captured in the savings algorithm since it is unlikely that the incentive made someone retire a unit that they weren’t already planning to retire. The savings therefore relate to the unit being taken off the grid as opposed to entering the secondary market. The Net to Gross factor applied to these units should incorporate adjustments that account for those participants who would have removed the unit from the grid anyway.

This measure was developed to be applicable to the following program types:  ERET.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

N/A. This measure relates to the retiring of an existing inefficient unit.

###### Definition of Baseline Equipment

The baseline condition is the existing inefficient room air conditioning unit.

###### Deemed Lifetime of Efficient Equipment

The assumed remaining useful life of the existing room air conditioning unit being retired is 4 years[[770]](#footnote-771).

###### Deemed Measure Cost

The actual implementation cost for recycling the existing unit should be used.

###### Loadshape

Loadshape R08 - Residential Cooling

###### Coincidence Factor

The coincidence factor for this measure is assumed to be 30%[[771]](#footnote-772).

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = ((FLHRoomAC \* Btu/hr \* (1/EERexist))/1000)

Where:

FLHRoomAC = Full Load Hours of room air conditioning unit

= dependent on location[[772]](#footnote-773):

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **FLHRoomAC** |
| 1 (Rockford) | 220 |
| 2 (Chicago) | 210 |
| 3 (Springfield) | 319 |
| 4 (Belleville) | 428 |
| 5 (Marion) | 374 |
| Weighted Average**[[773]](#footnote-774)** | 248 |

Btu/H = Size of retired unit

= Actual. If unknown assume 8500 Btu/hr [[774]](#footnote-775)

EERexist = Efficiency of existing unit

= 7.7[[775]](#footnote-776)

For example for an 8500 Btu/h unit in Springfield:

ΔkWh = ((319 \* 8500 \* (1/7.7)) / 1000)

= 352 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = (Btu/hr \* (1/EERexist))/1000) \* CF

Where:

CF = Summer Peak Coincidence Factor for measure

= 0.3[[776]](#footnote-777)

For example an 8500 Btu/h unit:

ΔkW = (8500 \* (1/7.7)) / 1000) \* 0.3

= 0.33 kW

###### Natural Gas Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-APL-RARC-V01-120601

### Residential ENERGY STAR Clothes Dryer

**Description**

This measure relates to the installation of a residential clothes dryer meeting the ENERGY STAR criteria. ENERGY STAR qualified clothes dryers save energy through a combination of more efficient drying and reduced runtime of the drying cycle. More efficient drying is achieved through increased insulation, modifying operating conditions such as air flow and/or heat input rate, improving air circulation through better drum design or booster fans, and improving efficiency of motors. Reducing the runtime of dryers through automatic termination by temperature and moisture sensors is believed to have the greatest potential for reducing energy use in clothes dryers[[777]](#footnote-778). ENERGY STAR provides criteria for both gas and electric clothes dryers.

This measure was developed to be applicable to the following program types: TOS, NC. If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

Clothes dryer must meet the ENERGY STAR criteria, as required by the program.

**Definition of Baseline Equipment**

The baseline condition is a clothes dryer meeting the minimum federal requirements for units manufactured on or after January 1, 2015.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 14 years[[778]](#footnote-779).

**Deemed Measure Cost**

The incremental cost for an ENERGY STAR clothes dryer is assumed to be $152[[779]](#footnote-780)

**Loadshape**

N/A

**Coincidence Factor**

The coincidence factor for this measure is 3.8%[[780]](#footnote-781).

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

∆kWh = (Load/CEFbase – Load/CEFeff) \* Ncycles \* %Electric

Where:

Load = The average total weight (lbs) of clothes per drying cycle. If dryer size is unknown, assume standard.

|  |  |
| --- | --- |
| **Dryer Size** | **Load (lbs)[[781]](#footnote-782)** |

|  |  |
| --- | --- |
| Standard | 8.45 |
| Compact | 3 |

CEFbase = Combined energy factor (CEF) (lbs/kWh) of the baseline unit is based on existing federal standards energy factor and adjusted to CEF as performed in the ENERGY STAR analysis[[782]](#footnote-783). If product class unknown, assume electric, standard.

| **Product Class** | **CEF (lbs/kWh)** |
| --- | --- |
| Vented Electric, Standard (≥ 4.4 ft3) | 3.11 |
| Vented Electric, Compact (120V) (< 4.4 ft3) | 3.01 |
| Vented Electric, Compact (240V) (<4.4 ft3) | 2.73 |
| Ventless Electric, Compact (240V) (<4.4 ft3) | 2.13 |
| Vented Gas | 2.84[[783]](#footnote-784) |

CEFeff = CEF (lbs/kWh) of the ENERGY STAR unit based on ENERGY STAR requirements.[[784]](#footnote-785) If product class unknown, assume electric, standard.

| **Product Class** | **CEF (lbs/kWh)** |
| --- | --- |
| Vented or Ventless Electric, Standard (≥ 4.4 ft3) | 3.93 |
| Vented or Ventless Electric, Compact (120V) (< 4.4 ft3) | 3.80 |
| Vented Electric, Compact (240V) (< 4.4 ft3) | 3.45 |
| Ventless Electric, Compact (240V) (< 4.4 ft3) | 2.68 |
| Vented Gas | 3.48a |

Ncycles = Number of dryer cycles per year. Use actual data if available. If unknown, use 283 cycles per year.[[785]](#footnote-786)

%Electric = The percent of overall savings coming from electricity

= 100% for electric dryers, 16% for gas dryers[[786]](#footnote-787)

**Example**

Time of Sale: For example, a standard, vented, electric clothes dryer:

ΔkWh = ((8.45/3.11 – 8.45/3.93) \* 283 \* 100%)

= 160 kWh

**Summer Coincident Peak Demand Savings**

ΔkW = ΔkWh/Hours \* CF

Where:

ΔkWh = Energy Savings as calculated above

Hours = Annual run hours of clothes dryer. Use actual data if available. If unknown, use 283 hours per year.[[787]](#footnote-788)

CF = Summer Peak Coincidence Factor for measure

= 3.8%[[788]](#footnote-789)

**Example**

Time of Sale: For example, a standard, vented, electric clothes dryer:

ΔkW = 160/283 \* 3.8%

= 0.0215 kW

**Natural Gas Savings**

Natural gas savings only apply to ENERGY STAR vented gas clothes dryers.

∆Therm = (Load/EFbase – Load/CEFeff) \* Ncycles \* Therm\_convert \* %Gas

Where:

Therm\_convert = Conversion factor from kWh to Therm

= 0.03413

%Gas = Percent of overall savings coming from gas

= 0% for electric units and 84% for gas units[[789]](#footnote-790)

**Example**

Time of Sale: For example, a standard, vented, gas clothes dryer:

ΔTherm = (8.45/2.84 – 8.45/3.48) \* 283 \* 0.03413 \* 0.84

= 4.44 therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

###### Measure Code: RS-APL-ESDR-V01-150601

## Consumer Electronics End Use

### Smart Strip

###### Description

This measure relates to Controlled Power Strips (or Smart Strips) which are multi-plug power strips with the ability to automatically disconnect specific connected loads depending upon the power draw of a control load, also plugged into the strip. Power is disconnected from the switched (controlled) outlets when the control load power draw is reduced below a certain adjustable threshold, thus turning off the appliances plugged into the switched outlets. By disconnecting, the standby load of the controlled devices, the overall load of a centralized group of equipment (i.e. entertainment centers and home office) can be reduced. Uncontrolled outlets are also provided that are not affected by the control device and so are always providing power to any device plugged into it. This measure characterization provides savings for a 5-plug strip and a 7-plug strip.

This measure was developed to be applicable to the following program types:  TOS, NC, DI.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The efficient case is the use of a 5 or 7-plug smart strip.

###### Definition of Baseline Equipment

The assumed baseline is a standard power strip that does not control connected loads.

###### Deemed Lifetime of Efficient Equipment

The assumed lifetime of the smart strip is 4 years[[790]](#footnote-791).

###### Deemed Measure Cost

The incremental cost of a smart strip over a standard power strip with surge protection is assumed to be $16 for a 5-plug and $26 for a 7-plug[[791]](#footnote-792).

###### Loadshape

Loadshape R13 - Residential Standby Losses – Entertainment

Loadshape R14 - Residential Standby Losses - Home Office

###### Coincidence Factor

The summer peak coincidence factor for this measure is assumed to be 80%[[792]](#footnote-793).

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh5-Plug = 56.5 kWh [[793]](#footnote-794)

ΔkWh7-Plug = 103 kWh [[794]](#footnote-795)

###### Summer Coincident Peak Demand Savings

∆kW**=** ∆kWh/ Hours \* CF

Where:

Hours = Annual number of hours during which the controlled standby loads are turned off by the Smart Strip.

= 7,129 [[795]](#footnote-796)

CF = Summer Peak Coincidence Factor for measure

= 0.8 [[796]](#footnote-797)

ΔkW5-Plug = 56.5 / 7129 \* 0.8

= 0.00634 kW

ΔkW7-Plug = 102.8 / 7129 \* 0.8

= 0.0115 kW

###### Natural Gas Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-CEL-SSTR-V01-120601

## HVAC End Use

### Air Source Heat Pump

###### Description

A heat pump provides heating or cooling by moving heat between indoor and outdoor air.

This measure characterizes:

1. Time of Sale:
   1. The installation of a new residential sized (<= 65,000 Btu/hr) air source heat pump that is more efficient than required by federal standards. This could relate to the replacement of an existing unit at the end of its useful life, or the installation of a new system in a new home.
2. Early Replacement:
   1. The early removal of functioning electric heating and cooling (SEER 10 or under if present) systems from service, prior to its natural end of life, and replacement with a new high efficiency air source heat pump unit. Savings are calculated between existing unit and efficient unit consumption during the remaining life of the existing unit, and between new baseline unit and efficient unit consumption for the remainder of the measure life.
   2. The assumption of the existing unit efficiency in the Early Replacement section of this TRM is based upon the average efficiency of units that were classified in Ameren’s PY3-PY4 as functioning and SEER <=10. Therefore it is only appropriate to use these Early Replacement assumptions where those conditions are met. The TAC defined “functioning” as the unit is fully operational – providing sufficient space conditioning (i.e. heat exchanger, compressors, pumps work effectively) and/or the cost of repair is under 20% of the new baseline replacement cost. Therefore in order to apply early replacement assumptions the programs should apply the following eligibility criteria: SEER <=10 and cost of any repairs <$249 per ton.
   3. A weighted average early replacement rate is provided for use when the actual baseline early replacement rates are unknown[[797]](#footnote-798).

Deemed Early Replacement Rates For ASHP

|  |  |
| --- | --- |
|  | **Deemed Early Replacement Rate** |
| Early Replacement Rate for ASHP participants | 7% |

This measure was developed to be applicable to the following program types:  TOS, NC, EREP.  If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

A new residential sized (<= 65,000 Btu/hr) air source heat pump with specifications to be determined by program.

###### Definition of Baseline Equipment

A new residential sized (<= 65,000 Btu/hr) air source heat pump meeting federal standards.

The baseline for the Time of Sale measure is based on the current Federal Standard efficiency level as of January 1st 2015; 14 SEER and 8.2HSPF.

The baseline for the early replacement measure is the efficiency of the existing equipment for the assumed remaining useful life of the unit and the new baseline as defined above for the remainder of the measure life.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 18 years[[798]](#footnote-799).

Remaining life of existing equipment is assumed to be 6 years[[799]](#footnote-800).

###### Deemed Measure Cost

Time of sale: The incremental capital cost for this measure is dependent on the efficiency and capacity of the new unit[[800]](#footnote-801). Note these costs are per ton of unit capacity:

|  |  |
| --- | --- |
| **Efficiency (SEER)** | **Incremental Cost per Ton of Capacity ($/ton)** |
| 15 | $137 |
| 16 | $274 |
| 17 | $411 |
| 18 | $548 |

Early replacement: The capital cost for this measure is the actual cost of removing the existing unit and installing the new one. If this is unknown, assume the following (note these costs are per ton of unit capacity)[[801]](#footnote-802):

|  |  |
| --- | --- |
| **Efficiency (SEER)** | **Full Retrofit Cost (including labor) per Ton of Capacity ($/ton)** |
| 15 | $1,518 |
| 16 | $1,655 |
| 17 | $1,792 |
| 18 | $1,929 |

Assumed deferred cost (after 6 years) of replacing existing equipment with new baseline unit is assumed to be $1,381 per ton of capacity[[802]](#footnote-803). This cost should be discounted to present value using the utilities discount rate.

###### Loadshape

Loadshape R10 - Residential Electric Heating and Cooling

###### Coincidence Factor

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.

CFSSP = Summer System Peak Coincidence Factor for Heat Pumps (during utility peak hour)

= 72%%[[803]](#footnote-804)

CFPJM   = PJM Summer Peak Coincidence Factor for Heat Pumps (average during PJM peak period)

= 46.6%[[804]](#footnote-805)

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

Time of sale:

ΔkWh = ((FLH\_cooling \* Capacity\_cooling \* (1/SEER\_base - 1/SEER\_ee)) / 1000) + ((FLH\_heat \* Capacity\_heating \* (1/HSPF\_base - 1/HSFP\_ee)) / 1000)

Early replacement[[805]](#footnote-806):

ΔkWH for remaining life of existing unit (1st 6 years):

= ((FLH\_cooling \* Capacity\_cooling \* (1/SEER\_exist - 1/SEER\_ee)) / 1000) + ((FLH\_heat \* Capacity\_heating \* (1/HSPF\_exist - 1/HSFP\_ee)) / 1000)

ΔkWH for remaining measure life (next 12 years):

= ((FLH\_cooling \* Capacity\_cooling \* (1/SEER\_base - 1/SEER\_ee)) / 1000) + ((FLH\_heat \* Capacity\_heating \* (1/HSPF\_base - 1/HSFP\_ee)) / 1000)

Where:

FLH\_cooling = Full load hours of air conditioning

= dependent on location[[806]](#footnote-807):

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **FLH\_cooling (single family)** | **FLH\_cooling (multi family)** |
| 1 (Rockford) | 512 | 467 |
| 2 (Chicago) | 570 | 506 |
| 3 (Springfield) | 730 | 663 |
| 4 (Belleville) | 1,035 | 940 |
| 5 (Marion) | 903 | 820 |
| Weighted Average[[807]](#footnote-808) | 629 | 564 |

Capacity\_cooling = Cooling Capacity of Air Source Heat Pump (Btu/hr)

= Actual (1 ton = 12,000Btu/hr)

SEER\_exist = Seasonal Energy Efficiency Ratio of existing cooling system (kBtu/kWh)

= Use actual SEER rating where it is possible to measure or reasonably estimate.

|  |  |
| --- | --- |
| **Existing Cooling System** | **SEER\_exist[[808]](#footnote-809)** |
| Air Source Heat Pump | 9.12 |
| Central AC | 8.60 |
| No central cooling[[809]](#footnote-810) | Make ‘1/SEER\_exist’ = 0 |

SEER\_base = Seasonal Energy Efficiency Ratio of baseline Air Source Heat Pump (kBtu/kWh)

= 14 [[810]](#footnote-811)

SEER\_ee = Seasonal Energy Efficiency Ratio of efficient Air Source Heat Pump (kBtu/kWh)

= Actual

FLH\_heat = Full load hours of heating

= Dependent on location[[811]](#footnote-812):

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **FLH\_heat** |
| 1 (Rockford) | 1,969 |
| 2 (Chicago) | 1,840 |
| 3 (Springfield) | 1,754 |
| 4 (Belleville) | 1,266 |
| 5 (Marion) | 1,288 |
| Weighted Average[[812]](#footnote-813) | 1,821 |

Capacity\_heating = Heating Capacity of Air Source Heat Pump (Btu/hr)

= Actual (1 ton = 12,000Btu/hr)

HSPF\_exist =Heating System Performance Factor[[813]](#footnote-814) of existing heating system (kBtu/kWh)

= Use actual HSPF rating where it is possible to measure or reasonably estimate. If not available use:

|  |  |
| --- | --- |
| **Existing Heating System** | **HSPF\_exist** |
| Air Source Heat Pump | 5.44 [[814]](#footnote-815) |
| Electric Resistance | 3.41[[815]](#footnote-816) |

HSPF\_base =Heating System Performance Factor of baseline Air Source Heat Pump (kBtu/kWh)

= 8.2 [[816]](#footnote-817)

HSFP\_ee =Heating System Performance Factor of efficient Air Source Heat Pump

(kBtu/kWh)

= Actual

Time of Sale:

For example, a three ton, 15 SEER, 12EER, 9 HSPF Air Source Heat Pump installed in Marion:

ΔkWh = ((903 \* 36,000 \* (1/14 - 1/15)) / 1000) + ((1,288 \* 36,000 \* (1/8.2 - 1/9)) / 1000)

= 657 kWh

Early Replacement:

For example, a three ton, 15 SEER, 12EER, 9 HSPF Air Source Heat Pump replaces an existing working Air Source Heat Pump with unknown efficiency ratings in Marion:

ΔkWH for remaining life of existing unit (1st 6 years):

= ((903 \* 36,000 \* (1/9.12 - 1/15)) / 1000) + ((1,288 \* 36,000 \* (1/5.44 - 1/9)) / 1000)

= 4769 kWh

ΔkWH for remaining measure life (next 12 years):

= ((903 \* 36,000 \* (1/14 - 1/15)) / 1000) + ((1,288 \* 36,000 \* (1/8.2 - 1/9)) / 1000)

= 657 kWh

###### Summer Coincident Peak Demand Savings

Time of sale:

ΔkW = (Capacity\_cooling \* (1/EER\_base - 1/EER\_ee)) / 1000) \* CF

Early replacement[[817]](#footnote-818):

ΔkW for remaining life of existing unit (1st 6 years):

= ((Capacity\_cooling \* (1/EERexist - 1/EERee))/1000 \* CF);

ΔkW for remaining measure life (next 12 years):

= ((Capacity\_cooling \* (1/EERbase - 1/EERee))/1000 \* CF)

Where:

EER\_exist = Energy Efficiency Ratio of existing cooling system (kBtu/hr / kW)

= Use actual EER rating where it is possible to measure or reasonably estimate. If EER unknown but SEER available convert using the equation:

EER\_base = (-0.02 \* SEER\_base2) + (1.12 \* SEER) [[818]](#footnote-819)

If SEER rating unavailable use:

|  |  |
| --- | --- |
| **Existing Cooling System** | **EER\_exist[[819]](#footnote-820)** |
| Air Source Heat Pump | 8.55 |
| Central AC | 8.15 |
| No central cooling[[820]](#footnote-821) | Make ‘1/EER\_exist’ = 0 |

EER\_base = Energy Efficiency Ratio of baseline Air Source Heat Pump (kBtu/hr / kW)

= 11.8 [[821]](#footnote-822)

EER\_ee = Energy Efficiency Ratio of baseline Air Source Heat Pump (kBtu/hr / kW)

= Actual, If not provided convert SEER to EER using this formula:[[822]](#footnote-823)

= (-0.02 \* SEER2) + (1.12 \* SEER)

CFSSP = Summer System Peak Coincidence Factor for Heat Pumps (during system peak hour)

= 72%%[[823]](#footnote-824)

CFPJM = PJM Summer Peak Coincidence Factor for Heat Pumps (average during peak period)

= 46.6%[[824]](#footnote-825)

Time of Sale:

For example, a three ton, 15 SEER, 12EER, 9 HSPF Air Source Heat Pump installed in Marion:

ΔkWSSP = ((36,000 \* (1/11.8 – 1/12)) / 1000) \* 0.72

= 0.037 kW

ΔkWPJM = ((36,000 \* (1/11.8 – 1/12)) / 1000) \* 0.466

= 0.024 kW

Early Replacement:

For example, a three ton, 15 SEER, 12EER, 9 HSPF Air Source Heat Pump replaces an existing working Air Source Heat Pump with unknown efficiency ratings in Marion:

ΔkWSSP for remaining life of existing unit (1st 6 years):

= ((36,000 \* (1/8.55 - 1/12)) / 1000) \* 0.72

= 0.872 kW

ΔkWSSP for remaining measure life (next 12 years):

= ((36,000 \* (1/11.8 – 1/12)) / 1000) \* 0.72

= 0.037 kW

ΔkWPJM for remaining life of existing unit (1st 6 years):

= ((36,000 \* (1/8.55 - 1/12)) / 1000) \* 0.466

= 0.564 kW

ΔkWPJM for remaining measure life (next 12 years):

= ((36,000 \* (1/11.8 – 1/12)) / 1000) \* 0.466

= 0.024 kW

###### Natural Gas Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-HVC-ASHP-V04-150601

### Boiler Pipe Insulation

###### Description

This measure describes adding insulation to un-insulated boiler pipes in un-conditioned basements or crawlspaces.

This measure was developed to be applicable to the following program types:  TOS, RNC, RF, DI.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The efficient case is installing pipe wrap insulation to a length of boiler pipe.

###### Definition of Baseline Equipment

The baseline is an un-insulated boiler pipe.

###### Deemed Lifetime of Efficient Equipment

The measure life is assumed to be 15 years[[825]](#footnote-826).

###### Deemed Measure Cost

The measure cost including material and installation is assumed to be $3 per linear foot[[826]](#footnote-827).

###### Loadshape

N/A

###### Coincidence Factor

N/A

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Savings

ΔTherm = (((1/Rexist \* Cexist) – (1/Rnew \* Cnew)) \* FLH\_heat \* L \* ΔT) / ηBoiler /100,000

Where:

Rexist = Pipe heat loss coefficient of uninsulated pipe (existing) [(hr-°F-ft2)/Btu]

= 0.5[[827]](#footnote-828)

Rnew = Pipe heat loss coefficient of insulated pipe (new) [(hr-°F-ft2)/Btu]

= Actual (0.5 + R value of insulation)

FLH\_heat = Full load hours of heating

= Dependent on location[[828]](#footnote-829):

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **FLH\_heat** |
| 1 (Rockford) | 1,969 |
| 2 (Chicago) | 1,840 |
| 3 (Springfield) | 1,754 |
| 4 (Belleville) | 1,266 |
| 5 (Marion) | 1,288 |
| Weighted Average[[829]](#footnote-830) | 1,821 |

L = Length of boiler pipe in unconditioned space covered by pipe wrap (ft)

= Actual

Cexist = Circumference of bare pipe (ft) (Diameter (in) \* π/12)

= Actual (0.5” pipe = 0.131ft, 0.75” pipe = 0.196ft)

Cnew  = Circumference of pipe with insulation (ft) (Diameter (in) \* π/12)

= Actual

ΔT = Average temperature difference between circulated heated water and unconditioned space air temperature (°F) [[830]](#footnote-831)

Pipes in unconditioned basement:

|  |  |
| --- | --- |
| **Outdoor reset controls** | **ΔT (°F)** |
| Boiler without reset control | 110 |
| Boiler with reset control | 70 |

Pipes in crawl space:

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **ΔT (°F)** | |
| **Boiler without reset control** | **Boiler with reset control** |
| 1 (Rockford) | 127 | 87 |
| 2 (Chicago) | 126 | 86 |
| 3 (Springfield) | 122 | 82 |
| 4 (Belleville) | 120 | 80 |
| 5 (Marion) | 120 | 80 |
| Weighted Average[[831]](#footnote-832) | 125 | 85 |

ηBoiler = Efficiency of boiler

= 0.819 [[832]](#footnote-833)

For example, insulating 10 feet of 0.75” pipe with R-3 wrap (0.75” thickness) in a crawl space of a Marion home with a boiler without reset control:

ΔTherm = (((1/0.5 \* 0.196) – (1/3.5 \* 0.589)) \* 10 \* 120 \* 1288) / 0.819 / 100,000

= 4.2 therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-HVC-PINS-V01-130601

### Central Air Conditioning > 14.5 SEER

**Description**

This measure characterizes:

1. Time of Sale:
   1. The installation of a new residential sized (<= 65,000 Btu/hr) Central Air Conditioning ducted split system meeting ENERGY STAR efficiency standards presented below. This could relate to the replacement of an existing unit at the end of its useful life, or the installation of a new system in a new home.
2. Early Replacement:
   1. The early removal of an existing residential sized (<= 65,000 Btu/hr) inefficient Central Air Conditioning unit from service, prior to its natural end of life, and replacement with a new ENERGY STAR qualifying unit. Savings are calculated between existing unit and efficient unit consumption during the remaining life of the existing unit, and between new baseline unit and efficient unit consumption for the remainder of the measure life.
   2. The assumption of the existing unit efficiency in the Early Replacement section of this TRM is based upon the average efficiency of units that were classified in Ameren’s PY3-PY4 as functioning and SEER <=10. Therefore it is only appropriate to use these Early Replacement assumptions where those conditions are met. The TAC defined “functioning” as the unit is fully operational – providing sufficient space conditioning (i.e. heat exchanger, compressors, pumps work effectively) and/or the cost of repair is under 20% of the new baseline replacement cost. Therefore in order to apply early replacement assumptions the programs should apply the following eligibility criteria: SEER <=10 and cost of any repairs <$190 per ton.
   3. A weighted average early replacement rate is provided for use when the actual baseline early replacement rate is unknown[[833]](#footnote-834).

**Deemed Early Replacement Rates For CAC Units in Combined System Replacement (CSR) Projects**

|  |  |
| --- | --- |
| **Replacement Scenario for the CAC Unit** | **Deemed Early Replacement Rate** |
| Early Replacement Rate for a CAC unit when the CAC unit is the Primary unit in a CSR project | 14% |
| Early Replacement Rate for a CAC unit when the CAC unit is the Secondary unit in a CSR project | 40% |

This measure was developed to be applicable to the following program types:  TOS, NC, EREP.  If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

In order for this characterization to apply, the efficient equipment is assumed to be a ducted split central air conditioning unit meeting the minimum ENERGY STAR efficiency level standards; 14.5 SEER and 12 EER.

**Definition of Baseline Equipment**

The baseline for the Time of Sale measure is based on the current Federal Standard efficiency level; 13 SEER and 11 EER.

The baseline for the early replacement measure is the efficiency of the existing equipment for the assumed remaining useful life of the unit and the new baseline as defined above[[834]](#footnote-835) for the remainder of the measure life.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 18 years [[835]](#footnote-836).

Remaining life of existing equipment is assumed to be 6 years[[836]](#footnote-837).

**Deemed Measure Cost**

Time of sale: The incremental capital cost for this measure is dependent on equipment size and efficiency. Assumed costs per ton of cooling capacity are provided below[[837]](#footnote-838):

|  |  |
| --- | --- |
| **Efficiency Level** | **Cost per Ton** |
| SEER 14 | $119 |
| SEER 15 | $238 |
| SEER 16 | $357 |
| SEER 17 | $476 |
| SEER 18 | $596 |
| SEER 19 | $715 |
| SEER 20 | $834 |
| SEER 21 | $908 |
| Average | $530 |

Early replacement: The incremental capital cost for this measure is the actual cost of removing the existing unit and installing the new one. If this is unknown, assume $3,413[[838]](#footnote-839).

Assumed deferred cost (after 6 years) of replacing existing equipment with new baseline unit is assumed to be $2,857[[839]](#footnote-840). This cost should be discounted to present value using the utilities discount rate.

**Loadshape**

Loadshape R08 - Residential Cooling

**Coincidence Factor**

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during system peak hour)

= 68%[[840]](#footnote-841)

CFPJM = PJM Summer Peak Coincidence Factor for Central A/C (average during PJM peak period)

= 46.6%[[841]](#footnote-842)

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

Time of sale:

ΔkWH = (FLHcool \* Btu/hr \* (1/SEERbase - 1/SEERee))/1000

Early replacement[[842]](#footnote-843):

ΔkWH for remaining life of existing unit (1st 6 years):

=((FLHcool \* Capacity \* (1/SEERexist - 1/SEERee))/1000);

ΔkWH for remaining measure life (next 12 years):

= ((FLHcool \* Capacity \* (1/SEERbase - 1/SEERee))/1000)

Where:

FLHcool = Full load cooling hours

= dependent on location and building type[[843]](#footnote-844):

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **FLHcool (single family)** | **FLHcool (multi family)** |
| 1 (Rockford) | 512 | 467 |
| 2 (Chicago) | 570 | 506 |
| 3 (Springfield) | 730 | 663 |
| 4 (Belleville) | 1035 | 940 |
| 5 (Marion) | 903 | 820 |
| Weighted Average[[844]](#footnote-845) | 629 | 564 |

Capacity = Size of new equipment in Btu/hr (note 1 ton = 12,000Btu/hr)

= Actual installed, or if actual size unknown 33,600Btu/hr for single-family buildings[[845]](#footnote-846)

SEERbase = Seasonal Energy Efficiency Ratio of baseline unit (kBtu/kWh)

= 13[[846]](#footnote-847)

SEERexist = Seasonal Energy Efficiency Ratio of existing unit (kBtu/kWh)

= Use actual SEER rating where it is possible to measure or reasonably estimate. If unknown assume 10.0[[847]](#footnote-848).

SEERee = Seasonal Energy Efficiency Ratio of ENERGY STAR unit (kBtu/kWh)

= Actual installed or 14.5 if unknown

Time of sale example: a 3 ton unit with SEER rating of 14.5, in unknown location:

ΔkWH = (629 \* 36,000 \* (1/13 – 1/14.5)) / 1000

= 180 kWh

Early replacement example: a 3 ton unit, with SEER rating of 14.5 replaces an existing unit in unknown location:

ΔkWH(for first 6 years) = (629 \* 36,000 \* (1/10 – 1/14.5)) / 1000

= 702 kWh

ΔkWH(for next 12 years) = (629 \* 36,000 \* (1/13 – 1/14.5)) / 1000

= 180 kWh

Therefore savings adjustment of 26% (180/702) after 6 years.

**Summer Coincident Peak Demand Savings**

Time of sale:

ΔkW = (Capacity \* (1/EERbase - 1/EERee))/1000 \* CF

Early replacement[[848]](#footnote-849):

ΔkW for remaining life of existing unit (1st 6 years):

= ((Capacity \* (1/EERexist - 1/EERee))/1000 \* CF);

ΔkW for remaining measure life (next 12 years):

= ((Capacity \* (1/EERbase - 1/EERee))/1000 \* CF)

Where:

EERbase = EER Efficiency of baseline unit

= 11.2 [[849]](#footnote-850)

EERexist = EER Efficiency of existing unit

= Actual EER of unit should be used, if EER is unknown, use 9.2[[850]](#footnote-851)

EERee = EER Efficiency of ENERGY STAR unit

= Actual installed or 12 if unknown

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during system peak hour)

= 68%[[851]](#footnote-852)

CFPJM    = PJM Summer Peak Coincidence Factor for Central A/C (average during peak period)

= 46.6%[[852]](#footnote-853)

Time of sale example: a 3 ton unit with EER rating of 12:

ΔkW SSP = (36,000 \* (1/11.2– 1/12)) / 1000 \* 0.68

= 0.146 kW

ΔkW PJM = (36,000 \* (1/11.2– 1/12)) / 1000 \* 0.466

= 0.100 kW

Early replacement example: a 3 ton unit with EER rating of 12 replaces an existing unit:

ΔkW SSP (for first 6 years) = (36,000 \* (1/9.2– 1/12)) / 1000 \* 0.68

= 0.621 kW

ΔkW SSP (for next 12 years) = (36,000 \* (1/11.2– 1/12)) / 1000 \* 0.68

= 0.146 kW

ΔkW PJM (for first 6 years) = (36,000 \* (1/9.2– 1/12)) / 1000 \* 0.466

= 0.425 kW

ΔkW PJM (for next 12 years)= (36,000 \* (1/11.2– 1/12)) / 1000 \* 0.466

= 0.100 kW

**Natural Gas Savings**

N/A

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: RS-HVC-CAC1-V04-150601**

### Duct Insulation and Sealing

**Description**

This measure describes evaluating the savings associated with performing duct sealing using mastic sealant or metal tape to the distribution system of homes with either central air conditioning or a ducted heating system.

Two methodologies for estimating the savings associate from sealing the ducts are provided. The first preferred method requires the use of a blower door and the second requires careful inspection of the duct work.

1. **Modified Blower Door Subtraction** – this technique is described in detail on p.44 of the Energy Conservatory Blower Door Manual; which can be found on the Energy Conservatory website (As of Oct 2014: http://www.energyconservatory.com/sites/default/files/documents/mod\_3-4\_dg700\_-\_new\_flow\_rings\_-\_cr\_-\_tpt\_-\_no\_fr\_switch\_manual\_ce\_0.pdf)
2. **Evaluation of Distribution Efficiency** – this methodology requires the evaluation of three duct characteristics below, and use of the Building Performance Institutes ‘Distribution Efficiency Look-Up Table’;

[http://www.bpi.org/files/pdf/DistributionEfficiencyTable-BlueSheet.pdf](http://www.cee1.org/com/com-lt/com-lt-main.php3)

* 1. Percentage of duct work found within the conditioned space
  2. Duct leakage evaluation
  3. Duct insulation evaluation

This measure was developed to be applicable to the following program types:  RF.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

The efficient condition is sealed duct work throughout the unconditioned space in the home.

**Definition of Baseline Equipment**

The existing baseline condition is leaky duct work within the unconditioned space in the home.

**Deemed Lifetime of Efficient Equipment**

The assumed lifetime of this measure is 20 years[[853]](#footnote-854).

**Deemed Measure Cost**

The actual duct sealing measure cost should be used.

**Loadshape**

|  |
| --- |
| Loadshape R08 - Residential Cooling |
| Loadshape R09 - Residential Electric Space Heat |
| Loadshape R10 - Residential Electric Heating and Cooling (Shell Measures) |

**Coincidence Factor**

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during utility peak hour)

= 68%[[854]](#footnote-855)

CFPJM   = PJM Summer Peak Coincidence Factor for Central A/C (average during PJM peak period)

= 46.6%[[855]](#footnote-856)

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

***Methodology 1: Modified Blower Door Subtraction***

1. Determine Duct Leakage rate before and after performing duct sealing:

Duct Leakage (CFM50DL) = (CFM50Whole House – CFM50Envelope Only) \* SCF

Where:

CFM50Whole House = Standard Blower Door test result finding Cubic Feet per Minute at 50 Pascal pressure differential

CFM50Envelope Only = Blower Door test result finding Cubic Feet per Minute at 50 Pascal pressure differential with all supply and return registers sealed.

SCF = Subtraction Correction Factor to account for underestimation of duct leakage due to connections between the duct system and the home. Determined by measuring pressure in duct system with registers sealed and using look up table provided by Energy Conservatory.

1. Calculate duct leakage reduction, convert to CFM25DL and factor in Supply and Return Loss Factors

Duct Leakage Reduction (∆CFM25DL) = (Pre CFM50DL – Post CFM50DL) \* 0.64 \* (SLF + RLF)

Where:

0.64 = Converts CFM50 to CFM25[[856]](#footnote-857)

SLF = Supply Loss Factor

= % leaks sealed located in Supply ducts \* 1 [[857]](#footnote-858)

Default = 0.5[[858]](#footnote-859)

RLF = Return Loss Factor

= % leaks sealed located in Return ducts \* 0.5[[859]](#footnote-860)

Default = 0.25[[860]](#footnote-861)

c) Calculate Electric Energy Savings:

ΔkWh = ΔkWhcooling + ΔkWhFan

ΔkWhcooling = ((*∆*CFM25DL)/ ((CapacityCool/12,000) \* 400)) \* FLHcool \* CapacityCool) / 1000 / ηCool

ΔkWhFan = (ΔTherms \* Fe \* 29.3)

Where:

∆CFM25DL = Duct leakage reduction in CFM25

= calculated above

CapacityCool = Capacity of Air Cooling system (Btu/hr)

=Actual

12,000 = Converts Btu/H capacity to tons

400 = Converts capacity in tons to CFM (400CFM / ton)[[861]](#footnote-862)

FLHcool = Full load cooling hours

= Dependent on location as below[[862]](#footnote-863):

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **FLHcool**  **Single Family** | **FLHcool**  **Multifamily** |
| 1 (Rockford) | 512 | 467 |
| 2 (Chicago) | 570 | 506 |
| 3 (Springfield) | 730 | 663 |
| 4 (Belleville) | 1,035 | 940 |
| 5 (Marion) | 903 | 820 |
| Weighted Average[[863]](#footnote-864) | 629 | 564 |

1000 = Converts Btu to kBtu

ηCool = Efficiency (SEER) of Air Conditioning equipment (kBtu/kWh)

= Actual. If unknown assume the following[[864]](#footnote-865):

|  |  |
| --- | --- |
| **Age of Equipment** | **SEER Estimate** |
| Before 2006 | 10 |
| After 2006 - 2014 | 13 |
| Central AC After 1/1/2015 | 13 |
| Heat Pump After 1/1/2015 | 14 |

ΔTherms = Therm savings as calculated in Natural Gas Savings

Fe = Furnace Fan energy consumption as a percentage of annual fuel consumption

= 3.14%[[865]](#footnote-866)

29.3 = kWh per therm

For example, duct sealing in a single family house in Springfield with a 36,000 Btu/H, SEER 11 central air conditioning, an 80% AFUE, 105,000 Btu/H natural gas furnace and the following blower door test results:

Before: CFM50Whole House = 4800 CFM50

CFM50Envelope Only = 4500 CFM50

House to duct pressure of 45 Pascals. = 1.29 SCF (Energy Conservatory look up table)

After: CFM50Whole House = 4600 CFM50

CFM50Envelope Only = 4500 CFM50

House to duct pressure of 43 Pascals = 1.39 SCF (Energy Conservatory look up table)

Duct Leakage:

CFM50DL before = (4800 – 4500) \* 1.29

= 387 CFM

CFM50DL after = (4600 – 4500) \* 1.39

= 139 CFM

Duct Leakage reduction at CFM25:

∆CFM25DL = (387 – 139) \* 0.64 \* (0.5 + 0.25)

= 119 CFM25

Energy Savings:

ΔkWhcooling = [((119 / ((36,000/12,000) \* 400)) \* 730 \* 36,000) / 1000 / 11] + (212 \* 0.0314 \* 29.3)

= 237 + 195

= 432 kWh

Heating savings for homes with electric heat (Heat Pump):

ΔkWhheating  = (((∆CFM25DL /((OutputCapacityHeat/12,000) \* 400)) \* FLHheat \* OutputCapacityHeat) / ηHeat / 3412

Where:

OutputCapacityHeat = Heating output capacity (Btu/hr) of electric heat

=Actual

FLHheat = Full load heating hours

= Dependent on location as below[[866]](#footnote-867):

| **Climate Zone**  **(City based upon)** | **FLH\_heat** |
| --- | --- |
| 1 (Rockford) | 1,969 |
| 2 (Chicago) | 1,840 |
| 3 (Springfield) | 1,754 |
| 4 (Belleville) | 1,266 |
| 5 (Marion) | 1,288 |
| Weighted Average[[867]](#footnote-868) | 1,821 |

ηHeat = Efficiency in COP of Heating equipment

= Actual. If not available use[[868]](#footnote-869):

|  |  |  |  |
| --- | --- | --- | --- |
| **System Type** | **Age of Equipment** | **HSPF Estimate** | **COP Estimate** |
| Heat Pump | Before 2006 | 6.8 | 2.00 |
| After 2006 - 2014 | 7.7 | 2.26 |
| 2015 on | 8.2 | 2.40 |
| Resistance | N/A | N/A | 1.00 |

3412 = Converts Btu to kWh

For example, duct sealing in a 36,000 Btu/H 2.5 COP heat pump heated single family house in Springfield with the blower door results described above:

ΔkWhheating = (((119 / ((36,000/12,000) \* 400)) \* 1,754 \* 36,000) / 2.5 / 3412

= 734 kWh

***Methodology 2: Evaluation of Distribution Efficiency***

Determine Distribution Efficiency by evaluating duct system before and after duct sealing using Building Performance Institute “Distribution Efficiency Look-Up Table”

ΔkWh = (((DEafter – DEbefore)/ DEafter)) \* FLHcool \* CapacityCool)/1000 / ηCool) + (ΔTherms \* Fe \* 29.3)

Where:

DEafter = Distribution Efficiency after duct sealing

DEbefore = Distribution Efficiency before duct sealing

FLHcool = Full load cooling hours

= Dependent on location as below[[869]](#footnote-870):

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **FLHcool**  **Single Family** | **FLHcool**  **Multifamily** |
| 1 (Rockford) | 512 | 467 |
| 2 (Chicago) | 570 | 506 |
| 3 (Springfield) | 730 | 663 |
| 4 (Belleville) | 1,035 | 940 |
| 5 (Marion) | 903 | 820 |
| Weighted Average[[870]](#footnote-871) | 629 | 564 |

CapacityCool = Capacity of Air Cooling system (Btu/hr)

=Actual

1000 = Converts Btu to kBtu

ηCool = Efficiency (SEER) of Air Conditioning equipment (kBtu/kWh)

= Actual. If unknown assume[[871]](#footnote-872):

|  |  |
| --- | --- |
| **Age of Equipment** | **SEER Estimate** |
| Before 2006 | 10 |
| After 2006 - 2014 | 13 |
| Central AC After 1/1/2015 | 13 |
| Heat Pump After 1/1/2015 | 14 |

For example, duct sealing in a single family house in Springfield, with 36,000 Btu/H SEER 11 central air conditioning, an 80% AFUE, 105,000 Btu/H natural gas furnace and the following duct evaluation results:

DEbefore = 0.85

DEafter = 0.92

Energy Savings:

ΔkWhcooling = (((0.92 – 0.85)/0.92) \* 730 \* 36,000) / 1000 / 11) + (212 \* 0.0314 \* 29.3)

= 182 + 195

= 377 kWh

Heating savings for homes with electric heat (Heat Pump):

ΔkWhheating = ((DEafter – DEbefore)/ DEafter)) \* FLHheat \* OutputCapacityHeat) / ηHeat / 3412

Where:

OutputCapacityHeat = Heating output capacity (Btu/hr) of the electric heat

=Actual

FLHheat = Full load heating hours

= Dependent on location as below[[872]](#footnote-873):

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **FLH\_heat** |
| 1 (Rockford) | 1,969 |
| 2 (Chicago) | 1,840 |
| 3 (Springfield) | 1,754 |
| 4 (Belleville) | 1,266 |
| 5 (Marion) | 1,288 |
| Weighted Average[[873]](#footnote-874) | 1,821 |

COP = Coefficient of Performance of electric heating system[[874]](#footnote-875)

= Actual. If not available use[[875]](#footnote-876):

|  |  |  |  |
| --- | --- | --- | --- |
| **System Type** | **Age of Equipment** | **HSPF Estimate** | **COP Estimate** |
| Heat Pump | Before 2006 | 6.8 | 2.00 |
| After 2006 - 2014 | 7.7 | 2.26 |
| 2015 on | 8.2 | 2.40 |
| Resistance | N/A | N/A | 1.00 |

For example, duct sealing in a 36,000 Btu/H, 2.5 COP heat pump heated single family house in Springfield with the following duct evaluation results:

DEafter = 0.92

DEbefore = 0.85

Energy Savings:

ΔkWhheating = ((0.92 – 0.85)/0.92) \* 1,967 \* 36,000) / 2.5) / 3412

= 632 kWh

**Summer Coincident Peak Demand Savings**

ΔkW = ΔkWhcooling/ FLHcool \* CF

Where:

FLHcool = Full load cooling hours:

= Dependent on location as below[[876]](#footnote-877):

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **FLHcool**  **Single Family** | **FLHcool**  **Multifamily** |
| 1 (Rockford) | 512 | 467 |
| 2 (Chicago) | 570 | 506 |
| 3 (Springfield) | 730 | 663 |
| 4 (Belleville) | 1,035 | 940 |
| 5 (Marion) | 903 | 820 |
| Weighted Average[[877]](#footnote-878) | 629 | 564 |

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during system peak hour)

= 68%[[878]](#footnote-879)

CFPJM = PJM Summer Peak Coincidence Factor for Central A/C (average during peak period)

= 46.6%[[879]](#footnote-880)

**Natural Gas Savings**

For homes with Natural Gas Heating:

***Methodology 1: Modified Blower Door Subtraction***

ΔTherm = (((∆CFM25DL / (InputCapacityHeat \* 0.0123)) \* FLHheat \* InputCapacityHeat \* (ηEquipment / ηSystem)) / 100,000

Where:

∆CFM25DL = Duct leakage reduction in CFM25

InputCapacityHeat = Heating input capacity (Btu/hr)

=Actual

0.0123 = Conversion of Capacity to CFM (0.0123CFM / Btu/hr)[[880]](#footnote-881)

FLHheat = Full load heating hours

=Dependent on location as below[[881]](#footnote-882):

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **FLH\_heat** |
| 1 (Rockford) | 1,969 |
| 2 (Chicago) | 1,840 |
| 3 (Springfield) | 1,754 |
| 4 (Belleville) | 1,266 |
| 5 (Marion) | 1,288 |
| Weighted Average[[882]](#footnote-883) | 1,821 |

100,000 = Converts Btu to therms

ηEquipment = Heating Equipment Efficiency = Actual[[883]](#footnote-884). If not available use 83%[[884]](#footnote-885)

ηSystem = Pre duct sealing Heating System Efficiency (Equipment Efficiency \* Pre Distribution Efficiency)[[885]](#footnote-886)

= Actual. If not available use 70%[[886]](#footnote-887)

For example, duct sealing in a house in Springfield with an 80% AFUE, 105,000 Btu/H (input capacity) natural gas furnace and the following blower door test results:

Before: CFM50Whole House = 4800 CFM50

CFM50Envelope Only = 4500CFM50

House to duct pressure of 45 Pascals = 1.29 SCF (Energy Conservatory look up table)

After: CFM50Whole House = 4600 CFM50

CFM50Envelope Only = 4500CFM50

House to duct pressure of 43 Pascals = 1.39 SCF (Energy Conservatory look up table)

Duct Leakage:

CFM50DL before = (4800 – 4500) \* 1.29

= 387 CFM

CFM50DL after = (4600 – 4500) \* 1.39

= 119 CFM

Duct Leakage reduction at CFM25:

∆CFM25DL = (387 – 139) \* 0.64 \* (0.5 + 0.25)

= 119 CFM25

Energy Savings:

Pre Distribution Efficiency = 1 – (387/4800) = 92%

ηSystem = 80% \* 92% = 74%

ΔTherm = ((119/ (105,000 \* 0.0123)) \* 1,754 \* 105,000 \* (0.8/0.74)) / 100,000

= 183 therms

***Methodology 2: Evaluation of Distribution Efficiency***

ΔTherm = ((DEafter – DEbefore)/ DEafter)) \* FLHheat \* InputCapacityHeat (ηEquipment / ηSystem)) / 100,000

Where:

DEafter = Distribution Efficiency after duct sealing

DEbefore = Distribution Efficiency before duct sealing

Other variables as defined above

For example, duct sealing in a house in Springfield an 80% AFUE, 105,000 Btu/H (input capacity) natural gas furnace and the following duct evaluation results:

DEafter = 0.92

DEbefore = 0.85

Energy Savings:

ηSystem = 80% \* 85% = 68%

ΔTherm = ((0.92 – 0.85)/0.92) \* 1,754 \* 105,000 \* (0.8/0.68)) / 100,000

= 164 therm

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: RS-HVC-DINS-V05-150601**

### Furnace Blower Motor

###### Description

A new furnace with a brushless permanent magnet (BPM) blower motor is installed instead of a new furnace with a lower efficiency motor. This measure characterizes only the electric savings associated with the fan and could be coupled with gas savings associated with a more efficient furnace. Savings decrease sharply with static pressure so duct improvements, and clean, low pressure drop filters can maximize savings. Savings improve when the blower is used for cooling as well and when it is used for continuous ventilation, but only if the non-BPM motor would have been used for continuous ventilation too. If the resident runs the BPM blower continuously because it is a more efficient motor and would not run a non-BPM motor that way, savings are near zero and possibly negative. This characterization uses a 2009 Focus on Energy study of BPM blower motor savings in Wisconsin, which accounted for the effects of this behavioral impact.

This measure was developed to be applicable to the following program types:  TOS, NC.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

A furnace with a brushless permanent magnet (BPM) blower motor, also known by the trademark ECM, BLDC, and other names.

###### Definition of Baseline Equipment

A furnace with a non-BPM blower motor.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 20 years[[887]](#footnote-888).

###### Deemed Measure Cost

The capital cost for this measure is assumed to be $97[[888]](#footnote-889).

###### Loadshape

|  |
| --- |
| Loadshape R08 - Residential Cooling |
| Loadshape R09 - Residential Electric Space Heat |
| Loadshape R10 - Residential Electric Heating and Cooling |

###### Coincidence Factor

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during utility peak hour)

= 68%[[889]](#footnote-890)

CFPJM   = PJM Summer Peak Coincidence Factor for Central A/C (average during PJM peak period)

= 46.6%[[890]](#footnote-891)

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = Heating Savings + Cooling Savings + Shoulder Season Savings

Where:

Heating Savings = Blower motor savings during heating season

= 418 kWh[[891]](#footnote-892)

Cooling Savings = Blower motor savings during cooling season

If Central AC = 263 kWh

If No Central AC = 175 kWh

If unknown (weighted average)

= 241 kWh[[892]](#footnote-893)

Shoulder Season Savings = Blower motor savings during shoulder seasons

= 51 kWh

For example, a blower motor in a home where Central AC presence is unknown:

ΔkWh = Heating Savings + Cooling Savings + Shoulder Season Savings

= 418 +251 + 51

= 721 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = Cooling Savings / FLH\_cooling \* CF

Where:

FLH\_cooling = Full load hours of air conditioning

= Dependent on location[[893]](#footnote-894):

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **FLH\_cooling** |
| 1 (Rockford) | 512 |
| 2 (Chicago) | 570 |
| 3 (Springfield) | 730 |
| 4 (Belleville) | 1,035 |
| 5 (Marion) | 903 |
| Weighted Average[[894]](#footnote-895) | 629 |

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during system peak hour)

= 68%[[895]](#footnote-896)

CFPJM = PJM Summer Peak Coincidence Factor for Central A/C (average during peak period)

= 46.6%[[896]](#footnote-897)

For example, a blower motor in a home of unknown location where Central AC prevalence is unknown:

ΔkWSSP = 251 / 629 \* 0.68

= 0.271 kW

ΔkWSSP = 251 / 629 \* 0.466

= 0.186 kW

###### Natural Gas Savings

Δtherms[[897]](#footnote-898) = - Heating Savings \* 0.03412 therms/kWh

= - (418 \* 0.03412)

= - 14.3 therms[[898]](#footnote-899)

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-HVC-FBMT-V02-140601

### Gas High Efficiency Boiler

###### Description

High efficiency boilers achieve most gas savings through the utilization of a sealed combustion chamber and multiple heat exchangers that remove a significant portion of the waste heat from flue gasses. Because multiple heat exchangers are used to remove waste heat from the escaping flue gasses, some of the flue gasses condense and must be drained.

This measure characterizes:

1. Time of Sale:
   1. The installation of a new high efficiency, gas-fired hot water boiler in a residential location. This could relate to the replacement of an existing unit at the end of its useful life, or the installation of a new system in a new home.
2. Early Replacement:
   1. The early removal of an existing functional AFUE 75% or less boiler from service, prior to its natural end of life, and replacement with a new high efficiency unit. Savings are calculated between existing unit and efficient unit consumption during the remaining life of the existing unit, and between new baseline unit and efficient unit consumption for the remainder of the measure life.
   2. The assumption of the existing unit efficiency in the Early Replacement section of this TRM is based upon the average efficiency of units that were classified in Ameren’s PY3-PY4 as functioning and AFUE <=75%. Therefore it is only appropriate to use these Early Replacement assumptions where those conditions are met. The TAC defined “functioning” as the unit is fully operational – providing sufficient space conditioning (i.e. heat exchanger, compressors, pumps work effectively) and/or the cost of repair is under 20% of the new baseline replacement cost. Therefore in order to apply early replacement assumptions the programs should apply the following eligibility criteria: AFUE <=75% and cost of any repairs <$709.
   3. A weighted average early replacement rate is provided for use when the actual baseline early replacement rates are unknown[[899]](#footnote-900).

Deemed Early Replacement Rates For Boilers

|  |  |
| --- | --- |
|  | **Deemed Early Replacement Rate** |
| Early Replacement Rate for Boiler participants | 7% |

This measure was developed to be applicable to the following program types:  TOS, NC, EREP.  If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed Boiler must be ENERGY STAR qualified (AFUE rated at or greater than 85% and input capacity less than 300,000 Btu/hr).

###### Definition of Baseline Equipment

Time of sale: The baseline equipment for this measure is a new, gas-fired, standard-efficiency water boiler. The current Federal Standard minimum AFUE rating is 80%. For boilers manufactured after September 2012 the Federal Standards is raised to 82% AFUE. Baseline assumptions are therefore provided below:

|  |  |
| --- | --- |
| **Program Year** | **AFUE** |
| June 2012 – May 2013[[900]](#footnote-901) | 80% |
| June 2013 on | 82% |

Early replacement: The baseline for this measure is the efficiency of the existing equipment for the assumed remaining useful life of the unit and the new baseline as defined above for the remainder of the measure life.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 25 years[[901]](#footnote-902).

Early replacement: Remaining life of existing equipment is assumed to be 8 years[[902]](#footnote-903).

###### Deemed Measure Cost

Time of sale: The incremental install cost for this measure is dependent on tier[[903]](#footnote-904):

|  |  |  |  |
| --- | --- | --- | --- |
|  |  | **Incremental Install Cost** | **Incremental Install Cost** |
| **Measure Type** | **Installation Cost** | **(June 2012 – May 2013)** | **(June 2013 on)** |
| AFUE 80% | $3334 | n/a | |
| AFUE 82% | $3543 |
| AFUE 85% (Energy Star Minimum) | $4268 | $934 | $725 |
| AFUE 90% | $4815 | $1,481 | $1,272 |
| AFUE 95% | $5328 | $1,994 | $1,785 |

Early Replacement: The full installation cost is provided in the table above. The assumed deferred cost (after 8 years) of replacing existing equipment with a new baseline unit is assumed to be $3543. This cost should be discounted to present value using the utilities discount rate.

###### Loadshape

N/A

###### Coincidence Factor

N/A

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Savings

Time of Sale:

ΔTherms = Gas\_Boiler\_Load \* (1/AFUE(base) - 1/AFUE(eff))

Early replacement[[904]](#footnote-905):

ΔTherms for remaining life of existing unit (1st 8 years):

= Gas\_Boiler\_Load \* (1/AFUE(exist) - 1/AFUE(eff)))

ΔTherms for remaining measure life (next 17 years):

= Gas\_Boiler\_Load \* (1/AFUE(base) - 1/AFUE(eff)))

Where:

Gas\_Boiler\_Load[[905]](#footnote-906)

= Estimate of annual household Load for gas boiler heated single-family homes. If location is unknown, assume the average below[[906]](#footnote-907).

= or Actual if informed by site-specific load calculations, ACCA Manual J or equivalent[[907]](#footnote-908).

| **Climate Zone**  **(City based upon)** | **Gas\_Boiler Load**  **(therms)** |
| --- | --- |
| 1 (Rockford) | 1275 |
| 2 (Chicago) | 1218 |
| 3 (Springfield) | 1043 |
| 4 (Belleville) | 805 |
| 5 (Marion) | 819 |
| Average | 1158 |

AFUE(exist) = Existing Boiler Annual Fuel Utilization Efficiency Rating

= Use actual AFUE rating where it is possible to measure or reasonably estimate.

If unknown, assume 61.6 AFUE% [[908]](#footnote-909).

AFUE(base) = Baseline Boiler Annual Fuel Utilization Efficiency Rating

= Dependent on year as listed below:

|  |  |
| --- | --- |
| **Program Year** | **AFUE(base)** |
| June 2012 – May 2013 | 80% |
| June 2013 on | 82% |

AFUE(eff) = Efficent Boiler Annual Fuel Utilization Efficiency Rating

= Actual. If unknown, use defaults dependent[[909]](#footnote-910) on tier as listed below:

|  |  |
| --- | --- |
| **Measure Type** | **AFUE(eff)** |
| ENERGY STAR® | 87.5% |
| AFUE 90% | 92.5% |
| AFUE 95% | 95% |

Time of Sale:

For example, a default sized ENERGY STAR boiler purchased and installed near Springfield in the year 2012

ΔTherms = (1043) \* (1/0.8) - 1/0.875)

= 112 Therms

Early Replacement:

For example, an existing function boiler with unknown efficiency is replaced with an ENERGY STAR boiler purchased and installed in Springfield in 2013.

ΔTherms for remaining life of existing unit (1st 8 years):

= 1043 \* (1/0.616 – 1/0.875)

= 501 Therms

ΔTherms for remaining measure life (next 17 years):

= (1043) \* (1/0.82 - 1/0.875)

= 80.0 Therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-HVC-GHEB-V03-150601

### Gas High Efficiency Furnace

**Description**

High efficiency furnace features may include improved heat exchangers and modulating multi-stage burners.

This measure characterizes:

1. Time of sale:
   1. The installation of a new high efficiency, gas-fired condensing furnace in a residential location. This could relate to the replacement of an existing unit at the end of its useful life, or the installation of a new system in a new home.
2. Early Replacement:
   1. The early removal of an existing functioning AFUE 75% or less furnace from service, prior to its natural end of life, and replacement with a new high efficiency unit. Savings are calculated between existing unit and efficient unit consumption during the remaining life of the existing unit, and between new baseline unit and efficient unit consumption for the remainder of the measure life. At time of writing, the DOE had rescinded the next Federal Standard change for furnaces, however it is likely that a new standard will be in effect after the assumed remaining useful life of the existing unit. For the purposes of this measure- the new baseline is assumed to be 90%.
   2. The assumption of the existing unit efficiency in the Early Replacement section of this TRM is based upon the average efficiency of units that were classified in Ameren’s PY3-PY4 as functioning and AFUE <=75%. Therefore it is only appropriate to use these Early Replacement assumptions where those conditions are met. The TAC defined “functioning” as the unit is fully operational – providing sufficient space conditioning (i.e. heat exchanger, compressors, pumps work effectively) and/or the cost of repair is under 20% of the new baseline replacement cost. Therefore in order to apply early replacement assumptions the programs should apply the following eligibility criteria: AFUE <=75% and cost of any repairs <$528.
   3. A weighted average early replacement rate is provided for use when the actual baseline early replacement rate is unknown[[910]](#footnote-911).

Deemed Early Replacement Rates For Furnaces

|  |  |
| --- | --- |
| **Replacement Scenario for the Furnace** | **Deemed Early Replacement Rate** |
| Early Replacement Rate for Furnace-only participants | 7% |
| Early Replacement Rate for a furnace when the furnace is the Primary unit in a Combined System Replacement (CSR) project | 14% |
| Early Replacement Rate for a furnace when the furnace is the Secondary unit in a CSR project | 46% |

This measure was developed to be applicable to the following program types:  TOS, NC, EREP.  If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

To qualify for this measure the installed equipment must be a residential sized (input energy less than 225,000 Btu/hr) natural gas fired furnace with an Annual Fuel Utilization Efficiency (AFUE) rating exceeding the program requirements.

**Definition of Baseline Equipment**

Time of Sale: Although the current Federal Standard for gas furnaces is an AFUE rating of 78%, based upon review of available product in the AHRI database, the baseline efficiency for this characterization is assumed to be 80%. The baseline will be adjusted when the Federal Standard is updated.

Early replacement: The baseline for this measure is the efficiency of the existing equipment for the assumed remaining useful life of the unit and a new baseline unit for the remainder of the measure life. As discussed above we estimate that the new baseline unit that could be purchased in the year the existing unit would have needed replacing is 90%.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 20 years[[911]](#footnote-912).

For early replacement: Remaining life of existing equipment is assumed to be 6 years[[912]](#footnote-913).

**Deemed Measure Cost**

Time of sale: The incremental installed cost (retail equipment cost plus installation cost) for this measure depends on efficiency as listed below[[913]](#footnote-914):

|  |  |  |
| --- | --- | --- |
| **AFUE** | **Installed Cost** | **Incremental Installed Cost** |
| 80% | $2011 | n/a |
| 90% | $2641 | $630 |
| 91% | $2727 | $716 |
| 92% | $2813 | $802 |
| 93% | $3025 | $1014 |
| 94% | $3237 | $1226 |
| 95% | $3449 | $1438 |
| 96% | $3661 | $1650 |

Early Replacement: The full installed cost is provided in the table above. The assumed deferred cost (after 6 years) of replacing existing equipment with a new baseline unit is assumed to be $2641. This cost should be discounted to present value using the utility’s discount rate.

**Loadshape**

N/A

**Coincidence Factor**

N/A

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

Electrical energy savings from the more fan-efficient (typically using brushless permanent magnet (BPM) blower motor) should also be claimed, please refer to “Furnace Blower Motor” characterization for details.

**Summer Coincident Peak Demand Savings**

If the blower motor is also used for cooling, coincident peak demand savings should also be claimed, please refer to “Furnace Blower Motor” characterization for savings details.

**Natural Gas Savings**

Time of Sale:

ΔTherms = Gas\_Furnace\_Heating\_Load \* (1/AFUE(base) - 1/AFUE(eff))

Early replacement[[914]](#footnote-915):

ΔTherms for remaining life of existing unit (1st 6 years):

= Gas\_Furnace\_Heating\_Load \* (1/AFUE(exist) - 1/AFUE(eff)))

ΔTherms for remaining measure life (next 14 years):

= Gas\_Furnace\_Heating\_Load \* (1/AFUE(base) - 1/AFUE(eff)))

Where:

Gas\_Furnace\_Heating\_Load

= Estimate of annual household heating load[[915]](#footnote-916) for gas furnace heated single-family homes. If location is unknown, assume the average below[[916]](#footnote-917).

= Actual if informed by site-specific load calculations, ACCA Manual J or equivalent[[917]](#footnote-918).

| **Climate Zone**  **(City based upon)** | **Gas\_Furnace\_Heating\_Load (therms)** |
| --- | --- |
| 1 (Rockford) | 873 |
| 2 (Chicago) | 834 |
| 3 (Springfield) | 714 |
| 4 (Belleville) | 551 |
| 5 (Marion) | 561 |
| Average | 793 |

HF = Household factor, to adjust heating consumption for non-single-family households.

|  |  |
| --- | --- |
| **Household Type** | **HF** |
| Single-Family | 100% |
| Multi-Family | 65%[[918]](#footnote-919) |
| Actual | Custom[[919]](#footnote-920) |

AFUE(exist) = Existing Furnace Annual Fuel Utilization Efficiency Rating

= Use actual AFUE rating where it is possible to measure or reasonably estimate.

If unknown, assume 64.4 AFUE% **[[920]](#footnote-921)**.

AFUE(base) = Baseline Furnace Annual Fuel Utilization Efficiency Rating

= Dependent on program type as listed below[[921]](#footnote-922):

|  |  |
| --- | --- |
| **Program Year** | **AFUE(base)** |
| Time of Sale | 80% |
| Early Replacement | 90% |

AFUE(eff) = Efficent Furnace Annual Fuel Utilization Efficiency Rating

= Actual. If unknown, assume 95%[[922]](#footnote-923)

Time of Sale:

For example, a 95% AFUE furnace near Rockford and purchased in the year 2014

ΔTherms = 873 \* (1/0.8 - 1/0.95)

=172 therms

Early Replacement:

For example, an existing functioning furnace with unknown efficiency is replaced with an 95% furnace purchased and installed in Rockford in 2014.

ΔTherms for remaining life of existing unit (1st 6 years):

= 873 \* (1/0.644 – 1/0.95)

= 437 therms

ΔTherms for remaining measure life (next 14 years):

= 873 \* (1/0.9 - 1/0.95)

=51.1 therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: RS-HVC-GHEF-V04-150601**

### Ground Source Heat Pump

###### Description

This measure characterizes the installation of a Ground Source Heat Pump under the following scenarios:

1. New Construction:
   1. The installation of a new residential sized Ground Source Heat Pump system meeting ENERGY STAR efficiency standards presented below in a new home.
   2. Note the baseline in this case should be determined via EM&V and the algorithms are provided to allow savings to be calculated from any baseline condition.
2. Time of Sale:
   1. The planned installation of a new residential sized Ground Source Heat Pump system meeting ENERGY STAR efficiency standards presented below to replace an existing system(s) that does not meet the criteria for early replacement described in section c below.
   2. Note the baseline in this case is an equivalent replacement system to that which exists currently in the home. The calculation of savings is dependent on whether an incentive for the installation has been provided by both a gas and electric utility, or just a gas utility.
   3. Additional DHW savings are calculated based upon the fuel and efficiency of the existing unit.
3. Early Replacement/Retrofit:
   1. The early removal of functioning either electric or gas space heating and/or cooling systems from service, prior to the natural end of life, and replacement with a new high efficiency Ground Source Heat Pump system.
   2. Note the baseline in this case is the existing equipment being replaced. The calculation of savings is dependent on whether an incentive for the installation has been provided by both a gas and electric utility, or just a gas utility.
   3. Additional DHW savings are calculated based upon the fuel and efficiency of the existing unit.
   4. The definitions for when an installation can be claimed as an early replacement are provided below. Note if one system (heating or cooling) has failed or does not meet the criteria below but the other system does, then the appropriate new baseline replacement should be used for the unit not meeting early replacement criteria and the existing system efficiency for the unit that does should be used in the algorithm:

|  |  |
| --- | --- |
| **Existing System** | **Early Replacement Criteria** |
| Air Source Heat Pump | SEER <=10 and cost of any repairs <$249 per ton |
| Central Air Conditioner | SEER <=10 and cost of any repairs <$190 per ton |
| Boiler | AFUE <= 75% and cost of any repairs <$709 |
| Furnace | AFUE <= 75% and cost of any repairs <$528 |
| Ground Source Heat Pump | SEER <=10 and cost of any repairs <$249 per ton |

The ENERGY STAR efficiency standards are presented below.

|  |  |  |
| --- | --- | --- |
| ENERGY STAR Requirements (Effective January 1, 2012) | | |
| **Product Type** | **Cooling EER** | **Heating COP** |
| **Water-to-air** | | |
| Closed Loop | 17.1 | 3.6 |
| Open Loop | 21.1 | 4.1 |
| **Water-to-Water** | | |
| Closed Loop | 16.1 | 3.1 |
| Open Loop | 20.1 | 3.5 |
| DGX | 16 | 3.6 |

This measure was developed to be applicable to the following program types:  TOS, NC, EREP.  If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

In order for this characterization to apply, the efficient equipment must be a Ground Source Heat Pump unit meeting the minimum ENERGY STAR efficiency level standards effective at the time of installation as detailed above.

**Definition of Baseline Equipment**

For these products, baseline equipment includes Air Conditioning, Space Heating and Water Heating.

New Construction:

To calculate savings with an electric baseline, the baseline equipment is assumed to be an Air Source Heat Pump meeting the Federal Standard efficiency level; 14 SEER, 8.2 HSPF and 11.8[[923]](#footnote-924) EER and a Federal Standard electric hot water heater.

To calculate savings with a furnace/central AC baseline, the baseline equipment is assumed to be an 80% AFUE Furnace and central AC meeting the Federal Standard efficiency level; 13 SEER, 11 EER. If a gas water heater, the Federal Standard baseline is calculated as follows[[924]](#footnote-925); for <=55 gallon tanks = 0.675 – (0.0015 \* storage size in gallons) and for tanks >55 gallon = 0.8012 – (0.00078 \* storage size in gallons). For a 40-gallon storage water heater this would be 0.615 EF.

Time of Sale: The baseline for this measure is a new replacement unit of the same system type as the existing unit, meeting the baselines provided below.

|  |  |
| --- | --- |
| **Unit Type** | **Efficiency Standard** |
| ASHP | 14 SEER, 11.8 EER, 8.2 HSPF |
| Gas Furnace | 80% AFUE |
| Gas Boiler | 82% AFUE |
| Central AC | 13 SEER, 11 EER |

Early replacement / Retrofit: The baseline for this measure is the efficiency of the *existing* heating, cooling and hot water equipment for the assumed remaining useful life of the existing unit and a new baseline heating and cooling system for the remainder of the measure life (as provided in table above except for Gas Furnace where new baseline assumption is 90% due to pending standard change).

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 25 years[[925]](#footnote-926).

For early replacement, the remaining life of existing equipment is assumed to be 8 years[[926]](#footnote-927).

###### Deemed Measure Cost

New Construction and Time of Sale: The actual installed cost of the Ground Source Heat Pump should be used (default of $3957 per ton[[927]](#footnote-928)), minus the assumed installation cost of the baseline equipment ($1936 per ton for ASHP[[928]](#footnote-929) or $2011 for a new baseline 80% AFUE furnace or $3543 for a new 82% AFUE boiler[[929]](#footnote-930) and $2,857[[930]](#footnote-931) for new baseline Central AC replacement).

Early Replacement: The full installation cost of the Ground Source Heat Pump should be used (default provided above). The assumed deferred cost (after 8 years) of replacing existing equipment with a new baseline unit is assumed to be $1936 per ton for a new baseline Air Source Heat Pump, or $2641[[931]](#footnote-932) for a new baseline 90% AFUE furnace or $3543 for a new 82% AFUE boiler and $2,857 for new baseline Central AC replacement. This future cost should be discounted to present value using the utilities discount rate.

###### Loadshape

Loadshape R08 - Residential Cooling (if replacing gas heat and central AC)

Loadshape R09 - Residential Electric Space Heat (if replacing electric heat with no cooling)

Loadshape R10 - Residential Electric Heating and Cooling (if replacing ASHP)

###### Coincidence Factor

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.

CFSSP = Summer System Peak Coincidence Factor for Heat Pumps (during utility peak hour)

= 72%%[[932]](#footnote-933)

CFPJM   = PJM Summer Peak Coincidence Factor for Heat Pumps (average during PJM peak period)

= 46.6%[[933]](#footnote-934)

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

New Construction and Time of Sale (non-fuel switch only):

ΔkWh = [Cooling savings] + [Heating savings] + [DHW savings]

= [(FLHcool \* Capacity\_cooling \* (1/SEERbase– (1/EERPL)/1000] + [Elecheat \* FLHheat \* Capacity\_heating \* (1/HSPFbase – (1/COPPL \* 3.412)))/1000] + [ElecDHW \* %DHWDisplaced \* (((1/EFELEC) \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 3412)]

New Construction and Time of Sale (fuel switch only):

If measure is supported by gas utility only, ΔkWH = 0

If measure is supported by gas and electric utility, electric utility claim savings calculated below:

ΔkWh = [Cooling savings] + [Heating savings from base ASHP to GSHP] + [DHW savings]

= [(FLHcool \* Capacity\_cooling \* (1/SEERbase– (1/EERPL)/1000] + [FLHheat \* Capacity\_heating \* (1/HSPFASHP – (1/COPPL \* 3.412)))/1000] + [ElecDHW \* %DHWDisplaced \* (((1/EFELEC) \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 3412)]

Early replacement (non-fuel switch only)[[934]](#footnote-935):

ΔkWH for remaining life of existing unit (1st 8 years):

= [Cooling savings] + [Heating savings] + [DHW savings]

= [(FLHcool \* Capacity\_cooling \* (1/SEERexist – (1/EERPL)/1000] + [ElecHeat \* (FLHheat \* Capacity\_heating \* (1/HSPFexist) – (1/COPPL \* 3.412)))/1000] + [ElecDHW \* %DHWDisplaced \* (((1/ EFELEC) \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 3412)]

ΔkWH for remaining measure life (next 17 years):

= [(FLHcool \* Capacity\_cooling \* (1/SEERbase – (1/EERPL)/1000] + [ElecHeat \* (FLHheat \* Capacity\_heating \* (1/HSPFbase) – (1/COPPL \* 3.412)))/1000] + [ElecDHW \* %DHWDisplaced \* (((1/ EFELEC) \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 3412)]

Early replacement - fuel switch only (see illustrative examples after Natural Gas section):

If measure is supported by gas utility only, ΔkWH = 0

If measure is supported by gas and electric utility, electric utility claim savings calculated below:

ΔkWh for remaining life of existing unit (1st 8 years):

= [Cooling savings] + [Heating savings from base ASHP to GSHP] + [DHW savings]

= [(FLHcool \* Capacity\_cooling \* (1/SEERexist – (1/EERPL)/1000] + [(FLHheat \* Capacity\_heating \* (1/HSPFASHP – (1/COPPL \* 3.412)))/1000] + [ElecDHW \* %DHWDisplaced \* (((1/ EFELEC) \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 3412)]

ΔkWh for remaining measure life (next 17 years):

= [Cooling savings] + [Heating savings from base ASHP to GSHP] + [DHW savings]

= [(FLHcool \* Capacity\_cooling \* (1/SEERbase – (1/EERPL)/1000] + [(FLHheat \* Capacity\_heating \* (1/HSPFASHP – (1/COPPL \* 3.412)))/1000] + [ElecDHW \* %DHWDisplaced \* (((1/ EFELEC) \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 3412)]

Where:

FLHcool = Full load cooling hours

Dependent on location as below[[935]](#footnote-936):

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **FLHcool**  **Single Family** | **FLHcool**  **Multifamily** |
| 1 (Rockford) | 512 | 467 |
| 2 (Chicago) | 570 | 506 |
| 3 (Springfield) | 730 | 663 |
| 4 (Belleville) | 1,035 | 940 |
| 5 (Marion) | 903 | 820 |
| Weighted Average[[936]](#footnote-937) | 629 | 564 |

Capacity\_cooling = Cooling Capacity of Ground Source Heat Pump (Btu/hr)

= Actual (1 ton = 12,000Btu/hr)

SEERbase = SEER Efficiency of new replacement baseline unit

|  |  |
| --- | --- |
| **Existing Cooling System** | **SEERbase** |
| Air Source Heat Pump | 14[[937]](#footnote-938) |
| Central AC | 13[[938]](#footnote-939) |
| No central cooling | 13[[939]](#footnote-940) |

SEERexist = SEER Efficiency of existing cooling unit

= Use actual SEER rating where it is possible to measure or reasonably estimate, if unknown assume default provided below:

|  |  |
| --- | --- |
| **Existing Cooling System** | **SEER\_exist** |
| Air Source Heat Pump | 9.12**[[940]](#footnote-941)** |
| Central AC | 8.60[[941]](#footnote-942) |
| No central cooling | 13 [[942]](#footnote-943) |

SEERASHP = SEER Efficiency of new baseline Air Source Heat Pump unit (for fuel switch)

= 14 [[943]](#footnote-944)

EERPL = Part Load EER Efficiency of efficient GSHP unit[[944]](#footnote-945)

= Actual installed

ElecHeat = 1 if existing building is electrically heated

= 0 if existing building is not electrically heated

FLHheat = Full load heating hours

Dependent on location as below[[945]](#footnote-946):

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **FLH\_heat** |
| 1 (Rockford) | 1,969 |
| 2 (Chicago) | 1,840 |
| 3 (Springfield) | 1,754 |
| 4 (Belleville) | 1,266 |
| 5 (Marion) | 1,288 |
| Weighted Average[[946]](#footnote-947) | 1,821 |

Capacity\_heating = Heating Capacity of Ground Source Heat Pump (Btu/hr)

= Actual (1 ton = 12,000Btu/hr)

HSPFbase =Heating System Performance Factor of new replacement baseline heating system (kBtu/kWh)

|  |  |
| --- | --- |
| **Existing Heating System** | **HSPF\_base** |
| Air Source Heat Pump | 8.2 |
| Electric Resistance | 3.41[[947]](#footnote-948) |

HSPF\_exist =Heating System Performance Factor of existing heating system (kBtu/kWh)

= Use actual HSPF rating where it is possible to measure or reasonably estimate. If unknown assume default:

|  |  |
| --- | --- |
| **Existing Heating System** | **HSPF\_exist** |
| Air Source Heat Pump | 5.44 |
| Electric Resistance | 3.41 |

HSPFASHP =Heating Season Performance Factor for new ASHP baseline unit (for fuel switch)

=8.2 [[948]](#footnote-949)

COPPL = Part Load Coefficient of Performance of efficient unit[[949]](#footnote-950)

= Actual Installed

3.412 = Constant to convert the COP of the unit to the Heating Season Performance Factor (HSPF).

ElecDHW = 1 if existing DHW is electrically heated

= 0 if existing DHW is not electrically heated

%DHWDisplaced = Percentage of total DHW load that the GSHP will provide

= Actual if known

= If unknown and if desuperheater installed assume 44%[[950]](#footnote-951)

= 0% if no desuperheater installed

EFELEC = Energy Factor (efficiency) of electric water heater

= Actual. If unknown or for new construction assume federal standard[[951]](#footnote-952):

For <=55 gallons: 0.96 – (0.0003 \* rated volume in gallons)

For >55 gallons: 2.057 – (0.00113 \* rated volume in gallons)

GPD = Gallons Per Day of hot water use per person

= 45.5 gallons hot water per day per household/2.59 people per household[[952]](#footnote-953)

= 17.6

Household = Average number of people per household

|  |  |
| --- | --- |
| **Household Unit Type** | **Household** |
| Single-Family - Deemed | 2.56[[953]](#footnote-954) |
| Custom | Actual Occupancy or Number of Bedrooms[[954]](#footnote-955) |

365.25 = Days per year

γWater = Specific weight of water

= 8.33 pounds per gallon

Tout = Tank temperature

= 125°F

Tin = Incoming water temperature from well or municiple system

= 54°F[[955]](#footnote-956)

1.0 = Heat Capacity of water (1 Btu/lb\*°F)

3412 = Conversion from Btu to kWh

Illustrative Examples

New Construction using ASHP baseline:

For example, a 3 ton unit with Part Load EER rating of 19 and Part Load COP of 4.4 with desuperheater is installed with a 50 gallon electric water heater in single family house in Springfield:

ΔkWh = [(FLHcool \* Capacity\_cooling \* (1/SEERbase – (1/EERPL)/1000] + [(FLHheat \* Capacity\_heating \* (1/HSPFbase – (1/COPPL \* 3.412)))/1000] + [ElecDHW \* %DHWDisplaced \* (((1/ EFELEC exist) \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 3412)]

ΔkWh = [(730 \* 36,000 \* (1/14 – 1/19)) / 1000] + [(1754\* 36,000 \* (1/8.2 – 1/ (4.4\*3.412))) / 1000] + [1 \* 0.44 \* (((1/0.945) \* 17.6 \* 2.56 \*365.25 \* 8.33 \* (125-54) \* 1)/3412)]

= 494 + 3494 + 1328

= 5316 kWh

Early Replacement – non-fuel switch (see example after Natural gas section for Fuel switch):

For example, a 3 ton unit with Part Load EER rating of 19 and Part Load COP of 4.4 with desuperheater is installed in single family house in Springfield with a 50 gallon electric water heater replacing an existing working Air Source Heat Pump with unknown efficiency ratings:

ΔkWH for remaining life of existing unit (1st 8 years):

= [(730 \* 36,000 \* (1/9.12 - 1/19)) / 1000] + [(1754 \* 36,000 \* (1/5.44 - 1/(4.4 \* 3.412))) / 1000] + [0.44 \* 1 \* (((1/0.945) \* 17.6 \* 2.56 \*365.25 \* 8.33 \* (125-54) \* 1)/3412)]

= 1498 + 7401 + 1328

= 10,227 kWh

ΔkWH for remaining measure life (next 17 years):

= [(730 \* 36,000 \* (1/14 – 1/28)) / 1000] + [(1967 \* 36,000 \* (1/8.2 – 1/ (4.4 \* 3.412)) / 1000] + [0.44 \* 1 \* (((1/0.945) \* 17.6 \* 2.56 \*365.25 \* 8.33 \* (125-54) \* 1)/3412)]

= 494 + 3494 + 1328

= 5316 kWh

###### Summer Coincident Peak Demand Savings

New Construction and Time of Sale:

ΔkW = (Capacity\_cooling \* (1/EERbase - 1/EERFL))/1000) \* CF

Early replacement:

ΔkW for remaining life of existing unit (1st 8 years):

= (Capacity\_cooling \* (1/EERexist - 1/EERFL))/1000) \* CF

ΔkW for remaining measure life (next 17 years):

= (Capacity\_cooling \* (1/EERbase - 1/EERFL))/1000) \* CF

Where:

EERbase = EER Efficiency of new replacement unit

|  |  |
| --- | --- |
| **Existing Cooling System** | **EER\_base** |
| Air Source Heat Pump | 11.8[[956]](#footnote-957) |
| Central AC | 11 [[957]](#footnote-958) |
| No central cooling | 11[[958]](#footnote-959) |

EERexist = Energy Efficiency Ratio of existing cooling unit (kBtu/hr / kW)

= Use actual EER rating where it is possible to measure or reasonably estimate. If EER unknown but SEER available convert using the equation:

EERexist = (-0.02 \* SEERexist2) + (1.12 \* SEERexist) [[959]](#footnote-960)

If SEER rating unavailable use:

|  |  |
| --- | --- |
| **Existing Cooling System** | **EER\_exist** |
| Air Source Heat Pump | 8.55[[960]](#footnote-961) |
| Central AC | 8.15[[961]](#footnote-962) |
| No central cooling | 11 [[962]](#footnote-963) |

EERFL = Full Load EER Efficiency of ENERGY STAR GSHP unit [[963]](#footnote-964)

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during system peak hour)

= 72%%[[964]](#footnote-965)

CFPJM = PJM Summer Peak Coincidence Factor for Central A/C (average during peak period)

= 46.6%[[965]](#footnote-966)

New Construction or Time of Sale:

For example, a 3 ton unit with Full Load EER rating of 19:

ΔkWSSP = ((36,000 \* (1/11.8 – 1/19))/1000) \* 0.72

= 0.83 kW

ΔkWPJM = ((36,000 \* (1/11 – 1/19))/1000) \* 0.466

= 0.54 kW

Early Replacement:

For example, a 3 ton Full Load 19 EER replaces an existing working Air Source Heat Pump with unknown efficiency ratings in Marion:

ΔkWSSP for remaining life of existing unit (1st 8 years):

= ((36,000 \* (1/8.55 – 1/19))/1000) \* 0.72

= 1.67 kW

ΔkWSSP for remaining measure life (next 17 years):

= ((36,000 \* (1/11.8 – 1/19))/1000) \* 0.72

= 0.83 kW

ΔkWPJM for remaining life of existing unit (1st 8 years):

= ((36,000 \* (1/8.55 – 1/19))/1000) \* 0.466

= 1.08 kW

ΔkWPJM for remaining measure life (next 17 years):

= ((36,000 \* (1/11.8 – 1/19))/1000) \* 0.466

= 0.54 kW

###### Natural Gas Savings

New Construction and Time of Sale with baseline gas heat and/or hot water:

If measure is supported by gas utility only, gas utility claim savings calculated below:

ΔTherms = [Heating Savings] + [DHW Savings]

= [Replaced gas consumption – therm equivalent of GSHP source kWh] + [DHW Savings]

= [(1 – ElecHeat) \* ((Gas\_Heating\_Load/AFUEbase) – (kWhtoTherm \* FLHheat \* Capacity\_heating \* 1/COPPL)/1000)] + [(1 – ElecDHW) \* %DHWDisplaced \* (1/ EFGas exist \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 100,000)]

If measure is supported by gas and electric utility, gas utility claim savings calculated below, (electric savings is provided in Electric Energy Savings section):

ΔTherms = [Heating Savings] + [DHW Savings]

= [Replaced gas consumption – therm equivalent of base ASHP source kWh] + [DHW Savings]

= [(1 – ElecHeat) \* ((Gas\_Heating\_Load/AFUEbase) – (kWhtoTherm \* FLHheat \* Capacity\_heating \* 1/(HSPFASHP/3.412))/1000)] + [(1 – ElecDHW) \* %DHWDisplaced \* (1/ EFGas exist \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 100,000)]

Early replacement for homes with existing gas heat and/or hot water:

If measure is supported by gas utility only, gas utility claim savings calculated below:

ΔTherms for remaining life of existing unit (1st 8 years):

= [Heating Savings] + [DHW Savings]

= [Replaced gas consumption – therm equivalent of GSHP source kWh] + [DHW Savings]

= [(1 – ElecHeat) \* ((Gas\_Heating\_Load/AFUEexist) – (kWhtoTherm \* FLHheat \* Capacity\_heating \* 1/(COPPL \* 3.412))/1000)] + [(1 – ElecDHW) \* %DHWDisplaced \* (1/ EFGas exist \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 100,000)]

ΔTherms for remaining measure life (next 17 years):

= [(1 – ElecHeat) \* ((Gas\_Heating\_Load/AFUEbaseER) – (kWhtoTherm \* FLHheat \* Capacity\_heating \* 1//(COPPL \* 3.412))/1000)] + [(1 – ElecDHW) \* %DHWDisplaced \* (1/ EFGas exist \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 100,000)]

If measure is supported by gas and electric utility, gas utility claim savings calculated below:

ΔTherms for remaining life of existing unit (1st 8 years):

ΔTherms = [Heating Savings] + [DHW Savings]

= [Replaced gas consumption – therm equivalent of base ASHP source kWh] + [DHW Savings]

= [(1 – ElecHeat) \* ((Gas\_Heating\_Load/AFUEexist) – (kWhtoTherm \* FLHheat \* Capacity\_heating \* 1/HSPFASHP)/1000)] + [(1 – ElecDHW) \* %DHWDisplaced \* (1/ EFGas exist \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 100,000)]

ΔTherms for remaining measure life (next 17 years):

= [(1 – ElecHeat) \* ((Gas\_Heating\_Load/AFUEbaseER) – (kWhtoTherm \* FLHheat \* Capacity\_heating \* 1/HSPFASHP)/1000)] + [(1 – ElecDHW) \* %DHWDisplaced \* (1/ EFGas exist \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 100,000)]

Where:

ElecHeat = 1 if existing building is electrically heated

= 0 if existing building is not electrically heated

Gas\_Heating\_Load

= Estimate of annual household heating load[[966]](#footnote-967) for gas furnace heated single-family homes. If location is unknown, assume the average below.

= Actual if informed by site-specific load calculations, ACCA Manual J or equivalent[[967]](#footnote-968).

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **Gas\_Heating\_Load if Furnace (therms)** [[968]](#footnote-969) | **Gas\_Heating\_Load if Boiler (therms)** [[969]](#footnote-970) |
| 1 (Rockford) | 873 | 1275 |
| 2 (Chicago) | 834 | 1218 |
| 3 (Springfield) | 714 | 1043 |
| 4 (Belleville) | 551 | 805 |
| 5 (Marion) | 561 | 819 |
| Average | 793 | 1158 |

AFUEbase = Baseline Annual Fuel Utilization Efficiency Rating

= 80% if furnace and 82% if boiler.

AFUEexist = Existing Annual Fuel Utilization Efficiency Rating

= Use actual AFUE rating where it is possible to measure or reasonably estimate.

If unknown, assume 64.4% if furnace and 61.6% [[970]](#footnote-971) if boiler.

AFUEbaseER = Baseline Annual Fuel Utilization Efficiency Rating for early replacement measure

= 90%[[971]](#footnote-972) if furnace and 82% if boiler.

kWhtoTherm = Converts source kWh to Therms

= Hgrid / 100000

Hgrid = Heat rate of the grid in btu/kWh[[972]](#footnote-973)

ComEd: 10,622 btu/kWh

Ameren: 10,967 btu/kWh

3.412 = Converts HSPF to COP

EFGas exist = Energy Factor (efficiency) of existing gas water heater

= Actual. If unknown assume federal standard[[973]](#footnote-974):

For <=55 gallons: 0.675 – (0.0015 \* tank\_size)

For > 55 gallons 0.8012 – (0.00078 \* tank size)

= If tank size unknown assume 40 gallons and EF\_Baseline of 0.615

All other variables provided above

Illustrative Examples *[for illustrative purposes a Heat Rate of 10,000 Btu/kWh is used]*

New construction using gas furnace and central AC baseline, *supported by Gas utility only*:

For example, a 3 ton unit with Part Load EER rating of 19 and Part Load COP of 4.4 in single family house in Springfield with a 40 gallon gas water heater is installed in place of a natural gas furnace and 3 ton Central AC unit:

ΔkWH = 0

ΔTherms = [Heating Savings] + [DHW Savings]

= [Replaced gas consumption – therm equivalent of GSHP source kWh] + [DHW Savings]

= [(1 – ElecHeat) \* ((Gas\_Heating\_Load/AFUEbase) – (kWhtoTherm \* FLHheat \* Capacity\_heating \* 1/(COPPL \* 3.412)/1000)] + [(1 – ElecDHW) \* %DHWDisplaced \* (1/ EFGas exist \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 100,000)]

= [(1-0) \* ((714/0.80) – (10000/100000 \* 1754 \* 36,000 \* 1/(4.4 \* 3.412))/1000)] + [(1 – 0) \* (0.44 \* (1/ 0.615 \* 17.6 \* 2.56 \*365.25 \* 8.33 \* (125-54) \* 1) / 100,000)]

= 472 + 70

= 542 therms

Early Replacement fuel switch, *supported by gas and electric utility*:

For example, a 3 ton unit with Part Load EER rating of 19 and Part Load COP of 4.4 in single family house in Springfield with a 40 gallon gas water heater replaces an existing working natural gas furnace and 3 ton Central AC unit with unknown efficiency ratings:

ΔkWh for remaining life of existing unit (1st 8 years):

= [Cooling savings] + [Heating savings from base ASHP to GSHP] + [DHW savings]

= [(FLHcool \* Capacity\_cooling \* (1/SEERexist – (1/EERPL)/1000] + [(FLHheat \* Capacity\_heating \* (1/HSPFASHP – (1/COPPL \* 3.412)))/1000] + [ElecDHW \* %DHWDisplaced \* (((1/ EFELEC) \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 3412)]

= [(730\* 36,000 \* (1/8.6 - 1/19)) / 1000] + [(1754 \* 36,000 \* (1/8.2 - 1/(4.4 \* 3.412))) / 1000] + [0 \* 0.44 \* (((1/0.904) \* 17.6 \* 2.56 \*365.25 \* 8.33 \* (125-54) \* 1)/3412)]

= 1673 + 3494 + 0

= 5167 kWh

Continued on next page.

Illustrative Example continued

ΔkWh for remaining measure life (next 17 years):

= [Cooling savings] + [Heating savings] + [DHW savings]

= [(FLHcool \* Capacity\_cooling \* (1/SEERbase – (1/EERPL)/1000] + [(FLHheat \* Capacity\_heating \* (1/HSPFASHP – (1/COPPL \* 3.412)))/1000] + [ElecDHW \* %DHWDisplaced \* (((1/ EFELEC) \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) /3412)]

= [(730 \* 36,000 \* (1/13 – 1/19)) / 1000] + [1754 \* 36,000 \* (1/8.2 – 1/ (4.4 \*3.412)) / 1000] + [0 \* 0.44 \* (((1/0.904) \* 17.6 \* 2.56 \*365.25 \* 8.33 \* (125-54) \*1)/3412)]

= 638 + 3494 + 0

= 4132 kWh

ΔTherms for remaining life of existing unit (1st 8 years):

= [Heating Savings] + [DHW Savings]

= [Replaced gas consumption – therm equivalent of base ASHP source kWh] + [DHW Savings]

= [(1 – ElecHeat) \* ((Gas\_Heating\_Load/AFUEexist) – (kWhtoTherm \* FLHheat \* Capacity\_heating \* 1/HSPFASHP)/1000)] + [(1 – ElecDHW) \* %DHWDisplaced \* (1/ EFGas exist \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 100,000)]

= [(1-0) \* ((714/0.644) – (10000/100000 \* 1754 \* 36,000 \* 1/8.2)/1000)] + [(1 – 0) \* (0.44 \* (1/ 0.615 \* 17.6 \* 2.56 \*365.25 \* 8.33 \* (125-54) \* 1) / 100,000)]

= 339 + 70

= 408 therms

ΔTherms for remaining measure life (next 17 years):

= [(1 – ElecHeat) \* ((Gas\_Heating\_Load/AFUEbaseER) – (kWhtoTherm \* FLHheat \* Capacity\_heating \* 1/HSPFASHP)/1000)] + [(1 – ElecDHW) \* %DHWDisplaced \* (1/ EFGas exist \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 100,000)]

= [(1-0) \* ((714/0.9) – (10000/100000 \* 1754 \* 36,000 \* 1/8.2)/1000)] + [(1 – 0) \* (0.44 \* (1/ 0.615 \* 17.6 \* 2.56 \*365.25 \* 8.33 \* (125-54) \* 1) / 100,000)]

= 23 + 70

= 93 therms

**Water Impact Descriptions and Calculation**

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Cost Effectiveness Screening when Fuel Switching

This measure can involve fuel switching from gas to electric. The inputs to cost effectiveness screening should reflect the actual impacts on the electric and fuel consumption at the customer meter and, for fuel switching measures, this will not match the output of the calculation/allocation methodolgy presented in the “Electric Energy Savings” and “Natural Gas Savings” sections below. Therefore in addition to the calculation of savings claimed, the following values should be used to assess the cost effectiveness of the measure.

ΔTherms = [Heating Consumption Replaced[[974]](#footnote-975)] + [DHW Savings if gas]

= [(1 – ElecHeat) \* ((Gas\_Heating\_Load/AFUEbase)] + [(1 – ElecDHW) \* %DHWDisplaced \* (1/ EFGas exist \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 100,000)]

ΔkWh = - [GSHP heating consumption] + [Cooling savings[[975]](#footnote-976)] + [DHW savings if electric]

= - [(FLHheat \* Capacity\_heating \* (1/COPPL \* 3.412))/1000] + [(FLHcool \* Capacity\_cooling \* (1/SEERbase - 1/EERPL))/1000] + [ElecDHW \* %DHWDisplaced \* ((1/EFELEC \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 3412)]

Illustrative Example of Cost Effectiveness Inputs for Fuel Switching

For example, a 3 ton unit with Part Load EER rating of 19 and Part Load COP of 4.4 in single family house in Springfield with a 40 gallon gas water heater replaces an existing working natural gas furnace and 3 ton Central AC unit with unknown efficiency ratings. [Note the calculation provides the annual savings for the first 8 years of the measure life, an additional calculation (not shown) would be required to calculated the annual savings for the remaining life (years 9-25)]:

ΔTherms = [(1 – ElecHeat) \* ((Gas\_Heating\_Load/AFUEexist)] + [(1 – ElecDHW) \* %DHWDisplaced \* (1/ EFGas exist \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 100,000)]

= [(1-0) \* (714/0.644)] + [((1 – 0) \* 0.44 \* (1/ 0.615 \* 17.6 \* 2.56 \*365.25 \* 8.33 \* (125-54) \* 1) / 100,000)]

= 1109 + 70

= 1179 therms

ΔkWh = - [(FLHheat \* Capacity\_heating \* (1/COPPL \* 3.412))/1000] + [(FLHcool \* Capacity\_cooling \* (1/SEERexist - 1/EERPL))/1000] + [ElecDHW \* %DHWDisplaced \* (((1/EFELEC) \* GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0) / 3412)]

= - [(1754 \* 36,000 \* (1/(4.4 \* 3.412)))/ 1000] + [(730 \* 36,000 \* (1/8.6 - 1/19))/ 1000)] + [0 \* 0.44 \* (((1/0.904) \* 17.6 \* 2.56 \*365.25 \* 8.33 \* (125-54) \* 1)/3412)]

= -4206 + 1673 + 0

= -2533 kWh

###### Measure Code: RS-HVC-GSHP-V04-150601

### High Efficiency Bathroom Exhaust Fan

###### Description

This market opportunity is defined by the need for continuous mechanical ventilation due to reduced air-infiltration from a tighter building shell. In retrofit projects, existing fans may be too loud, or insufficient in other ways, to be operated as required for proper ventilation. This measure assumes a fan capacity of 50 CFM rated at a sound level of less than 2.0 sones at 0.1 inches of water column static pressure. This measure may be applied to larger capacity, up to 130 CFM, efficient fans with bi-level controls because the savings and incremental costs are very similar. All eligible installations shall be sized to provide the mechanical ventilation rate indicated by ASHRAE 62.2.

This measure was developed to be applicable to the following program types:  TOS, NC, RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

New efficient (average CFM/watt of 8.3 [[976]](#footnote-977)) exhaust-only ventilation fan, quiet (< 2.0 sones) Continuous operation in accordance with recommended ventilation rate indicated by ASHRAE 62.2[[977]](#footnote-978)

###### Definition of Baseline Equipment

New standard efficiency (average CFM/Watt of 3.1[[978]](#footnote-979)) exhaust-only ventilation fan, quiet (< 2.0 sones) operating in accordance with recommended ventilation rate indicated by ASHRAE 62.2 [[979]](#footnote-980)

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 19 years[[980]](#footnote-981).

###### Deemed Measure Cost

Incremental cost per installed fan is $43.50 for quiet, efficient fans[[981]](#footnote-982).

###### Loadshape

Loadshape R11 - Residential Ventilation

###### Coincidence Factor

The summer Peak Coincidence Factor is assumed to be 100% because the fan runs continuously.

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = (CFM \* (1/η,Baseline - 1/ηEfficient)/1000) \* Hours

Where:

CFM = Nominal Capacity of the exhaust fan

= 50 CFM[[982]](#footnote-983)

ηBaseline = Average efficacy for baseline fan

= 3.1 CFM/Watt[[983]](#footnote-984)

ηEffcient = Average efficacy for efficient fan

= 8.3 CFM/Watt[[984]](#footnote-985)

Hours = assumed annual run hours,

= 8766 for continuous ventilation.

ΔkWh = (50 \* (1/3.1 – 1/8.3)/1000) \* 8766

= 88.6 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = (CFM \* (1/ηBaseline - 1/ηEfficient)/1000) \* CF

Where:

CF = Summer Peak Coincidence Factor

= 1.0 (continuous operation)

Other variables as defined above

ΔkW = (50 \* (1/3.1 – 1/8.3)/1000) \* 1.0

= 0.0101 kW

###### Natural Gas Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-HVC-BAFA-V01-120601

### HVAC Tune Up (Central Air Conditioning or Air Source Heat Pump)

###### Description

This measure involves the measurement of refrigerant charge levels and airflow over the central air conditioning or heat pump unit coil, correction of any problems found and post-treatment re-measurement.  Measurements must be performed with standard industry tools and the results tracked by the efficiency program.

Savings from this measure are developed using a reputable Wisconsin study. It is recommended that future evaluation be conducted in Illinois to generate a more locally appropriate characterization.

This measure was developed to be applicable to the following program types:  RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

N/A

###### Definition of Baseline Equipment

This measure assumes that the existing unit being maintained is either a residential central air conditioning unit or an air source heat pump that has not been serviced for at least 3 years.

###### Deemed Lifetime of Efficient Equipment

The measure life is assumed to be 2 years[[985]](#footnote-986).

###### Deemed Measure Cost

If the implementation mechanism involves delivering and paying for the tune up service, the actual cost should be used. If however the customer is provided a rebate and the program relies on private contractors performing the work, the measure cost should be assumed to be $175[[986]](#footnote-987).

###### Loadshape

Loadshape R08 - Residential Cooling

###### Coincidence Factor

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during utility peak hour)

= 68%[[987]](#footnote-988)

CFSSP = Summer System Peak Coincidence Factor for Heat Pumps (during system peak hour)

= 72%%[[988]](#footnote-989)

CFPJM   = PJM Summer Peak Coincidence Factor for Central A/C (average during PJM peak period)

= 46.6%[[989]](#footnote-990)

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

ΔkWhCentral AC  = (FLHcool \* Capacity\_cooling\* (1/SEERCAC))/1000 \* MFe

ΔkWhAir Source Heat Pump = ((FLHcool \* Capacity\_cooling \* (1/SEERASHP))/1000 \* MFe) + (FLHheat \* Capacity\_heating \* (1/HSPFASHP))/1000 \* MFe)

Where:

FLHcool = Full load cooling hours

Dependent on location as below:[[990]](#footnote-991)

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **FLHcool**  **Single Family** | **FLHcool**  **Multifamily** |
| 1 (Rockford) | 512 | 467 |
| 2 (Chicago) | 570 | 506 |
| 3 (Springfield) | 730 | 663 |
| 4 (Belleville) | 1,035 | 940 |
| 5 (Marion) | 903 | 820 |
| Weighted Average[[991]](#footnote-992) | 629 | 564 |

Capacity\_cooling = Cooling cpacity of equipment in Btu/hr (note 1 ton = 12,000 Btu/hr)

= Actual

SEERCAC = SEER Efficiency of existing central air conditioning unit receiving maintenence

= Actual. If unknown assume 10 SEER [[992]](#footnote-993)

MFe = Maintenance energy savings factor

= 0.05[[993]](#footnote-994)

SEERASHP = SEER Efficiency of existing air source heat pump unit receiving maintenence

= Actual. If unknown assume 10 SEER [[994]](#footnote-995)

FLHheat = Full load heating hours

Dependent on location:[[995]](#footnote-996)

| **Climate Zone**  **(City based upon)** | **FLHheat** |
| --- | --- |
| 1 (Rockford) | 2208 |
| 2 (Chicago) | 2064 |
| 3 (Springfield) | 1967 |
| 4 (Belleville) | 1420 |
| 5 (Marion) | 1445 |
| Weighted Average[[996]](#footnote-997) | 1821 |

Capacity\_heating = Heating cpacity of equipment in Btu/hr (note 1 ton = 12,000 Btu/hr)

= Actual

HSPFbase = Heating Season Performance Factor of existing air source heat pump unit receiving maintenence

= Actual. If unknown assume 6.8 HSPF [[997]](#footnote-998)

For example, maintenance of a 3-ton, SEER 10 air conditioning unit in a single family house in Springfield:

ΔkWhCAC  = (730 \* 36,000 \* (1/10))/1000 \* 0.05

= 131 kWh

For example, maintenance of a 3-ton, SEER 10, HSPF 6.8 air source heat pump unit in a single family house in Springfield:

ΔkWhASHP = ((730 \* 36,000 \* (1/10))/1000 \* 0.05) + (1967 \* 36,000 \* (1/6.8))/1000 \* 0.05)

= 652 kWh

###### Summer Coincident Peak Demand Savings

∆kW**=** Capacity\_cooling \* (1/EER)/1000 \* MFd \* CF

Where:

EER = EER Efficiency of existing unit receiving maintenance in Btu/H/Watts

= Calculate using Actual SEER

= - 0.02\*SEER2 + 1.12\*SEER [[998]](#footnote-999)

MFd = Maintenance demand savings factor

= 0.02 [[999]](#footnote-1000)

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during system peak hour)

= 68%[[1000]](#footnote-1001)

CFSSP = Summer System Peak Coincidence Factor for Heat Pumps (during system peak hour)

= 72%%[[1001]](#footnote-1002)

CFPJM = PJM Summer Peak Coincidence Factor for Central A/C (average during peak period)

= 46.6%[[1002]](#footnote-1003)

For example, maintenance of 3-ton, SEER 10 (equals EER 9.2) CAC unit:

ΔkWSSP = 36,000 \* 1/(9.2)/1000 \* 0.02 \* 0.68

= 0.0532 kW

ΔkWPJM = 36,000 \* 1/(9.2)/1000 \* 0.02 \* 0.466

= 0.0365 kW

###### Natural Gas Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

Conservatively not included.

###### Measure Code: RS-HVC-TUNE-V02-140601

### Programmable Thermostats

###### Description

This measure characterizes the household energy savings from the installation of a new or reprogramming of an existing Programmable Thermostat for reduced heating energy consumption through temperature set-back during unoccupied or reduced demand times. Because a literature review was not conclusive in providing a defensible source of prescriptive cooling savings from programmable thermostats, cooling savings from programmable thermostats are assumed to be zero for this version of the measure. It is not appropriate to assume a similar pattern of savings from setting a thermostat down during the heating season and up during the cooling season.  Note that the EPA’s EnergyStar program is developing a new specification for this project category, and if/when evaluation results demonstrate consistent cooling savings, subsequent versions of this measure will revisit this assumption[[1003]](#footnote-1004). Energy savings are applicable at the household level; all thermostats controlling household heat should be programmable and installation of multiple programmable thermostats per home does not accrue additional savings.

This measure was developed to be applicable to the following program types:  TOS, NC, RF, DI.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The criteria for this measure are established by replacement of a manual-only temperature control, with one that has the capability to adjust temperature setpoints according to a schedule without manual intervention. This category of equipment is broad and rapidly advancing in regards to the capability, and usability of the controls and their sophistication in setpoint adjustment and information display, but for the purposes of this characterization, eligibility is perhaps most simply defined by what it isn't: a manual only temperature control.

For the thermostat reprogramming measure, the auditor consults with the homeowner to determine an appropriate set back schedule, reprograms the thermostat and educates the homeowner on its appropriate use.

###### Definition of Baseline Equipment

For new thermostats the baseline is a non-programmable thermostat requiring manual intervention to change temperature setpoint.

For the purpose of thermostat reprogramming, an existing programmable thermostat that an auditor determines is being used in override mode or otherwise effectively being operated like a manual thermostat.

###### Deemed Lifetime of Efficient Equipment

The expected measure life of a programmable thermostat is assumed to be 10 years[[1004]](#footnote-1005) based upon equipment life only[[1005]](#footnote-1006). For the purposes of claiming savings for a new programmable thermostat, this is reduced by a 50% persistence factor to give final measures life of 5 years. For reprogramming, this is reduced further to give a measure life of 2 years.

###### Deemed Measure Cost

Actual material and labor costs should be used if the implementation method allows. If unknown (e.g. through a retail program) the capital cost for the new installation measure is assumed to be $30[[1006]](#footnote-1007). The cost for reprogramming is assumed to be $10 to account for the auditors time to reprogram and educate the homeowner.

###### Loadshape

Loadshape R09 - Residential Electric Space Heat

###### Coincidence Factor

N/A due to no savings attributable to cooling during the summer peak period.

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh[[1007]](#footnote-1008) = %ElectricHeat \* Elec\_Heating\_Consumption \* Heating\_Reduction \* HF \* Eff\_ISR + (∆Therms \* Fe \* 29.3)

Where:

%ElectricHeat = Percentage of heating savings assumed to be electric

|  |  |
| --- | --- |
| **Heating fuel** | **%ElectricHeat** |
| Electric | 100% |
| Natural Gas | 0% |
| Unknown | 13%[[1008]](#footnote-1009) |

Elec\_Heating\_ Consumption

= Estimate of annual household heating consumption for electrically heated single-family homes[[1009]](#footnote-1010). If location and heating type is unknown, assume 15,678 kWh[[1010]](#footnote-1011)

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **Electric Resistance**  **Elec\_Heating\_ Consumption**  **(kWh)** | **Electric Heat Pump**  **Elec\_Heating\_ Consumption**  **(kWh)** |
| 1 (Rockford) | 21,741 | 12,789 |
| 2 (Chicago) | 20,771 | 12,218 |
| 3 (Springfield) | 17,789 | 10,464 |
| 4 (Belleville) | 13,722 | 8,072 |
| 5 (Marion) | 13,966 | 8,215 |
| Average | **19,743** | **11,613** |

Heating\_Reduction = Assumed percentage reduction in total household heating energy consumption due to programmable thermostat

= 6.2%[[1011]](#footnote-1012)

HF = Household factor, to adjust heating consumption for non-single-family households.

|  |  |
| --- | --- |
| **Household Type** | **HF** |
| Single-Family | 100% |
| Multi-Family | 65%[[1012]](#footnote-1013) |
| Actual | Custom[[1013]](#footnote-1014) |

Eff\_ISR = Effective In-Service Rate, the percentage of thermostats installed and programmed effectively

|  |  |
| --- | --- |
| **Program Delivery** | **Eff\_ISR** |
| Direct Install | 100% |
| Other, or unknown | 56%[[1014]](#footnote-1015) |

∆Therms = Therm savings if Natural Gas heating system

= See calculation in Natural Gas section below

Fe = Furnace Fan energy consumption as a percentage of annual fuel consumption

= 3.14%[[1015]](#footnote-1016)

29.3 = kWh per therm

For example, a programmable thermostat directly installed in an electric resistance heated, single-family home in Springfield:

ΔkWH = 1 \* 17,789 \* 0.062 \* 100% \* 100% + (0 \* 0.0314 \* 29.3)

= 1,103 kWh

###### Summer Coincident Peak Demand Savings

N/A due to no savings from cooling during the summer peak period.

###### Natural Gas Energy Savings

∆Therms = %FossilHeat \* Gas\_Heating\_Consumption \* Heating\_Reduction \* HF \* Eff\_ISR

Where:

%FossilHeat = Percentage of heating savings assumed to be Natural Gas

|  |  |
| --- | --- |
| **Heating fuel** | **%FossilHeat** |
| Electric | 0% |
| Natural Gas | 100% |
| Unknown | 87%[[1016]](#footnote-1017) |

Gas\_Heating\_Consumption

= Estimate of annual household heating consumption for gas heated single-family homes. If location is unknown, assume the average below[[1017]](#footnote-1018).

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **Gas\_Heating\_ Consumption**  **(therms)** |
| 1 (Rockford) | 1,052 |
| 2 (Chicago) | 1,005 |
| 3 (Springfield) | 861 |
| 4 (Belleville) | 664 |
| 5 (Marion) | 676 |
| Average | 955 |

For example, a programmable thermostat directly-installed in a gas heated single-family home in Chicago:

∆Therms = 1.0 \* 1005 \* 0.062 \* 100% \* 100%

= 62.3 therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-HVC-PROG-V03-140601

### Ductless Heat Pumps

**Description**

This measure is designed to calculate electric savings for supplementing existing electric HVAC systems with ductless heat pumps. Existing systems can include: electric resistance heating or ducted air-source heat pumps. For ducted air source heat pumps, cooling savings are also possible if there is an existing air conditioning system.

Savings are achieved by displacing some of the heating or cooling load currently provided by the existing system and meeting that load with the more efficient ductless heat pump instead. The offset of the home’s heating load is likely for the milder heating periods. The limitations on heating offset increase as the outdoor temperature drops, because the DHP capacity decreases, and the point-source nature of the heater is less able to satisfy heating loads in remote rooms.

For cooling, the proposed savings calculations are aligned with those of typical replacement systems. In most cases, the DHP is expected to replace (rather than offset) a comparable amount of cooling in homes with electric resistance heat—at a much higher efficiency than the previously used cooling.

In order for this measure to apply, the control strategy for the heat pump is assumed to be chosen to maximize savings per installer recommendation.[[1018]](#footnote-1019)

This measure was developed to be applicable to the following program types:  RF.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

In order for this characterization to apply, the new equipment must be a high-efficiency, variable-capacity (typically “inverter-driven” DC motor) ductless heat pump system that exceeds the current Federal Standard. This means the unit must meet or exceed 8.2 HSPF (heating mode) and 14 SEER (cooling mode)[[1019]](#footnote-1020).

This measure only applies to the *first* ductless heat pump installed in a residence[[1020]](#footnote-1021).

**Definition of Baseline Equipment**

In order for this characterization to apply, baseline equipment must include a permanent electric resistance heating source or a ducted air-source heat pump. For multifamily buildings, each residence must have existing individual heating equipment. Multifamily residences with central heating do not qualify for this characterization. Existing cooling equipment is assumed to be standard efficiency. Note that in order to claim cooling savings, there must be an existing air conditioning system.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 18 years[[1021]](#footnote-1022).

**Deemed Measure Cost**

The incremental cost for this measure is provided below:

|  |  |
| --- | --- |
| **Unit Size** | **Incremental Cost[[1022]](#footnote-1023)** |
| 1-Ton | $3,000 |
| 1.5-Ton | $3750 |
| 2-Ton | $4,500 |

**Loadshape**

Loadshape R10 - Residential Electric Heating and Cooling

**Coincidence Factor**

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market. Both values provided are based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren.

CFSSP = Summer System Peak Coincidence Factor for ASHP (during utility peak hour)

= 72%%[[1023]](#footnote-1024)

CFPJM = PJM Summer Peak Coincidence Factor for Central A/C (average during PJM peak period)

= 46.6%[[1024]](#footnote-1025)

**Algorithms**

**Calculation of Savings**

**Electric Energy Savings**

Electric savings

ΔkWh = ΔkWhheat + ΔkWhcool

ΔkWhheat = PLD\*AHHL\*HF\*(1/HSPFexist-1/HSPFee)\*3.413

ΔkWhcool = Capacitycool\*HF\*(1/SEERexist-1/SEERee)\*EFLHcool

Where:

PLD = Percent Load Displaced. The average total annual heating load displaced from the existing heating system and now provided by the ductless heat pump[[1025]](#footnote-1026)

For a first DHP installed in a given home.

|  |  |  |  |
| --- | --- | --- | --- |
|  | **PLD5** | | |
| Climate zone | 1-ton unit | 1.5-ton unit | 2-ton unit |
| Rockford | 26% | 39% | 39% |
| Chicago | 27% | 40% | 42% |
| Springfield | 31% | 47% | 48% |
| Belleville | 30% | 45% | 48% |
| Marion | 31% | 46% | 50% |

AHHL = Annual Household Heating Load in kWh[[1026]](#footnote-1027)

|  |  |  |
| --- | --- | --- |
| **Climate Zone** | **Annual Household**  **Heating Load Resistance (kWh)** | **Annual Household Heating Load ASHP (kWh)** |
| 1 (Rockford) | 21,741 | 25,578 |
| 2 (Chicago) | 20,771 | 24,436 |
| 3 (Springfield) | 17,789 | 20,928 |
| 4 (Belleville) | 13,722 | 16,144 |
| 5 (Marion) | 13,966 | 16,431 |
| Average | 19,743 | 23,227 |

HF = Household factor, to adjust heating consumption for non-single-family households.

|  |  |
| --- | --- |
| **Household Type** | **HF** |
| Single-Family | 100% |
| Multi-Family | 65%[[1027]](#footnote-1028) |
| Actual | Custom[[1028]](#footnote-1029) |

Capacitycool = the cooling capacity of the ductless heat pump unit in kBtu/hr[[1029]](#footnote-1030).

= Actual installed

HSPFee = HSPF rating of new equipment

= Actual installed

HSPFexist = HSPF rating of existing equipment

|  |  |
| --- | --- |
| **Existing Equipment Type** | **HSPFbase** |
| Electric resistance heating | 3.41[[1030]](#footnote-1031) |
| Air Source Heat Pump | 5.44[[1031]](#footnote-1032) |

SEERee = SEER rating of new equipment

= Actual installed[[1032]](#footnote-1033)

SEERexist = SEER rating of existing equipment

= Use actual value. If unknown, see table below

|  |  |
| --- | --- |
| **Equipment Type** | **SEERexist[[1033]](#footnote-1034)** |
| PTAC | 7.4 SEER |
| PTHP | 7.4 SEER |
| SPVAC < 65kBtu/hr | 9.0 SEER |
| SPVHP < 65 kBtu/hr | 9.0 SEER |
| Room AC | 7.0 SEER |
| Ducted ASHP | 13.0 SEER |
| No existing system | No cooling savings. |

EFLHcool = Equivalent Full Load Hours for cooling. Depends on location. See table below[[1034]](#footnote-1035).

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **FLHRoomAC** |
| 1 (Rockford) | 220 |
| 2 (Chicago) | 210 |
| 3 (Springfield) | 319 |
| 4 (Belleville) | 428 |
| 5 (Marion) | 374 |
| Weighted Average[[1035]](#footnote-1036) | 248 |

**Summer Coincident Peak Demand Savings**

For example, installing a 1.5-ton (heating and cooling capacity) ductless heat pump unit rated at 8 HSPF and 14 SEER in a single-family home in Chicago to displace electric baseboard heat and replace a window air conditioner, savings are:

ΔkWhheat = 40% x 20,771kWh x 100% x (1/3.41 – 1/8) x 3.413 = 4,771kWh

ΔkWhcool = 18 x 100% x (1/7 – 1/14) x 210 = 270kWh

ΔkWh = 4,771 + 270 = 5,041kWh

ΔkW = (Capacity\_cooling \*HF\* (1/EER\_exist - 1/EER\_ee)) / 1000) \* CF

Where:

Where:

EER\_exist = Energy Efficiency Ratio of existing cooling system (kBtu/hr / kW)

= Use actual EER rating otherwise:

|  |  |
| --- | --- |
| **Equipment Type** | **EERexist** |
| PTAC | 8.1EER[[1036]](#footnote-1037) |
| PTHP | 8.1EER[[1037]](#footnote-1038) |
| SPVAC < 65kBtu/hr | 9.9 EER [[1038]](#footnote-1039) |
| SPVHP < 65 kBtu/hr | 9.9 EER[[1039]](#footnote-1040) |
| Room AC | 7.7 EER[[1040]](#footnote-1041) |
| Ducted ASHP | 11.2 EER [[1041]](#footnote-1042) |
| No existing system |  |

EER\_ee = Energy Efficiency Ratio of new ductless Air Source Heat Pump (kBtu/hr / kW)

= Actual, If not provided convert SEER to EER using this formula:

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during system peak hour)

= 72%%[[1042]](#footnote-1043)

CFPJM = PJM Summer Peak Coincidence Factor for Central A/C (average during peak period)

= 46.6%[[1043]](#footnote-1044)

**Natural Gas Savings**

N/A

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

**Measure Code: RS-HVC-DHP-V02-150601**

### Residential Furnace Tune-Up

**Description**

This measure is for a natural gas Residential furnace that provides space heating. The tune-up will improve furnace performance by inspecting, cleaning and adjusting the furnace and appurtenances for correct and efficient operation. Additional savings maybe realized through a complete system tune-up.

This measure was developed to be applicable to the following program types: Residential.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

To qualify for this measure an approved technician must complete the tune-up requirements[[1044]](#footnote-1045) listed below:

* Measure combustion efficiency using an electronic flue gas analyzer
* Check and clean blower assembly and components per manufacturer’s recommendations
* Where applicable Lubricate motor and inspect and replace fan belt if required
* Inspect for gas leaks
* Clean burner per manufacturer’s recommendations and adjust as needed
* Check ignition system and safety systems and clean and adjust as needed
* Check and clean heat exchanger per manufacturer’s recommendations
* Inspect exhaust/flue for proper attachment and operation
* Inspect control box, wiring and controls for proper connections and performance
* Check air filter and clean or replace per manufacturer’s
* Inspect duct work connected to furnace for leaks or blockages
* Measure temperature rise and adjust flow as needed
* Check for correct line and load volts/amps
* Check thermostat operation is per manufacturer’s recommendations(if adjustments made, refer to ‘Residential Programmable Thermostat’ measure for savings estimate)
* Perform Carbon Monoxide test and adjust heating system until results are within standard industry acceptable limits

**Definition of Baseline Equipment**

The baseline is furnace assumed not to have had a tune-up in the past 2 years.

**Deemed Lifetime of Efficient Equipment**

The measure life for the tune up is 2 years.[[1045]](#footnote-1046)

**Deemed Measure Cost**

The incremental cost for this measure should be the actual cost of tune up.

**Deemed O&M Cost Adjustments**

There are no expected O&M savings associated with this measure.

**Loadshape**

Loadshape R09 - Residential Electric Space Heat

**Coincidence Factor**

N/A

**Algorithms**

**Calculation of Energy Savings**

**Electric Energy Savings**

ΔkWh = ΔTherms \* Fe \* 29.3

Where:

ΔTherms = as calculated below

Fe = Furnace Fan energy consumption as a percentage of annual fuel consumption

= 3.14%[[1046]](#footnote-1047)

29.3 = kWh per therm

**Summer Coincident Peak Demand Savings**

N/A

**Natural Gas Savings**

Δtherms =( Gas\_Furnace\_Heating\_Load \*HF \* (1/ Effbefore – 1/ (Effbefore + Ei)))

Where:

Gas\_Furnace\_Heating\_Load = Estimate of annual household heating load[[1047]](#footnote-1048) for gas furnace heated single-family homes. If location is unknown, assume the average below[[1048]](#footnote-1049).

= Actual if informed by site-specific load calculations, ACCA Manual J or equivalent[[1049]](#footnote-1050).

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **Gas\_Furnace\_Heating\_Load (therms)** |
| 1 (Rockford) | 873 |
| 2 (Chicago) | 834 |
| 3 (Springfield) | 714 |
| 4 (Belleville) | 551 |
| 5 (Marion) | 561 |
| Average | 793 |

HF = Household factor, to adjust heating consumption for non-single-family households.

|  |  |
| --- | --- |
| **Household Type** | **HF** |
| Single-Family | 100% |
| Multi-Family | 65%[[1050]](#footnote-1051) |
| Actual | Custom[[1051]](#footnote-1052) |

Effbefore = Efficiency of the furnace before the tune-up

= Actual

EI = Efficiency Improvement of the furnace tune-up measure

= Actual

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**O&M Cost Adjustment Calculation**

N/A

**Measure Code: RS-HVC-FTUN-V01-150601**

### Boiler Reset Controls

**Description**

This measure relates to improving system efficiency by adding controls to residential heating boilers to vary the boiler entering water temperature relative to heating load as a function of the outdoor air temperature to save energy. The water can be run a little cooler during fall and spring, and a little hotter during the coldest parts of the winter. A boiler reset control has two temperature sensors - one outside the house and one in the boiler water. As the outdoor temperature goes up and down, the control adjusts the water temperature setting to the lowest setting that is meeting the house heating demand. There are also limits in the controls to keep a boiler from operating outside of its safe performance range.[[1052]](#footnote-1053)

This measure was developed to be applicable to the following program types: RF.

**Definition of Efficient Equipment**

Natural gas single family residential customer adding boiler reset controls capable of resetting the boiler supply water temperature in an inverse fashion with outdoor air temperature. The system must be set so that the minimum temperature is not more than 10 degrees above manufacturer’s recommended minimum return temperature. This boiler reset measure is limited to existing condensing boilers serving a single family residence. Boiler reset controls for non-condensing boilers in single family residences should be implemented as a custom measure, and the cost-effectiveness should be confirmed.

**Definition of Baseline Equipment**

Existing condensing boiler in a single family residential setting without boiler reset controls.

**Deemed Lifetime of Efficient Equipment**

The life of this measure is 20 years***[[1053]](#footnote-1054)***

**Deemed Measure Cost**

The cost of this measure is $612[[1054]](#footnote-1055)

**Loadshape**

NA

**Coincidence Factor**

NA

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

NA

**Summer Coincident Peak Demand Savings**

NA

**Natural Gas Savings**

ΔTherms = Gas\_Boiler\_Load \* (1/AFUE) \* Savings Factor

Where:

Gas\_Boiler\_Load[[1055]](#footnote-1056)

= Estimate of annual household Load for gas boiler heated single-family homes. If location is unknown, assume the average below[[1056]](#footnote-1057).

= or Actual if informed by site-specific load calculations, ACCA Manual J or equivalent[[1057]](#footnote-1058).

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **Gas\_Boiler Load**  **(therms)** |
| 1 (Rockford) | 1275 |
| 2 (Chicago) | 1218 |
| 3 (Springfield) | 1043 |
| 4 (Belleville) | 805 |
| 5 (Marion) | 819 |
| Average | 1158 |

AFUE = Existing Condensing Boiler Annual Fuel Utilization Efficiency Rating

= Actual.

SF = Savings Factor, 5%[[1058]](#footnote-1059)

EXAMPLE

For example, boiler reset controls on a 92.5 AFUE boiler at a household in Rockford, IL

ΔTherms = 1275 \* (1/0.925) \* 0.05

= 69 Therms

**Water Impact Descriptions and Calculation**

NA

**Deemed O&M Cost Adjustment Calculation**

NA

**Measure Code: RS-HVC-BREC-V01-150601**

### ENERGY STAR Ceiling Fan

**Description**

A ceiling fan/light unit meeting the efficiency specifications of ENERGY STAR is installed in place of a model meeting the federal standard. ENERGY STAR qualified ceiling fan/light combination units are over 60% more efficient than conventional fan/light units, and use improved motors and blade designs[[1059]](#footnote-1060).

Due to the savings from this measure being derived from more efficient ventilation and more efficient lighting, and the loadshape and measure life for each component being very different, the savings are split in to the component parts and should be claimed together. Lighting savings should be estimated utilizing the 5.5.1 ENERGY STAR Compact Fluorescent Lamp measure.

This measure was developed to be applicable to the following program types:  TOS, NC, RF.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

The efficient equipment is defined as an ENERGY STAR certified ceiling fan with integral CFL bulbs.

**Definition of Baseline Equipment**

**Deemed Lifetime of Efficient Equipment**

The fan savings measure life is assumed to be 10 years.2

The lighting savings measure life is assumed to be 5 years for lighting savings, see 5.5.1 ENERGY STAR Compact Fluorescent Lamp measure.

**Deemed Measure Cost**

Incremental cost of unit is $46.[[1060]](#footnote-1061)

**Loadshape**

R06 - Residential Indoor Lighting

R11 - Residential Ventilation

**Coincidence Factor**

The summer peak coincidence factor for the ventilation savings is assumed to be 30%.[[1061]](#footnote-1062)

For lighting savings, see 5.5.1 ENERGY STAR Compact Fluorescent Lamp measure.

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

∆kWh = ΔkWhfan + ΔkWhLight

∆kWhfan = [Days\* FanHours \* ((%Lowbase \* WattsLowbase) + (%Medbase \* WattsMedbase) + (%Highbase \* WattsHighbase))/1000 ] - [Days\* FanHours \* ((%LowES \* WattsLowES) + (%MedES \* WattsMedES) + (%HighES \* WattsHighES))/1000]

∆kWhlight = see 5.5.1 ENERGY STAR Compact Fluorescent Lamp measure.

[(LightWatts

Where[[1062]](#footnote-1063):

Days = Days used per year

= Actual. If unknown use 365.25 days/year

FanHours = Daily Fan “On Hours”

= Actual. If unknown use 3 hours

%Lowbase = Percent of time spent at Low speed of baseline

= 40%

WattsLowbase = Fan wattage at Low speed of baseline

= Actual. If unknown use 15 watts

%Medbase = Percent of time spent at Medium speed of baseline

= 40%

WattsMedbase = Fan wattage at Medium speed of baseline

= Actual. If unknown use 34 watts

%Highbase = Percent of time spent at High speed of baseline

= 20%

WattsHighbase = Fan wattage at High speed of baseline

= Actual. If unknown use 67 watts

%LowES = Percent of time spent at Low speed of ENERGY STAR

= 40%

WattsLowES = Fan wattage at Low speed of ENERGY STAR

= Actual. If unknown use 6 watts

%MedES  = Percent of time spent at Medium speed of ENERGY STAR

= 40%

WattsMedES = Fan wattage at Medium speed of ENERGY STAR

= Actual. If unknown use 23 watts

%HighES  = Percent of time spent at High speed of ENERGY STAR

= 20%

WattsHighES = Fan wattage at High speed of ENERGY STAR

= Actual. If unknown use 56 watts

For ease of reference, the fan assumptions are provided below in table form:

|  |  |  |  |
| --- | --- | --- | --- |
|  | **Low Speed** | **Medium Speed** | **High Speed** |
| **Percent of Time at Given Speed** | 40% | 40% | 20% |
| **Conventional Unit Wattage** | 15 | 34 | 67 |
| **ENERGY STAR Unit Wattage** | 6 | 23 | 56 |
| **∆W** | 9 | 11 | 11 |

If the lighting WattsBase and WattsEE is unknown, assume the following

WattsBase = 3 x 43 = 129 W

WattsEE = 1 x 42 = 42 W

**Example**

For example, a ceiling fan with three 43W bulb light fixtures, replaced with an ES ceiling fan with one 42W bulb light fixture, the savings are:

ΔkWhfan = [365.25\*3\*((0.4\*15)+(0.4\*34)+(0.2\*67))/1000] – [365.25\*3\*((0.4\*6)+(0.4\*23)+(0.2\*56))/1000]

= 36.2 – 25.0 = 11.2 kWh

ΔkWhlight  =((129 – 42)/1000) \*759 \* 1.06

= 70.0 kWh

ΔkWh = 11.2 + 70

=81.2 kWh

Using the default assumptions provided above, the deemed savings is 81.2 kWh.

**Summer Coincident Peak Demand Savings**

ΔkW = ΔkWFan + ΔkWlight

ΔkWFan = ((WattsHighbase - WattsHighES)/1000) \* CFfan

ΔkWLight = see 5.5.1 ENERGY STAR Compact Fluorescent Lamp measure.

((LightWatts

Where:

CFfan = Summer Peak coincidence factor for ventilation savings

= 30%[[1063]](#footnote-1064)

CFlight = Summer Peak coincidence factor for lighting savings

= 7.1%[[1064]](#footnote-1065)

**Example**

For example a ceiling fan with three 43W bulb light fixtures, replaced with an ES ceiling fan with one 42W bulb light fixture, the savings are:

ΔkWfan = ((67-56)/1000) \* 0.3

=0.0033 kW

ΔkWlight =((129 – 42)/1000) \* 1.11 \* 0.071

= 0.0068 kW

ΔkW = 0.0033 + 0.0068

= 0.010 kW

Using the default assumptions provided above, the deemed savings is 0.010kW.

**Natural Gas Savings**

N/A

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

See 5.5.1 ENERGY STAR Compact Fluorescent Lamp measure for bulb replacement costs.

**Measure code: RS-HVC-CFAN-V01-150601**

## Hot Water End Use

### Domestic Hot Water Pipe Insulation

###### Description

This measure describes adding insulation to un-insulated domestic hot water pipes. The measure assumes the pipe wrap is installed to the first length of both the hot and cold pipe up to the first elbow. This is the most cost effective section to insulate since the water pipes act as an extension of the hot water tank up to the first elbow which acts as a heat trap. Insulating this length therefore helps reduce standby losses. Default savings are provided per 3ft length and are appropriate up to 6ft of the hot water pipe and 3ft of the cold.

This measure was developed to be applicable to the following program types:  TOS, NC, RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The efficient case is installing pipe wrap insulation to a length of hot water pipe.

###### Definition of Baseline Equipment

The baseline is an un-insulated hot water pipe.

###### Deemed Lifetime of Efficient Equipment

The measure life is assumed to be 15 years[[1065]](#footnote-1066).

###### Deemed Measure Cost

The measure cost including material and installation is assumed to be $3 per linear foot[[1066]](#footnote-1067).

###### Loadshape

Loadshape C53 - Flat

###### Coincidence Factor

This measure assumes a flat loadshape since savings relate to reducing standby losses and as such the coincidence factor is 1.

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

For electric DHW systems:

ΔkWh = ((1/Rexist – 1/Rnew) \* (L \* C) \* ΔT \* 8,766)/ ηDHW / 3413

Where:

Rexist = Pipe heat loss coefficient of uninsulated pipe (existing) [(hr-°F-ft)/Btu]

= 1.0[[1067]](#footnote-1068)

Rnew = Pipe heat loss coefficient of insulated pipe (new) [(hr-°F-ft)/Btu]

= Actual (1.0 + R value of insulation)

L = Length of pipe from water heating source covered by pipe wrap (ft)

= Actual

C = Circumference of pipe (ft) (Diameter (in) \* π/12)

= Actual (0.5” pipe = 0.131ft, 0.75” pipe = 0.196ft)

ΔT = Average temperature difference between supplied water and outside air temperature (°F)

= 60°F [[1068]](#footnote-1069)

8,766 = Hours per year

ηDHW = Recovery efficiency of electric hot water heater

= 0.98 [[1069]](#footnote-1070)

3412 = Conversion from Btu to kWh

For example, insulating 5 feet of 0.75” pipe with R-5 wrap:

ΔkWh = ((1/Rexist – 1/Rnew) \* (L \* C) \* ΔT \* 8,766) / ηDHW / 3412

= ((1/1– 1/5) \* (5 \* 0.196) \* 60 \* 8766) / 0.98 /3412

= 123 kWh

If inputs above are not available the following default per 3ft R-5 length can be used for up to 6 ft length on the hot pipe and 3 ft on the cold pipe.

ΔkWh = ((1/Rexist – 1/Rnew) \* (L \* C) \* ΔT \* 8,766) / ηDHW / 3412

= ((1/1– 1/5) \* (3 \* 0.196) \* 60 \* 8766) / 0.98 /3412

= 74.0 kWh per 3ft length

###### Summer Coincident Peak Demand Savings

∆kW**=** ∆kWh/ 8766

Where:

ΔkWh = kWh savings from pipe wrap installation

8766 = Number of hours in a year (since savings are assumed to be constant over year).

For example, insulating 5 feet of 0.75” pipe with R-5 wrap:

ΔkW = 123/8766

= 0.014kW

If inputs above are not available the following default per 3ft R-4 length can be used for up to 6 ft length on the hot pipe and 3 ft on the cold pipe.

ΔkW = 73.9/8766

= 0.0084 kW

###### Natural Gas Savings

For Natural Gas DHW systems:

ΔTherm = ((1/Rexist – 1/Rnew) \* (L \* C) \* ΔT \* 8,766) / ηDHW /100,000

Where:

ηDHW = Recovery efficiency of gas hot water heater

= 0.78 [[1070]](#footnote-1071)

Other variables as defined above

For example, insulating 5 feet of 0.75” pipe with R-5 wrap:

ΔTherm = ((1/1– 1/5) \* (5 \* 0.196) \* 60 \* 8766) / 0.78 / 100,000

= 5.29 therms

If inputs above are not available the following default per 3ft R-4 length can be used for up to 6ft length on the hot pipe and 3ft on the cold pipe.

ΔTherm = ((1/Rexist – 1/Rnew) \* (L \* C) \* ΔT \* 8,766) / ηDHW / 100,000

= ((1/1– 1/5) \* (3 \* 0.196) \* 60 \* 8766) / 0.78 /100,000

= 3.17 therms per 3ft length

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-HWE-PINS-V01-120601

### Gas Water Heater

###### Description

This measure characterizes:

1. Time of sale or new construction:

The purchase and installation of a new efficient gas-fired water heater, in place of a Federal Standard unit in a residential setting. Savings are provided for power-vented, condensing storage, and whole-house tankless units meeting specific EF criteria.

1. Early replacement:

The early removal of an existing functioning natural gas water heater from service, prior to its natural end of life, and replacement with a new high efficiency unit. Savings are calculated between existing unit and efficient unit consumption during the remaining life of the existing unit, and between new baseline unit and efficient unit consumption for the remainder of the measure life.

This measure was developed to be applicable to the following program types:  TOS, NC, EREP.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the efficient equipment must be a water heater rated with the following minimum efficiency ratings:

|  |  |
| --- | --- |
| **Water Heater Type** | **Minimum Energy Factor** |
| Gas Storage | 0.67 |
| Condensing gas storage | 0.80 |
| Tankless whole-house unit | 0.82 |

###### Definition of Baseline Equipment

Time of Sale or New Construction: The baseline condition is assumed to be a standard gas storage water heater of the same capacity as the efficient unit, rated at the federal minimum. For <=55 gallon tanks the Federal Standard is calculated as 0.675 – (0.0015 \* storage size in gallons) and for tanks >55 gallon 0.8012 – (0.00078 \* storage size in gallons)[[1071]](#footnote-1072). For a 40-gallon storage water heater this would be 0.615 EF.

Early replacement: The baseline for this measure is the efficiency of the existing equipment for the assumed remaining useful life of the unit and a new baseline unit for the remainder of the measure life.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 13 years.[[1072]](#footnote-1073)

For early replacement: Remaining life of existing equipment is assumed to be 4 years[[1073]](#footnote-1074).

###### Deemed Measure Cost

Time of Sale or New Construction:

The incremental capital cost for this measure is dependent on the type of water heater as listed below[[1074]](#footnote-1075).

Early Replacement: The full installed cost is provided in the table below. The assumed deferred cost (after 4 years) of replacing existing equipment with a new baseline unit is assumed to be $614[[1075]](#footnote-1076). This cost should be discounted to present value using the utility’s discount rate.

|  |  |  |
| --- | --- | --- |
| **Water heater Type** | **Incremental Cost** | **Full Install Cost** |
| Gas Storage | $400 | $1014 |
| Condensing gas storage | $685 | $1299 |
| Tankless whole-house unit | $605 | $1219 |

###### Loadshape

N/A

###### Coincidence Factor

N/A

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

N/A

###### Summer Coincident Peak Demand Savings

N/A

###### Natural Gas Energy Savings

Time of Sale or New Construction:

ΔTherms = (1/ EFbase - 1/EFefficient) \* (GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0 )/100,000

Early replacement[[1076]](#footnote-1077):

ΔTherms for remaining life of existing unit (1st 4 years):

= (1/ EFExisting - 1/EFefficient) \* (GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0 )/100,000

ΔTherms for remaining measure life (next 9 years):

= (1/ EFbase - 1/EFefficient) \* (GPD \* Household \* 365.25 \* γWater \* (TOUT – Tin) \* 1.0 )/100,000

Where:

EF\_Baseline = Energy Factor rating for baseline equipment

For <=55 gallons: 0.675 – (0.0015 \* tank\_size)

For > 55 gallons: 0.8012 – (0.00078 \* tank size)

= If tank size unknown assume 40 gallons and EF\_Baseline of 0.615

EF\_Efficient = Energy Factor Rating for efficient equipment

= Actual. If Tankless whole-house multiply rated efficiency by 0.91[[1077]](#footnote-1078). If unknown assume values in look up in table below

|  |  |
| --- | --- |
| **Water Heater Type** | **EF\_Efficient** |
| Condensing Gas Storage | 0.80 |
| Gas Storage | 0.67 |
| Tankless whole-house | 0.82 \* 0.91 = 0.75 |

EF\_Existing = Energy Factor rating for existing equipment

= Use actual EF rating where it is possible to measure or reasonably estimate.

= if unknown assume 0.52 [[1078]](#footnote-1079)

GPD = Gallons Per Day of hot water use per person

= 45.5 gallons hot water per day per household/2.59 people per household[[1079]](#footnote-1080)

= 17.6

Household = Average number of people per household

|  |  |
| --- | --- |
| **Household Unit Type** | **Household** |
| Single-Family - Deemed | 2.56[[1080]](#footnote-1081) |
| Multi-Family - Deemed | 2.1[[1081]](#footnote-1082) |
| Custom | Actual Occupancy or Number of Bedrooms[[1082]](#footnote-1083) |

365.25 = Days per year, on average

γWater  = Specific Weight of water

= 8.33 pounds per gallon

Tout = Tank temperature

= 125°F

Tin = Incoming water temperature from well or municipal system

= 54°F[[1083]](#footnote-1084)

1.0 = Heat Capacity of water (1 Btu/lb\*°F)

For example, a 40 gallon condensing gas storage water heater, with an energy factor of 0.80 in a single family house:

ΔTherms = (1/0.615 - 1/0.8) \* (17.6 \* 2.56 \* 365.25\* 8.33 \* (125 – 54) \* 1) / 100,000

= 36.6 therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-HWE-GWHT-V04-150601

### Heat Pump Water Heaters

This measure relates to the installation of a low flow faucet aerator in a household kitchen or bath faucet fixture.

This measure may be used for units provided through Efficiency Kit’s however the in service rate for such measures should be derived through evaluation results specifically for this implementation methodology.

This measure was developed to be applicable to the following program types:  TOS, NC, RF, DI, KITS.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

To qualify for this measure the installed equipment must be a low flow faucet aerator, for bathrooms rated at 1.5 gallons per minute (GPM) or less, or for kitchens rated at 2.2 GPM or less. Savings are calculated on an average savings per faucet fixture basis.

**Definition of Baseline Equipment**

The baseline condition is assumed to be a standard bathroom faucet aerator rated at 2.25 GPM or greater, or a standard kitchen faucet aerator rated at 2.75 GPM or greater. Average measured flow rates are used in the algorithm and are lower, reflecting the penetration of previously installed low flow fixtures (and therefore the freerider rate for this measure should be 0), use of the faucet at less than full flow, debris buildup, and lower water system pressure than fixtures are rated at. Note if flow rates are measured, for example through a Direct Install program, then actual baseline flow rates should be used as opposed to the deemed values.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 9 years.[[1084]](#footnote-1085)

**Deemed Measure Cost**

The incremental cost for this measure is $8[[1085]](#footnote-1086) or program actual.

For faucet aerators provided in Efficiency Kits, the actual program delivery costs should be utilized.

**Loadshape**

Loadshape R03 - Residential Electric DHW

**Coincidence Factor**

The coincidence factor for this measure is assumed to be 2.2%.[[1086]](#footnote-1087)

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

**Note these savings are *per* faucet retrofitted[[1087]](#footnote-1088) (unless faucet type is unknown, then it is per household).**

ΔkWh = %ElectricDHW \* ((GPM\_base \* L\_base - GPM\_low \* L\_low) \* Household \* 365.25 \*DF / FPH) \* EPG\_electric \* ISR

Where:

%ElectricDHW = proportion of water heating supplied by electric resistance heating

|  |  |
| --- | --- |
| **DHW fuel** | **%ElectricDHW** |
| Electric | 100% |
| Natural Gas | 0% |
| Unknown | 16%[[1088]](#footnote-1089) |

GPM\_base = Average flow rate, in gallons per minute, of the baseline faucet “as-used.” This includes the effect of existing low flow fixtures and therefore the freerider rate for this measure should be 0.

= 1.39[[1089]](#footnote-1090) or custom based on metering studies[[1090]](#footnote-1091) or if measured during DI:

= Measured full throttle flow \* 0.83 throttling factor[[1091]](#footnote-1092)

GPM\_low = Average flow rate, in gallons per minute, of the low-flow faucet aerator “as-used”

= 0.94[[1092]](#footnote-1093) or custom based on metering studies[[1093]](#footnote-1094) or if measured during DI:

= Rated full throttle flow \* 0.95 throttling factor[[1094]](#footnote-1095)

L\_base = Average baseline daily length faucet use per capita for faucet of interest in minutes

= if available custom based on metering studies, if not use:

|  |  |
| --- | --- |
| **Faucet Type** | **L\_base (min/person/day)** |
| Kitchen | 4.5[[1095]](#footnote-1096) |
| Bathroom | 1.6[[1096]](#footnote-1097) |
| If location unknown (total for household): Single-Family | 9.0[[1097]](#footnote-1098) |
| If location unknown (total for household): Multi-Family | 6.9[[1098]](#footnote-1099) |

L\_low = Average retrofit daily length faucet use per capita for faucet of interest in minutes

= if available custom based on metering studies, if not use:

|  |  |
| --- | --- |
| **Faucet Type** | **L\_low (min/person/day)** |
| Kitchen | 4.5[[1099]](#footnote-1100) |
| Bathroom | 1.6[[1100]](#footnote-1101) |
| If location unknown (total for household): Single-Family | 9.0[[1101]](#footnote-1102) |
| If location unknown (total for household): Multi-Family | 6.9[[1102]](#footnote-1103) |

Household = Average number of people per household

|  |  |
| --- | --- |
| **Household Unit Type** | **Household** |
| Single-Family - Deemed | 2.56[[1103]](#footnote-1104) |
| Multi-Family - Deemed | 2.1[[1104]](#footnote-1105) |
| Custom | Actual Occupancy or Number of Bedrooms[[1105]](#footnote-1106) |

365.25 = Days in a year, on average.

DF = Drain Factor

|  |  |
| --- | --- |
| **Faucet Type** | **Drain Factor[[1106]](#footnote-1107)** |
| Kitchen | 75% |
| Bath | 90% |
| Unknown | 79.5% |

FPH = Faucets Per Household

|  |  |
| --- | --- |
| **Faucet Type** | **FPH** |
| Kitchen Faucets Per Home (KFPH) | 1 |
| Bathroom Faucets Per Home (BFPH): Single-Family | 2.83[[1107]](#footnote-1108) |
| Bathroom Faucets Per Home (BFPH): Multi-Family | 1.5[[1108]](#footnote-1109) |
| If location unknown (total for household): Single-Family | 3.83 |
| If location unknown (total for household): Multi-Family | 2.5 |

EPG\_electric = Energy per gallon of water used by faucet supplied by electric water heater

= (8.33 \* 1.0 \* (WaterTemp - SupplyTemp)) / (RE\_electric \* 3412)

= (8.33 \* 1.0 \* (86 – 54.1)) / (0.98 \* 3412)

= 0.0795 kWh/gal (Bath), 0.0969 kWh/gal (Kitchen), 0.0919 kWh/gal (Unknown)

8.33 = Specific weight of water (lbs/gallon)

1.0 = Heat Capacity of water (btu/lb-°F)

WaterTemp = Assumed temperature of mixed water

= 86F for Bath, 93F for Kitchen 91F for Unknown[[1109]](#footnote-1110)

SupplyTemp = Assumed temperature of water entering house

= 54.1F [[1110]](#footnote-1111)

RE\_electric = Recovery efficiency of electric water heater

= 98% [[1111]](#footnote-1112)

3412 = Converts Btu to kWh (btu/kWh)

ISR = In service rate of faucet aerators dependant on install method as listed in table below

|  |  |
| --- | --- |
| **Selection** | **ISR** |
| Direct Install - Single Family | 0.95[[1112]](#footnote-1113) |
| Direct Install – Multi Family Kitchen | 0.91[[1113]](#footnote-1114) |
| Direct Install – Multi Family Bathroom | 0.95[[1114]](#footnote-1115) |
| Efficiency Kits | To be determined through evaluation |

For example, a direct installed kitchen low flow faucet aerator in a single-family electric DHW home:

ΔkWh = 1.0 \* (((1.39 \* 4.5 – 0.94 \* 4.5) \* 2.56 \* 365.25 \*0.75) / 1) \* 0.0969 \* 0.95

= 131 kWh

For example, a direct installed bath low flow faucet aerator in a multi-family electric DHW home:

ΔkWh = 1.0 \* (((1.39 \* 1.6 – 0.94 \* 1.6) \* 2.1 \* 365.25 \* 0.90) /1.5) \* 0.0795 \* 0.95

= 25.0 kWh

For example, a direct installed low flow faucet aerator in unknown faucet in a single-family electric DHW home:

ΔkWh = 1.0 \* (((1.39 \* 9.0 – 0.94 \* 9.0) \* 2.56 \* 365.25 \* 0.795) /3.83) \* 0.0919 \* 0.95

= 68.6 kWh

**Summer Coincident Peak Demand Savings**

ΔkW = ΔkWh / Hours \* CF

Where:

ΔkWh = calculated value above

Hours = Annual electric DHW recovery hours for faucet use per faucet

= ((GPM\_base \* L\_base) \* Household/FPH \* 365.25 \* DF ) \* 0.545[[1115]](#footnote-1116) / GPH

|  |  |  |  |
| --- | --- | --- | --- |
| **Building Type** | **Faucet location** | **Calculation** | **Hours per faucet** |
| Single Family | Kitchen | ((1.39 \* 4.5) \* 2.56/1 \* 365.25 \* 0.75) \* 0.545 / 25.5 | 94 |
| Bathroom | ((1. 39 \* 1.6) \* 2.56/2.83 \* 365.25 \* 0.9) \* 0.545 / 25.5 | 14 |
| Unknown | ((1. 39 \* 9.0) \* 2.56/3.83 \* 365.25 \* 0.795) \* 0.545 / 25.5 | 52 |
| Multi Family | Kitchen | ((1. 39 \* 4.5) \* 2.1/1 \* 365.25 \* 0.75) \* 0.545 / 25.5 | 77 |
| Bathroom | ((1. 39 \* 1.6) \* 2.1/1.5 \* 365.25 \* 0.9) \* 0.545 / 25.5 | 22 |
| Unknown | ((1. 39 \* 6.9) \* 2.1/2.5 \* 365.25 \* 0.795) \* 0.545 / 25.5 | 50 |

GPH = Gallons per hour recovery of electric water heater calculated for 70.9F temp rise (125-54.1), 98% recovery efficiency, and typical 4.5kW electric resistance storage tank.

= 25.5

CF = Coincidence Factor for electric load reduction

= 0.022[[1116]](#footnote-1117)

For example, a direct installed kitchen low flow faucet aerator in a single family electric DHW home:

ΔkW = 131/94 \* 0.022

= 0.0306 kW

**Natural Gas Savings**

ΔTherms = %FossilDHW \* ((GPM\_base \* L\_base - GPM\_low \* L\_low) \* Household \* 365.25 \*DF / FPH) \* EPG\_gas \* ISR

Where:

%FossilDHW = proportion of water heating supplied by Natural Gas heating

|  |  |
| --- | --- |
| **DHW fuel** | **%Fossil\_DHW** |
| Electric | 0% |
| Natural Gas | 100% |
| Unknown | 84%[[1117]](#footnote-1118) |

EPG\_gas = Energy per gallon of Hot water supplied by gas

= (8.33 \* 1.0 \* (WaterTemp - SupplyTemp)) / (RE\_gas \* 100,000)

= 0.00341 Therm/gal for SF homes (Bath), 0.00415 Therm/gal for SF homes (Kitchen), 0.00394 Therm/gal for SF homes (Unknown)

= 0.00397 Therm/gal for MF homes (Bath), 0.00484 Therm/gal for MF homes (Kitchen), 0.00459 Therm/gal for MF homes (Unknown)

RE\_gas = Recovery efficiency of gas water heater

= 78% For SF homes[[1118]](#footnote-1119)

= 67% For MF homes[[1119]](#footnote-1120)

100,000 = Converts Btus to Therms (btu/Therm)

Other variables as defined above.

For example, a direct-installed kitchen low flow faucet aerator in a fuel DHW single-family home:

ΔTherms = 1.0 \* (((1.39 \* 4.5 – 0.94 \* 4.5) \* 2.56 \* 365.25 \*0.75) / 1) \* 0.00415 \* 0.95

= 5.60 Therms

For example, a direct installed bath low flow faucet aerator in a fuel DHW multi-family home:

ΔTherms = 1.0 \* (((1.39 \* 1.6 – 0.94 \* 1.6) \* 2.1 \* 365.25 \* 0.90) /1.5) \* 0.003974 \* 0.95

= 1.25 Therms

For example, a direct installed low flow faucet aerator in unknown faucet in a fuel DHW single-family home:

ΔTherms = 1.0 \* (((1.39 \* 6.1– 0.94 \* 6.1) \* 2.56 \* 365.25 \* 0.795) /3.83) \* 0.00394 \* 0.95

= 1.99 Therms

**Water Impact Descriptions and Calculation**

Δgallons = ((GPM\_base \* L\_base - GPM\_low \* L\_low) \* Household \* 365.25 \*DF / FPH) \* ISR

Variables as defined above

For example, a direct-installed kitchen low flow aerator in a single family home

Δgallons = (((1.39 \* 4.5 – 0.94 \* 4.5) \* 2.56 \* 365.25 \*0.75) / 1) \* 0.95

= 1350 gallons

For example, a direct installed bath low flow faucet aerator in a multi-family home:

Δgallons = (((1.39 \* 1.6 – 0.94 \* 1.6) \* 2.1 \* 365.25 \* 0.90) /1.5) \* 0.95

= 314 gallons

For example, a direct installed low flow faucet aerator in unknown faucet in a single-family home:

Δgallons = (((1.39 \* 9.0 – 0.94 \* 9.0) \* 2.56 \* 365.25 \* 0.795) /3.83) \* 0.95

= 747 gallons

**Deemed O&M Cost Adjustment Calculation**

N/A

**Sources**

|  |  |
| --- | --- |
| **Source ID** | **Reference** |
| 1 | 2011, DeOreo, William. California Single Family Water Use Efficiency Study. April 20, 2011. |
| 2 | 2000, Mayer, Peter, William DeOreo, and David Lewis. Seattle Home Water Conservation Study. December 2000. |
| 3 | 1999, Mayer, Peter, William DeOreo. Residential End Uses of Water. Published by AWWA Research Foundation and American Water Works Association. 1999. |
| 4 | 2003, Mayer, Peter, William DeOreo. Residential Indoor Water Conservation Study. Aquacraft, Inc. Water Engineering and Management. Prepared for East Bay Municipal Utility District and the US EPA. July 2003. |
| 5 | 2011, DeOreo, William. Analysis of Water Use in New Single Family Homes. By Aquacraft. For Salt Lake City Corporation and US EPA. July 20, 2011. |
| 6 | 2011, Aquacraft. Albuquerque Single Family Water Use Efficiency and Retrofit Study. For Albuquerque Bernalillo County Water Utility Authority. December 1, 2011. |
| 7 | 2008, Schultdt, Marc, and Debra Tachibana. Energy related Water Fixture Measurements: Securing the Baseline for Northwest Single Family Homes. 2008 ACEEE Summer Study on Energy Efficiency in Buildings. |

**Measure Code: RS-HWE-LFFA-V04-140601**

### Low Flow Faucet Aerators

This measure relates to the installation of a low flow faucet aerator in a household kitchen or bath faucet fixture.

This measure may be used for units provided through Efficiency Kit’s however the in service rate for such measures should be derived through evaluation results specifically for this implementation methodology.

This measure was developed to be applicable to the following program types:  TOS, NC, RF, DI, KITS.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a low flow faucet aerator, for bathrooms rated at 1.5 gallons per minute (GPM) or less, or for kitchens rated at 2.2 GPM or less. Savings are calculated on an average savings per faucet fixture basis.

###### Definition of Baseline Equipment

The baseline condition is assumed to be a standard bathroom faucet aerator rated at 2.25 GPM or greater, or a standard kitchen faucet aerator rated at 2.75 GPM or greater. Average measured flow rates are used in the algorithm and are lower, reflecting the penetration of previously installed low flow fixtures (and therefore the freerider rate for this measure should be 0), use of the faucet at less than full flow, debris buildup, and lower water system pressure than fixtures are rated at.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 9 years.[[1120]](#footnote-1121)

###### Deemed Measure Cost

The incremental cost for this measure is $8[[1121]](#footnote-1122) or program actual.

For faucet aerators provided in Efficiency Kits, the actual program delivery costs should be utilized.

###### Loadshape

Loadshape R03 - Residential Electric DHW

###### Coincidence Factor

The coincidence factor for this measure is assumed to be 2.2%.[[1122]](#footnote-1123)

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

###### Note these savings are *per* faucet retrofitted[[1123]](#footnote-1124) (unless faucet type is unknown, then it is per household).

ΔkWh = %ElectricDHW \* ((GPM\_base \* L\_base - GPM\_low \* L\_low) \* Household \* 365.25 \*DF / FPH) \* EPG\_electric \* ISR

Where:

%ElectricDHW = proportion of water heating supplied by electric resistance heating

|  |  |
| --- | --- |
| **DHW fuel** | **%ElectricDHW** |
| Electric | 100% |
| Natural Gas | 0% |
| Unknown | 16%[[1124]](#footnote-1125) |

GPM\_base = Average flow rate, in gallons per minute, of the baseline faucet “as-used.” This includes the effect of existing low flow fixtures and therefore the freerider rate for this measure should be 0.

= 1.39[[1125]](#footnote-1126) or custom based on metering studies[[1126]](#footnote-1127) or if measured during DI:

= Measured full throttle flow \* 0.83 throttling factor[[1127]](#footnote-1128)

GPM\_low = Average flow rate, in gallons per minute, of the low-flow faucet aerator “as-used”

= 0.94[[1128]](#footnote-1129) or custom based on metering studies[[1129]](#footnote-1130) or if measured during DI:

= Rated full throttle flow \* 0.95 throttling factor[[1130]](#footnote-1131)

L\_base = Average baseline daily length faucet use per capita for faucet of interest in minutes

= if available custom based on metering studies, if not use:

|  |  |
| --- | --- |
| **Faucet Type** | **L\_base (min/person/day)** |
| Kitchen | 4.5[[1131]](#footnote-1132) |
| Bathroom | 1.6[[1132]](#footnote-1133) |
| If location unknown (total for household): Single-Family | 9.0[[1133]](#footnote-1134) |
| If location unknown (total for household): Multi-Family | 6.9[[1134]](#footnote-1135) |

L\_low = Average retrofit daily length faucet use per capita for faucet of interest in minutes

= if available custom based on metering studies, if not use:

|  |  |
| --- | --- |
| **Faucet Type** | **L\_low (min/person/day)** |
| Kitchen | 4.5[[1135]](#footnote-1136) |
| Bathroom | 1.6[[1136]](#footnote-1137) |
| If location unknown (total for household): Single-Family | 9.0[[1137]](#footnote-1138) |
| If location unknown (total for household): Multi-Family | 6.9[[1138]](#footnote-1139) |

Household = Average number of people per household

|  |  |
| --- | --- |
| **Household Unit Type** | **Household** |
| Single-Family - Deemed | 2.56[[1139]](#footnote-1140) |
| Multi-Family - Deemed | 2.1[[1140]](#footnote-1141) |
| Custom | Actual Occupancy or Number of Bedrooms[[1141]](#footnote-1142) |

365.25 = Days in a year, on average.

DF = Drain Factor

|  |  |
| --- | --- |
| **Faucet Type** | **Drain Factor[[1142]](#footnote-1143)** |
| Kitchen | 75% |
| Bath | 90% |
| Unknown | 79.5% |

FPH = Faucets Per Household

|  |  |
| --- | --- |
| **Faucet Type** | **FPH** |
| Kitchen Faucets Per Home (KFPH) | 1 |
| Bathroom Faucets Per Home (BFPH): Single-Family | 2.83[[1143]](#footnote-1144) |
| Bathroom Faucets Per Home (BFPH): Multi-Family | 1.5[[1144]](#footnote-1145) |
| If location unknown (total for household): Single-Family | 3.83 |
| If location unknown (total for household): Multi-Family | 2.5 |

EPG\_electric = Energy per gallon of water used by faucet supplied by electric water heater

= (8.33 \* 1.0 \* (WaterTemp - SupplyTemp)) / (RE\_electric \* 3412)

= (8.33 \* 1.0 \* (86 – 54.1)) / (0.98 \* 3412)

= 0.0795 kWh/gal (Bath), 0.0969 kWh/gal (Kitchen), 0.0919 kWh/gal (Unknown)

8.33 = Specific weight of water (lbs/gallon)

1.0 = Heat Capacity of water (btu/lb-°F)

WaterTemp = Assumed temperature of mixed water

= 86F for Bath, 93F for Kitchen 91F for Unknown[[1145]](#footnote-1146)

SupplyTemp = Assumed temperature of water entering house

= 54.1F [[1146]](#footnote-1147)

RE\_electric = Recovery efficiency of electric water heater

= 98% [[1147]](#footnote-1148)

3412 = Converts Btu to kWh (btu/kWh)

ISR = In service rate of faucet aerators dependant on install method as listed in table below

|  |  |
| --- | --- |
| **Selection** | **ISR** |
| Direct Install - Single Family | 0.95[[1148]](#footnote-1149) |
| Direct Install – Multi Family Kitchen | 0.91[[1149]](#footnote-1150) |
| Direct Install – Multi Family Bathroom | 0.95[[1150]](#footnote-1151) |
| Efficiency Kits | To be determined through evaluation |

For example, a direct installed kitchen low flow faucet aerator in a single-family electric DHW home:

ΔkWh = 1.0 \* (((1.39 \* 4.5 – 0.94 \* 4.5) \* 2.56 \* 365.25 \*0.75) / 1) \* 0.0969 \* 0.95

= 131 kWh

For example, a direct installed bath low flow faucet aerator in a multi-family electric DHW home:

ΔkWh = 1.0 \* (((1.39 \* 1.6 – 0.94 \* 1.6) \* 2.1 \* 365.25 \* 0.90) /1.5) \* 0.0795 \* 0.95

= 25.0 kWh

For example, a direct installed low flow faucet aerator in unknown faucet in a single-family electric DHW home:

ΔkWh = 1.0 \* (((1.39 \* 9.0 – 0.94 \* 9.0) \* 2.56 \* 365.25 \* 0.795) /3.83) \* 0.0919 \* 0.95

= 68.6 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = ΔkWh / Hours \* CF

Where:

ΔkWh = calculated value above

Hours = Annual electric DHW recovery hours for faucet use per faucet

= ((GPM\_base \* L\_base) \* Household/FPH \* 365.25 \* DF ) \* 0.545[[1151]](#footnote-1152) / GPH

|  |  |  |  |
| --- | --- | --- | --- |
| **Building Type** | **Faucet location** | **Calculation** | **Hours per faucet** |
| Single Family | Kitchen | ((1.39 \* 4.5) \* 2.56/1 \* 365.25 \* 0.75) \* 0.545 / 25.5 | 94 |
| Bathroom | ((1. 39 \* 1.6) \* 2.56/2.83 \* 365.25 \* 0.9) \* 0.545 / 25.5 | 14 |
| Unknown | ((1. 39 \* 9.0) \* 2.56/3.83 \* 365.25 \* 0.795) \* 0.545 / 25.5 | 52 |
| Multi Family | Kitchen | ((1. 39 \* 4.5) \* 2.1/1 \* 365.25 \* 0.75) \* 0.545 / 25.5 | 77 |
| Bathroom | ((1. 39 \* 1.6) \* 2.1/1.5 \* 365.25 \* 0.9) \* 0.545 / 25.5 | 22 |
| Unknown | ((1. 39 \* 6.9) \* 2.1/2.5 \* 365.25 \* 0.795) \* 0.545 / 25.5 | 50 |

GPH = Gallons per hour recovery of electric water heater calculated for 70.9F temp rise (125-54.1), 98% recovery efficiency, and typical 4.5kW electric resistance storage tank.

= 25.5

CF = Coincidence Factor for electric load reduction

= 0.022[[1152]](#footnote-1153)

For example, a direct installed kitchen low flow faucet aerator in a single family electric DHW home:

ΔkW = 131/94 \* 0.022

= 0.0306 kW

###### Natural Gas Savings

ΔTherms = %FossilDHW \* ((GPM\_base \* L\_base - GPM\_low \* L\_low) \* Household \* 365.25 \*DF / FPH) \* EPG\_gas \* ISR

Where:

%FossilDHW = proportion of water heating supplied by Natural Gas heating

|  |  |
| --- | --- |
| **DHW fuel** | **%Fossil\_DHW** |
| Electric | 0% |
| Natural Gas | 100% |
| Unknown | 84%[[1153]](#footnote-1154) |

EPG\_gas = Energy per gallon of Hot water supplied by gas

= (8.33 \* 1.0 \* (WaterTemp - SupplyTemp)) / (RE\_gas \* 100,000)

= 0.00341 Therm/gal for SF homes (Bath), 0.00415 Therm/gal for SF homes (Kitchen), 0.00394 Therm/gal for SF homes (Unknown)

= 0.00397 Therm/gal for MF homes (Bath), 0.00484 Therm/gal for MF homes (Kitchen), 0.00459 Therm/gal for MF homes (Unknown)

RE\_gas = Recovery efficiency of gas water heater

= 78% For SF homes[[1154]](#footnote-1155)

= 67% For MF homes[[1155]](#footnote-1156)

100,000 = Converts Btus to Therms (btu/Therm)

Other variables as defined above.

For example, a direct-installed kitchen low flow faucet aerator in a fuel DHW single-family home:

ΔTherms = 1.0 \* (((1.39 \* 4.5 – 0.94 \* 4.5) \* 2.56 \* 365.25 \*0.75) / 1) \* 0.00415 \* 0.95

= 5.60 Therms

For example, a direct installed bath low flow faucet aerator in a fuel DHW multi-family home:

ΔTherms = 1.0 \* (((1.39 \* 1.6 – 0.94 \* 1.6) \* 2.1 \* 365.25 \* 0.90) /1.5) \* 0.003974 \* 0.95

= 1.25 Therms

For example, a direct installed low flow faucet aerator in unknown faucet in a fuel DHW single-family home:

ΔTherms = 1.0 \* (((1.39 \* 6.1– 0.94 \* 6.1) \* 2.56 \* 365.25 \* 0.795) /3.83) \* 0.00394 \* 0.95

= 1.99 Therms

###### Water Impact Descriptions and Calculation

Δgallons = ((GPM\_base \* L\_base - GPM\_low \* L\_low) \* Household \* 365.25 \*DF / FPH) \* ISR

Variables as defined above

For example, a direct-installed kitchen low flow aerator in a single family home

Δgallons = (((1.39 \* 4.5 – 0.94 \* 4.5) \* 2.56 \* 365.25 \*0.75) / 1) \* 0.95

= 1350 gallons

For example, a direct installed bath low flow faucet aerator in a multi-family home:

Δgallons = (((1.39 \* 1.6 – 0.94 \* 1.6) \* 2.1 \* 365.25 \* 0.90) /1.5) \* 0.95

= 314 gallons

For example, a direct installed low flow faucet aerator in unknown faucet in a single-family home:

Δgallons = (((1.39 \* 9.0 – 0.94 \* 9.0) \* 2.56 \* 365.25 \* 0.795) /3.83) \* 0.95

= 747 gallons

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Sources

|  |  |
| --- | --- |
| **Source ID** | **Reference** |
| 1 | 2011, DeOreo, William. California Single Family Water Use Efficiency Study. April 20, 2011. |
| 2 | 2000, Mayer, Peter, William DeOreo, and David Lewis. Seattle Home Water Conservation Study. December 2000. |
| 3 | 1999, Mayer, Peter, William DeOreo. Residential End Uses of Water. Published by AWWA Research Foundation and American Water Works Association. 1999. |
| 4 | 2003, Mayer, Peter, William DeOreo. Residential Indoor Water Conservation Study. Aquacraft, Inc. Water Engineering and Management. Prepared for East Bay Municipal Utility District and the US EPA. July 2003. |
| 5 | 2011, DeOreo, William. Analysis of Water Use in New Single Family Homes. By Aquacraft. For Salt Lake City Corporation and US EPA. July 20, 2011. |
| 6 | 2011, Aquacraft. Albuquerque Single Family Water Use Efficiency and Retrofit Study. For Albuquerque Bernalillo County Water Utility Authority. December 1, 2011. |
| 7 | 2008, Schultdt, Marc, and Debra Tachibana. Energy related Water Fixture Measurements: Securing the Baseline for Northwest Single Family Homes. 2008 ACEEE Summer Study on Energy Efficiency in Buildings. |

###### Measure Code: RS-HWE-LFFA-V03-140601

### Low Flow Showerheads

###### Description

This measure relates to the installation of a low flow showerhead in a single or multi-family household.

This measure may be used for units provided through Efficiency Kit’s however the in service rate for such measures should be derived through evaluation results specifically for this implementation methodology.

This measure was developed to be applicable to the following program types:  TOS, RF, NC, DI, KITS.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the installed equipment must be a low flow showerhead rated at 2.0 gallons per minute (GPM) or less. Savings are calculated on a per showerhead fixture basis.

###### Definition of Baseline Equipment

For Direct-install programs, the baseline condition is assumed to be a standard showerhead rated at 2.5 GPM or greater.

For retrofit and time-of-sale programs, the baseline condition is assumed to be a representative average of existing showerhead flow rates of participating customers including a range of low flow showerheads, standard-flow showerheads, and high-flow showerheads.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 10 years.[[1156]](#footnote-1157)

###### Deemed Measure Cost

The incremental cost for this measure is $12[[1157]](#footnote-1158) or program actual.

For low flow showerheads provided in Efficiency Kits, the actual program delivery costs should be utilized.

###### Loadshape

Loadshape R03 - Residential Electric DHW

###### Coincidence Factor

The coincidence factor for this measure is assumed to be 2.78%.[[1158]](#footnote-1159)

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

Note these savings are per showerhead fixture

ΔkWh = %ElectricDHW \* ((GPM\_base \* L\_base - GPM\_low \* L\_low) \* Household \* SPCD \* 365.25 / SPH) \* EPG\_electric \* ISR

Where:

%ElectricDHW = proportion of water heating supplied by electric resistance heating

|  |  |
| --- | --- |
| **DHW fuel** | **%ElectricDHW** |
| Electric | 100% |
| Natural Gas | 0% |
| Unknown | 16%[[1159]](#footnote-1160) |

GPM\_base = Flow rate of the baseline showerhead

|  |  |
| --- | --- |
| **Program** | **GPM\_base** |
| Direct-install | 2.67[[1160]](#footnote-1161) |
| Retrofit or TOS | 2.35[[1161]](#footnote-1162) |

GPM\_low = As-used flow rate of the low-flow showerhead, which may, as a result of measurements of program evaulations deviate from rated flows, see table below:

|  |
| --- |
| **Rated Flow** |
| 2.0 GPM |
| 1.75 GPM |
| 1.5 GPM |
| Custom or Actual[[1162]](#footnote-1163) |

L\_base = Shower length in minutes with baseline showerhead

= 7.8 min[[1163]](#footnote-1164)

L\_low = Shower length in minutes with low-flow showerhead

= 7.8 min[[1164]](#footnote-1165)

Household = Average number of people per household

|  |  |
| --- | --- |
| **Household Unit Type[[1165]](#footnote-1166)** | **Household** |
| Single-Family - Deemed | 2.56[[1166]](#footnote-1167) |
| Multi-Family - Deemed | 2.1[[1167]](#footnote-1168) |
| Custom | Actual Occupancy or Number of Bedrooms[[1168]](#footnote-1169) |

SPCD = Showers Per Capita Per Day

= 0.6[[1169]](#footnote-1170)

365.25 = Days per year, on average.

SPH = Showerheads Per Household so that per-showerhead savings fractions can be determined

|  |  |
| --- | --- |
| **Household Type** | **SPH** |
| Single-Family | 1.79[[1170]](#footnote-1171) |
| Multi-Family | 1.3[[1171]](#footnote-1172) |
| Custom | Actual |

EPG\_electric = Energy per gallon of hot water supplied by electric

= (8.33 \* 1.0 \* (ShowerTemp - SupplyTemp)) / (RE\_electric \* 3412)

= (8.33 \* 1.0 \* (101 – 54.1)) / (0.98 \* 3412)

= 0.117 kWh/gal

8.33 = Specific weight of water (lbs/gallon)

1.0 = Heat Capacity of water (btu/lb-°)

ShowerTemp = Assumed temperature of water

= 101F [[1172]](#footnote-1173)

SupplyTemp = Assumed temperature of water entering house

= 54.1F [[1173]](#footnote-1174)

RE\_electric = Recovery efficiency of electric water heater

= 98% [[1174]](#footnote-1175)

3412 = Converts Btu to kWh (btu/kWh)

ISR = In service rate of showerhead

= Dependant on program delivery method as listed in table below

|  |  |
| --- | --- |
| **Selection** | **ISR** |
| Direct Install - Single Family | 0.98**[[1175]](#footnote-1176)** |
| Direct Install – Multi Family | 0.95[[1176]](#footnote-1177) |
| Efficiency Kits | To be determined through evaluation |

For example, a direct-installed 1.5 GPM low flow showerhead in a single family home with electric DHW where the number of showers is not known:

ΔkWh = 1.0 \* ((2.67 \* 7.8 – 1.5 \* 7.8) \* 2.56 \* 0.6 \* 365.25 / 1.79) \* 0.117 \* 0.98

= 328 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = ΔkWh/Hours \* CF

Where:

ΔkWh = calculated value above

Hours = Annual electric DHW recovery hours for showerhead use

= ((GPM\_base \* L\_base) \* Household \* SPCD \* 365.25 ) \* 0.712[[1177]](#footnote-1178) / GPH

= 302 for SF Direct Install; 248 for MF Direct Install

= 266 for SF Retrofit and TOS; 218 for MF Retrofit and TOS

GPH = Gallons per hour recovery of electric water heater calculated for 65.9F temp rise (120-54.1), 98% recovery efficiency, and typical 4.5kW electric resistance storage tank.

= 27.51

CF = Coincidence Factor for electric load reduction

= 0.0278[[1178]](#footnote-1179)

For example, a direct installed 1.5 GPM low flow showerhead in a single family home with electric DHW where the number of showers is not known:

ΔkW = 328/302 \* 0.0278

= 0.0302 kW

###### Natural Gas Savings

ΔTherms = %FossilDHW \* ((GPM\_base \* L\_base - GPM\_low \* L\_low) \* Household \* SPCD \* 365.25 / SPH) \* EPG\_gas \* ISR

Where:

%FossilDHW = proportion of water heating supplied by Natural Gas heating

|  |  |
| --- | --- |
| **DHW fuel** | **%Fossil\_DHW** |
| Electric | 0% |
| Natural Gas | 100% |
| Unknown | 84%[[1179]](#footnote-1180) |

EPG\_gas = Energy per gallon of Hot water supplied by gas

= (8.33 \* 1.0 \* (ShowerTemp - SupplyTemp)) / (RE\_gas \* 100,000)

= 0.00501 Therm/gal for SF homes

= 0.00583 Therm/gal for MF homes

RE\_gas = Recovery efficiency of gas water heater

= 78% For SF homes[[1180]](#footnote-1181)

= 67% For MF homes[[1181]](#footnote-1182)

100,000 = Converts Btus to Therms (btu/Therm)

Other variables as defined above.

For example, a direct installed 1.5 GPM low flow showerhead in a gas fired DHW single family home where the number of showers is not known:

ΔTherms = 1.0 \* ((2.67 \* 7.8 – 1.5 \* 7.8) \* 2.56 \* 0.6 \* 365.25 / 1.79) \* 0.00501 \* 0.98

= 14.0 therms

###### Water Impact Descriptions and Calculation

Δgallons = ((GPM\_base \* L\_base - GPM\_low \* L\_low) \* Household \* SPCD \* 365.25 / SPH) \* ISR

Variables as defined above

For example, a direct installed 1.5 GPM low flow showerhead in a single family home where the number of showers is not known:

Δgallons = ((2.67 \* 7.8 – 1.5 \* 7.8) \* 2.56 \* 0.6 \* 365.25 / 1.79) \* 0.98

= 2803 gallons

###### Deemed O&M Cost Adjustment Calculation

N/A

**Sources**

|  |  |
| --- | --- |
| **Source ID** | **Reference** |
| 1 | 2011, DeOreo, William. California Single Family Water Use Efficiency Study. April 20, 2011. |
| 2 | 2000, Mayer, Peter, William DeOreo, and David Lewis. Seattle Home Water Conservation Study. December 2000. |
| 3 | 1999, Mayer, Peter, William DeOreo. Residential End Uses of Water. Published by AWWA Research Foundation and American Water Works Association. 1999. |
| 4 | 2003, Mayer, Peter, William DeOreo. Residential Indoor Water Conservation Study. Aquacraft, Inc. Water Engineering and Management. Prepared for East Bay Municipal Utility District and the US EPA. July 2003. |
| 5 | 2011, DeOreo, William. Analysis of Water Use in New Single Family Homes. By Aquacraft. For Salt Lake City Corporation and US EPA. July 20, 2011. |
| 6 | 2011, Aquacraft. Albuquerque Single Family Water Use Efficiency and Retrofit Study. For Albuquerque Bernalillo County Water Utility Authority. December 1, 2011. |
| 7 | 2008, Schultdt, Marc, and Debra Tachibana. Energy related Water Fixture Measurements: Securing the Baseline for Northwest Single Family Homes. 2008 ACEEE Summer Study on Energy Efficiency in Buildings. |

###### Measure Code: RS-HWE-LFSH-V03-140601

### Water Heater Temperature Setback

**Description**

This measure was developed to be applicable to the following program types:  NC, RF, DI, KITS.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

High efficiency is a hot water tank with the thermostat reduced to no lower than 120 degrees.

**Definition of Baseline Equipment**

The baseline condition is a hot water tank with a thermostat setting that is higher than 120 degrees, typically systems with settings of 130 degrees or higher. Note if there are more than one DHW tanks in the home at or higher than 130 degrees and they are all turned down, then the savings per tank can be multiplied by the number of tanks.

**Deemed Lifetime of Efficient Equipment**

The assumed lifetime of the measure is 2 years.

**Deemed Measure Cost**

The incremental cost of a setback is assumed to be $5 for contractor time, or no cost if the measure is self-installed.

**Loadshape**

Loadshape R03 - Residential Electric DHW

**Coincidence Factor**

The summer peak coincidence factor for this measure is assumed to be 1.

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

For homes with electric DHW tanks:

ΔkWh[[1182]](#footnote-1183)= (UA \* (Tpre – Tpost) \* Hours) / (3412 \* RE\_electric)

Where:

U = Overall heat transfer coefficient of tank (Btu/Hr-°F-ft­­2).

= Actual if known. If unknown assume R-12, U = 0.083

A = Surface area of storage tank (square feet)

= Actual if known. If unknown use table below based on capacity of tank. If capacity unknown assume 50 gal tank; A = 24.99ft2

|  |  |
| --- | --- |
| **Capacity (gal)** | **A (ft2)[[1183]](#footnote-1184)** |
| 30 | 19.16 |
| 40 | 23.18 |
| 50 | 24.99 |
| 80 | 31.84 |

Tpre = Actual hot water setpoint prior to adjustment

Tpost = Actual new hot water setpoint, which may not be lower than 120 degrees

|  |  |
| --- | --- |
| **Default Hot Water Temperature Inputs** | |
| Tpre | 135 |
| Tpost | 120 |

Hours = Number of hours in a year (since savings are assumed to be constant over year).

= 8766

3412 = Conversion from Btu to kWh

RE\_electric = Recovery efficiency of electric hot water heater

= 0.98 [[1184]](#footnote-1185)

A deemed savings assumption, where site specific assumptions are not available would be as follows:

ΔkWh= (UA \* (Tpre – Tpost) \* Hours) / (3412 \* RE\_electric)

= (((0.083 \* 24.99) \* (135 – 120) \* 8766) / (3412 \* 0.98)

= 81.6 kWh

**Summer Coincident Peak Demand Savings**

∆kW**=** ∆kWh/ Hours \* CF

Where:

Hours = 8766

CF = Summer Peak Coincidence Factor for measure

= 1

A deemed savings assumption, where site specific assumptions are not available would be as follows:

ΔkW = (81.6/ 8766) \* 1

ΔkW default = 0.00931 kW

**Natural Gas Savings**

For homes with gas water heaters:

ΔTherms= (UA \* (Tpre – Tpost) \* Hours) / (100,000 \* RE\_gas)

Where

100,000 = Converts Btus to Therms (btu/Therm)

RE\_gas = Recovery efficiency of gas water heater

= 78% For SF homes[[1185]](#footnote-1186)

= 67% For MF homes[[1186]](#footnote-1187)

A deemed savings assumption, where site specific assumptions are not available would be as follows:

For Single Family homes:

ΔTherms= (UA \* (Tpre – Tpost) \* Hours) / (RE\_gas)

= (((0.083 \* 24.99) \* (135 – 120) \* 8766) / (100,000 \* 0.78)

= 3.5 Therms

For Multi Family homes:

ΔTherms= (UA \* (Tpre – Tpost) \* Hours) / (RE\_gas)

= (((0.083 \* 24.99) \* (135 – 120) \* 8766) / (100,000 \* 0.67)

= 4.1 Therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: RS-HWE-TMPS-V04-150601**

### Water Heater Wrap

###### Description

This measure relates to a Tank Wrap or insulation “blanket” that is wrapped around the outside of a hot water tank to reduce stand-by losses. This measure applies only for homes that have an electric water heater that is not already well insulated. Generally this can be determined based upon the appearance of the tank.[[1187]](#footnote-1188)

This measure was developed to be applicable to the following program types: RF, DI.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The measure is a properly installed, R-8 or greater insulating tank wrap to reduce standby energy losses from the tank to the surrounding ambient area.

###### Definition of Baseline Equipment

The baseline is a standard electric domestic hot water tank without an additional tank wrap. Gas storage water heaters are excluded due to the limitations of retrofit wrapping and the associated impacts on reduced savings and safety.

###### Deemed Lifetime of Efficient Equipment

The measure life is assumed to be 5 years[[1188]](#footnote-1189).

###### Deemed Measure Cost

The incremental cost for this measure will be the actual material cost of procuring and labor cost of installing the tank wrap.

###### Loadshape

Loadshape R03 - Residential Electric DHW

###### Coincidence Factor

This measure assumes a flat loadshape and as such the coincidence factor is 1.

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

For electric DHW systems:

ΔkWh = ((UbaseAbase – UinsulAinsul) \* ΔT \* Hours) / (3412 \* ηDHW)

Where:

Ubase = Overall heat transfer coefficient prior to adding tank wrap (Btu/Hr-°F-ft­­2).

Uinsul  = Overall heat transfer coefficient after addition of tank wrap (Btu/Hr-°F-ft­­2).

Abase  = Surface area of storage tank prior to adding tank wrap (square feet)[[1189]](#footnote-1190)

Ainsul = Surface area of storage tank after addition of tank wrap (square feet)[[1190]](#footnote-1191)

ΔT = Average temperature difference between tank water and outside air temperature (°F)

= 60°F [[1191]](#footnote-1192)

Hours = Number of hours in a year (since savings are assumed to be constant over year).

= 8766

3412 = Conversion from Btu to kWh

ηDHW = Recovery efficiency of electric hot water heater

= 0.98 [[1192]](#footnote-1193)

The following table has default savings for various tank capacity and pre and post R-values.

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
| **Capacity (gal)** | **Rbase** | **Rinsul** | **Abase (ft2)[[1193]](#footnote-1194)** | **Ainsul (ft2)[[1194]](#footnote-1195)** | **ΔkWh** | **ΔkW** |
| 30 | 8 | 16 | 19.16 | 20.94 | 171 | 0.0195 |
| 30 | 10 | 18 | 19.16 | 20.94 | 118 | 0.0135 |
| 30 | 12 | 20 | 19.16 | 20.94 | 86 | 0.0099 |
| 30 | 8 | 18 | 19.16 | 20.94 | 194 | 0.0221 |
| 30 | 10 | 20 | 19.16 | 20.94 | 137 | 0.0156 |
| 30 | 12 | 22 | 19.16 | 20.94 | 101 | 0.0116 |
| 40 | 8 | 16 | 23.18 | 25.31 | 207 | 0.0236 |
| 40 | 10 | 18 | 23.18 | 25.31 | 143 | 0.0164 |
| 40 | 12 | 20 | 23.18 | 25.31 | 105 | 0.0120 |
| 40 | 8 | 18 | 23.18 | 25.31 | 234 | 0.0268 |
| 40 | 10 | 20 | 23.18 | 25.31 | 165 | 0.0189 |
| 40 | 12 | 22 | 23.18 | 25.31 | 123 | 0.0140 |
| 50 | 8 | 16 | 24.99 | 27.06 | 225 | 0.0257 |
| 50 | 10 | 18 | 24.99 | 27.06 | 157 | 0.0179 |
| 50 | 12 | 20 | 24.99 | 27.06 | 115 | 0.0131 |
| 50 | 8 | 18 | 24.99 | 27.06 | 255 | 0.0291 |
| 50 | 10 | 20 | 24.99 | 27.06 | 180 | 0.0206 |
| 50 | 12 | 22 | 24.99 | 27.06 | 134 | 0.0153 |
| 80 | 8 | 16 | 31.84 | 34.14 | 290 | 0.0331 |
| 80 | 10 | 18 | 31.84 | 34.14 | 202 | 0.0231 |
| 80 | 12 | 20 | 31.84 | 34.14 | 149 | 0.0170 |
| 80 | 8 | 18 | 31.84 | 34.14 | 328 | 0.0374 |
| 80 | 10 | 20 | 31.84 | 34.14 | 232 | 0.0265 |
| 80 | 12 | 22 | 31.84 | 34.14 | 173 | 0.0198 |

###### Summer Coincident Peak Demand Savings

∆kW**=** ∆kWh/ 8766 \* CF

Where:

ΔkWh = kWh savings from tank wrap installation

8766 = Number of hours in a year (since savings are assumed to be constant over year).

CF = Summer Coincidence Factor for this measure

= 1.0

The table above has default kW savings for various tank capacity and pre and post R-values.

###### Natural Gas Savings

N/A

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-HWE-WRAP-V02-150601

### Thermostatic Restrictor Shower Valve

**Description**

The measure is the installation of a thermostatic restrictor shower valve in a single or multi-family household. This is a valve attached to a residential showerhead which restricts hot water flow through the showerhead once the water reaches a set point (generally 95F or lower).

This measure was developed to be applicable to the following program types: RF, NC, DI. If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

To qualify for this measure the installed equipment must be a thermostatic restrictor shower valve installed on a residential showerhead.

**Definition of Baseline Equipment**

The baseline equipment is the residential showerhead without the restrictor valve installed.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 10 years. [[1195]](#footnote-1196)

**Deemed Measure Cost**

The incremental cost of the measure should be the actual program cost or $30[[1196]](#footnote-1197) if not available.

**Loadshape**

Loadshape R03 - Residential Electric DHW

**Coincidence Factor**

The coincidence factor for this measure is assumed to be 0.22%.[[1197]](#footnote-1198)

**Algorithm**

**Calculation of Energy Savings**

**Electric Energy Savings**

ΔkWh = %ElectricDHW \* ((GPM\_base\_S \* L\_showerdevice) \* Household \* SPCD \* 365.25 / SPH) \* ISR

Where:

%ElectricDHW = proportion of water heating supplied by electric resistance heating

|  |  |
| --- | --- |
| **DHW fuel** | **%ElectricDHW** |
| Electric | 100% |
| Natural Gas | 0% |
| Unknown | 16%[[1198]](#footnote-1199) |

GPM\_base\_S = Flow rate of the basecase showerhead, or actual if available

|  |  |
| --- | --- |
| **Program** | **GPM** |
| Direct-install, device only | 2.67[[1199]](#footnote-1200) |
| New Construction or direct install of device and low flow showerhead | Rated or actual flow of program-installed showerhead |
| Retrofit or TOS | 2.35[[1200]](#footnote-1201) |

L\_showerdevice = Hot water waste time avoided due to thermostatic restrictor valve

= 0.89 minutes[[1201]](#footnote-1202)

Household = Average number of people per household

|  |  |
| --- | --- |
| **Household Unit Type[[1202]](#footnote-1203)** | **Household** |
| Single-Family - Deemed | 2.56[[1203]](#footnote-1204) |
| Multi-Family - Deemed | 2.1[[1204]](#footnote-1205) |
| Custom | Actual Occupancy or Number of Bedrooms[[1205]](#footnote-1206) |

SPCD = Showers Per Capita Per Day

= 0.6[[1206]](#footnote-1207)

365.25 = Days per year, on average.

SPH = Showerheads Per Household so that per-showerhead savings fractions can be determined

|  |  |
| --- | --- |
| **Household Type** | **SPH** |
| Single-Family | 1.79[[1207]](#footnote-1208) |
| Multi-Family | 1.3[[1208]](#footnote-1209) |
| Custom | Actual |

EPG\_electric = Energy per gallon of hot water supplied by electric

= (8.33 \* 1.0 \* (ShowerTemp - SupplyTemp)) / (RE\_electric \* 3412)

= (8.33 \* 1.0 \* (101 – 54.1)) / (0.98 \* 3412)

= 0.117 kWh/gal

8.33 = Specific weight of water (lbs/gallon)

1.0 = Heat Capacity of water (btu/lb-°)

ShowerTemp = Assumed temperature of water

= 101F [[1209]](#footnote-1210)

SupplyTemp = Assumed temperature of water entering house

= 54.1F [[1210]](#footnote-1211)

RE\_electric = Recovery efficiency of electric water heater

= 98% [[1211]](#footnote-1212)

3412 = Converts Btu to kWh (btu/kWh)

ISR = In service rate of showerhead

= Dependent on program delivery method as listed in table below

|  |  |
| --- | --- |
| **Selection** | **ISR** |
| Direct Install - Single Family | 0.98**[[1212]](#footnote-1213)** |
| Direct Install – Multi Family | 0.95[[1213]](#footnote-1214) |
| Efficiency Kits | To be determined through evaluation |

**Example**

For example, a direct installed valve in a single-family home with electric DHW:

ΔkWh = 1.0 \* (2.67 \* 0.89 \* 2.56 \* 0.6 \* 365.25 / 1.79) \* 0.117 \* 0.98

= 85 kWh

**Summer Coincident Peak Demand Savings**

ΔkW = ΔkWh/Hours \* CF

Where:

ΔkWh = calculated value above

Hours = Annual electric DHW recovery hours for wasted showerhead use prevented by device

= ((GPM\_base\_S \* L\_showerdevice) \* Household \* SPCD \* 365.25 ) \* 0.712[[1214]](#footnote-1215) / GPH

GPH = Gallons per hour recovery of electric water heater calculated for 65.9F temp rise (120-54.1), 98% recovery efficiency, and typical 4.5kW electric resistance storage tank.

= 27.51

= 34.4 for SF Direct Install; 28.3 for MF Direct Install

= 30.3 for SF Retrofit and TOS; 24.8 for MF Retrofit and TOS

CF = Coincidence Factor for electric load reduction

= 0.0022[[1215]](#footnote-1216)

**Example**

For example, a direct installed thermostatic restrictor device in a single family home with electric DHW where the number of showers is not known.

ΔkW = 85.3/34.4 \* 0.0022

= 0.0055 kW

**Natural Gas Savings**

ΔTherms = %FossilDHW \* ((GPM\_base\_S \* L\_showerdevice)\* Household \* SPCD \* 365.25 / SPH) \* EPG\_gas \* ISR

Where:

%FossilDHW = proportion of water heating supplied by Natural Gas heating

|  |  |
| --- | --- |
| **DHW fuel** | **%Fossil\_DHW** |
| Electric | 0% |
| Natural Gas | 100% |
| Unknown | 84%[[1216]](#footnote-1217) |

EPG\_gas = Energy per gallon of Hot water supplied by gas

= (8.33 \* 1.0 \* (ShowerTemp - SupplyTemp)) / (RE\_gas \* 100,000)

= 0.00501 Therm/gal for SF homes

= 0.00583 Therm/gal for MF homes

RE\_gas = Recovery efficiency of gas water heater

= 78% For SF homes[[1217]](#footnote-1218)

= 67% For MF homes[[1218]](#footnote-1219)

100,000 = Converts Btus to Therms (btu/Therm)

Other variables as defined above.

**Example**

For example, a direct installed thermostatic restrictor device in a gas fired DHW single family home where the number of showers is not known:

ΔTherms = 1.0 \* ((2.67 \* 0.89) \* 2.56 \* 0.6 \* 365.25 / 1.79) \* 0.00501 \* 0.98

= 3.7 therms

**Water Impact Descriptions and Calculation**

Δgallons = ((GPM\_base\_S \* L\_showerdevice) \* Household \* SPCD \* 365.25 / SPH) \* ISR

Variables as defined above

**Example**

For example, a direct installed thermostatic restrictor device in a single family home where the number of showers is not known:

Δgallons = ((2.67 \* 0.89) \* 2.56 \* 0.6 \* 365.25 / 1.79) \* 0.98

= 730 gallons

**Deemed O&M Cost Adjustment Calculation**

N/A

**Sources**

|  |  |
| --- | --- |
| **Source ID** | **Reference** |
| 1 | 2011, DeOreo, William. California Single Family Water Use Efficiency Study. April 20, 2011. |
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| 3 | 1999, Mayer, Peter, William DeOreo. Residential End Uses of Water. Published by AWWA Research Foundation and American Water Works Association. 1999. |
| 4 | 2003, Mayer, Peter, William DeOreo. Residential Indoor Water Conservation Study. Aquacraft, Inc. Water Engineering and Management. Prepared for East Bay Municipal Utility District and the US EPA. July 2003. |
| 5 | 2011, DeOreo, William. Analysis of Water Use in New Single Family Homes. By Aquacraft. For Salt Lake City Corporation and US EPA. July 20, 2011. |
| 6 | 2011, Aquacraft. Albuquerque Single Family Water Use Efficiency and Retrofit Study. For Albuquerque Bernalillo County Water Utility Authority. December 1, 2011. |
| 7 | 2008, Schultdt, Marc, and Debra Tachibana. Energy related Water Fixture Measurements: Securing the Baseline for Northwest Single Family Homes. 2008 ACEEE Summer Study on Energy Efficiency in Buildings. |
| 8 | 2011, Lutz, Jim. “Water and Energy Wasted During Residential Shower Events: Findings from a Pilot Field Study of Hot Water Distribution Systems”, Energy Analysis Department Lawrence Berkeley National Laboratory, September 2011. |
| 9 | 2008, Water Conservation Program: ShowerStart Pilot Project White Paper, City of San Diego, CA. |
| 10 | 2012, Pacific Gas and Electric Company, Work Paper PGECODHW113, Low Flow Showerhead and Thermostatic Shower Restriction Valve, Revision # 4, August 2012. |
| 11 | 2008, “Simply & Cost Effectively Reducing Shower Based Warm-Up Waste: Increasing Convenience & Conservation by Attaching ShowerStart to Existing Showerheads”, ShowerStart LLC. |
| 12 | 2014, New York State Record of Revision to the TRM, Case 07-M-0548, June 19, 2014. |

**Measure Code: RS-HWE-TRVA-V01-150601**

## Lighting End Use

### ENERGY STAR Compact Fluorescent Lamp (CFL)

###### Description

A low wattage ENERGY STAR qualified compact fluorescent screw-in bulb (CFL) is installed in place of a baseline screw-in bulb.

This characterization assumes that the CFL is installed in a residential location. If the implementation strategy does not allow for the installation location to be known (e.g. an upstream retail program), a deemed split of 96% Residential and 4% Commercial assumptions should be used[[1219]](#footnote-1220).

Federal legislation stemming from the Energy Independence and Security Act of 2007 (EISA) required all general-purpose light bulbs between 40W and 100W to be approximately 30% more energy efficient than current incandescent bulbs. Production of 100W, standard efficacy incandescent lamps ended in 2012, followed by restrictions on 75W in 2013 and 60W and 40W in 2014. The baseline for this measure has therefore become bulbs (improved incandescent or halogen) that meet the new standard.

A provision in the EISA regulations requires that by January 1, 2020, all lamps meet efficiency criteria of at least 45 lumens per watt, in essence making the baseline equivalent to a current day CFL. Therefore the measure life (number of years that savings should be claimed) should be reduced once the assumed lifetime of the bulb exceeds 2020. Due to expected delay in clearing retail inventory and to account for the operating life of a halogen incandescent potentially spanning over 2020, this shift is assumed not to occur until mid-2020.

This measure was developed to be applicable to the following program types:  TOS, NC, DI, KITS.  If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

In order for this characterization to apply, the high-efficiency equipment must be a standard ENERGY STAR qualified compact fluorescent lamp.

###### Definition of Baseline Equipment

The baseline equipment is assumed to be an EISA qualified incandescent or halogen as provided in the table provided in the Electric Energy Savings section.

###### Deemed Lifetime of Efficient Equipment

Residential, Multi Family In unit bulbs and Unknown: The expected measure life (number of years that savings should be claimed) for bulbs installed June 2012 – May 2015 is assumed to be 5.2 years[[1220]](#footnote-1221). For bulbs installed June 2015 – May 2016, this would be reduced to 5 years and then for every subsequent year should be reduced by one year[[1221]](#footnote-1222).

Exterior bulbs: The expected measure life is 3.2 years[[1222]](#footnote-1223) for bulbs installed June 2012 – May 2016. For bulbs installed June 2017-May 2018 this would be reduced to 3 years.

###### Deemed Measure Cost

For the Retail (Time of Sale) measure, the incremental capital cost is $1.25 from June 2014 – May 2015, $1.6 from June 2015 to May 2016 and $1.70 from June 2017 to May 2018[[1223]](#footnote-1224).

For the Direct Install measure, the full cost of $2.50 per bulb should be used, plus $5 labor cost[[1224]](#footnote-1225) for a total of $7.50 per bulb. However actual program delivery costs should be utilized if available.

For bulbs provided in Efficiency Kits, the actual program delivery costs should be utilized.

###### Loadshape

|  |
| --- |
| Loadshape R06 - Residential Indoor Lighting |
| Loadshape R07 - Residential Outdoor Lighting |

###### Coincidence Factor

The summer peak coincidence factor is assumed to be 7.1% for Time of Sale Residential and in-unit Multi Family bulbs, 27.3% for exterior bulbs and 8.1% for unknown[[1225]](#footnote-1226) and 7.4% for Residential Direct Install[[1226]](#footnote-1227).

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

∆kWh = ((WattsBase - WattsEE) / 1000) \* ISR \* (1-Leakage) \* Hours \* WHFe

Where:

WattsBase = Based on lumens of CFL bulb and program year installed:

|  |  |  |
| --- | --- | --- |
| **Minimum Lumens** | **Maximum Lumens** | **Incandescent Equivalent**  **Post-EISA 2007**  **(WattsBase)** |
| 5280 | 6209 | 300 |
| 3000 | 5279 | 200 |
| 2601 | 2999 | 150 |
| 1490 | 2600 | 72 |
| 1050 | 1489 | 53 |
| 750 | 1049 | 43 |
| 310 | 749 | 29 |
| 250 | 309 | 25 |

WattsEE = Actual wattage of CFL purchased / installed

ISR = In Service Rate, the percentage of units rebated that are actually in service.

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
| **Program** | | **Weighted Average 1st Year In Service Rate (ISR)** | **2nd year Installations** | **3rd year Installations** | **Final Lifetime In Service Rate** |
| Retail (Time of Sale) | | 73.2%[[1227]](#footnote-1228) | 13.4% | 11.4% | 98.0%[[1228]](#footnote-1229) |
| Direct Install | | 96.9%[[1229]](#footnote-1230) |  |  |  |
| Efficiency Kits[[1230]](#footnote-1231) | CFL Distribution[[1231]](#footnote-1232) | 59% | 13% | 11% | 83% |
| School Kits[[1232]](#footnote-1233) | 61% | 13% | 11% | 86% |
| Direct Mail Kits[[1233]](#footnote-1234) | 66% | 14% | 12% | 93% |

Leakage = Adjustment to account for the percentage of bulbs purchased that move out (and in if deemed appropriate) of the Utility Jurisdiction.

Upstream (TOS) Lighting programs = Determined through evaluation[[1234]](#footnote-1235).

All other programs = 0

Hours = Average hours of use per year

| **Program Delivery** | **Installation Location** | **Hours[[1235]](#footnote-1236)** |
| --- | --- | --- |
| Retail(Time of Sale) and Efficiency Kits | Residential and in-unit Multi Family | 759 |
| Exterior | 2,475 [[1236]](#footnote-1237) |
| Unknown | 847 [[1237]](#footnote-1238) |
| Direct Install | Residential | 793 |

WHFe = Waste heat factor for energy to account for cooling energy savings from efficient lighting

|  |  |
| --- | --- |
| Bulb Location | WHFe |
| Interior single family or unknown location | 1.06 [[1238]](#footnote-1239) |
| Multi family in unit | 1.04 [[1239]](#footnote-1240) |
| Exterior or uncooled location | 1.0 | |

###### Deferred Installs

As presented above, the characterization assumes that a percentage of bulbs purchased are not installed until Year 2 and Year 3 (see ISR assumption above). The Illinois Technical Advisory Committee has determined the following methodology for calculating the savings of these future installs.

Year 1 (Purchase Year) installs: Characterized using assumptions provided above or evaluated assumptions if available.

Year 2 and 3 installs: Characterized using delta watts assumption and hours of use from the Install Year i.e. the actual deemed (or evaluated if available) assumptions active in Year 2 and 3 should be applied.

The NTG factor for the Purchase Year should be applied.

For example, for a 14W CFL (60W standard incandescent and 43W EISA qualified incandescent/halogen) purchased in 2014.

ΔkWH1st year installs = ((43 - 14) / 1000) \* 0.722 \* 847 \* 1.06

= 18.8 kWh

ΔkWH2nd year installs = ((43 - 14) / 1000) \* 0.139 \* 847 \* 1.06

= 3.6 kWh

Note: Here we assume no change in hours assumption. NTG value from Purchase year applied.

ΔkWH3rd year installs = ((43 - 14) / 1000) \* 0.119 \* 847 \* 1.06

= 3.1 kWh

###### Heating Penalty

If electric heated home (if heating fuel is unknown assume gas, see Natural Gas section):

∆kWh[[1240]](#footnote-1241) = - (((WattsBase - WattsEE) / 1000) \* ISR \* Hours \* HF) / ηHeat

Where:

HF = Heating Factor or percentage of light savings that must be heated

= 49%[[1241]](#footnote-1242) for interior or unknown location

= 0% for exterior or unheated location

ηHeat = Efficiency in COP of Heating equipment

= actual. If not available use[[1242]](#footnote-1243):

|  |  |  |  |
| --- | --- | --- | --- |
| **System Type** | **Age of Equipment** | **HSPF Estimate** | **ηHeat**  **(COP Estimate)** |
| Heat Pump | Before 2006 | 6.8 | 2.00 |
| 2006 - 2014 | 7.7 | 2.26 |
| 2015 on | 8.2 | 2.40 |
| Resistance | N/A | N/A | 1.00 |

For example, a 14W standard CFL is purchased in 2014 and installed in home with 2.0 COP Heat Pump:

∆kWh1st year = - (((43 - 14) / 1000) \* 0.722 \* 759 \* 0.49) / 2.0

= - 3.9 kWh

Second and third year install savings should be calculated using the appropriate ISR and the delta watts and hours from the install year.

###### Summer Coincident Peak Demand Savings

∆kW = ((WattsBase - WattsEE) / 1 000) \* ISR \* WHFd \* CF

Where:

WHFd = Waste heat factor for demand to account for cooling savings from efficient lighting.

|  |  |
| --- | --- |
| **Bulb Location** | **WHFd** |
| Interior single family or unknown location | 1.11[[1243]](#footnote-1244) |
| Multi family in unit | 1.07[[1244]](#footnote-1245) |
| Exterior or uncooled location | 1.0 |

CF = Summer Peak Coincidence Factor for measure.

|  |  |  |
| --- | --- | --- |
| **Program Delivery** | **Bulb Location** | **CF[[1245]](#footnote-1246)** |
| Retail(Time of Sale) | Interior single family or Multi Family in unit | 7.1% |
| Exterior | 27.3% |
| Unknown location | 8.1% |
| Direct Install | Residential | 7.4% |

Other factors as defined above

For example, a 14W standard CFL is purchased and installed in a single family interior location in 2014:

ΔkW = ((43 - 14) / 1000) \* 0.722 \* 1.11 \* 0.071

= 0.0017 kW

Second and third year install savings should be calculated using the appropriate ISR and the delta watts and hours from the install year.

###### Natural Gas Savings

Heating Penalty if Natural Gas heated home (or if heating fuel is unknown):

ΔTherms[[1246]](#footnote-1247) = - (((WattsBase - WattsEE) / 1000) \* ISR \* Hours \* HF \* 0.03412) / ηHeat

Where:

HF = Heating Factor or percentage of light savings that must be heated

= 49%[[1247]](#footnote-1248) for interior or unknown location

= 0% for exterior or unheated location

0.03412 =Converts kWh to Therms

ηHeat = Efficiency of heating system

=70%[[1248]](#footnote-1249)

For example, a14 standard CFL is purchased and installed in a home in 2014:

∆Therms = - (((43 - 14) / 1000) \* 0.722 \* 759 \* 0.49 \* 0.03412) / 0.7

= - 0.38 Therms

Second and third year install savings should be calculated using the appropriate ISR and the delta watts and hours from the install year.

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

Bulb replacement costs assumed in the O&M calculations are provided below[[1249]](#footnote-1250).

|  |  |  |
| --- | --- | --- |
|  | **Std Inc.** | **EISA Compliant Halogen** |
| 2014 | $0.34 | $1.25 |
| 2015 | $0.34 | $0.90 |
| 2016 | $0.34 | $0.80 |
| 2017 | $0.34 | $0.70 |
| 2018 | $0.34 | $0.60 |
| 2019 | $0.34 | $0.60 |
| 2020 & after | $0.34 | N/A |

In order to account for the falling EISA Qualified bulb replacement cost provided above, an equivalent annual levelized baseline replacement cost over the lifetime of the CFL bulb is calculated. Note that the measure life for these measures is capped to the number of years remaining until 2020.

The NPV for replacement lamps and annual levelized replacement costs using the statewide real discount rate of 5.23% are presented below:

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| **Location** | **Lumen Level** | **NPV of replacement costs for period** | | | **Levelized annual replacement cost savings** | | |
| **June 2015 - May 2016** | **June 2016 - May 2017** | **June 2017 - May 2018** | **June 2015 - May 2016** | **June 2016 - May 2017** | **June 2017 - May 2018** |
| Residential and in-unit Multi Family | Lumens <310 or >2600 (EISA exempt) | $0.86 | $0.66 | $0.45 | $0.19 | $0.15 | $0.13 |
| Lumens ≥ 310 and ≤ 2600 (EISA compliant) | $1.73 | $1.24 | $0.80 | $0.39 | $0.29 | $0.23 |
| Exterior | Lumens <310 or >2600 (EISA exempt) | $2.91 | $2.64 | $1.96 | $1.00 | $0.91 | $0.56 |
| Lumens ≥ 310 and ≤ 2600 (EISA compliant) | $6.21 | $5.31 | $3.60 | $2.14 | $1.83 | $1.02 |
| Unknown | Lumens <310 or >2600 (EISA exempt) | $0.97 | $0.74 | $0.51 | $0.22 | $0.17 | $0.14 |
| Lumens ≥ 310 and ≤ 2600 (EISA compliant) | $1.93 | $1.39 | $0.90 | $0.43 | $0.32 | $0.25 |

Note incandescent lamps in lumen range <310 and >2600 are exempt from EISA. For halogen bulbs, we assume the same replacement cycle as incandescent bulbs.[[1250]](#footnote-1251) The replacement cycle is based on the location of the lamp and varies based on the hours of use for that location. Both incandescent and halogen lamps are assumed to last for 1,000 hours before needing replacement.

###### Measure Code: RS-LTG-ESCF-V04-150601

### ENERGY STAR Specialty Compact Fluorescent Lamp (CFL)

###### Description

An ENERGY STAR qualified specialty compact fluorescent bulb is installed in place of an incandescent specialty bulb.

This characterization assumes that the specialty CFL is installed in a residential location. If the implementation strategy does not allow for the installation location to be known (e.g. an upstream retail program) a deemed split of 97% Residential and 3% Commercial assumptions should be used[[1251]](#footnote-1252).

This measure was developed to be applicable to the following program types:  TOS, NC, DI, KITS.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

Energy Star qualified specialty CFL bulb based upon the draft ENERGY STAR specification for lamps (<http://energystar.gov/products/specs/sites/products/files/ENERGY_STAR_Lamps_V1_0_Draft%203.pdf>).

###### Definition of Baseline Equipment

The baseline is a specialty incandescent light bulb including those exempt of the EISA 2007 standard: three-way, plant light, daylight bulb, bug light, post light, globes G40 (<40W), candelabra base (<60W), vibration service bulb, decorative candle with medium or intermediate base (<40W), shatter resistant and reflector bulbs and standard bulbs greater than 2601 lumens, and those non-exempt from EISA 2007: dimmable, globes (less than 5” diameter and >40W), candle (shapes B, BA, CA >40W, candelabra base lamps (>60W) and intermediate base lamps (>40W).

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 6.8 year[[1252]](#footnote-1253).

Exterior bulbs: The expected measure life is 3.2 years[[1253]](#footnote-1254) for bulbs installed June 2012 – May 2017. For bulbs installed June 2017-May 2018 this would be reduced to 3 years.

###### Deemed Measure Cost

For the Retail (Time of Sale) measure, the incremental capital cost for this measure is $5[[1254]](#footnote-1255).

For the Direct Install measure, the full cost of $8.50 should be used plus $5 labor[[1255]](#footnote-1256) for a total of $13.50. However actual program delivery costs should be utilized if available.

For bulbs provided in Efficiency Kits, the actual program delivery costs should be utilized..

###### Loadshape

|  |
| --- |
| Loadshape R06 - Residential Indoor Lighting |
| Loadshape R07 - Residential Outdoor Lighting |

###### Coincidence Factor

Unlike standard CFLs that could be installed in any room, certain types of specialty CFLs are more likely to be found in specific rooms, which affects the coincident peak factor. Coincidence factors by bulb types are presented below[[1256]](#footnote-1257)

|  |  |
| --- | --- |
| **Bulb Type** | **Peak CF** |
| Three-way | 0.078 |
| Dimmable | 0.078 |
| Interior reflector (incl. dimmable) | 0.091 |
| Exterior reflector | 0.273 |
| Candelabra base and candle medium and intermediate base | 0.121 |
| Bug light | 0.273 |
| Post light (>100W) | 0.273 |
| Daylight | 0.081 |
| Plant light | 0.081 |
| Globe | 0.075 |
| Vibration or shatterproof | 0.081 |
| Standard spirals >= 2601 lumens, Residential, Multi-family in unit | 0.071 |
| Standard spirals >= 2601 lumens, unknown | 0.081 |
| Standard spirals >= 2601 lumens, exterior | 0.273 |
| Specialty - Generic | 0.081 |

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

∆kWh = ((WattsBase - WattsEE) / 1000) \* ISR \* (1-Leakage) \* Hours \* WHFe

Where:

WattsBase = Actual wattage equivalent of incandescent specialty bulb, use the tables below to obtain the incandescent bulb equivalent wattage[[1257]](#footnote-1258); use 60W if unknown[[1258]](#footnote-1259)

EISA exempt bulb types:

| **Bulb Type** | **Lower Lumen Range** | **Upper Lumen Range** | **WattsBase** |
| --- | --- | --- | --- |
| **Standard Spirals >=2601** | 2601 | 2999 | 150 |
| 3000 | 5279 | 200 |
| 5280 | 6209 | 300 |
| **3-Way** | 250 | 449 | 25 |
| 450 | 799 | 40 |
| 800 | 1099 | 60 |
| 1100 | 1599 | 75 |
| 1600 | 1999 | 100 |
| 2000 | 2549 | 125 |
| 2550 | 2999 | 150 |
| **Globe**  **(medium and intermediate bases less than 750 lumens)** | 90 | 179 | 10 |
| 180 | 249 | 15 |
| 250 | 349 | 25 |
| 350 | 749 | 40 |
| **Decorative**  **(Shapes B, BA, C, CA, DC, F, G, medium and intermediate bases less than 750 lumens)** | 70 | 89 | 10 |
| 90 | 149 | 15 |
| 150 | 299 | 25 |
| 300 | 749 | 40 |
| **Globe**  **(candelabra bases less than 1050 lumens)** | 90 | 179 | 10 |
| 180 | 249 | 15 |
| 250 | 349 | 25 |
| 350 | 499 | 40 |
| 500 | 1049 | 60 |
| **Decorative**  **(Shapes B, BA, C, CA, DC, F, G, candelabra bases less than 1050 lumens)** | 70 | 89 | 10 |
| 90 | 149 | 15 |
| 150 | 299 | 25 |
| 300 | 499 | 40 |
| 500 | 1049 | 60 |
| **Reflector with medium screw bases w/ diameter <=2.25"** | 400 | 449 | 40 |
| 450 | 499 | 45 |
| 500 | 649 | 50 |
| 650 | 1199 | 65 |
| **R, PAR, ER, BR, BPAR or similar bulb shapes with medium screw bases w/ diameter >2.5" (\*see exceptions below)** | 640 | 739 | 40 |
| 740 | 849 | 45 |
| 850 | 1179 | 50 |
| 1180 | 1419 | 65 |
| 1420 | 1789 | 75 |
| 1790 | 2049 | 90 |
| 2050 | 2579 | 100 |
| 2580 | 3429 | 120 |
| 3430 | 4270 | 150 |
| **R, PAR, ER, BR, BPAR or similar bulb shapes with medium screw bases w/ diameter > 2.26'' and ≤ 2.5" (\*see exceptions below)** | 540 | 629 | 40 |
| 630 | 719 | 45 |
| 720 | 999 | 50 |
| 1000 | 1199 | 65 |
| 1200 | 1519 | 75 |
| 1520 | 1729 | 90 |
| 1730 | 2189 | 100 |
| 2190 | 2899 | 120 |
| 2900 | 3850 | 150 |
| **\*ER30, BR30, BR40, or ER40** | 400 | 449 | 40 |
| 450 | 499 | 45 |
| 500 | 649-1179[[1259]](#footnote-1260) | 50 |
| **\*BR30, BR40, or ER40** | 650 | 1419 | 65 |
| **\*R20** | 400 | 449 | 40 |
| 450 | 719 | 45 |
| **\*All reflector lamps**  **below lumen ranges specified above** | 200 | 299 | 20 |
| 300 | 399-639[[1260]](#footnote-1261) | 30 |

EISA non-exempt bulb types:

| **Bulb Type** | **Lower Lumen Range** | **Upper Lumen Range** | **Incandescent Equivalent**  **Post-EISA 2007**  **(WattsBase)** |
| --- | --- | --- | --- |
| **Dimmable Twist, Globe (less than 5" in diameter and > 749 lumens), candle (shapes B, BA, CA > 749 lumens), Candelabra Base Lamps (>1049 lumens), Intermediate Base Lamps (>749 lumens)** | 310 | 749 | 29 |
| 750 | 1049 | 43 |
| 1050 | 1489 | 53 |
| 1490 | 2600 | 72 |

WattsEE = Actual wattage of energy efficient specialty bulb purchased, use 15W if unknown[[1261]](#footnote-1262)

ISR = In Service Rate, the percentage of units rebated that are actually in service.

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
| **Program** | | **Weighted Average 1st year In Service Rate (ISR)** | **2nd year Installations** | **3rd year Installations** | **Final Lifetime In Service Rate** |
| Retail (Time of Sale) | | 88.0%[[1262]](#footnote-1263) | 5.4% | 4.6% | 98.0%[[1263]](#footnote-1264) |
| Direct Install | | 96.9%[[1264]](#footnote-1265) |  |  |  |
| Efficiency Kits[[1265]](#footnote-1266) | CFL Distribution[[1266]](#footnote-1267) | 59% | 13% | 11% | 83% |
| School Kits[[1267]](#footnote-1268) | 61% | 13% | 11% | 86% |
| Direct Mail Kits[[1268]](#footnote-1269) | 66% | 14% | 12% | 93% |

Leakage = Adjustment to account for the percentage of bulbs purchased that move out (and in if deemed appropriate) of the Utility Jurisdiction.

Upstream (TOS) Lighting programs = Determined through evaluation[[1269]](#footnote-1270).

All other programs = 0

Hours = Average hours of use per year, varies by bulb type as presented below:[[1270]](#footnote-1271)

|  |  |
| --- | --- |
| **Bulb Type** | **Annual hours of use (HOU)** |
| Three-way | 850 |
| Dimmable | 850 |
| Interior reflector (incl. dimmable) | 861 |
| Exterior reflector | 2475 |
| Candelabra base and candle medium and intermediate base | 1190 |
| Bug light | 2475 |
| Post light (>100W) | 2475 |
| Daylight | 847 |
| Plant light | 847 |
| Globe | 639 |
| Vibration or shatterproof | 847 |
| Standard Spiral >2601 lumens, Residential, Multi Family in-unit | 759 |
| Standard Spiral >2601 lumens, unknown | 847 |
| Standard Spiral >2601 lumens, Exterior | 2475 |
| Specialty - Generic | 847 |

WHFe = Waste heat factor for energy to account for cooling savings from efficient lighting

|  |  |
| --- | --- |
| **Bulb Location** | **WHFe** |
| Interior single family or unknown location | 1.06 [[1271]](#footnote-1272) |
| Multi family in unit | 1.04 [[1272]](#footnote-1273) |
| Exterior or uncooled location | 1.0 |

###### Deferred Installs

As presented above, the characterization assumes that a percentage of bulbs purchased are not installed until Year 2 and Year 3 (see ISR assumption above). The Illinois Technical Advisory Committee has determined the following methodology for calculating the savings of these future installs.

Year 1 (Purchase Year) installs: Characterized using assumptions provided above or evaluated assumptions if available.

Year 2 and 3 installs: Characterized using delta watts assumption and hours of use from the Install Year i.e. the actual deemed (or evaluated if available) assumptions active in Year 2 and 3 should be applied.

The NTG factor for the Purchase Year should be applied.

###### 

For example, for a 13W dimmable CFL impacted by EISA 2007 (60W standard incandescent and 43W EISA qualified incandescent/halogen) purchased in 2013.

ΔkWH1st year installs = ((60 - 13) / 1000) \* 0.823 \* 850 \* 1.06

= 34.9 kWh

ΔkWH2nd year installs = ((43 - 13) / 1000) \* 0.085 \* 850 \* 1.06

= 2.3 kWh

Note: Here we assume no change in hours assumption. NTG value from Purchase year applied.

ΔkWH3rd year installs = ((43 - 13) / 1000) \* 0.072 \* 850 \* 1.06

= 1.9 kWh

Note: delta watts is equivalent to install year. Here we assume no change in hours assumption.

###### Heating Penalty

If electric heated home (if heating fuel is unknown assume gas, see Natural Gas section):

∆kWh[[1273]](#footnote-1274)  = - (((WattsBase - WattsEE) / 1000) \* ISR \* Hours \* HF) / ηHeat

Where:

HF = Heating Factor or percentage of light savings that must be heated

= 49%[[1274]](#footnote-1275) for interior or unknown location

= 0% for exterior location

ηHeat = Efficiency in COP of Heating equipment

= actual. If not available use[[1275]](#footnote-1276):

|  |  |  |  |
| --- | --- | --- | --- |
| **System Type** | **Age of Equipment** | **HSPF Estimate** | **ηHeat**  **(COP Estimate)** |
| Heat Pump | Before 2006 | 6.8 | 2.00 |
| 2006 - 2014 | 7.7 | 2.26 |
| 2015 on | 8.2 | 2.40 |
| Resistance | N/A | N/A | 1.00 |

For example, a 15W globe CFL replacing a 60W incandescent specialty bulb installed in home with 2.0 COP Heat Pump:

∆kWh1st year    = - (((60 - 15) / 1000) \* 0.823 \* 639 \* 0.49) / 2.0

= - 5.8 kWh

Second and third year savings should be calculated using the appropriate ISR.

###### Summer Coincident Peak Demand Savings

∆kW =((WattsBase - WattsEE) / 1000) \* ISR \* WHFd \* CF

Where:

WHFd = Waste heat factor for demand to account for cooling savings from efficient lighting.

|  |  |
| --- | --- |
| **Bulb Location** | **WHFd** |
| Interior single family or unknown location | 1.11[[1276]](#footnote-1277) |
| Multi family in unit | 1.07[[1277]](#footnote-1278) |
| Exterior or uncooled location | 1.0 |

CF = Summer Peak Coincidence Factor for measure. Coincidence factors by bulb types are presented below[[1278]](#footnote-1279)

|  |  |
| --- | --- |
| **Bulb Type** | **Peak CF** |
| Three-way | 0.078[[1279]](#footnote-1280) |
| Dimmable | 0.078[[1280]](#footnote-1281) |
| Interior reflector (incl. dimmable) | 0.091 |
| Exterior reflector | 0.273 |
| Candelabra base and candle medium and intermediate base | 0.121 |
| Bug light | 0.273 |
| Post light (>100W) | 0.273 |
| Daylight | 0.081 |
| Plant light | 0.081 |
| Globe | 0.075 |
| Vibration or shatterproof | 0.081 |
| Standard Spiral >=2601 lumens, Residential, Multi-family in unit | 0.071 |
| Standard spirals >= 2601 lumens, unknown | 0.081 |
| Standard spirals >= 2601 lumens, exterior | 0.273 |
| Specialty - Generic | 0.081 |

Other factors as defined above

For example, a 15W specialty CFL replacing a 60W incandescent specialty bulb:

ΔkW1st year = ((60 - 15) / 1000) \* 0.823 \* 1.11 \* 0.081

= 0.003 kW

Second and third year savings should be calculated using the appropriate ISR.

###### Natural Gas Savings

Heating Penalty if Natural Gas heated home (or if heating fuel is unknown):

∆Therms[[1281]](#footnote-1282) = - (((WattsBase - WattsEE) / 1000) \* ISR \* Hours \* HF \* 0.03412) / ηHeat

Where:

HF = Heating Factor or percentage of light savings that must be heated

= 49%[[1282]](#footnote-1283) for interior or unknown location

= 0% for exterior location

0.03412 =Converts kWh to Therms

ηHeat = Efficiency of heating system

=70%[[1283]](#footnote-1284)

For example, a 15W Globe specialty CFL replacing a 60W incandescent specialty bulb:

∆Therms = - (((60 - 15) / 1000) \* 0. 823 \* 639 \* 0.49 \* 0.03412) / 0.7

= - 0.57 Therms

Second and third year savings should be calculated using the appropriate ISR.

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

For those bulbs types exempt from EISA the following O&M assumptions should be used: Life of the baseline bulb is assumed to be 1.32 year[[1284]](#footnote-1285); baseline replacement cost is assumed to be $3.5[[1285]](#footnote-1286).

For non-exempt EISA bulb types defined above, the following O&M assumptions should be used: Life of the baseline bulb is assumed to be 1.32 year[[1286]](#footnote-1287); baseline replacement cost is assumed to be $5[[1287]](#footnote-1288).

###### Measure Code: RS-LTG-ESCC-V03-150601

### ENERGY STAR Torchiere

###### Description

A high efficiency ENERGY STAR fluorescent torchiere is purchased in place of a baseline mix of halogen and incandescent torchieres and installed in a residential setting.

This measure was developed to be applicable to the following program types:  TOS, NC.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

To qualify for this measure the fluorescent torchiere must meet ENERGY STAR efficiency standards.

###### Definition of Baseline Equipment

The baseline is based on a mix of halogen and incandescent torchieres.

###### Deemed Lifetime of Efficient Equipment

The lifetime of the measure is assumed to be 8 years[[1288]](#footnote-1289).

###### Deemed Measure Cost

The incremental cost for this measure is assumed to be $5[[1289]](#footnote-1290).

###### Loadshape

|  |
| --- |
| Loadshape R06 - Residential Indoor Lighting |
| Loadshape R07 - Residential Outdoor Lighting |

###### Coincidence Factor

The summer peak coincidence factor for this measure is 7.1% for Residential and in-unit Multi Family bulbs and 8.1% for bulbs installed in unknown locations[[1290]](#footnote-1291)..

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = ((ΔWatts) /1000) \* ISR \* (1-Leakage) \* HOURS \* WHFe

Where:

ΔWatts = Average delta watts per purchased ENERGY STAR torchiere

= 115.8 [[1291]](#footnote-1292)

ISR = In Service Rate or percentage of units rebated that get installed.

= 0.86 [[1292]](#footnote-1293)

Leakage = Adjustment to account for the percentage of bulbs purchased that move out (and in if deemed appropriate) of the Utility Jurisdiction.

Upstream (TOS) Lighting programs = Determined through evaluation[[1293]](#footnote-1294).

All other programs = 0

HOURS = Average hours of use per year

|  |  |
| --- | --- |
| **Installation Location** | **Hours** |
| Residential and in-unit Multi Family | 1095 (3.0 hrs per day)[[1294]](#footnote-1295) |

WHFe = Waste Heat Factor for Energy to account for cooling savings from efficient lighting

|  |  |
| --- | --- |
| **Bulb Location** | **WHFe** |
| Interior single family or unknown location | 1.06 [[1295]](#footnote-1296) |
| Multi family in unit | 1.04 [[1296]](#footnote-1297) |
| Exterior or uncooled location | 1.0 |

For single family buildings:

ΔkWh = (115.8 /1000) \* 0.86 \* 1095 \* 1.06

= 116 kWh

For multi family in unit:

ΔkWh = (115.8 /1000) \* 0.86 \* 1095 \* 1.04

= 113 kWh

###### Heating Penalty

If electric heated home (if heating fuel is unknown assume gas, see Natural Gas section):

∆kWh[[1297]](#footnote-1298)  = - ((ΔWatts) /1000) \* ISR \* HOURS \* HF) / ηHeat

Where:

HF = Heating Factor or percentage of light savings that must be heated

= 49%[[1298]](#footnote-1299) for interior or unknown location

ηHeat = Efficiency in COP of Heating equipment

= Actual. If not available use defaults provided below[[1299]](#footnote-1300):

|  |  |  |  |
| --- | --- | --- | --- |
| **System Type** | **Age of Equipment** | **HSPF Estimate** | **ηHeat (COP Estimate)** |
| Heat Pump | Before 2006 | 6.8 | 2.00 |
| 2006 - 2014 | 7.7 | 2.26 |
| 2015 on | 8.2 | 2.40 |
| Resistance | N/A | N/A | 1.00 |

For example, an ES torchiere installed in a house with a newer heat pump:

ΔkWh = - ((115.8) / 1000) \* 0.86 \* 1095 \* 0.49) / 2.26

= - 23.6 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = ((ΔWatts) /1000) \* ISR \* WHFd \* CF

Where:

WHFd = Waste Heat Factor for Demand to account for cooling savings from efficient lighting

|  |  |  |
| --- | --- | --- |
| **Bulb Location** | **WHFd** | |
| Interior single family or unknown location | 1.11[[1300]](#footnote-1301) | |
| Multi family in unit | 1.07[[1301]](#footnote-1302) | |
| Exterior or uncooled location | 1.0 |

CF = Summer Peak Coincidence Factor for measure

|  |  |
| --- | --- |
| Bulb Location | CF**[[1302]](#footnote-1303)** |
| Interior single family or Multi family in unit | 7.1% |
| Unknown location | 8.1% |

For single family and multi-family in unit buildings:

ΔkW = (115.8 / 1000) \* 0.86 \* 1.11 \* 0.071

= 0.008kW

For unknown location:

ΔkW = (115.8 / 1000) \* 0.86 \* 1.07 \* 0.081

= 0.009 kW

###### Natural Gas Savings

Heating penalty if Natural Gas heated home, or if heating fuel is unknown.

∆ThermsWH= - (((ΔWatts) /1000) \* ISR \* HOURS \* 0.03412 \* HF) / ηHeat

Where:

∆ThermsWH = gross customer annual heating fuel increased usage for the measure from the reduction in lighting heat in therms.

0.03412 = conversion from kWh to therms

HF = Heating Factor or percentage of light savings that must be heated

= 49% [[1303]](#footnote-1304)

ηHeat = average heating system efficiency

= 70% [[1304]](#footnote-1305)

∆ThermsWH = - ((115.8 / 1000) \* 0.86 \* 1095 \* 0.03412 \* 0.49) / 0.70

= - 2.60 therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

Life of the baseline bulb is assumed to be 1.83 years[[1305]](#footnote-1306) for residential and multifamily in unit. Baseline bulb cost replacement is assumed to be $6.**[[1306]](#footnote-1307)**

###### Measure Code: RS-LTG-ESTO-V02-150601

### Exterior Hardwired Compact Fluorescent Lamp (CFL) Fixture

**Description**

An ENERGY STAR lighting fixture wired for exclusive use with pin-based compact fluorescent lamps is installed in an exterior residential setting. This measure could relate to either a fixture replacement or new installation (i.e. time of sale).

Federal legislation stemming from the Energy Independence and Security Act of 2007 required all general-purpose light bulbs between 40 and 100W to be approximately 30% more energy efficient than current incandescent bulbs. Production of 100W, standard efficacy incandescent lamps ends in 2012, followed by restrictions on 75W in 2013 and 60W and 40W in 2014. The baseline for this measure has therefore become bulbs (improved incandescent or halogen) that meet the new standard.

A provision in the EISA regulations requires that by January 1, 2020, all lamps meet efficiency criteria of at least 45 lumens per watt, in essence making the baseline equivalent to a current day CFL. Therefore the measure life (number of years that savings should be claimed) should be reduced once the assumed lifetime of the bulb exceeds 2020. Due to expected delay in clearing retail inventory and to account for the operating life of a halogen incandescent potentially spanning over 2020, this shift is assumed not to occur until mid-2020.

This measure was developed to be applicable to the following program types:  TOS, NC.  If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

The efficient condition is an ENERGY STAR lighting exterior fixture for pin-based compact fluorescent lamps.

**Definition of Baseline Equipment**

The baseline condition is a standard EISA qualified incandescent or halogen exterior fixture as provided in the table provided in the Electric Energy Savings section.

**Deemed Lifetime of Efficient Equipment**

The expected life of an exterior fixture is 20 years[[1307]](#footnote-1308). However due to the backstop provision in the Energy Independence and Security Act of 2007 that requires by January 1, 2020, all lamps meet efficiency criteria of at least 45 lumens per watt, the baseline replacement would become a CFL in that year. The expected measure life for CFL fixtures installed June 2012 – May 2013 is therefore assumed to be 8 years. For bulbs installed June 2013 – May 2014, this would be reduced to 7 years and should be reduced each year[[1308]](#footnote-1309).

**Deemed Measure Cost**

The incremental cost for an exterior fixture is assumed to be $32[[1309]](#footnote-1310).

**Loadshape**

|  |
| --- |
| Loadshape R07 - Residential Outdoor Lighting |

**Coincidence Factor**

The summer peak coincidence factor is assumed to be 27.3%[[1310]](#footnote-1311).

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

ΔkWh =((WattsBase - WattsEE) / 1000) \* ISR \* (1-Leakage) \* Hours

Where:

WattsBase = Based on lumens of CFL bulb and program year purchased:

|  |  |  |
| --- | --- | --- |
| **Minimum Lumens** | **Maximum Lumens** | **Incandescent Equivalent**  **Post-EISA 2007**  **(WattsBase)** |
| 5280 | 6209 | 300 |
| 3000 | 5279 | 200 |
| 2601 | 2999 | 150 |
| 1490 | 2600 | 72 |
| 1050 | 1489 | 53 |
| 750 | 1049 | 43 |
| 310 | 749 | 29 |
| 250 | 309 | 25 |

WattsEE = Actual wattage of CFL purchased

ISR = In Service Rate or the percentage of units rebated that get installed.

| **Program** | **Weighted Average 1st year In Service Rate (ISR)** | **2nd year Installations** | **3rd year Installations** | **Final Lifetime In Service Rate** |
| --- | --- | --- | --- | --- |
| Retail (Time of Sale) | 87.5%[[1311]](#footnote-1312) | 5.7% | 4.8% | 98.0%[[1312]](#footnote-1313) |
| Direct Install | 96.9[[1313]](#footnote-1314) |  |  |  |

Leakage = Adjustment to account for the percentage of bulbs purchased that move out (and in if deemed appropriate) of the Utility Jurisdiction.

Upstream (TOS) Lighting programs = Determined through evaluation[[1314]](#footnote-1315).

All other programs = 0

Hours = Average hours of use per year

=2475 (6.78 hrs per day)[[1315]](#footnote-1316)

**Deferred Installs**

As presented above, the characterization assumes that a percentage of bulbs purchased are not installed until Year 2 and Year 3 (see ISR assumption above). The Illinois Technical Advisory Committee has determined the following methodology for calculating the savings of these future installs.

Year 1 (Purchase Year) installs: Characterized using assumptions provided above or evaluated assumptions if available.

Year 2 and 3 installs: Characterized using delta watts assumption and hours of use from the Install Year i.e. the actual deemed (or evaluated if available) assumptions active in Year 2 and 3 should be applied.

The NTG factor for the Purchase Year should be applied.

For example, for a 2 x 14W pin based CFL fixture (43W EISA qualified incandescent/halogen) purchased in 2014.

ΔkWH1st year installs = ((86 - 28) / 1000) \* 0.875 \* 2475

= 125.6 kWh

ΔkWH2nd year installs = ((86 - 28) / 1000) \* 0.057 \* 2475

= 8.2 kWh

Note: Here we assume no change in hours assumption. NTG value from Purchase year applied.

ΔkWH3rd year installs = ((86 - 28) / 1000) \* 0.048 \* 2475

= 6.9 kWh

**Summer Coincident Peak Demand Savings**

ΔkW = ((WattsBase - WattsEE) / 1 000) \* ISR \* CF

Where:

CF = Summer Peak Coincidence Factor for measure.

= 27.3%[[1316]](#footnote-1317)

Other factors as defined above

For example, a 2 x 14W pin-based CFL fixture is purchased in 2013:

ΔkW1st year = ((86 - 28) / 1000) \* 0.875 \* 0.273

= 0.0142 kW

Second and third year install savings should be calculated using the appropriate ISR and the delta watts and hours from the install year.

**Natural Gas Savings**

N/A

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

Bulb replacement costs assumed in the O&M calculations are provided below[[1317]](#footnote-1318).

|  |  |  |
| --- | --- | --- |
|  | **Std Inc.** | **EISA Compliant Halogen** |
| 2014 | $0.34 | $1.25 |
| 2015 | $0.34 | $0.90 |
| 2016 | $0.34 | $0.80 |
| 2017 | $0.34 | $0.70 |
| 2018 | $0.34 | $0.60 |
| 2019 | $0.34 | $0.60 |
| 2020 & after | $0.34 | N/A |

In order to account for the falling EISA Qualified bulb replacement cost provided above, an equivalent annual levelized baseline replacement cost over the lifetime of the CFL bulb is calculated. Note that the measure life for these measures is capped to the number of years remaining until 2020 and that the efficient case also assumes replacement cost only if the first replacement occurs before the end of the measure life. The delta O&M cost should be used in cost effectiveness screening

The NPV for replacement lamps and annual levelized replacement costs using the statewide real discount rate of 5.23% are presented below:

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
| **Lumen Level** | **NPV of replacement costs for period** | | | **Levelized annual replacement cost savings** | | |
| **June 2015 - May 2016** | **June 2016 - May 2017** | **June 2017 - May 2018** | **June 2015 - May 2016** | **June 2016 - May 2017** | **June 2017 - May 2018** |
| Lumens <310 or >2600 (non-EISA compliant) | $3.30 | $2.64 | $1.96 | $0.65 | $0.61 | $0.56 |
| Lumens ≥ 310 and ≤ 2600 (EISA compliant) | $6.90 | $5.17 | $3.60 | $1.37 | $1.20 | $1.02 |
| Efficient bulb CFL | $0.06 | $0 - No replacement bulb within measure life | | $0.01 | $0 - No replacement bulb within measure life | |

For halogen bulbs, we assume the same replacement cycle as incandescent bulbs.[[1318]](#footnote-1319) The replacement cycle is based on the location of the lamp and varies based on the hours of use for that location. Both incandescent and halogen lamps are assumed to last for 1,000 hours before needing replacement, CFLs in Residential and in-unit multifamily assume 8000 hours and multifamily common areas assume 10,000 (longer run hours and less switching leads to longer lamp life).

**Measure Code: RS-LTG-EFIX-V04-150601**

### Interior Hardwired Compact Fluorescent Lamp (CFL) Fixture

###### Description

An ENERGY STAR lighting fixture wired for exclusive use with pin-based compact fluorescent lamps is installed in an interior residential setting. This measure could relate to either a fixture replacement or new installation (i.e. time of sale).

Federal legislation stemming from the Energy Independence and Security Act of 2007 required all general-purpose light bulbs between 40 and 100W to be approximately 30% more energy efficient than current incandescent bulbs. Production of 100W, standard efficacy incandescent lamps ends in 2012, followed by restrictions on 75W in 2013 and 60W and 40W in 2014. The baseline for this measure has therefore become bulbs (improved incandescent or halogen) that meet the new standard.

A provision in the EISA regulations requires that by January 1, 2020, all lamps meet efficiency criteria of at least 45 lumens per watt, in essence making the baseline equivalent to a current day CFL. Therefore the measure life (number of years that savings should be claimed) should be reduced once the assumed lifetime of the bulb exceeds 2020. Due to expected delay in clearing retail inventory and to account for the operating life of a halogen incandescent potentially spanning over 2020, this shift is assumed not to occur until mid-2020.

This measure was developed to be applicable to the following program types:  TOS, NC.  If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The efficient condition is an ENERGY STAR lighting interior fixture for pin-based compact fluorescent lamps.

###### Definition of Baseline Equipment

The baseline condition is a standard EISA qualified incandescent or halogen interior fixture as provided in the table provided in the Electric Energy Savings section.

###### Deemed Lifetime of Efficient Equipment

The expected life of an interior fixture is 20 years[[1319]](#footnote-1320). However due to the backstop provision in the Energy Independence and Security Act of 2007 that requires by January 1, 2020, all lamps meet efficiency criteria of at least 45 lumens per watt, the baseline replacement would become equivalent to a CFL in that year. The expected measure life for CFL fixtures installed June 2012 – May 2013 is therefore assumed to be 8 years. For bulbs installed June 2013 – May 2014, this would be reduced to 7 years and should be reduced each year[[1320]](#footnote-1321).

###### Deemed Measure Cost

The incremental cost for an interior fixture is assumed to be $32[[1321]](#footnote-1322).

###### Loadshape

|  |
| --- |
| Loadshape R06 - Residential Indoor Lighting |
|  |

###### Coincidence Factor

The summer peak coincidence factor is assumed to be 7.1%[[1322]](#footnote-1323) for Residential and in-unit Multi Family bulbs.

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = ((WattsBase - WattsEE) / 1000) \* ISR \* (1-Leakage) \* Hours \* WHFe

Where:

WattsBase = Based on lumens of CFL bulb and program year purchased:

|  |  |  |
| --- | --- | --- |
| **Minimum Lumens** | **Maximum Lumens** | **Incandescent Equivalent**  **Post-EISA 2007**  **(WattsBase)** |
| 5280 | 6209 | 300 |
| 3000 | 5279 | 200 |
| 2601 | 2999 | 150 |
| 1490 | 2600 | 72 |
| 1050 | 1489 | 53 |
| 750 | 1049 | 43 |
| 310 | 749 | 29 |
| 250 | 309 | 25 |

WattsEE = Actual wattage of CFL purchased

ISR = In Service Rate or the percentage of units rebated that get installed.

| **Program** | **Weighted Average 1st year In Service Rate (ISR)** | **2nd year Installations** | **3rd year Installations** | **Final Lifetime In Service Rate** |
| --- | --- | --- | --- | --- |
| Retail (Time of Sale) | 87.5%[[1323]](#footnote-1324) | 5.7% | 4.8% | 98.0%[[1324]](#footnote-1325) |
| Direct Install | 96.9[[1325]](#footnote-1326) |  |  |  |

Leakage = Adjustment to account for the percentage of bulbs purchased that move out (and in if deemed appropriate) of the Utility Jurisdiction.

Upstream (TOS) Lighting programs = Determined through evaluation[[1326]](#footnote-1327).

All other programs = 0

Hours = Average hours of use per year

|  |  |
| --- | --- |
| **Installation Location** | **Hours** |
| Residential and in-unit Multi Family | 759 [[1327]](#footnote-1328) |

WHFe = Waste heat factor for energy to account for cooling energy savings from efficient lighting

|  |  |
| --- | --- |
| **Bulb Location** | **WHFe** |
| Interior single family or unknown location | 1.06 [[1328]](#footnote-1329) |
| Multi family in unit | 1.04 [[1329]](#footnote-1330) |

###### Deferred Installs

As presented above, the characterization assumes that a percentage of bulbs purchased are not installed until Year 2 and Year 3 (see ISR assumption above). The Illinois Technical Advisory Committee has determined the following methodology for calculating the savings of these future installs.

Year 1 (Purchase Year) installs: Characterized using assumptions provided above or evaluated assumptions if available.

Year 2 and 3 installs: Characterized using delta watts assumption and hours of use from the Install Year i.e. the actual deemed (or evaluated if available) assumptions active in Year 2 and 3 should be applied.

The NTG factor for the Purchase Year should be applied.

For example, for a 2 x 14W pin based CFL fixture (43W EISA qualified incandescent/halogen) purchased in 2013.

ΔkWH1st year installs = ((86 - 28) / 1000) \* 0.875 \* 759 \* 1.06

= 40.8 kWh

ΔkWH2nd year installs = ((86 - 28) / 1000) \* 0.057 \* 759 \* 1.06

= 2.7 kWh

Note: Here we assume no change in hours assumption. NTG value from Purchase year applied.

ΔkWH3rd year installs = ((86 - 28) / 1000) \* 0.048 \* 759 \* 1.06

= 2.2 kWh

###### Heating Penalty

If electric heated building:

∆kWh[[1330]](#footnote-1331) = - (((WattsBase - WattsEE) / 1000) \* ISR \* Hours \* HF) / ηHeat

Where:

HF = Heating Factor or percentage of light savings that must be heated

= 49%[[1331]](#footnote-1332) for interior or unknown location

= 0% for unheated location

ηHeat = Efficiency in COP of Heating equipment

= actual. If not available use[[1332]](#footnote-1333):

|  |  |  |  |
| --- | --- | --- | --- |
| **System Type** | **Age of Equipment** | **HSPF Estimate** | **ηHeat**  **(COP Estimate)** |
| Heat Pump | Before 2006 | 6.8 | 2.00 |
| 2006 -2014 | 7.7 | 2.26 |
| 2015 on | 8.2 | 2.40 |
| Resistance | N/A | N/A | 1.00 |

For example, a 2 x 14W pin-based CFL fixture is purchased in 2013 and installed in home with 2.0 COP Heat Pump:

∆kWh1st year  = - (((86 – 28) / 1000) \* 0.875 \* 759 \* 0.49) / 2.0

= - 9.4 kWh

Second and third year install savings should be calculated using the appropriate ISR and the delta watts and hours from the install year.

###### Summer Coincident Peak Demand Savings

ΔkW = ((WattsBase - WattsEE) / 1 000) \* ISR \* WHFd \* CF

Where:

WHFd = Waste heat factor for demand to account for cooling savings from efficient lighting.

|  |  |
| --- | --- |
| Bulb Location | WHFd |
| Interior single family or unknown location | 1.11[[1333]](#footnote-1334) |
| Multi family in unit | 1.07[[1334]](#footnote-1335) |
| Exterior or uncooled location | 1.0 |

CF = Summer Peak Coincidence Factor for measure.

|  |  |
| --- | --- |
| **Bulb Location** | **CF[[1335]](#footnote-1336)** |
| Interior single family or unknown location | 7.1% |
| Multi family in unit | 7.1% |

Other factors as defined above

For example, a 14W pin-based CFL fixture is purchased in 2013:

∆kW1st year  = ((86- 28) / 1000) \* 0.875 \* 1.11 \* 0.071

= 0.004 kW

Second and third year install savings should be calculated using the appropriate ISR and the delta watts and hours from the install year.

###### Natural Gas Savings

ΔTherms[[1336]](#footnote-1337) = - (((WattsBase - WattsEE) / 1000) \* ISR \* Hours \* HF \* 0.03412) / ηHeat

Where:

HF = Heating Factor or percentage of light savings that must be heated

= 49%[[1337]](#footnote-1338) for interior or unknown location

= 0% for unheated location

0.03412 =Converts kWh to Therms

ηHeat = Efficiency of heating system

=70%[[1338]](#footnote-1339)

For example, a 2 x 14W pin-based CFL fixture is purchased in 2013 and installed in home with gas heat at 70% efficiency:

ΔTherms1st year  = -((86 - 28) / 1000) \* 0.875 \* 759 \* 0.49 \* 0.03412) / 0.7

= - 0.9 Therms

Second and third year install savings should be calculated using the appropriate ISR and the delta watts and hours from the install year.

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

Bulb replacement costs assumed in the O&M calculations are provided below[[1339]](#footnote-1340).

|  |  |  |
| --- | --- | --- |
|  | **Std Inc.** | **EISA Compliant Halogen** |
| 2014 | $0.34 | $1.25 |
| 2015 | $0.34 | $0.90 |
| 2016 | $0.34 | $0.80 |
| 2017 | $0.34 | $0.70 |
| 2018 | $0.34 | $0.60 |
| 2019 | $0.34 | $0.60 |
| 2020 & after | $0.34 | N/A |

In order to account for the falling EISA Qualified bulb replacement cost provided above, an equivalent annual levelized baseline replacement cost over the lifetime of the CFL bulb is calculated. Note that the measure life for these measures is capped to the number of years remaining until 2020 and that the efficient case also assumes replacement cost only if the first replacement occurs before the end of the measure life. The delta O&M cost should be used in cost effectiveness screening

The NPV for replacement lamps and annual levelized replacement costs using the statewide real discount rate of 5.23% are presented below:

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| **Location** | **Lumen Level** | **NPV of replacement costs for period** | | | **Levelized annual replacement cost savings** | | |
| **June 2015 - May 2016** | **June 2016 - May 2017** | **June 2017 - May 2018** | **June 2015 - May 2016** | **June 2016 - May 2017** | **June 2017 - May 2018** |
| Residential and in-unit Multi Family | Lumens <310 or >2600 (non-EISA compliant) | $0.86 | $0.66 | $0.45 | $0.17 | $0.15 | $0.13 |
| Lumens ≥ 310 and ≤ 2600 (EISA compliant) | $1.73 | $1.24 | $0.80 | $0.34 | $0.29 | $0.23 |
| Efficient bulb CFL | $0 - No replacement bulb within measure life | | | $0 - No replacement bulb within measure life | | |

For halogen bulbs, we assume the same replacement cycle as incandescent bulbs.[[1340]](#footnote-1341) The replacement cycle is based on the location of the lamp and varies based on the hours of use for that location. Both incandescent and halogen lamps are assumed to last for 1,000 hours before needing replacement, CFLs in Residential and in-unit multi family assume 8000 hours

###### Measure Code: RS-LTG-IFIX-V04-150601

### LED Downlights

**Description**

This measure describes savings from a variety of LED downlight lamp types. This characterization assumes that the LED lamp or fixture is installed in a residential location. Where the implementation strategy does not allow for the installation location to be known (e.g. an upstream retail program) evaluation data could be used to determine an appropriate residential v commercial split. If this is not available, it is recommended to use this residential characterization for all installs in unknown locations to be appropriately conservative in savings assumptions.

This measure was developed to be applicable to the following program types:  TOS, NC.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

To qualify for this measure the installed equipment must be an ENERGY STAR LED lamp or fixture.

**Definition of Baseline Equipment**

The baseline condition is assumed to be an incandescent/halogen lamp for all lamp types.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is given in the following table.[[1341]](#footnote-1342)

|  |  |
| --- | --- |
| **Bulb Type** | **Measure Life (yr)** |
| PAR20, PAR30, PAR38 screw-in lamps | 10 |
| MR16/PAR16 pin-based lamps | 10 |
| Recessed downlight luminaries | 15 |
| Track lights | 15 |

**Deemed Measure Cost**

The price of LED lamps is falling quickly. Where possible the actual cost should be used and compared to the baseline cost provided below. If the incremental cost is unknown, assume the following[[1342]](#footnote-1343):

|  |  |  |  |
| --- | --- | --- | --- |
| **Bulb Type** | **Baseline Cost** | **LED Cost** | **Incremental Cost** |
| PAR20, PAR30, PAR38 screw-in lamps | $4.00 | $44.00 | $40.00 |
| MR16/PAR16 pin-based lamps | $3.00 | $28.00 | $25.00 |
| Recessed downlight luminaries | $4.00 | $94.00 | $90.00 |
| Track lights | $4.00 | $60.00 | $56.00 |

**Loadshape**

|  |
| --- |
| Loadshape R06 - Residential Indoor Lighting |
| Loadshape R07 - Residential Outdoor Lighting |

**Coincidence Factor**

The summer Peak Coincidence Factor is assumed to be 9.1% for Residential and in-unit Multi Family bulbs, 27.3% for bulbs installed in Exterior locations, and 9.4% for bulbs installed in unknown locations[[1343]](#footnote-1344).

and 75%

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

∆kWh = ((WattsBase - WattsEE) / 1000) \* ISR \* (1-Leakage) \* Hours \* WHFe

Where:

WattsBase = Baseline lamp wattage of equivalent lumens

| **Bulb Type** | **Lower Lumen Range** | **Upper Lumen Range** | **WattsBase** |
| --- | --- | --- | --- |
| Reflector with medium screw bases w/ diameter <=2.25" | 400 | 449 | 40 |
| 450 | 499 | 45 |
| 500 | 649 | 50 |
| 650 | 1199 | 65 |
| R, PAR, ER, BR, BPAR or similar bulb shapes with medium screw bases w/ diameter >2.5" (\*see exceptions below) | 640 | 739 | 40 |
| 740 | 849 | 45 |
| 850 | 1179 | 50 |
| 1180 | 1419 | 65 |
| 1420 | 1789 | 75 |
| 1790 | 2049 | 90 |
| 2050 | 2579 | 100 |
| 2580 | 3429 | 120 |
| 3430 | 4270 | 150 |
| R, PAR, ER, BR, BPAR or similar bulb shapes with medium screw bases w/ diameter > 2.26'' and ≤ 2.5" (\*see exceptions below) | 540 | 629 | 40 |
| 630 | 719 | 45 |
| 720 | 999 | 50 |
| 1000 | 1199 | 65 |
| 1200 | 1519 | 75 |
| 1520 | 1729 | 90 |
| 1730 | 2189 | 100 |
| 2190 | 2899 | 120 |
| 2900 | 3850 | 150 |
| \*ER30, BR30, BR40, or ER40 | 400 | 449 | 40 |
| 450 | 499 | 45 |
| 500 | 649 | 50 |
| \*BR30, BR40, or ER40 | 650 | 1419 | 65 |
| \*R20 | 400 | 449 | 40 |
| 450 | 719 | 45 |
| \*All reflector lamps below lumen ranges specified above | 200 | 299 | 20 |
| 300 | 399 -639[[1344]](#footnote-1345) | 30 |

WattsEE = Actual wattage of energy efficient LED lamp purchased

ISR = In Service Rate or the percentage of units rebated that get installed[[1345]](#footnote-1346)

|  |  |
| --- | --- |
| **Bulb Type** | **ISR** |
| PAR20, PAR30, PAR38 screw-in lamps | 0.95 |
| MR16/PAR16 pin-based lamps | 0.95 |
| Recessed downlight luminaries | 1.0 |
| Track lights | 1.0 |

Leakage = Adjustment to account for the percentage of bulbs purchased that move out (and in if deemed appropriate) of the Utility Jurisdiction.

Upstream (TOS) Lighting programs = Determined through evaluation[[1346]](#footnote-1347).

All other programs = 0

Hours = Average hours of use per year

|  |  |
| --- | --- |
| **Installation Location** | **Hours[[1347]](#footnote-1348)** |
| Residential and in-unit Multi Family | 1,010861 |

|  |  |
| --- | --- |
| Unknown location | 891 |
| Exterior | 2475 |

WHFe = Waste heat factor for energy to account for cooling savings from efficient lighting

|  |  |
| --- | --- |
| **Bulb Location** | **WHFe** |
| Interior single family or unknown location | 1.06 [[1348]](#footnote-1349) |
| Multi family in unit | 1.04 [[1349]](#footnote-1350) |
| Exterior or uncooled location | 1.0 |

For example, a 13W PAR20 LED is installed in place of a 750 lumen PAR20 incandescent screw-in lamp with medium screw base, diameter >2.5", installed in single family interior location:

ΔkWh = ((45 - 13) / 1000) \* 0.95 \* 861 \* 1.06

= 27.7 kWh

**Heating Penalty**

If electric heated home (if heating fuel is unknown assume gas, see Natural Gas section):

∆kWh[[1350]](#footnote-1351)  = - (((WattsBase - WattsEE) / 1000) \* ISR \* Hours \* HF) / ηHeat

Where:

HF = Heating Factor or percentage of light savings that must be heated

= 49%[[1351]](#footnote-1352) for interior or unknown location

= 0% for exterior location

ηHeat = Efficiency in COP of Heating equipment

= Actual. If not available use:[[1352]](#footnote-1353)

|  |  |  |  |
| --- | --- | --- | --- |
| **System Type** | **Age of Equipment** | **HSPF Estimate** | **ηHeat (COP Estimate)** |
| Heat Pump | Before 2006 | 6.8 | 2.00 |
| After 2006 - 2014 | 7.7 | 2.26 |
| 2015 on | 8.2 | 2.40 |
| Resistance | N/A | N/A | 1.00 |

For example, a 13W PAR20 LED is installed in place of a 750 lumen PAR20 incandescent screw-in lamp with medium screw base, diameter >2.5",installed in single family interior location:

ΔkWh = - ((45 - 13) / 1000) \* 0.95 \* 861 \* 0.49) / 2.26

= - 5.67 kWh

**Summer Coincident Peak Demand Savings**

∆kW = ((WattsBase - WattsEE) / 1000) \* ISR \* WHFd \* CF

Where:

WHFd = Waste heat factor for demand to account for cooling savings from efficient lighting.

|  |  |
| --- | --- |
| **Bulb Location** | **WHFd** |
| Interior single family or unknown location | 1.11[[1353]](#footnote-1354) |
| Multi family in unit | 1.07[[1354]](#footnote-1355) |
| Exterior or uncooled location | 1.0 |

CF = Summer Peak Coincidence Factor for measure, see above for values.

|  |  |
| --- | --- |
| **Bulb Location** | **CF[[1355]](#footnote-1356)** |
| Interior single family or Multi-family in unit | 9.59.1% |
| Unknown Location | 9.4% |
| Exterior Locations | 27.3% |

Other factors as defined above

For example, a 13W PAR20 LED is installed in place of a 750 lumen PAR20 incandescent screw-in lamp with medium screw base, diameter >2.5", installed in single family interior location:

ΔkW = ((45 - 13) / 1000) \* 0.95 \* 1.11\* 0.091

= 0.0031 kW

**Natural Gas Savings**

Heating penalty if Natural Gas heated home, or if heating fuel is unknown.

Δtherms = - (((WattsBase - WattsEE) / 1000) \* ISR \* Hours \* HF \* 0.03412) / ηHeat

Where:

HF = Heating factor, or percentage of lighting savings that must be replaced by heating system.

= 49% [[1356]](#footnote-1357) for interior or unknown location

= 0% for exterior location

0.03412 = Converts kWh to Therms

ηHeat = Average heating system efficiency.

= 0.70 [[1357]](#footnote-1358)

Other factors as defined above

For example, a 13W PAR20 LED is installed in place of a 750 lumen PAR20 incandescent screw-in lamp with medium screw base, diameter >2.5", installed in single family interior location with gas heating at 70% total efficiency:

Δtherms = - (((45 - 13) / 1000) \* 0.95 \* 861 \* 0.49\* 0.03412) / 0.70

= - 0.63 therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

The life of the baseline bulb and the cost of its replacement is presented in the following table:

|  |  |  |  |
| --- | --- | --- | --- |
| **Lamp Type** | **Baseline Lamp Life (hours)** | **Baseline Life**  **(Single Family and in unit Multifamily - 1010 hours)** | **Baseline Replacement Cost** |
| PAR20, PAR30, PAR38 screw-in lamps | 2000 | 2.0 | $4.00 |
| MR16/PAR16 pin-based lamps | 2000 | 2.0 | $3.00 |
| Recessed downlight luminaries | 2000 | 2.0 | $4.00 |
| Track lights | 2000 | 2.0 | $4.00 |

**Measure Code: RS-LTG-LEDD-V04-150601**

### LED Exit Signs

###### Description

This measure characterizes the savings associated with installing a Light Emitting Diode (LED) exit sign in place of a fluorescent or incandescent exit sign in a MultiFamily building. Light Emitting Diode exit signs have a string of very small, typically red or green, glowing LEDs arranged in a circle or oval. The LEDs may also be arranged in a line on the side, top or bottom of the exit sign. LED exit signs provide the best balance of safety, low maintenance, and very low energy usage compared to other exit sign technologies.

This measure was developed to be applicable to the following program types:  TOS, NC, RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

The efficient equipment is assumed to be an exit sign illuminated by LEDs.

###### Definition of Baseline Equipment

The baseline equipment is assumed to be a fluorescent or incandescent model.

###### Deemed Lifetime of Efficient Equipment

The measure life is assumed to be 16 years[[1358]](#footnote-1359).

###### Deemed Measure Cost

The incremental cost for this measure is assumed to be $30[[1359]](#footnote-1360).

###### Loadshape

Loadshape C53 - Flat

###### Coincidence Factor

The summer peak coincidence factor for this measure is assumed to be 100%[[1360]](#footnote-1361).

**Algorithm**

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = ((WattsBase - WattsEE) / 1000) \* HOURS \* WHFe

Where:

WattsBase = Actual wattage if known, if unknown assume the following:

|  |  |
| --- | --- |
| **Baseline Type** | **WattsBase** |
| Incandescent | 35W[[1361]](#footnote-1362) |
| Fluorescent | 11W[[1362]](#footnote-1363) |
| Unknown (e.g. time of sale) | 11W |

WattsEE = Actual wattage if known, if unknown assume 2W[[1363]](#footnote-1364)

HOURS = Annual operating hours

= 8766

WHFe = Waste heat factor for energy; accounts for cooling savings from efficient lighting.

= 1.04[[1364]](#footnote-1365) for multi family buildings

Default if replacing incandescent fixture

ΔkWH = (35 – 2)/1000 \* 8766 \* 1.04

= 301 kWh

Default if replacing fluorescent fixture

ΔkWH = (11 – 2)/1000 \* 8766 \* 1.04

= 82 kWh

###### Heating Penalty

If electric heated building (if heating fuel is unknown assume gas, see Natural Gas section):

∆kWh[[1365]](#footnote-1366)  = - (((WattsBase - WattsEE) / 1000) \* Hours \* HF) / ηHeat

Where:

HF = Heating Factor or percentage of light savings that must be heated

= 49%[[1366]](#footnote-1367)

ηHeat = Efficiency in COP of Heating equipment

= Actual. If not available use:[[1367]](#footnote-1368)

|  |  |  |  |
| --- | --- | --- | --- |
| **System Type** | **Age of Equipment** | **HSPF Estimate** | **ηHeat (COP Estimate)** |
| Heat Pump | Before 2006 | 6.8 | 2.00 |
| After 2006 | 7.7 | 2.26 |
| Resistance | N/A | N/A | 1.00 |

For example, a 2.0COP Heat Pump heated building:

If incandescent fixture: ΔkWH = -((35 – 2)/1000 \* 8766 \* 0.49) / 2

= -71 kWh

If fluorescent fixture ΔkWH = -((11 – 2)/1000 \* 8766 \* 0.49) / 2

= -19 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = ((WattsBase - WattsEE) / 1000) \* WHFd \* CF

Where:

WHFd = Waste heat factor for demand to account for cooling savings from efficient lighting. The cooling savings are only added to the summer peak savings.

=1.07[[1368]](#footnote-1369) for multi family buildings

CF = Summer Peak Coincidence Factor for measure

= 1.0

Default if incandescent fixture

ΔkW = (35 – 2)/1000 \* 1.07 \* 1.0

= 0.035 kW

Default if fluorescent fixture

ΔkW = (11 – 2)/1000 \* 1.07 \* 1.0

= 0.0096 kW

###### Natural Gas Savings

Heating penalty if Natural Gas heated building, or if heating fuel is unknown.

Δtherms = - (((WattsBase - WattsEE) / 1000) \* Hours \* HF \* 0.03412) / ηHeat

Where:

HF = Heating factor, or percentage of lighting savings that must be replaced by heating system.

= 49% [[1369]](#footnote-1370)

0.03412 = Converts kWh to Therms

ηHeat = Average heating system efficiency.

= 0.70 [[1370]](#footnote-1371)

Other factors as defined above

Default if incandescent fixture

Δtherms = - (((35 - 2) / 1000) \* 8766 \* 0.49\* 0.03412) / 0.70

= -6.9 therms

Default if fluorescent fixture

Δtherms = - (((11 - 2) / 1000) \* 8766 \* 0.49\* 0.03412) / 0.70

= -1.9 therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

The annual O&M Cost Adjustment savings should be calculated using the following component costs and lifetimes.

|  |  |  |
| --- | --- | --- |
|  | **Baseline Measures** | |
| Component | Cost | Life (yrs) |
| Lamp | $7.00[[1371]](#footnote-1372) | 1.37 years[[1372]](#footnote-1373) |

###### Measure Code: RS-LTG-LEDE-V01-120601

### LED Screw Based Omnidirectional Bulbs

**Description**

This characterization provides savings assumptions for LED Screw Based Omnidirectional (e.g. A-Type lamps) lamps within the residential and multifamily sectors. This characterization assumes that the LED lamp or fixture is installed in a residential location. Where the implementation strategy does not allow for the installation location to be known (e.g. an upstream retail program) evaluation data could be used to determine an appropriate residential v commercial split. If this is not available, it is recommended to use this residential characterization for all installs in unknown locations to be appropriately conservative in savings assumptions.

This measure was developed to be applicable to the following program types:  TOS, NC, RF.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

In order for this characterization to apply, new lamps must be Energy Star labeled.

**Definition of Baseline Equipment**

In 2012, Federal legislation stemming from the Energy Independence and Security Act of 2007 (EIAS) will require all general-purpose light bulbs between 40 watts and 100 watts to have ~30% increased efficiency, essentially phasing out standard incandescent technology. In 2012, the 100 w lamp standards apply; in 2013 the 75 w lamp standards will apply, followed by restrictions on the 60 w and 40 w lamps in 2014. Since measures installed under this TRM all occur after 2014, baseline equipment are the values after EISA. These are shown in the baseline table below.

**Deemed Lifetime of Efficient Equipment**

13.7 years (exterior) to 26 years (residential home), however all installations are capped at 10 years[[1373]](#footnote-1374).

**Deemed Measure Cost**

Wherever possible, actual incremental costs should be used. Refer to reference table “Residential LED component Cost & Lifetime” for defaults.

**Loadshape**

|  |
| --- |
| Loadshape R06 – Residential Indoor Lighting |
| Loadshape R07 – Residential Outdoor Lighting |

**Coincidence Factor**

The summer peak coincidence factor is assumed to be 7.1% for Residential and in-unit Multi Family bulbs, 27.3% for exterior bulbs and 8.1% for unknown[[1374]](#footnote-1375).

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

ΔkWh = ((Wattsbase-WattsEE)/1000) \* ISR \* (1-Leakage) \* Hours \*WHFe

Where:

Wattsbase = Input wattage of the existing system. Reference the “LED New and Baseline Assumptions” table for default values.

WattsEE = Actual wattage of LED purchased / installed. If unknown, use default provided below:

**LED New and Baseline Assumptions Table**

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| **Minimum Lumens** | **Maximum Lumens** | **Lumens used to calculate LED Wattage**  **(midpoint)** | **LED Wattage [[1375]](#footnote-1376) (WattsEE)** | **Baseline 2014-2019 (WattsBase)** | **Delta Watts 2014-2019 (WattsEE)** | **Baseline Post EISA 2020 requirement[[1376]](#footnote-1377)  (WattsBase)** | **Delta Watts Post 2020 (WattsEE)** |
|
|
| 5280 | 6209 | 5745 | 104.4 | 300.0 | 195.6 | 300.0 | 195.6 |
| 3000 | 5279 | 4140 | 75.3 | 200.0 | 124.7 | 200.0 | 124.7 |
| 2601 | 2999 | 2800 | 50.9 | 150.0 | 99.1 | 150.0 | 99.1 |
| 1490 | 2600 | 2045 | 37.2 | 72.0 | 34.8 | 45.4 | 8.3 |
| 1050 | 1489 | 1270 | 23.1 | 53.0 | 29.9 | 28.2 | 5.1 |
| 750 | 1049 | 900 | 16.4 | 43.0 | 26.6 | 20.0 | 3.6 |
| 310 | 749 | 530 | 9.6 | 29.0 | 19.4 | 11.8 | 2.1 |
| 250 | 309 | 280 | 5.6 | 25.0 | 19.4 | 25.0 | 19.4 |

ISR = In Service Rate, the percentage of units rebated that are actually in service.

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
| **Program** | | **Weighted Average 1st year In Service Rate (ISR)** | **2nd year Installations** | **3rd year Installations** | **Final Lifetime In Service Rate** |
| Retail (Time of Sale) | | 9295%[[1377]](#footnote-1378) | 3.21.6% | 2.81.4% | 98.0%[[1378]](#footnote-1379) |
| Direct Install | | 96.9%[[1379]](#footnote-1380) |  |  |  |
| Efficiency Kits[[1380]](#footnote-1381) | CFL Distribution[[1381]](#footnote-1382) | 59% | 13% | 11% | 83% |
| School Kits[[1382]](#footnote-1383) | 61% | 13% | 11% | 86% |
| Direct Mail Kits[[1383]](#footnote-1384) | 66% | 14% | 12% | 93% |

Leakage = Adjustment to account for the percentage of bulbs purchased that move out (and in if deemed appropriate) of the Utility Jurisdiction.

Upstream (TOS) Lighting programs = Determined through evaluation[[1384]](#footnote-1385).

All other programs = 0

Hours = Average hours of use per year

|  |  |
| --- | --- |
| **Installation Location** | **Hours[[1385]](#footnote-1386)** |
| Residential and in-unit Multi Family | 759 |
| Exterior | 2475 |
| Unknown | 847 |

WHFe = Waste heat factor for energy to account for cooling energy savings from efficient lighting

|  |  |  |
| --- | --- | --- |
| **Bulb Location** | **WHFe** | |
| Interior single family or unknown location | 1.06 [[1386]](#footnote-1387) | |
| Multi family in unit | 1.04 [[1387]](#footnote-1388) | |
| Exterior or uncooled location | | 1.0 |

**Mid Life Baseline Adjustment**

During the lifetime of a standard Omnidirectional LED, the baseline incandescent/halogen bulb would need to be replaced multiple times. Since the baseline bulb changes over time (except for <300 and 2600+ lumen lamps) the annual savings claim must be reduced within the life of the measure to account for this baseline shift.

For example, for 60W equivalent bulbs installed in 2014, the full savings (as calculated above in the Algorithm) should be claimed for the first six years, but a reduced annual savings (calculated energy savings above multiplied by the adjustment factor in the table below) claimed for the remainder of the measure life.

| **Minimum Lumens** | **Maximum Lumens** | **LED Wattage (WattsEE)** | **Delta Watts 2014-2019 (WattsEE)** | **Delta Watts Post 2020 (WattsEE)** | **Mid Life adjustment (made from June 2020) to first year savings** |
| --- | --- | --- | --- | --- | --- |
| 1490 | 2600 | 37.2 | 34.8 | 8.3 | 23.8% |
| 1050 | 1489 | 23.1 | 29.9 | 5.1 | 17.1% |
| 750 | 1049 | 16.4 | 26.6 | 3.6 | 13.5% |
| 310 | 749 | 9.6 | 19.4 | 2.1 | 10.8% |

For example, an 8W LED lamp, 450 lumens, is installed in the interior of a home in 2014. The customer purchased the lamp through an upstream program:

ΔkWH = ((29-8 /1000) \* 847 \* 1.06 \* 0.92

= 17.3 kWh

This value should be claimed for six years, i.e. June 2014 – May 2020, but from May 2020 until the end of the measure life for that same bulb, savings should be reduced to (17.3 \* 0.108 =) 1.9 kWh for the remainder of the measure life. Note these adjustments should be applied to kW and fuel impacts as well.

**Deferred Installs**

As presented above, the characterization assumes that a percentage of bulbs purchased are not installed until Year 2 and Year 3 (see ISR assumption above). The Illinois Technical Advisory Committee has determined the following methodology for calculating the savings of these future installs.

Year 1 (Purchase Year) installs: Characterized using assumptions provided above or evaluated assumptions if available.

Year 2 and 3 installs: Characterized using delta watts assumption and hours of use from the Install Year i.e. the actual deemed (or evaluated if available) assumptions active in Year 2 and 3 should be applied.

The NTG factor for the Purchase Year should be applied.

Using the example from above, for an 8W LED, 450 Lumens purchased for the interior of a residential homes through an upstream program in 2014.

ΔkWH1st year installs = ((29-8/1000)\*847\*1.06\*0.92

= 17.3 kWh

ΔkWH2nd year installs = ((29-8/1000)\*847\*1.06\*0.032

= 0.6 kWh

Note: Here we assume no change in hours assumption. NTG value from Purchase year applied.

ΔkWH3rd year installs = ((29-8/1000)\*847\*1.06\*0.028

= 0.5 kWh

**Heating Penalty**

If electric heated home (if heating fuel is unknown assume gas, see Natural Gas section):

∆kWh[[1388]](#footnote-1389) = - (((WattsBase - WattsEE) / 1000) \* ISR \* Hours \* HF) / ηHeat

Where:

HF = Heating Factor or percentage of light savings that must be heated

= 49%[[1389]](#footnote-1390) for interior or unknown location

= 0% for exterior or unheated location

ηHeat = Efficiency in COP of Heating equipment

= actual. If not available use[[1390]](#footnote-1391):

|  |  |  |  |
| --- | --- | --- | --- |
| **System Type** | **Age of Equipment** | **HSPF Estimate** | **ηHeat**  **(COP Estimate)** |
| Heat Pump | Before 2006 | 6.8 | 2.00 |
| After 2006 - 2014 | 7.7 | 2.26 |
| 2015 on | 8.2 | 2.40 |
| Resistance | N/A | N/A | 1.00 |

Using the same 8 W LED that is installed in home with 2.0 COP Heat Pump (i.e., the heat pump was installed prior to 2006):

∆kWh1st year = - (((29-8) / 1000) \* 0.92 \* 759 \* 0.49) / 2.0

= - 3.6 kWh

Second and third year install savings should be calculated using the appropriate ISR and the delta watts and hours from the install year. The appropriate baseline shift adjustment should then be applied to all installs.

**Summer Coincident Peak Demand Savings**

∆kW = ((WattsBase - WattsEE) / 1 000) \* ISR \* WHFd \* CF

Where:

WHFd = Waste heat factor for demand to account for cooling savings from efficient lighting.

|  |  |
| --- | --- |
| **Bulb Location** | **WHFd** |
| Interior single family or unknown location | 1.11[[1391]](#footnote-1392) |
| Multi family in unit | 1.07[[1392]](#footnote-1393) |
| Exterior or uncooled location | 1.0 |

CF = Summer Peak Coincidence Factor for measure.

|  |  |
| --- | --- |
| **Bulb Location** | **CF[[1393]](#footnote-1394)** |
| Interior single family or unknown location or Multi family in unit | 9.57.1% |
| Exterior | 27.3% |
| Unknown | 8.1% |

Other factors as defined above

For the same 8 W LED that is installed in a single family interior location in 2014, the demand savings are:

ΔkW = ((29-8) / 1000) \* 0.92\* 1.11 \* 0.071

= 0.0015 kW

Second and third year install savings should be calculated using the appropriate ISR and the delta watts and hours from the install year. The appropriate baseline shift adjustment should then be applied to all installs.

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

Bulb replacement costs assumed in the O&M calculations are provided below[[1394]](#footnote-1395).

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
|  | **Std Inc.** | **EISA Compliant Halogen** | **CFL** | **LED-A** |
| 2014 | $0.34 | $1.25 | $2.50 | $13.81 |
| 2015 | $0.34 | $0.90 | $2.50 | $10.86 |
| 2016 | $0.34 | $0.80 | $2.50 | $8.60 |
| 2017 | $0.34 | $0.70 | $2.50 | $7.74 |
| 2018 | $0.34 | $0.60 | $2.50 | $6.96 |
| 2019 | $0.34 | $0.60 | $2.50 | $6.27 |
| 2020 & after | $0.34 | N/A | $2.50 | $5.64 |

In order to account for the shift in baseline due to the Energy Independence and Security Act of 2007, an equivalent annual levelized baseline replacement cost over the lifetime of the LED bulb is calculated. The key assumptions used in this calculation are documented below:

| **Installation Location** | **Omnidirectional LED Measure Hours** | **Hours of Use per year [[1395]](#footnote-1396)** | **Measure Life in Years**  **(capped at 10)** |
| --- | --- | --- | --- |
| Residential and in-unit Multi Family | 25,000 | 938 759 | 10 |
| Exterior | 25,000 | 1,8252475 | 10 |
| Unknown | 25,000 | 1,000847 | 10 |

The NPV for replacement lamps and annual levelized replacement costs using the statewide real discount rate of 5.23% are presented below:

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| **Location** | **Lumen Level** | **NPV of replacement costs for period** | | | **Levelized annual replacement cost savings** | | |
| **June 2015 - May 2016** | **June 2016 - May 2017** | **June 2017 - May 2018** | **June 2015 - May 2016** | **June 2016 - May 2017** | **June 2017 - May 2018** |
| Residential and in-unit Multi Family | Lumens <310 or >2600 (non-EISA compliant) | $1.73 | $1.73 | $1.73 | $0.23 | $0.23 | $0.23 |
| Lumens ≥ 310 and ≤ 2600 (EISA compliant) | $2.52 | $2.22 | $1.97 | $0.33 | $0.29 | $0.26 |
| Exterior | Lumens <310 or >2600 (non-EISA compliant) | $6.10 | $6.10 | $6.10 | $0.80 | $0.80 | $0.80 |
| Lumens ≥ 310 and ≤ 2600 (EISA compliant) | $9.48 | $8.35 | $7.55 | $1.24 | $1.09 | $0.99 |
| Unknown | Lumens <310 or >2600 (non-EISA compliant) | $1.93 | $1.93 | $1.93 | $0.25 | $0.25 | $0.25 |
| Lumens ≥ 310 and ≤ 2600 (EISA compliant) | $2.81 | $2.47 | $2.20 | $0.37 | $0.32 | $0.29 |

Note incandescent lamps in lumen range <310 and >2600 are exempt from EISA. For halogen bulbs, we assume the same replacement cycle as incandescent bulbs.[[1396]](#footnote-1397) The replacement cycle is based on the location of the lamp and varies based on the hours of use for that location. Both incandescent and halogen lamps are assumed to last for 1,000 hours before needing replacement.

**Measure Code: RS-LTG-LEDA-V03-150601**

## Shell End Use

### Air Sealing

###### Description

Thermal shell air leaks are sealed through strategic use and location of air-tight materials. Leaks are detected and leakage rates measured with the assistance of a blower-door. The algorithm for this measure can be used when the program implementation does not allow for more detailed forecasting through the use of residential modeling software.

This measure was developed to be applicable to the following program types:  RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

Air sealing materials and diagnostic testing should meet all eligibility program qualification criteria. The initial and final tested leakage rates should be performed in such a manner that the identified reductions can be properly discerned, particularly in situations wherein multiple building envelope measures may be implemented simultaneously.

###### Definition of Baseline Equipment

The existing air leakage should be determined through approved and appropriate test methods using a blower door. The baseline condition of a building upon first inspection significantly impacts the opportunity for cost-effective energy savings through air-sealing.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 15 years.[[1397]](#footnote-1398)

###### Deemed Measure Cost

The actual capital cost for this measure should be used in screening.

###### Loadshape

|  |
| --- |
| Loadshape R08 - Residential Cooling |
| Loadshape R09 - Residential Electric Space Heat |
| Loadshape R10 - Residential Electric Heating and Cooling |

###### Coincidence Factor

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during utility peak hour)

= 68%[[1398]](#footnote-1399)

CFSSP = Summer System Peak Coincidence Factor for Heat Pumps (during system peak hour)

= 72%%[[1399]](#footnote-1400)

CFPJM   = PJM Summer Peak Coincidence Factor for Central A/C (average during PJM peak period)

= 46.6%[[1400]](#footnote-1401)

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

ΔkWh = ΔkWh\_cooling + ΔkWh\_heating

Where:

ΔkWh\_cooling = If central cooling, reduction in annual cooling requirement due to air sealing

= [(((CFM50\_existing - CFM50\_new)/N\_cool) \* 60 \* 24 \* CDD \* DUA \* 0.018) / (1000 \* ηCool)] \* LM

CFM50\_existing = Infiltration at 50 Pascals as measured by blower door before air sealing.

= Actual

CFM50\_new = Infiltration at 50 Pascals as measured by blower door after air sealing.

= Actual

N\_cool = Conversion factor from leakage at 50 Pascal to leakage at natural conditions

=Dependent on exposure:[[1401]](#footnote-1402)

|  |  |  |
| --- | --- | --- |
| **Climate Zone** | **Exposure** | **N-Factor** |
| Zone 2 | Well Shielded | 22.2 |
| Normal | 18.5 |
| Exposed | 16.7 |
| Zone 3 | Well Shielded | 25.8 |
| Normal | 21.5 |
| Exposed | 19.4 |

60 \* 24 = Converts Cubic Feet per Minute to Cubic Feet per Day

CDD = Cooling Degree Days

= Dependent on location[[1402]](#footnote-1403):

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **CDD 65** |
| 1 (Rockford) | 820 |
| 2 (Chicago) | 842 |
| 3 (Springfield) | 1,108 |
| 4 (Belleville) | 1,570 |
| 5 (Marion) | 1,370 |

DUA = Discretionary Use Adjustment (reflects the fact that people do not always operate their AC when conditions may call for it).

= 0.75 [[1403]](#footnote-1404)

0.018 = Specific Heat Capacity of Air (Btu/ft3\*°F)

1000 = Converts Btu to kBtu

ηCool = Efficiency (SEER) of Air Conditioning equipment (kBtu/kWh)

= Actual (where it is possible to measure or reasonably estimate). If unknown assume the following[[1404]](#footnote-1405):

|  |  |
| --- | --- |
| **Age of Equipment** | **SEER Estimate** |
| Before 2006 | 10 |
| 2006 - 2014 | 13 |
| Central AC After 1/1/2015 | 13 |
| Heat Pump After 1/1/2015 | 14 |

LM = Latent multiplier to account for latent cooling demand

= dependent on location: [[1405]](#footnote-1406)

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **LM** |
| 1 (Rockford) | 8.5 |
| 2 (Chicago) | 6.2 |
| 3 (Springfield) | 6.6 |
| 4 (St. Louis, MO) | 5.8 |
| 5 (Evansville, IN) | 6.6 |

ΔkWh\_heating = If electric heat (resistance or heat pump), reduction in annual electric heating due to air sealing

= (((CFM50\_existing - CFM50\_new)/N\_heat) \* 60 \* 24 \* HDD \* 0.018) / (ηHeat \* 3,412)

N\_heat = Conversion factor from leakage at 50 Pascal to leakage at natural conditions

= Based on climate zone, building height and exposure level:[[1406]](#footnote-1407)

|  | **# Stories:** | **1** | **1.5** | **2** | **3** |
| --- | --- | --- | --- | --- | --- |
| Zone 2 | Well Shielded | 22.2 | 20.0 | 17.8 | 15.5 |
| Normal | 18.5 | 16.7 | 14.8 | 13.0 |
| Exposed | 16.7 | 15.0 | 13.3 | 11.7 |
| Zone 3 | Well Shielded | 25.8 | 23.2 | 20.6 | 18.1 |
| Normal | 21.5 | 19.4 | 17.2 | 15.1 |
| Exposed | 19.4 | 17.4 | 15.5 | 13.5 |

HDD = Heating Degree Days

= Dependent on location:[[1407]](#footnote-1408)

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **HDD 65** |
| 1 (Rockford) | 6,569 |
| 2 (Chicago) | 6,339 |
| 3 (Springfield) | 5,497 |
| 4 (Belleville) | 4,379 |
| 5 (Marion) | 4,476 |

ηHeat = Efficiency of heating system

= Actual. If not available refer to default table below[[1408]](#footnote-1409):

|  |  |  |  |
| --- | --- | --- | --- |
| **System Type** | **Age of Equipment** | **HSPF Estimate** | **ηHeat (Effective COP Estimate)= (HSPF/3.413)\*0.85** |
| Heat Pump | Before 2006 | 6.8 | 1.7 |
| 2006 - 2014 | 7.7 | 1.92 |
| 2015 on | 8.2 | 2.40 |
| Resistance | N/A | N/A | 1 |

3412 = Converts Btu to kWh

For example, a well shielded, 2 story single family home in Chicago with 10.5 SEER central cooling and a heat pump with COP of 2 (1.92 including distribution losses), has pre and post blower door test results of 3,400 and 2,250:

ΔkWh = ΔkWh\_cooling + ΔkWh\_heating

= [((((3,400 – 2,250) / 22.2) \* 60 \* 24 \* 842 \* 0.75 \* 0.018) / (1000 \* 10.5)) \* 6.2] + [((3,400 – 2,250) / 17.8)) \* 60 \* 24 \* 6339 \* 0.018 / (1.92 \* 3,412)]

= 501 + 1620

= 2,121 kWh

ΔkWh\_heating = If gas *furnace* heat, kWh savings for reduction in fan run time

= ΔTherms \* Fe \* 29.3

Fe = Furnace Fan energy consumption as a percentage of annual fuel consumption

= 3.14%[[1409]](#footnote-1410)

29.3 = kWh per therm

For example, a well shielded, 2 story single family home in Chicago with a gas furnace with system efficiency of 70%, has pre and post blower door test results of 3,400 and 2,250 (see therm calculation in Natural Gas Savings section:

ΔkWh = 152 \* 0.0314 \* 29.3

= 140 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = (ΔkWh\_cooling / FLH\_cooling) \* CF

Where:

FLH\_cooling = Full load hours of air conditioning

= Dependent on location[[1410]](#footnote-1411):

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **Single Family** | **Multifamily** |
| 1 (Rockford) | 512 | 467 |
| 2 (Chicago) | 570 | 506 |
| 3 (Springfield) | 730 | 663 |
| 4 (Belleville) | 1,035 | 940 |
| 5 (Marion) | 903 | 820 |

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during system peak hour)

= 68%[[1411]](#footnote-1412)

CFSSP = Summer System Peak Coincidence Factor for Heat Pumps (during system peak hour)

= 72%%[[1412]](#footnote-1413)

CFPJM = PJM Summer Peak Coincidence Factor for Central A/C (average during peak period)

= 46.6%[[1413]](#footnote-1414)

Other factors as defined above

For example, a well shielded, 2 story single family home in Chicago with 10.5 SEER central cooling and a heat pump with COP of 2.0, has pre and post blower door test results of 3,400 and 2,250:

ΔkWSSP = 501 / 570 \* 0.68

= 0.60 kW

ΔkWPJM = 501 / 570 \* 0.466

= 0.410 kW

###### Natural Gas Savings

If Natural Gas heating:

ΔTherms = (((CFM50\_existing - CFM50\_new)/N\_heat) \* 60 \* 24 \* HDD \* 0.018) / (ηHeat \* 100,000)

Where:

N\_heat = Conversion factor from leakage at 50 Pascal to leakage at natural conditions

= Based on climate zone, building height and exposure level[[1414]](#footnote-1415):

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
|  | **# Stories:** | **1** | **1.5** | **2** | **3** |
| Zone 2 | Well Shielded | 22.2 | 20.0 | 17.8 | 15.5 |
| Normal | 18.5 | 16.7 | 14.8 | 13.0 |
| Exposed | 16.7 | 15.0 | 13.3 | 11.7 |
| Zone 3 | Well Shielded | 25.8 | 23.2 | 20.6 | 18.1 |
| Normal | 21.5 | 19.4 | 17.2 | 15.1 |
| Exposed | 19.4 | 17.4 | 15.5 | 13.5 |

HDD = Heating Degree Days

= dependent on location[[1415]](#footnote-1416):

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **HDD 65** |
| 1 (Rockford) | 6,569 |
| 2 (Chicago) | 6,339 |
| 3 (Springfield) | 5,497 |
| 4 (Belleville) | 4,379 |
| 5 (Marion) | 4,476 |

ηHeat = Efficiency of heating system

= Equipment efficiency \* distribution efficiency

= Actual[[1416]](#footnote-1417). If not available use 70%[[1417]](#footnote-1418).

Other factors as defined above

For example, a well shielded, 2 story single family home in Chicago with a gas furnace with system efficiency of 70%, has pre and post blower door test results of 3,400 and 2,250:

ΔTherms = ((3,400 – 2,250)/17.8) \* 60 \* 24 \* 6339 \* 0.018) / (0.7 \* 100,000)

= 152 therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-SHL-AIRS-V03-150601

### Basement Sidewall Insulation

###### Description

Insulation is added to a basement or crawl space. Insulation added above ground in conditioned space is modeled the same as wall insulation. Below ground insulation is adjusted with an approximation of the thermal resistance of the ground. Insulation in unconditioned spaces is modeled by reducing the degree days to reflect the smaller but non-zero contribution to heating and cooling load. Cooling savings only consider above grade insulation, as below grade has little temperature difference during the cooling season.

This measure was developed to be applicable to the following program types:  RF.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

This measure requires a member of the implementation staff or a participating contractor to evaluate the pre and post R-values and measure surface areas. The requirements for participation in the program will be defined by the utilities.

**Definition of Baseline Equipment**

The existing condition will be evaluated by implementation staff or a participating contractor and is likely to be no basement wall or ceiling insulation.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 25 years.[[1418]](#footnote-1419)

**Deemed Measure Cost**

The actual installed cost for this measure should be used in screening.

**Deemed O&M Cost Adjustments**

N/A

**Loadshape**

|  |
| --- |
| Loadshape R08 - Residential Cooling |
| Loadshape R09 - Residential Electric Space Heat |
| Loadshape R10 - Residential Electric Heating and Cooling |

**Coincidence Factor**

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during utility peak hour)

= 68%[[1419]](#footnote-1420)

CFSSP = Summer System Peak Coincidence Factor for Heat Pumps (during system peak hour)

= 72%%[[1420]](#footnote-1421)

CFPJM   = PJM Summer Peak Coincidence Factor for Central A/C (average during PJM peak period)

= 46.6%[[1421]](#footnote-1422)

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

Where available savings from shell insulation measures should be determined through a custom analysis. When that is not feasible for the program the following engineering algorithms can be used with the inclusion of an adjustment factor to de-rate the heating savings.

ΔkWh = (ΔkWh\_cooling + ΔkWh\_heating)

Where:

ΔkWh\_cooling = If central cooling, reduction in annual cooling requirement due to insulation

= (((1/R\_old\_AG - 1/(R\_added+R\_old\_AG)) \* L\_basement\_wall\_total \* H\_basement\_wall\_AG \* (1-Framing\_factor)) \* 24 \* CDD \* DUA) / (1000 \* ηCool))

R\_added = R-value of additional spray foam, rigid foam, or cavity insulation.

R\_old\_AG = R-value value of foundation wall above grade.

= Actual, if unknown assume 1.0[[1422]](#footnote-1423)

L\_basement\_wall\_total = Length of basement wall around the entire insulated perimeter (ft)

H\_basement\_wall\_AG = Height of insulated basement wall above grade (ft)

Framing\_factor = Adjustment to account for area of framing when cavity insulation is used

= 0% if Spray Foam or External Rigid Foam

= 25% if studs and cavity insulation[[1423]](#footnote-1424)

24 = Converts hours to days

CDD = Cooling Degree Days

= Dependent on location and whether basement is conditioned:[[1424]](#footnote-1425)

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **Conditioned CDD 65** | **Unconditioned**  **CDD 65[[1425]](#footnote-1426)** |
| 1 (Rockford) | 820 | 263 |
| 2 (Chicago) | 842 | 281 |
| 3 (Springfield) | 1,108 | 436 |
| 4 (Belleville) | 1,570 | 538 |
| 5 (Marion) | 1,370 | 570 |
| Weighted Average[[1426]](#footnote-1427) | 947 | 325 |

DUA = Discretionary Use Adjustment (reflects the fact that people do not always operate their AC when conditions may call for it).

= 0.75 [[1427]](#footnote-1428)

1000 = Converts Btu to kBtu

ηCool = Seasonal Energy Efficiency Ratio of cooling system (kBtu/kWh)

= Actual (where it is possible to measure or reasonably estimate). If unknown assume the following:[[1428]](#footnote-1429)

|  |  |
| --- | --- |
| **Age of Equipment** | **ηCool Estimate** |
| Before 2006 | 10 |
| 2006 - 2014 | 13 |
| Central AC After 1/1/2015 | 13 |
| Heat Pump After 1/1/2015 | 14 |

ΔkWh\_heating = If electric heat (resistance or heat pump), reduction in annual electric heating due to insulation

= ([((1/R\_old\_AG - 1/(R\_added+R\_old\_AG)) \* L\_basement\_wall\_total \* H\_basement\_wall\_AG \* (1-Framing\_factor)) + ((1/(R\_old\_BG - 1/(R\_added+R\_old\_BG)) \* L\_basement\_wall\_total \* (H\_basement\_wall\_total - H\_basement\_wall\_AG) \* (1-Framing\_factor))] \* 24 \* HDD) / (3,412 \* ηHeat)) \* ADJBasement

R\_old\_BG = R-value value of foundation wall below grade (including thermal resistance of the earth) [[1429]](#footnote-1430)

= dependent on depth of foundation (H\_basement\_wall\_total – H\_basement\_wall\_AG):

= Actual R-value of wall plus average earth R-value by depth in table below

|  |  |  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| **Below Grade R-value** |  |  |  |  |  |  |  |  |  |
| **Depth below grade (ft)** | **0** | **1** | **2** | **3** | **4** | **5** | **6** | **7** | **8** |
| Earth R-value (°F-ft2-h/Btu) | 2.44 | 4.50 | 6.30 | 8.40 | 10.44 | 12.66 | 14.49 | 17.00 | 20.00 |
| Average Earth R-value (°F-ft2-h/Btu) | 2.44 | 3.47 | 4.41 | 5.41 | 6.42 | 7.46 | 8.46 | 9.53 | 10.69 |
| Total BG R-value (earth + R-1.0 foundation) default | 3.44 | 4.47 | 5.41 | 6.41 | 7.42 | 8.46 | 9.46 | 10.53 | 11.69 |

H\_basement\_wall\_total = Total height of basement wall (ft)

HDD = Heating Degree Days

= dependent on location and whether basement is conditioned:[[1430]](#footnote-1431)

| **Climate Zone**  **(City based upon)** | **Conditioned**  **HDD 60** | **Unconditioned**  **HDD 50** |
| --- | --- | --- |
| 1 (Rockford) | 5,352 | 3,322 |
| 2 (Chicago) | 5,113 | 3,079 |
| 3 (Springfield) | 4,379 | 2,550 |
| 4 (Belleville) | 3,378 | 1,789 |
| 5 (Marion) | 3,438 | 1,796 |
| Weighted Average[[1431]](#footnote-1432) | 4,860 | 2,895 |

ηHeat = Efficiency of heating system

= Actual. If not available refer to default table below:[[1432]](#footnote-1433)

|  |  |  |  |
| --- | --- | --- | --- |
| **System Type** | **Age of Equipment** | **HSPF Estimate** | **ηHeat (Effective COP Estimate) (HSPF/3.413)\*0.85** |
| Heat Pump | Before 2006 | 6.8 | 1.7 |
| After 2006 -2014 | 7.7 | 1.92 |
| 2015 on | 8.2 | 2.40 |
| Resistance | N/A | N/A | 1 |

ADJBasement = Adjustment for basement wall insulation to account for prescriptive engineering algorithms overclaiming savings.

= 88%[[1433]](#footnote-1434)

For example, a single family home in Chicago with a 20 by 25 by 7 foot R-2.25 basement, with 3 feet above grade, insulated with R-13 of interior spray foam, 10.5 SEER Central AC and 2.26 COP Heat Pump:

ΔkWh = (ΔkWh\_cooling + ΔkWh\_heating)

= [(((1/2.25 - 1/(13 + 2.25))\*(20+25+20+25) \* 3 \* (1 - 0)) \* 24 \* 281 \* 0.75)/(1000 \* 10.5)] + [(((((1/2.25 - 1/(13 + 2.25)) \* (20+25+20+25) \* 3 \* (1-0)) + ((1 / (2.25 + 6.42) – 1 / (13 + 2.25 + 6.42)) \* (20+25+20+25) \* 4 \* (1-0))) \* 24 \* 3079) / (3412 \* 1.92)) \* 0.88]

= (49.3 + 1263.0)

= 1312.3 kWh

ΔkWh\_heating = If gas *furnace* heat, kWh savings for reduction in fan run time

= ΔTherms \* Fe \* 29.3

Fe = Furnace Fan energy consumption as a percentage of annual fuel consumption

= 3.14%[[1434]](#footnote-1435)

29.3 = kWh per therm

For example, a single family home in Chicago with a 20 by 25 by 7 foot unconditioned basement, with 3 feet above grade, insulated with R-13 of interior spray foam, and a 70% efficient furnace (for therm calculation see Natural Gas Savings section :

= 118.1 \* 0.0314 \* 29.3

= 109 kWh

**Summer Coincident Peak Demand**

ΔkW = (ΔkWh\_cooling / FLH\_cooling) \* CF

Where:

FLH\_cooling = Full load hours of air conditioning

= dependent on location[[1435]](#footnote-1436):

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **Single Family** | **Multifamily** |
| 1 (Rockford) | 512 | 467 |
| 2 (Chicago) | 570 | 506 |
| 3 (Springfield) | 730 | 663 |
| 4 (Belleville) | 1,035 | 940 |
| 5 (Marion) | 903 | 820 |
| Weighted Average[[1436]](#footnote-1437) | 629 | 564 |

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during system peak hour)

= 68%[[1437]](#footnote-1438)

CFSSP = Summer System Peak Coincidence Factor for Heat Pumps (during system peak hour)

= 72%%[[1438]](#footnote-1439)

CFPJM = PJM Summer Peak Coincidence Factor for Central A/C (average during peak period)

= 46.6%[[1439]](#footnote-1440)

For example, a single family home in Chicago with a 20 by 25 by 7 foot unconditioned basement, with 3 feet above grade, insulated with R-13 of interior spray foam, 10.5 SEER Central AC and 2.26 COP Heat Pump:

ΔkWSSP = 49.3 / 570 \* 0.68

= 0.059 kW

ΔkWPJM = 49.3 / 570 \* 0.466

= 0.040 kW

**Natural Gas Savings**

If Natural Gas heating:

ΔTherms = [(([((1/R\_old\_AG - 1/(R\_added+R\_old\_AG)) \* L\_basement\_wall\_total \* H\_basement\_wall\_AG \* (1-Framing\_factor) + (1/(R\_old\_BG - 1/(R\_added+R\_old\_BG)) \* L\_basement\_wall\_total \* (H\_basement\_wall\_total - H\_basement\_wall\_AG) \* (1-Framing\_factor)] \* 24 \* HDD) / (ηHeat \* 100,067)] \* ADJBasement

ηHeat = Efficiency of heating system

= Equipment efficiency \* distribution efficiency

= Actual. If unknown assume 70%[[1440]](#footnote-1441)

Other factors as defined above

For example, a single family home in Chicago with a 20 by 25 by 7 foot R-2.25 basement, with 3 feet above grade, insulated with R-13 of interior spray foam, and a 70% efficient furnace:

= ((1/2.25 - 1/(13 + 2.25)) \* (20+25+20+25) \* 3 \* (1-0) + (1/8.67 - 1/(13 + 8.67)) \* (20+25+20+25) \* 4 \* (1 - 0)) \* 24 \* 3079) / (0.7 \* 100,067) \* 0.88

= 118.1 therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

**Measure Code: RS-SHL-BINS-V06-150601**

### Floor Insulation Above Crawlspace

**Description**

Insulation is added to the floor above a vented crawl space that does not contain pipes or HVAC equipment. If there are pipes, HVAC, or a basement, it is desirable to keep them within the conditioned space by insulating the crawl space walls and ground. Insulating the floor separates the conditioned space above from the space below the floor, and is only acceptable when there is nothing underneath that could freeze or would operate less efficiently in an environment resembling the outdoors. Even in the case of an empty, unvented crawl space, it is still considered best practice to seal and insulate the crawl space perimeter rather than the floor. Not only is there generally less area to insulate this way, but there are also moisture control benefits. There is a “Basement Insulation” measure for perimeter sealing and insulation. This measure assumes the insulation is installed above an unvented crawl space and should not be used in other situations.

This measure was developed to be applicable to the following program types:  RF.

If applied to other program types, the measure savings should be verified.

**Definition of Efficient Equipment**

This measure requires a member of the implementation staff or a participating contractor to evaluate the pre and post R-values and measure surface areas. The requirements for participation in the program will be defined by the utilities.

**Definition of Baseline Equipment**

The existing condition will be evaluated by implementation staff or a participating contractor and is likely to be no insulation on any surface surrounding a crawl space.

**Deemed Lifetime of Efficient Equipment**

The expected measure life is assumed to be 25 years.[[1441]](#footnote-1442)

**Deemed Measure Cost**

The actual installed cost for this measure should be used in screening.

**Deemed O&M Cost Adjustments**

N/A

###### Loadshape

|  |
| --- |
| Loadshape R08 - Residential Cooling |
| Loadshape R09 - Residential Electric Space Heat |
| Loadshape R10 - Residential Electric Heating and Cooling |

**Coincidence Factor**

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during utility peak hour)

= 68%[[1442]](#footnote-1443)

CFSSP = Summer System Peak Coincidence Factor for Heat Pumps (during system peak hour)

= 72%%[[1443]](#footnote-1444)

CFPJM   = PJM Summer Peak Coincidence Factor for Central A/C (average during PJM peak period)

= 46.6%[[1444]](#footnote-1445)

**Algorithm**

**Calculation of Savings**

**Electric Energy Savings**

Where available savings from shell insulation measures should be determined through a custom analysis. When that is not feasible for the program the following engineering algorithms can be used with the inclusion of an adjustment factor to de-rate the heating savings.

ΔkWh = (ΔkWh\_cooling + ΔkWh\_heating)

Where: ΔkWh\_cooling = If central cooling, reduction in annual cooling requirement due to insulation

= (((1/R\_old - 1/(R\_added+R\_old)) \* Area \* (1-Framing\_factor)) \* 24 \* CDD \* DUA) / (1000 \* ηCool))

R\_old = R-value value of floor before insulation, assuming 3/4” plywood subfloor and carpet with pad

= Actual. If unknown assume 3.96 [[1445]](#footnote-1446)

R\_added = R-value of additional spray foam, rigid foam, or cavity insulation.

Area = Total floor area to be insulated

Framing\_factor = Adjustment to account for area of framing

= 12% [[1446]](#footnote-1447)

24 = Converts hours to days

CDD = Cooling Degree Days

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **Unconditioned**  **CDD[[1447]](#footnote-1448)** |
| 1 (Rockford) | 263 |
| 2 (Chicago) | 281 |
| 3 (Springfield) | 436 |
| 4 (Belleville) | 538 |
| 5 (Marion) | 570 |
| Weighted Average[[1448]](#footnote-1449) | 325 |

DUA = Discretionary Use Adjustment (reflects the fact that people do not always operate their AC when conditions may call for it).

= 0.75 [[1449]](#footnote-1450)

1000 = Converts Btu to kBtu

ηCool = Seasonal Energy Efficiency Ratio of cooling system (kBtu/kWh)

= Actual (where it is possible to measure or reasonably estimate). If unknown assume the following:[[1450]](#footnote-1451)

|  |  |
| --- | --- |
| **Age of Equipment** | **ηCool Estimate** |
| Before 2006 | 10 |
| 2006 - 2014 | 13 |
| Central AC After 1/1/2015 | 13 |
| Heat Pump After 1/1/2015 | 14 |

ΔkWh\_heating = If electric heat (resistance or heat pump), reduction in annual electric heating due to insulation

= ((((1/R\_old - 1/(R\_added + R\_old)) \* Area \* (1-Framing\_factor) \* 24 \* HDD)/ (3,412 \* ηHeat)) \* ADJFloor

HDD = Heating Degree Days:[[1451]](#footnote-1452)

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **Unconditioned HDD** |
| 1 (Rockford) | 3,322 |
| 2 (Chicago) | 3,079 |
| 3 (Springfield) | 2,550 |
| 4 (Belleville) | 1,789 |
| 5 (Marion) | 1,796 |
| Weighted Average[[1452]](#footnote-1453) | 2,895 |

ηHeat = Efficiency of heating system

= Actual. If not available refer to default table below:[[1453]](#footnote-1454)

|  |  |  |  |
| --- | --- | --- | --- |
| **System Type** | **Age of Equipment** | **HSPF Estimate** | **ηHeat (Effective COP Estimate) (HSPF/3.413)\*0.85** |
| Heat Pump | Before 2006 | 6.8 | 1.7 |
| 2006 - 2014 | 7.7 | 1.92 |
| 2015 on | 8.2 | 2.40 |
| Resistance | N/A | N/A | 1 |

ADJFloor = Adjustment for floor insulation to account for prescriptive engineering algorithms overclaiming savings.

= 88%[[1454]](#footnote-1455)

Other factors as defined above

For example, a single family home in Chicago with a 20 by 25 footprint, insulated with R-30 spray foam above the crawlspace, a 10.5 SEER Central AC and a newer heat pump:

ΔkWh = (ΔkWh\_cooling + ΔkWh\_heating)

= (((1/3.96 -1/(30+3.96))\*(20\*25)\*(1-0.12)\* 24 \* 281\*0.75)/(1000\*10.5) + (((1/3.96 -1/(30+3.96))\*(20\*25)\*(1-0.15) \* 24 \* 3079)/(3412\*1.92)) \* 0.88)

= (47.3 + 941.1)

= 988.4 kWh

ΔkWh\_heating = If gas *furnace* heat, kWh savings for reduction in fan run time

= ΔTherms \* Fe \* 29.3

Fe = Furnace Fan energy consumption as a percentage of annual fuel consumption

= 3.14%[[1455]](#footnote-1456)

29.3 = kWh per therm

For example, a single family home in Chicago with a 20 by 25 footprint, insulated with R-30 spray foam above the crawlspace, and a 70% efficient furnace (for therm calculation see Natural Gas Savings section):

ΔkWh = 91.2 \* 0.0314 \* 29.3

= 83.9 kWh

**Summer Coincident Peak Demand Savings**

ΔkW = (ΔkWh\_cooling / FLH\_cooling) \* CF

Where:

FLH\_cooling = Full load hours of air conditioning

= Dependent on location:[[1456]](#footnote-1457)

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **Single Family** | **Multifamily** |
| 1 (Rockford) | 512 | 467 |
| 2 (Chicago) | 570 | 506 |
| 3 (Springfield) | 730 | 663 |
| 4 (Belleville) | 1,035 | 940 |
| 5 (Marion) | 903 | 820 |
| Weighted Average[[1457]](#footnote-1458) | 629 | 564 |

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during system peak hour)

= 68%[[1458]](#footnote-1459)

CFSSP = Summer System Peak Coincidence Factor for Heat Pumps (during system peak hour)

= 72%%[[1459]](#footnote-1460)

CFPJM = PJM Summer Peak Coincidence Factor for Central A/C (average during peak period)

= 46.6%[[1460]](#footnote-1461)

For example, a single family home in Chicago with a 20 by 25 footprint, insulated with R-30 spray foam above the crawlspace, a 10.5 SEER Central AC and a newer heat pump:

ΔkWSSP = 47.3 / 570 \* 0.68

= 0.056 kW

ΔkWSSP = 47.3 / 570 \* 0.466

= 0.039 kW

###### Natural Gas Savings

If Natural Gas heating:

ΔTherms = (1/R\_old - 1/(R\_added+R\_old)) \* Area \* (1-Framing\_factor)) \* 24 \* HDD) / (100,000 \* ηHeat) \* ADJFloorGasHeat

ηHeat = Efficiency of heating system

= Equipment efficiency \* distribution efficiency

= Actual. If unknown assume 70%[[1461]](#footnote-1462)

Other factors as defined above

For example, a single family home in Chicago with a 20 by 25 footprint, insulated with R-30 spray foam above the crawlspace, and a 70% efficient furnace:

ΔTherms = (1 / 3.96 – 1 /(30 + 3.96))\*(20 \* 25) \* (1 - 0.12) \* 24 \* 3079) / (100,000 \* 0.70) \* 0.88

= 91.2 therms

**Water Impact Descriptions and Calculation**

N/A

**Deemed O&M Cost Adjustment Calculation**

N/A

###### Measure Code: RS-SHL-FINS-V06-150601

### Wall and Ceiling/Attic Insulation

###### Description

Insulation is added to wall cavities, and/or attic. This measure requires a member of the implementation staff evaluating the pre and post R-values and measure surface areas. The efficiency of the heating and cooling equipment in the home should also be evaluated if possible.

This measure was developed to be applicable to the following program types:  RF.

If applied to other program types, the measure savings should be verified.

###### Definition of Efficient Equipment

This measure requires a member of the implementation staff or a participating contractor to evaluate the pre and post R-values and measure surface areas. The requirements for participation in the program will be defined by the utilities.

###### Definition of Baseline Equipment

The existing condition will be evaluated by implementation staff or a participating contractor and is likely to be empty wall cavities and little or no attic insulation.

###### Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 25 years.[[1462]](#footnote-1463)

###### Deemed Measure Cost

The actual installed cost for this measure should be used in screening.

###### Loadshape

|  |
| --- |
| Loadshape R08 - Residential Cooling |
| Loadshape R09 - Residential Electric Space Heat |
| Loadshape R10 - Residential Electric Heating and Cooling |

###### Coincidence Factor

The summer peak coincidence factor for cooling is provided in two different ways below. The first is used to estimate peak savings during the utility peak hour and is most indicative of actual peak benefits, and the second represents the *average* savings over the defined summer peak period, and is presented so that savings can be bid into PJM’s Forward Capacity Market.

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during utility peak hour)

= 68%[[1463]](#footnote-1464)

CFSSP = Summer System Peak Coincidence Factor for Heat Pumps (during system peak hour)

= 72%%[[1464]](#footnote-1465)

CFPJM   = PJM Summer Peak Coincidence Factor for Central A/C (average during PJM peak period)

= 46.6%[[1465]](#footnote-1466)

Algorithm

###### Calculation of Savings

###### Electric Energy Savings

Where available savings from shell insulation measures should be determined through a custom analysis. When that is not feasible for the program the following engineering algorithms can be used with the inclusion of an adjustment factor to de-rate the heating savings.

ΔkWh = (ΔkWh\_cooling + ΔkWh\_heating)

Where:ΔkWh\_cooling = If central cooling, reduction in annual cooling requirement due to insulation

= [((1/R\_old - 1/R\_wall) \* A\_wall \* (1-Framing\_factor\_wall) + (1/R\_old - 1/R\_attic) \* A\_attic \* (1-Framing\_factor\_attic)) \* 24 \* CDD \* DUA] / (1000 \* ηCool)

R\_wall = R-value of new wall assembly (including all layers between inside air and outside air).

R\_attic = R-value of new attic assembly (including all layers between inside air and outside air).

R\_old = R-value value of existing assemble and any existing insulation.

(Minimum of R-5 for uninsulated assemblies[[1466]](#footnote-1467))

A\_wall = Net area of insulated wall (ft2)

A\_attic = Total area of insulated ceiling/attic (ft2)

Framing\_factor\_wall = Adjustment to account for area of framing

= 25%[[1467]](#footnote-1468)

Framing\_factor\_attic = Adjustment to account for area of framing

= 7%[[1468]](#footnote-1469)

24 = Converts hours to days

CDD = Cooling Degree Days

= dependent on location:[[1469]](#footnote-1470)

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **CDD 65** |
| 1 (Rockford) | 820 |
| 2 (Chicago) | 842 |
| 3 (Springfield) | 1,108 |
| 4 (Belleville) | 1,570 |
| 5 (Marion) | 1,370 |
| Weighted Average[[1470]](#footnote-1471) | 947 |

DUA = Discretionary Use Adjustment (reflects the fact that people do not always operate their AC when conditions may call for it).

= 0.75 [[1471]](#footnote-1472)

1000 = Converts Btu to kBtu

ηCool = Seasonal Energy Efficiency Ratio of cooling system (kBtu/kWh)

= Actual (where it is possible to measure or reasonably estimate). If unknown assume the following:[[1472]](#footnote-1473)

|  |  |
| --- | --- |
| **Age of Equipment** | **ηCool Estimate** |
| Before 2006 | 10 |
| 2006 - 2014 | 13 |
| Central AC After 1/1/2015 | 13 |
| Heat Pump After 1/1/2015 | 14 |

kWh\_heating = If electric heat (resistance or heat pump), reduction in annual electric heating due to insulation

= (((1/R\_old - 1/R\_wall) \* A\_wall \* (1-Framing\_factor\_wall) \* ADJWall ) + (1/R\_old - 1/R\_attic) \* A\_attic \* (1-Framing\_factor\_attic) \* ADJAttic) \* 24 \* HDD] / (ηHeat \* 3412)

HDD = Heating Degree Days

= Dependent on location:[[1473]](#footnote-1474)

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **HDD 60** |
| 1 (Rockford) | 5,352 |
| 2 (Chicago) | 5,113 |
| 3 (Springfield) | 4,379 |
| 4 (Belleville) | 3,378 |
| 5 (Marion) | 3,438 |
| Weighted Average[[1474]](#footnote-1475) | 4,860 |

ηHeat = Efficiency of heating system

= Actual. If not available refer to default table below:[[1475]](#footnote-1476)

| **System Type** | **Age of Equipment** | **HSPF Estimate** | **ηHeat (Effective COP Estimate) (HSPF/3.413)\*0.85** |
| --- | --- | --- | --- |
| Heat Pump | Before 2006 | 6.8 | 1.7 |
| 2006 - 2014 | 7.7 | 1.92 |
| 2015 on | 8.2 | 2.40 |
| Resistance | N/A | N/A | 1 |

3412 = Converts Btu to kWh

ADJWall = Adjustment for wall insulation to account for prescriptive engineering algorithms overclaiming savings.

= 63%[[1476]](#footnote-1477)

ADJAttic = Adjustment for attic insulation to account for prescriptive engineering algorithms overclaiming savings.

= 74%[[1477]](#footnote-1478)

For example, a single family home in Chicago with 990 ft2 of R-5 walls insulated to R-11 and 700 ft2 of R-5 attic insulated to R-38, 10.5 SEER Central AC and 2.26 (1.92 including distribution losses) COP Heat Pump:

ΔkWh = (ΔkWh\_cooling + ΔkWh\_heating)

= ((((1/5 - 1/11) \* 990 \* (1-0.25)) + ((1/5 - 1/38) \* 700 \* (1-0.07))) \* 842 \* 0.75 \* 24)/ (1000 \* 10.5)) + (((((1/5 - 1/11) \* 990 \* (1-0.25) \* 0.63) + ((1/5 - 1/38) \* 700 \* (1-0.07) \* 0.74)) \* 5113 \* 24) / (1.92 \* 3412))

= 280 + 2523

= 2803 kWh

ΔkWh\_heating = If gas *furnace* heat, kWh savings for reduction in fan run time

= ΔTherms \* Fe \* 29.3

Fe = Furnace Fan energy consumption as a percentage of annual fuel consumption

= 3.14%[[1478]](#footnote-1479)

29.3 = kWh per therm

For example, a single family home in Chicago with 990 ft2 of R-5 walls insulated to R-11 and 700 ft2 of R-5 attic insulated to R-38, with a gas furnace with system efficiency of 66% (for therm calculation see Natural Gas Savings section):

ΔkWh = 250.3 \* 0.0314 \* 29.3

= 230 kWh

###### Summer Coincident Peak Demand Savings

ΔkW = (ΔkWh\_cooling / FLH\_cooling) \* CF

Where:

FLH\_cooling = Full load hours of air conditioning

= Dependent on location as below:[[1479]](#footnote-1480)

|  |  |  |
| --- | --- | --- |
| **Climate Zone**  **(City based upon)** | **Single Family** | **Multifamily** |
| 1 (Rockford) | 512 | 467 |
| 2 (Chicago) | 570 | 506 |
| 3 (Springfield) | 730 | 663 |
| 4 (Belleville) | 1,035 | 940 |
| 5 (Marion) | 903 | 820 |
| Weighted Average[[1480]](#footnote-1481) | 629 | 564 |

CFSSP = Summer System Peak Coincidence Factor for Central A/C (during system peak hour)

= 68%[[1481]](#footnote-1482)

CFSSP = Summer System Peak Coincidence Factor for Heat Pumps (during system peak hour)

72%%[[1482]](#footnote-1483)

CFPJM = PJM Summer Peak Coincidence Factor for Central A/C (average during peak period)

= 46.6%[[1483]](#footnote-1484)

For example, a single family home in Chicago with 990 ft2 of R-5 walls insulated to R-11 and 700 ft2 of R-5 attic insulated to R-38, 10.5SEER Central AC and 2.26 COP Heat Pump:

ΔkWSSP = 280 / 570 \* 0.68

= 0.33 kW

ΔkWPJM = 280 / 570 \* 0.466

= 0.23 kW

###### Natural Gas Savings

If Natural Gas heating:

ΔTherms = ((((1/R\_old - 1/R\_wall) \* A\_wall \* (1-Framing\_factor\_wall) \* ADJWall ) + ((1/R\_old - 1/R\_attic) \* A\_attic \* (1-Framing\_factor\_attic) \* ADJAttic)) \* 24 \* HDD) / (ηHeat \* 100,067 Btu/therm)

Where:

HDD = Heating Degree Days

= Dependent on location:[[1484]](#footnote-1485)

|  |  |
| --- | --- |
| **Climate Zone**  **(City based upon)** | **HDD 60** |
| 1 (Rockford) | 5,352 |
| 2 (Chicago) | 5,113 |
| 3 (Springfield) | 4,379 |
| 4 (Belleville) | 3,378 |
| 5 (Marion) | 3,438 |
| Weighted Average[[1485]](#footnote-1486) | 4,860 |

ηHeat = Efficiency of heating system

= Equipment efficiency \* distribution efficiency

= Actual.[[1486]](#footnote-1487) If unknown assume 70%.[[1487]](#footnote-1488)

Other factors as defined above

For example, a single family home in Chicago with 990 ft2 of R-5 walls insulated to R-11 and 700 ft2 of R-5 attic insulated to R-38, with a gas furnace with system efficiency of 66%:

ΔTherms = ((((1/5 - 1/11) \* 990 \* (1-0.25) \*0.63) + ((1/5 - 1/38) \* 700 \* (1-0.07)\*0.74)) \* 24 \* 5113) / (0.66 \* 100,067)

= 250.3 therms

###### Water Impact Descriptions and Calculation

N/A

###### Deemed O&M Cost Adjustment Calculation

N/A

###### Measure Code: RS-SHL-AINS-V05-150201

1. Being an open forum, this list of SAG stakeholders and participants may change at any time. [↑](#footnote-ref-2)
2. 220 ILCS 5/8-103 and 220 ILCS 5/8-104. [↑](#footnote-ref-3)
3. In addition to DCEO, the Program Administrators include: Ameren Illinois, ComEd, Peoples Gas, North Shore Gas, and Nicor Gas (collectively, the Utilities). [↑](#footnote-ref-4)
4. The Illinois TRC test is defined in 220 ILCS 5/8-104(b) and 20 ILCS 3855/1-10. [↑](#footnote-ref-5)
5. Illinois Statewide Technical Reference Manual Request for Proposals, August 22, 2011, pages 3-4, <http://ilsag.org/yahoo_site_admin/assets/docs/TRM_RFP_Final_part_1.230214520.pdf> [↑](#footnote-ref-6)
6. The Illinois Utilities subject to this TRM include: Ameren Illinois Company d/b/a Ameren Illinois (Ameren), Commonwealth Edison Company (ComEd), The Peoples Gas Light and Coke Company and North Shore Gas Company (Integrys), and Northern Illinois Gas Company d/b/a Nicor Gas. [↑](#footnote-ref-7)
7. [http://www.icc.illinois.gov/docket/files.aspx?no=10-0570&docId=159809](http://www.eia.gov/consumption/residential/data/2009/xls/HC7.9%20Air%20Conditioning%20in%20Midwest%20Region.xls?no=10-0570&docId=159809) [↑](#footnote-ref-8)
8. [http://www.icc.illinois.gov/docket/files.aspx?no=10-0568&docId=167031](http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117_RLW_CF%20Res%20RAC.pdf?no=10-0568&docId=167031) [↑](#footnote-ref-9)
9. [http://www.icc.illinois.gov/docket/files.aspx?no=10-0564&docId=167023](http://www.icc.illinois.gov/downloads/public/edocket/303835.pdf?no=10-0564&docId=167023) [↑](#footnote-ref-10)
10. [http://www.icc.illinois.gov/docket/files.aspx?no=10-0562&docId=167027](http://www.aquacraft.com/sites/default/files/pub/DeOreo-(2001)-Disaggregated-Hot-Water-Use-in-Single-Family-Homes-Using-Flow-Trace-Analysis.pdf?no=10-0562&docId=167027) [↑](#footnote-ref-11)
11. <http://www.icc.illinois.gov/docket/files.aspx?no=12-0528&docId=187554> [↑](#footnote-ref-12)
12. <http://www.icc.illinois.gov/docket/files.aspx?no=13-0437&docId=200492> [↑](#footnote-ref-13)
13. <http://www.icc.illinois.gov/docket/files.aspx?no=13-0077&docId=203903>; <http://www.icc.illinois.gov/docket/files.aspx?no=13-0077&docId=195913>; <http://www.icc.illinois.gov/downloads/public/edocket/339744.pdf> [↑](#footnote-ref-14)
14. <http://www.icc.illinois.gov/docket/files.aspx?no=14-0189&docId=210478> <http://www.icc.illinois.gov/downloads/public/Illinois_Statewide_TRM_Effective_060114_Version_3.0_022414_Clean.pdf> [↑](#footnote-ref-15)
15. Errata as well as links to the official IL-TRM documents, dockets, and policy documents are available on the following ICC webpage: <http://www.icc.illinois.gov/electricity/TRM.aspx> [↑](#footnote-ref-16)
16. Emphasis has been added to denote the difference between a “deemed value” and a “deemed savings estimate”. A deemed value refers to a single input value to an algorithm, while a deemed savings estimate is the result of calculating the end result of all of the values in the savings algorithm. [↑](#footnote-ref-17)
17. Note that the Public sector buildings and low income measures that DCEO administers are not listed as a separate Market Sector. The Public building type is one of a series of building types that are included in the appropriate measures in the Commercial and Industrial Sector. [↑](#footnote-ref-18)
18. Please note that this is not an exhaustive list of end-uses and that others may be included in future versions of the TRM. [↑](#footnote-ref-19)
19. To gain access to the SharePoint web site, please contact the TRM Administrator, Nikki Clace at [iltrmadministrator@veic.org](mailto:nclace@veic.org). [↑](#footnote-ref-20)
20. At the time of this draft, we understand that some standard T8 lamps may meet the federal standard, and in that event, some T12 retrofits may end up being completed with standard T8s instead of high performance T8s. [↑](#footnote-ref-21)
21. These criteria were documented in a memo entitled, “Early Replacement Measure Issue Summary\_0409.docx.” [↑](#footnote-ref-22)
22. Appliance Standards Awareness Project, <http://www.appliance-standards.org/product/furnaces> [↑](#footnote-ref-23)
23. Illinois Statewide Technical Reference Manual, May 13, 2013, pp 191, 439 [↑](#footnote-ref-24)
24. Source: US EPA, [www.energystar.gov](http://www.energystar.gov/ia/business/bulk_purchasing/bpsavings_calc/CalculatorConsumerDishwasher.xls), Space Type Definitions [↑](#footnote-ref-25)
25. Measures that apply to the multifamily and public housing building types describe how to handle tenant versus master metered buildings. [↑](#footnote-ref-26)
26. Docket No. 07-0540, Final Order at 32-33, February 6, 2008.

    [http://www.icc.illinois.gov/downloads/public/edocket/215193.pdf](http://www.epelectricefficiency.com/downloads.asp) [↑](#footnote-ref-27)
27. All loadshape information has been posted to the project’s Sharepoint site, and may be provided publically through the Stakeholder Advisory Group’s web site at their discretion. <http://www.ilsag.info/technical-reference-manual.html> [↑](#footnote-ref-28)
28. 30-year normals have been used instead of Typical Meteorological Year (TMY) data due to the fact that few of the measures in the TRM are significantly affected by solar insolation, which is one of the primary benefits of using the TMY approach. [↑](#footnote-ref-29)
29. Belzer and Cort, Pacific Northwest National Laboratory in “Statistical Analysis of Historical State-Level Residential Energy Consumption Trends,” 2004. [↑](#footnote-ref-30)
30. Energy Center of Wisconsin, May 2008 metering study; “Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research”, p. 32 (amended in 2010). [↑](#footnote-ref-31)
31. This value is based upon experience, and it is preferable to use building-specific base temperatures when available. [↑](#footnote-ref-32)
32. For more information, please refer to the document, ‘Dealing with interactive Effects During Measure Characterization” Memo to the Stakeholder Advisory Group dated 12/9/11. [↑](#footnote-ref-33)
33. Equipment life is expected to be longer, but measure life is more conservative to account for possible attrition in use over time. [↑](#footnote-ref-34)
34. Based on bulk pricing reported by EnSave, which administers the rebate in Vermont [↑](#footnote-ref-35)
35. Act on Energy Commercial Technical Reference Manual No. 2010-4 [↑](#footnote-ref-36)
36. Ibid. [↑](#footnote-ref-37)
37. Ibid. [↑](#footnote-ref-38)
38. Ibid. [↑](#footnote-ref-39)
39. Ibid. [↑](#footnote-ref-40)
40. Act on Energy Commercial Technical Reference Manual No. 2010-4 [↑](#footnote-ref-41)
41. Ibid. [↑](#footnote-ref-42)
42. Ibid. [↑](#footnote-ref-43)
43. Ibid. [↑](#footnote-ref-44)
44. Ibid. [↑](#footnote-ref-45)
45. Act on Energy Commercial Technical Reference Manual No. 2010-4 [↑](#footnote-ref-46)
46. Ibid. [↑](#footnote-ref-47)
47. Ibid. [↑](#footnote-ref-48)
48. Ibid. [↑](#footnote-ref-49)
49. Ibid. [↑](#footnote-ref-50)
50. http://www.fishnick.com/saveenergy/rebates/combis.pdf [↑](#footnote-ref-51)
51. Deemed values from Nicor Gas were used. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011. [↑](#footnote-ref-52)
52. Ibid. [↑](#footnote-ref-53)
53. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011.These deemed values should be compared to PY evaluation and revised as necessary. [↑](#footnote-ref-54)
54. 2008 Database for Energy-Efficiency Resources (DEER), Version 2008.2.05, “Effective/Remaining Useful Life Values”, California Public Utilities Commission, December 16, 2008.

    http://www.ctsavesenergy.org/files/Measure%20Life%20Report%202007.pdf [↑](#footnote-ref-55)
55. Estimates of the incremental cost of commercial refrigerators and freezers varies widely by source. Nadel, S., Packaged Commercial Refrigeration Equipment: A Briefing Report for Program Planners and Implementers, ACEEE, December 2002, indicates that incremental cost is approximately zero. Efficiency Vermont Technical Reference User Manual (TRM) Measure Savings Algorithms and Cost Assumptions, February, 19, 2010, assumed incremental cost ranging from $75 to $125 depending on equipment volume. ACEEE notes that incremental cost ranges from 0 to 10% of the baseline unit cost <http://www.aceee.org/ogeece/ch5\_reach.htm>. For the purposes of this characterization, assume and incremental cost adder of 5% on the full unit costs presented in Goldberg et al, State of Wisconsin Public Service Commission of Wisconsin, Focus on Energy Evaluation, Business Programs: Incremental Cost Study, KEMA, October 28, 2009. [↑](#footnote-ref-56)
56. The CF for Commercial Refrigeration was calculated based upon the Ameren provided eShapes [↑](#footnote-ref-57)
57. Energy Policy Act of 2005. Accessed on 7/7/10. <http://www.epa.gov/oust/fedlaws/publ\_109-058.pdf> [↑](#footnote-ref-58)
58. ENERGY STAR Program Requirements for Commercial Refrigerators and Freezers Partner Commitments Version 2.0, U.S. Environmental Protection Agency, Accessed on 7/7/10. < http://www.energystar.gov/ia/partners/product\_specs/program\_reqs/commer\_refrig\_glass\_prog\_req.pdf> [↑](#footnote-ref-59)
59. California DEER 2008 which is also used by both the Food Service Technology Center and ENERGY STAR®. [↑](#footnote-ref-60)
60. Source for incremental cost for efficient natural gas steamer is RSG Commercial Gas Steamer Workpaper, January 2012. [↑](#footnote-ref-61)
61. Source for efficient electric steamer incremental cost is $2,490 per 2009 PG&E Workpaper - PGECOFST104.1 - Commercial Steam Cooker - Electric and Gas as reference by KEMA in the ComEd C & I TRM. [↑](#footnote-ref-62)
62. Minnesota 2012 Technical Reference Manual, [Electric Food Service\_v03.2.xls](http://www.icc.illinois.gov/downloads/public/edocket/303835.pdf), <http://mn.gov/commerce/energy/topics/conservation/Design-Resources/Deemed-Savings.jspech>. Unknown is an average of other location types [↑](#footnote-ref-63)
63. Food Service Technology Center 2011 Savings Calculator [↑](#footnote-ref-64)
64. Food Service Technology Center 2011 Savings Calculator [↑](#footnote-ref-65)
65. Production capacity per Food Service Technology Center 2011 Savings Calculator of 23.3333 lb/hr per pan for electric baseline steam cookers and 21.6667 lb/hr per pan for natural gas baseline steam cookers. ENERGY STAR® savings calculator uses 23.3 lb/hr per pan for both electric and natural gas baseline steamers. [↑](#footnote-ref-66)
66. Reference ENERGY STAR® savings calculator at http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COC. [↑](#footnote-ref-67)
67. Reference Food Service Technology Center 2011 Savings Calculator values as used by Consortium for Energy Efficiency, Inc. for baseline electric and natural gas steamer heavy cooking load energy efficiencies. [↑](#footnote-ref-68)
68. Minnesota 2012 Technical Reference Manual, [Electric Food Service\_v03.2.xls](http://www1.eere.energy.gov/buildings/building_america/analysis_spreadsheets.html), http://mn.gov/commerce/energy/topics/conservation/Design-Resources/Deemed-Savings.jspech [↑](#footnote-ref-69)
69. Unknown is average of other locations [↑](#footnote-ref-70)
70. Reference amount used by both Food Service Technology Center and ENERGY STAR® savings calculator [↑](#footnote-ref-71)
71. Reference information from the Food Service Technology Center siting that ENERGY STAR® steamers are not typically operated in constant steam mode, but rather are used in timed mode. Reference ENERGY STAR® savings calculator at http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COC for efficient steamer. Both baseline & efficient steamer mode values should be considered for users in Illinois market. [↑](#footnote-ref-72)
72. Food Service Technology Center 2011 Savings Calculator [↑](#footnote-ref-73)
73. Production capacity per Food Service Technology Center 2011 Savings Calculator of 18.3333 lb/hr per pan for gas ENERGY STAR® steam cookers and 16.6667  lb/hr per pan for electric ENERGY STAR® steam cookers.  ENERGY STAR® savings calculator uses 16.7 lb/hr per pan for electric and 20 lb/hr for natural gas ENERGY STAR® steamers. [↑](#footnote-ref-74)
74. Reference Food Service Technology Center 2011 Savings Calculator values as used by Consortium for Energy Efficiency, Inc. for Tier 1A and Tier 1B qualified electric and natural gas steamer heavy cooking load energy efficiencies and http://www.energystar.gov/ia/partners/product\_specs/program\_reqs/Commercial\_Steam\_Cookers\_Program\_Requirements.pdf?7010-36eb [↑](#footnote-ref-75)
75. Reference ENERGY STAR® savings calculator at http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COC and Food [↑](#footnote-ref-76)
76. Reference ENERGY STAR® savings calculator at http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COC and Food [↑](#footnote-ref-77)
77. Ohio TRM which references 2002 Food Service Technology Center "Commercial Cooking Appliance Technology Assessment" Chapter 8: Steamers. This is time also used by ENERGY STAR® savings calculator at [http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COC](http://www.bpa.gov/energy/n/reports/evaluation/residential/faucet_aerator.cfm?fuseaction=find_a_product.showProductGroup&pgw_code=COC). 11,000 Btu/preheat is from 72,000 Btu/hr \* 15 min/hr /60 min/hr for gas steamers and 0.5 kWh/preheat is from 6 kW/preheat \* 15 min/hr / 60 min/hr [↑](#footnote-ref-78)
78. Reference Food Service Technology Center 2011 Savings Calculator values for Baseline Preheat Energy. [↑](#footnote-ref-79)
79. Reference Food Service Technology Center 2011 Savings Calculator values as used by Consortium for Energy Efficiency, Inc. for baseline electric and natural gas steamer heavy cooking load energy efficiencies. [↑](#footnote-ref-80)
80. Ibid. [↑](#footnote-ref-81)
81. Amount used by both Food Service Technology Center and ENERGY STAR® savings calculator [↑](#footnote-ref-82)
82. Reference ENERGY STAR® savings calculator at http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COC. [↑](#footnote-ref-83)
83. Ibid. [↑](#footnote-ref-84)
84. Ibid. [↑](#footnote-ref-85)
85. Minnesota 2012 Technical Reference Manual, [Electric Food Service\_v03.2.xls](http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls), http://mn.gov/commerce/energy/topics/conservation/Design-Resources/Deemed-Savings.jspech [↑](#footnote-ref-86)
86. FSTC (2002). Commercial Cooking Appliance Technology Assessment. Chapter 8: Steamers. [↑](#footnote-ref-87)
87. Source Consortium for Energy Efficiency, Inc. September 2010 "Program Design Guidance for Steamers" for Tier 1A and Tier 1B water requirements. Ohio Technical Reference Manual 2010 for 10 gal/hr water consumption which can be used when Tier level is not known. [↑](#footnote-ref-88)
88. Source for 365.25 days/yr is ENERGY STAR® savings calculator which references Food Service Technology research on average use, 2009. [↑](#footnote-ref-89)
89. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011 [↑](#footnote-ref-90)
90. Ibid. [↑](#footnote-ref-91)
91. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011.These deemed values should be compared to PY evaluation and revised as necessary [↑](#footnote-ref-92)
92. Lifetime from ENERGY STAR commercial griddle which cites reference as “FSTC research on available models, 2009” http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-93)
93. Measure cost from ENERGY STAR which cites reference as “EPA research on available models using AutoQuotes, 2010” http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-94)
94. Algorithms and assumptions derived from ENERGY STAR Oven Commercial Kitchen Equipment Savings Calculator.http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-95)
95. Lifetime from ENERGY STAR HFHC which cites reference as “FSTC research on available models, 2009” http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-96)
96. Measure cost from ENERGY STAR which cites reference as “EPA research on available models using AutoQuotes, 2010” http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-97)
97. Minnesota 2012 Technical Reference Manual, [Electric Food Service\_v03.2.xls](http://www.aquacraft.com/sites/default/files/pub/DeOreo-(2001)-Disaggregated-Hot-Water-Use-in-Single-Family-Homes-Using-Flow-Trace-Analysis.pdf), http://mn.gov/commerce/energy/topics/conservation/Design-Resources/Deemed-Savings.jspech [↑](#footnote-ref-98)
98. Algorithms and assumptions derived from ENERGY STAR Commercial Kitchen Equipment Savings Calculator.http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-99)
99. Lifetime from ENERGY STAR commercial griddle which cites reference as “FSTC research on available models, 2009” http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-100)
100. Measure cost from ENERGY STAR which cites reference as “EPA research on available models using AutoQuotes, 2010” http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-101)
101. Algorithms and assumptions derived from ENERGY STAR fryer Commercial Kitchen Equipment Savings Calculator.http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-102)
102. Lifetime from ENERGY STAR commercial griddle which cites reference as “FSTC research on available models, 2009” http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-103)
103. Measure cost from ENERGY STAR which cites reference as “EPA research on available models using AutoQuotes, 2010” http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-104)
104. Minnesota 2012 Technical Reference Manual, [Electric Food Service\_v03.2.xls](http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls), http://mn.gov/commerce/energy/topics/conservation/Design-Resources/Deemed-Savings.jspech [↑](#footnote-ref-105)
105. Algorithms and assumptions derived from ENERGY STAR Griddle Commercial Kitchen Equipment Savings Calculator.http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-106)
106. Lifetime from ENERGY STAR HFHC which cites reference as “FSTC research on available models, 2009” http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-107)
107. Measure cost from ENERGY STAR which cites reference as “EPA research on available models using AutoQuotes, 2010” http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-108)
108. Minnesota 2012 Technical Reference Manual, [Electric Food Service\_v03.2.xls](http://neep.org/uploads/EMV%20Forum/EMV%20Studies/measure_life_GDS%5b1%5d.pdf), http://mn.gov/commerce/energy/topics/conservation/Design-Resources/Deemed-Savings.jspech [↑](#footnote-ref-109)
109. Algorithms and assumptions derived from ENERGY STAR Commercial Kitchen Equipment Savings Calculator.http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=COG [↑](#footnote-ref-110)
110. DEER 2008 [↑](#footnote-ref-111)
111. These values are from electronic work papers prepared in support of San Diego Gas & Electric’s “Application for Approval of Electric and Gas Energy Efficiency Programs and Budgets for Years 2009-2011”, SDGE, March 2, 2009. Accessed on 7/7/10 <http://www.sdge.com/regulatory/documents/ee2009-2011Workpapers/SW-ComB/Food%20Service/Food%20Service%20Electic%20Measure%20Workpapers%2011-08-05.DOC>. [↑](#footnote-ref-112)
112. Baseline reflects federal standards which apply to units manufactured on or after January 1, 2010 <http://ecfr.gpoaccess.gov/cgi/t/text/text-idx?c=ecfr&rgn=div6&view=text&node=10:3.0.1.4.17.8&idno=10>. [↑](#footnote-ref-113)
113. ENERGY STAR Program Requirements for Commercial Ice Machines, Partner Commitments, U.S. Environmental Protection Agency, Accessed on 7/7/10 <http://www.energystar.gov/ia/partners/product\_specs/program\_reqs/ice\_machine\_prog\_req.pdf> [↑](#footnote-ref-114)
114. Duty cycle varies considerably from one installation to the next. TRM assumptions from Vermont, Wisconsin, and New York vary from 40 to 57%, whereas the ENERGY STAR Commercial Ice Machine Savings Calculator < [http://www.energystar.gov/ia/business/bulk\_purchasing/bpsavings\_calc/Calc\_Ice\_Machines.xls](http://www.deeresources.com)> assumes a value of 75%. A field study of eight ice machines in California indicated an average duty cycle of 57% (“A Field Study to Characterize Water and Energy Use of Commercial Ice-Cube Machines and Quantify Saving Potential”, Food Service Technology Center, December 2007). Furthermore, a report prepared by ACEEE assumed a value of 40% (Nadel, S., Packaged Commercial Refrigeration Equipment: A Briefing Report for Program Planners and Implementers, ACEEE, December 2002). The value of 57% was utilized since it appears to represent a high quality data source. [↑](#footnote-ref-115)
115. Unit is assumed to be connected to power 24 hours per day, 365.25 days per year. [↑](#footnote-ref-116)
116. AHRI Certification Directory, Accessed on 7/7/10. <http://www.ahridirectory.org/ahridirectory/pages/home.aspx> [↑](#footnote-ref-117)
117. Verification measurements taken at 195 installations showed average pre and post flowrates of 2.23 and 1.12 gallon per minute, respectively.” from IMPACT AND PROCESS EVALUATION FINAL REPORT for CALIFORNIA URBAN WATER CONSERVATION COUNCIL 2004-5 PRE-RINSE SPRAY VALVE INSTALLATION PROGRAM (PHASE 2) (PG&E Program # 1198-04; SoCalGas Program 1200-04) (“CUWCC Report”, Feb 2007) [↑](#footnote-ref-118)
118. Reference 2010 Ohio Technical Reference Manual, Act on Energy Business Program Technical Reference Manual Rev05, and Federal Energy Management Program (2004), "How to Buy a Low-Flow Pre-Rinse Spray Valve." [↑](#footnote-ref-119)
119. Costs range from $60 Chicagoland (Integrys for North Shore & People's Gas) to $150 referenced by Nicor's CLEAResultWorkpaper WPRSGCCODHW102 "Pre-Rinse Spray Valve." Act on Energy references $100. [↑](#footnote-ref-120)
120. If unknown, assume a 70 degree temperature rise from Tin per Food Service Technology Center calculator assumptions to account for variations in mixing and water heater efficiencies [↑](#footnote-ref-121)
121. August 31, 2011 Memo of Savings for Hot Water Savings Measures to Nicor Gas from Navigant states that 54.1°F was calculated from the weighted average of monthly water mains temperatures reported in the 2010 Building America Benchmark Study for Chicago-Waukegan, Illinois. [↑](#footnote-ref-122)
122. This efficiency value is based on IECC 2012 performance requirement for electric resistant water heaters rounded without the slight adjustment allowing for reduction based on size of storage tank. [↑](#footnote-ref-123)
123. IECC 2012, Table C404.2, Minimum Performance of Water-Heating Equipment [↑](#footnote-ref-124)
124. In order to calculate energy savings, water savings must first be calculated [↑](#footnote-ref-125)
125. The baseline equipment is assumed to be 1.6 gallons per minute. The Energy Policy Act (EPAct) of 2005 sets the maximum flow rate for pre-rinse spray valves at 1.6 gallons per minute at 60 pounds per square inch of water pressure when tested in accordance with ASTM F2324-03. This performance standard went into effect January 1, 2006. www1.eere.energy.gov/femp/pdfs/spec\_prerinsesprayvavles.pdf. [↑](#footnote-ref-126)
126. Verification measurements taken at 195 installations showed average pre and post flowrates of 2.23 and 1.12 gallon per minute, respectively.” from IMPACT AND PROCESS EVALUATION FINAL REPORT for CALIFORNIA URBAN WATER CONSERVATION COUNCIL 2004-5 PRE-RINSE SPRAY VALVE INSTALLATION PROGRAM (PHASE 2) (PG&E Program # 1198-04; SoCalGas Program 1200-04) (“CUWCC Report”, Feb 2007) [↑](#footnote-ref-127)
127. 1.6 gallons per minute used to be the high efficiency flow, but more efficient spray valves are available ranging down to 0.64 gallons per minute per Federal Energy Management Program which references the Food Services Technology Center web site with the added note that even more efficient models may be available since publishing the data. The average of the nozzles listed on the FSTC website is 1.06. [↑](#footnote-ref-128)
128. 1.6 gallons per minute used to be the high efficiency flow, but more efficient spray valves are available ranging down to 0.64 gallons per minute per Federal Energy Management Program which references the Food Services Technology Center web site with the added note that even more efficient models may be available since publishing the data. The average of the nozzles listed on the FSTC website is 1.06. [↑](#footnote-ref-129)
129. Hours primarily based on PG& E savings estimates, algorithms, sources (2005), Food Service Pre-Rinse Spray Valves with review of 2010 Ohio Technical Reference Manual and Act on Energy Business Program Technical Resource Manual Rev05. [↑](#footnote-ref-130)
130. Food Service Technology Center, ENERGY STAR and CEE do not currently provide calculators for this type of equipment therefore deemed values from Nicor Gas were used. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011 [↑](#footnote-ref-131)
131. Ibid. [↑](#footnote-ref-132)
132. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011.These deemed values should be compared to PY evaluation and revised as necessary. [↑](#footnote-ref-133)
133. Food Service Technology Center, ENERGY STAR and CEE do not currently provide calculators for this type of equipment therefore deemed values from Nicor Gas were used. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011 [↑](#footnote-ref-134)
134. Ibid. [↑](#footnote-ref-135)
135. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011.These deemed values should be compared to PY evaluation and revised as necessary. [↑](#footnote-ref-136)
136. Food Service Technology Center, ENERGY STAR and CEE do not currently provide calculators for this type of equipment therefore deemed values from Nicor Gas were used. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011 [↑](#footnote-ref-137)
137. Ibid. [↑](#footnote-ref-138)
138. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011.These deemed values should be compared to PY evaluation and revised as necessary. [↑](#footnote-ref-139)
139. Food Service Technology Center, ENERGY STAR and CEE do not currently provide calculators for this type of equipment therefore deemed values from Nicor Gas were used. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011 [↑](#footnote-ref-140)
140. Ibid. [↑](#footnote-ref-141)
141. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011.These deemed values should be compared to PY evaluation and revised as necessary [↑](#footnote-ref-142)
142. PG&E Workpaper: Commercial Kitchen Demand Ventilation Controls-Electric, 2004 - 2005 [↑](#footnote-ref-143)
143. Ibid. [↑](#footnote-ref-144)
144. PGE Workpaper, Commercial Kitchen Demand Ventilation Controls, PGECOFST116, June 1, 2009, 4,734 cfm reduction on average , with 7.75 fan horsepower on average. [↑](#footnote-ref-145)
145. Food Service Technology Center Outside Air Load Calculator, <http://www.fishnick.com/ventilation/oalc/oac.php>, with inputs of one cfm, and hours from Commercial Kitchen Demand Ventilation Controls (Average 17.8 hours a day 4.45 am to 10.30 pm). Savings for Rockford, Chicago, and Springfield were obtained from the calculator; values for Belleview and Marion were obtained by using the average savings per HDD from the other values. [↑](#footnote-ref-146)
146. Work Paper WPRRSGNGRO301 CLEAResult"Boiler Tune-Up" which cites Focus on Energy Evaluation Business Programs: Deemed Savings Manual V1.0, PA Consulting, KEMA, March 22, 2010 [↑](#footnote-ref-147)
147. Food Service Technology Center, ENERGY STAR and CEE do not currently provide calculators for this type of equipment therefore deemed values from Nicor Gas were used. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011 [↑](#footnote-ref-148)
148. Ibid. [↑](#footnote-ref-149)
149. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011.These deemed values should be compared to PY evaluation and revised as necessary. [↑](#footnote-ref-150)
150. Food Service Technology Center, ENERGY STAR and CEE do not currently provide calculators for this type of equipment therefore deemed values from Nicor Gas were used. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011 [↑](#footnote-ref-151)
151. Ibid. [↑](#footnote-ref-152)
152. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011.These deemed values should be compared to PY evaluation and revised as necessary [↑](#footnote-ref-153)
153. Food Service Technology Center (FSTC). Default value from life cycle cost calculator. <http://www.fishnick.com/saveenergy/tools/calculators/eovencalc.php> [↑](#footnote-ref-154)
154. Based on data from the Regional Technical Forum for the Northwest Council (<http://rtf.nwcouncil.org/measures/com/ComCookingConvectionOven_v2_0.xlsm>) using actual list prices for 23 units from 2012, see “ComCookingConvectionOven\_v2\_0.xlsm”. [↑](#footnote-ref-155)
155. Minnesota 2012 Technical Reference Manual, [Electric Food Service\_v03.2.xls](http://www.icc.illinois.gov/downloads/public/edocket/303835.pdf), <http://mn.gov/commerce/energy/topics/conservation/Design-Resources/Deemed-Savings.jspech>. Unknown is an average of other location types [↑](#footnote-ref-156)
156. Minnesota 2012 Technical Reference Manual, [Electric Food Service\_v03.2.xls](http://www1.eere.energy.gov/buildings/building_america/analysis_spreadsheets.html), http://mn.gov/commerce/energy/topics/conservation/Design-Resources/Deemed-Savings.jspech [↑](#footnote-ref-157)
157. Unknown is average of other locations [↑](#footnote-ref-158)
158. Food Service Technology Center (FSTC). Default value from life cycle cost calculator. <http://www.fishnick.com/saveenergy/tools/calculators/eovencalc.php> [↑](#footnote-ref-159)
159. Food Service Technology Center (2002). *Commercial Cooking Appliance Technology Assessment*. Prepared by Don Fisher. Chapter 7: Ovens [↑](#footnote-ref-160)
160. American Society for Testing and Materials. Industry standard for Commercial Ovens [↑](#footnote-ref-161)
161. Food Service Technology Center (FSTC). Default value from life cycle cost calculator. <http://www.fishnick.com/saveenergy/tools/calculators/eovencalc.php> [↑](#footnote-ref-162)
162. Food Service Technology Center (FSTC). Default values from life cycle cost calculator. <http://www.fishnick.com/saveenergy/tools/calculators/eovencalc.php> [↑](#footnote-ref-163)
163. Average ratings of units on ENERGY STAR qualified list as of 10/2014. Preheat energy is not provided so default is provided based on FSTC life cycle cost calculator. [↑](#footnote-ref-164)
164. Minnesota 2012 Technical Reference Manual, [Electric Food Service\_v03.2.xls](http://www.icc.illinois.gov/downloads/public/edocket/303835.pdf), <http://mn.gov/commerce/energy/topics/conservation/Design-Resources/Deemed-Savings.jspech>. Unknown is an average of other location types [↑](#footnote-ref-165)
165. Act on Energy Commercial Technical Reference Manual No. 2010-4 [↑](#footnote-ref-166)
166. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011 [↑](#footnote-ref-167)
167. Gas Storage Water Heater 0.67. Work Paper WPRSGNGDHW106. Resource Solutions Group. December 2010 [↑](#footnote-ref-168)
168. Ibid. [↑](#footnote-ref-169)
169. Ibid. [↑](#footnote-ref-170)
170. Ibid. [↑](#footnote-ref-171)
171. Ibid. [↑](#footnote-ref-172)
172. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011. These deemed values should be compared to PY evaluation and revised as necessary [↑](#footnote-ref-173)
173. Gas Storage Water Heater 0.67. Work Paper WPRSGNGDHW106. Resource Solutions Group. December 2010 [↑](#footnote-ref-174)
174. Table C-6, Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007. "http://neep.org/Assets/uploads/files/emv/emv-library/measure\_life\_GDS%5B1%5D.pdf" [↑](#footnote-ref-175)
175. Direct-install price per faucet assumes cost of aerator and install time. (2011, Market research average of $3 and assess and install time of $5 (20min @ $15/hr) [↑](#footnote-ref-176)
176. This algorithm calculates the amount of energy saved per aerator by determining the fraction of water consumption savings for the upgraded fixture. Due to the distribution of water consumption by fixture type, as well as the different number of fixtures in a building, several variables must be incorporated. [↑](#footnote-ref-177)
177. [Maureen](http://portal.veic.org/projects/illinoistrm/Lists/TRM%20Request%20Tracker/Attachments/287/%20Maureen) Hodgins, email message to TAC/SAG, August 26, 2014 [↑](#footnote-ref-178)
178. Measurement should be based on actual average flow consumed over a period of time rather than a onetime spot measurement for maximum flow. Studies have shown maximum flow rates do not correspond well to average flow rate due to occupant behavior which does not always use maximum flow. [↑](#footnote-ref-179)
179. 2008, Schultdt, Marc, and Debra Tachibana. Energy related Water Fixture Measurements: Securing the Baseline for Northwest Single Family Homes. 2008 ACEEE Summer Study on Energy Efficiency in Buildings. Page 1-265. www.seattle.gov/light/Conserve/Reports/paper\_10.pdf [↑](#footnote-ref-180)
180. Average retrofit flow rate for kitchen and bathroom faucet aerators from sources 2, 4, 5, and 7. This accounts for all throttling and differences from rated flow rates. Assumes all kitchen aerators at 2.2 gpm or less and all bathroom aerators at 1.5 gpm or less. The most comprehensive available studies did not disaggregate kitchen use from bathroom use, but instead looked at total flow and length of use for all faucets. This makes it difficult to reliably separate kitchen water use from bathroom water use. It is possible that programs installing low flow aerators lower than the 2.2 gpm for kitchens and 1.5 gpm for bathrooms will see a lower overall average retrofit flow rate. [↑](#footnote-ref-181)
181. Measurement should be based on actual average flow consumed over a period of time rather than a onetime spot measurement for maximum flow. Studies have shown maximum flow rates do not correspond well to average flow rate due to occupant behavior which does not always use maximum flow. [↑](#footnote-ref-182)
182. 2008, Schultdt, Marc, and Debra Tachibana. Energy related Water Fixture Measurements: Securing the Baseline for Northwest Single Family Homes. 2008 ACEEE Summer Study on Energy Efficiency in Buildings. Page 1-265. www.seattle.gov/light/Conserve/Reports/paper\_10.pdf [↑](#footnote-ref-183)
183. Table 2-45 Chapter 49, Service Water Heating, 2007 ASHRAE Handbook, HVAC Applications. [↑](#footnote-ref-184)
184. Estimated based on data provided in Appendix E; “Waste Not, Want Not: The Potential for Urban Water Conservation in California”; http://www.pacinst.org/reports/urban\_usage/appendix\_e.pdf [↑](#footnote-ref-185)
185. Based on review of the Illinois plumbing code (Employees and students per faucet). Retail, grocery, warehouse and health are estimates. Meals per faucet estimated as 4 bathroom and 3 kitchen faucets and average meals per day of 250 (based on California study above) – 250/7 = 36. Fast food assumption estimated. [↑](#footnote-ref-186)
186. Cadmus and Opinion Dynamics Showerhead and Faucet Aerator Meter Study Memorandum dated June 2013, directed to Michigan Evaluation Working Group. If the aerator location is unknown an average of 91% should be used which is based on the assumption that 70% of household water runs through the kitchen faucet and 30% through the bathroom (0.7\*93)+(0.3\*86)=0.91. [↑](#footnote-ref-187)
187. US DOE Building America Program. Building America Analysis Spreadsheet. For Chicago, IL <http://www1.eere.energy.gov/buildings/building_america/analysis_spreadsheets.html>. [↑](#footnote-ref-188)
188. Electric water heaters have recovery efficiency of 98%: <http://www.ahridirectory.org/ahridirectory/pages/home.aspx> [↑](#footnote-ref-189)
189. ComEd Energy Efficiency/ Demand Response Plan: Plan Year 2 (6/1/2009-5/31/2010) Evaluation Report: All Electric Single Family Home Energy Performance Tune-Up Program Table 3-8 <http://ilsagfiles.org/SAG_files/Evaluation_Documents/ComEd/ComEd%20EPY2%20Evaluation%20Reports/ComEd_All_Electric_Single_Family_HEP_PY2_Evaluation_Report_Final.pdf> [↑](#footnote-ref-190)
190. 54.5% is the proportion of hot 120F water mixed with 54.1F supply water to give 90°F mixed faucet water. [↑](#footnote-ref-191)
191. Calculated as follows: Assumptions for percentage of usage during peak period (1-5pm) were made and then multiplied by 65/365 (65 being the number of days in peak period) and by the number of total annual recovery hours to give an estimate of the number of hours of recovery during peak periods. There are 260 hours in the peak period so the probability you will see savings during the peak period is calculated as the number of hours of recovery during peak divided by 260. See ‘C&I Faucet Aerator.xls’ for details. [↑](#footnote-ref-192)
192. Review of AHRI Directory suggests range of recovery efficiency ratings for new Gas DHW units of 70-87%. Average of existing units is estimated at 75%. Commercial properties are more similar to MF homes than SF homes. MF hot water is often provided by a larger commercial boiler. This suggests that the average recovery efficiency is somewhere between a typical central boiler efficiency of .59 and the .75 for single family home. An average is used for this analysis by default. [↑](#footnote-ref-193)
193. Table C-6, Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007. Evaluations indicate that consumer dissatisfaction may lead to reductions in persistence, particularly in Multi-Family , "http://neep.org/uploads/EMV%20Forum/EMV%20Studies/measure\_life\_GDS%5B1%5D.pdf" [↑](#footnote-ref-194)
194. Direct-install price per showerhead assumes cost of showerhead (Market research average of $7 and assess and install time of $5 (20min @ $15/hr) [↑](#footnote-ref-195)
195. Calculated as follows: Assume 11% showers take place during peak hours (based on: <http://www.aquacraft.com/sites/default/files/pub/DeOreo-%282001%29-Disaggregated-Hot-Water-Use-in-Single-Family-Homes-Using-Flow-Trace-Analysis.pdf>). There are 65 days in the summer peak period, so the percentage of total annual aerator use in peak period is 0.11\*65/365 = 1.96%. The number of hours of recovery during peak periods is therefore assumed to be 1.96% \* 369 = 7.23 hours of recovery during peak period. There are 260 hours in the peak period so the probability you will see savings during the peak period is 7,23/260 = 0..0278 [↑](#footnote-ref-196)
196. Based on excel spreadsheet 120911.xls …on SharePoint [↑](#footnote-ref-197)
197. Table HC8.9. Water Heating in U.S. Homes in Midwest Region, Divisions, and States, 2009 (RECS) [↑](#footnote-ref-198)
198. Based on measured data from Ameren IL EM&V of Direct-Install program. Program targets showers that are rated 2.5 GPM or above. [↑](#footnote-ref-199)
199. Note that actual values may be either a) program-specific minimum flow rate, or b)program-specific evaluation-based value of actual effective flow-rate due to increased duration or temperatures. The latter increases in likelihood as the rated flow drops and may become significant at or below rated flows of 1.5 GPM. The impact can be viewed as the inverse of the throttling described in the footnote for baseline flowrate. [↑](#footnote-ref-200)
200. Representative value from sources 1, 2, 3, 4, 5, and 6 (See Source Table at end of measure section) [↑](#footnote-ref-201)
201. Set equal to L\_base. [↑](#footnote-ref-202)
202. Shower temperature cited from SBW Consulting, Evaluation for the Bonneville Power Authority, 1994, <http://www.bpa.gov/energy/n/reports/evaluation/residential/faucet_aerator.cfm> [↑](#footnote-ref-203)
203. US DOE Building America Program. Building America Analysis Spreadsheet. For Chicago, IL <http://www1.eere.energy.gov/buildings/building_america/analysis_spreadsheets.html>. [↑](#footnote-ref-204)
204. Electric water heaters have recovery efficiency of 98%: <http://www.ahridirectory.org/ahridirectory/pages/home.aspx> [↑](#footnote-ref-205)
205. Deemed values are from ComEd Energy Efficiency/ Demand Response Plan: Plan Year 2 (6/1/2009-5/31/2010) Evaluation Report: All Electric Single Family Home Energy Performance Tune-Up Program Table 3-8. Alternative ISRs may be developed for program delivery methods based on evaluation results. [↑](#footnote-ref-206)
206. 77.3% is the proportion of hot 120F water mixed with 54.1°F supply water to give 105°F shower water [↑](#footnote-ref-207)
207. Calculated as follows: Assume 11% showers take place during peak hours (based on: <http://www.aquacraft.com/sites/default/files/pub/DeOreo-%282001%29-Disaggregated-Hot-Water-Use-in-Single-Family-Homes-Using-Flow-Trace-Analysis.pdf>). There are 65 days in the summer peak period, so the percentage of total annual aerator use in peak period is 0.11\*65/365.25 = 1.96%. The number of hours of recovery during peak periods is therefore assumed to be 1.96% \* 369 = 7.23 hours of recovery during peak period where 369 equals the average annual electric DHW recovery hours for showerhead use including SF and MF homes with Direct Install and Retrofit/TOS measures. There are 260 hours in the peak period so the probability you will see savings during the peak period is 7.23/260 = 0.0278 [↑](#footnote-ref-208)
208. Default assumption for unknown fuel is based on EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used [↑](#footnote-ref-209)
209. Review of AHRI Directory suggests range of recovery efficiency ratings for new Gas DHW units of 70-87%. Average of existing units is estimated at 75%. Commercial properties are more similar to MF homes than SF homes. MF hot water is often provided by a larger commercial boiler. This suggests that the average recovery efficiency is somewhere between a typical central boiler efficiency of .59 and the .75 for single family home. An average is used for this analysis by default. [↑](#footnote-ref-210)
210. The effective useful life of a pool cover is typically one year longer than its warranty period. SolaPool Covers. Pool Covers Website, FAQ- "How long will my SolaPool cover blanket last?". Pool covers are typically offered with 3 and 5 year warranties with at least one company offering a 6 year warranty. Conversation with Trade Ally. Knorr Systems [↑](#footnote-ref-211)
211. Pool Cover Costs: Lincoln Commercial Pool Equipment website. Accessed 8/26/11. <http://www.lincolnaquatics.com/shop/catalog/Pool+and+Spa+Covers+and+Accessories/product.html?ProductID=84-010> [↑](#footnote-ref-212)
212. Full method and supporting information found in reference document: IL TRM - Business Pool Covers WorkPaper.docx [↑](#footnote-ref-213)
213. Business Pool Covers.xlsx [↑](#footnote-ref-214)
214. Ibid. [↑](#footnote-ref-215)
215. Ohio Technical Reference Manual 8/2/2010 referencing CenterPoint Energy-Triennial CIP/DSM Plan 2010-2012 Report; Additional reference stating >20 years is at Energy Savers.Gov online at http://www.energysavers.gov/your\_home/water\_heating/index.cfm/mytopic=12820 [↑](#footnote-ref-216)
216. Ibid. [↑](#footnote-ref-217)
217. Act on Energy Technical Reference Manual, Table 9.6.2-3 [↑](#footnote-ref-218)
218. Based on AOE historical average installation data of 42 tankless gas hot water heaters [↑](#footnote-ref-219)
219. <http://www.mncee.org/getattachment/7b8982e9-4d95-4bc9-8e64-f89033617f37/>, Low contractor estimate used to reflect less labor required in new construction of venting. [↑](#footnote-ref-220)
220. Water heaters (WH) require annual maintenance. There are different levels of effort for annual maintenance depending if the unit is gas or electric, tanked or tankless. Electric and gas tank water heater manufacturers recommend an annual tank drain to clear sediments. Also recommended are “periodic” inspections by qualified service professionals of operating controls, heating element and wiring for electric WHs and thermostat, burner, relief valve internal flue-way and venting systems for gas WHs. Tankless WH require annual maintenance by licensed professionals to clean control compartments, burners, venting system and heat exchangers. This information is from WH manufacturer product brochures including GE, Rennai, Rheem, Takagi and Kenmore. References for incremental O&M costs were not found. Therefore the incremental cost of the additional annual maintenance for tankless WH is estimated at $100. [↑](#footnote-ref-221)
221. Act on Energy Technical Reference Manual, Table 9.6.2-3 [↑](#footnote-ref-222)
222. Ibid. [↑](#footnote-ref-223)
223. 21,915 gallons is an estimate of 60 gal/day for 365.25 days/yr. If building type is known, reference 2007 ASHRAE Handbook HVAC Applications p. 49.14 Table 7 Hot Water Demands and Use for Various Types of Buildings to help estimate hot water consumption. [↑](#footnote-ref-224)
224. Based on 2010 Ohio Techical Reference Manual and NAHB Research Center, (2002) Performance Comparison of Residential hot Water Systems. Prepared for National Renewable Energy Laboratory, Golden, Colorado. [↑](#footnote-ref-225)
225. August 31, 2011 Memo of Savings for Hot Water Savings Measures to Nicor Gas from Navigant states that 54.1°F was calculated from the weighted average of monthly water mains temperatures reported in the 2010 Building America Benchmark Study for Chicago-Waukegan, Illinois. [↑](#footnote-ref-226)
226. IECC 2012, Table C404.2, Minimum Performance of Water-Heating Equipment [↑](#footnote-ref-227)
227. Specifications of energy efficient tankless water heater. Reference Consortium for Energy Efficiency (CEE) which maintains a list of high efficiency tankless water heaters which currently have Energy Factors up to .96. Ameren currently requires minimum .82 energy factor. [↑](#footnote-ref-228)
228. Stand-by loss is provided 2012 International Energy Conservation Code (IECC2012), Table C404.2, Minimum Performance of Water-Heating Equipment [↑](#footnote-ref-229)
229. International Energy Conservation Code (IECC)2012 [↑](#footnote-ref-230)
230. Aligned with other national energy efficiency programs and confirmed with national vendors [↑](#footnote-ref-231)
231. Average costs per unit of capacity were generated using data collected from existing ozone laundry projects that received incentives under the Non-Residential Retrofit Demand Reduction program (NRR-DR), as well as from the Nicor Custom Incentive Program, and the Nicor Emerging Technology Program (ETP). See referenced document Table 2 and RSMeans Mechanical Cost Data, 31st Annual Edition (2008) [↑](#footnote-ref-232)
232. Washer savings were reviewed but were considered negligible and not included in the algorithm (0.00082 kWh / lbs-capacity, determined through site analysis through Nicor Emerging Technology Program (ETP) and confirmed with national vendors). Note that washer savings from Nicor’s site analysis are smaller than those reported in a WI Focus on Energy case study (0.23kWh/100lbs, Hampton Inn Brookfield, November 2010). Electric impact of operating ozone generator (0.0021 kWh / lbs-capacity same source as washer savings) was also considered negligible and not included in calculations. Values should continue to be studied and monitored through additional studies due to limited data points used for this determination. [↑](#footnote-ref-233)
233. Assumed average horsepower for boilers connected to applicable washer [↑](#footnote-ref-234)
234. Engineered estimate provided by CLEAResult review of Nicor custom projects. Machines spent approximately 7 minutes per hour filling with water and were in operation approximately 20 hours per day. Total pump time therefore estimated as 7/60 \* 20 \* 365 = 852 hours, and rounded down conservatively to 800 hours. [↑](#footnote-ref-235)
235. Average water reduction factors were generated using data collected from existing ozone laundry projects that received incentives under the Non-Residential Retrofit Demand Reduction program (NRR-DR). Table 6 summarizes data gathered from several NRR-DR projects, Nicor Custom projects, and Nicor ETP projects. Nicor Savings Numbers are associated with ACEE\_AWE\_Ozone Laundry / From Gas Savings Calculations [↑](#footnote-ref-236)
236. Average lbs-capacity per project site was generated using data collected from existing ozone laundry projects that received incentives under the Non-Residential Retrofit Demand Reduction program (NRR-DR), as well as from the Nicor Custom Incentive Program, and the Nicor Emerging Technology Program (ETP). See referenced document Table 2 [↑](#footnote-ref-237)
237. Assuming boiler efficiency is the regulated minimum efficiency (80%), per Title 20 Appliance Standard of the California Energy Regulations (October 2007). The incoming municipal water temperature is assumed to be 55 °F with an average hot water supply temperature of 140°F, based on default test procedures on clothes washers set by the Department of Energy’s Office of Energy Efficiency and Renewable Energy (Federal Register, Vol. 52, No. 166). Enthalpies for these temperatures (107 btu/lbs at 140F, 23.07 btu/lbs at 55F) were obtained from ASHRAE Fundamentals [↑](#footnote-ref-238)
238. Average utilization factors were generated using data collected from existing ozone laundry projects that received incentives under the NRR-DR program. Table 3 summarizes data gathered from several NRR-DR projects, Nicor Custom projects, and Nicor ETP projects [↑](#footnote-ref-239)
239. Average hot water usage factors were generated using data collected from existing ozone laundry projects that received incentives under the NRR-DR program. summarizes data gathered from several NRR-DR projects: [↑](#footnote-ref-240)
240. Average hot water reduction factors were generated using data collected from existing ozone laundry projects that received incentives under the Non-Residential Retrofit Demand Reduction program (NRR-DR). Table 5 summarizes data gathered from several NRR-DR projects, Nicor Custom projects, and Nicor ETP projects. Nicor Savings Numbers are associated with ACEE\_AWE\_Ozone Laundry / From Gas Savings Calculations [↑](#footnote-ref-241)
241. Average water usage factors were generated using data collected from existing ozone laundry projects that received incentives under the NRR-DR program. summarizes data gathered from several NRR-DR projects [↑](#footnote-ref-242)
242. Average utilization factors were generated using data collected from existing ozone laundry projects that received incentives under the NRR-DR program. Table 3 summarizes data gathered from several NRR-DR projects, Nicor Custom projects, and Nicor ETP projects [↑](#footnote-ref-243)
243. Average water reduction factors were generated using data collected from existing ozone laundry projects that received incentives under the Non-Residential Retrofit Demand Reduction program (NRR-DR). Table 6 summarizes data gathered from several NRR-DR projects, Nicor Custom projects, and Nicor ETP projects. Nicor Savings Numbers are associated with ACEE\_AWE\_Ozone Laundry / From Gas Savings Calculations [↑](#footnote-ref-244)
244. Confirmed through communications with national vendors and available references E.g. <http://ozonelaundry.wordpress.com/2010/11/17/the-importance-of-maintenance/> [↑](#footnote-ref-245)
245. IECC 2012, Table C404.2, Minimum Performance of Water-Heating Equipment [↑](#footnote-ref-246)
246. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011. [↑](#footnote-ref-247)
247. Baseline install costs are based on data from the W017 Itron California Measure Cost Study, accessed via <http://www.energydataweb.com/cpuc/search.aspx>. The data is provided in a file named “MCS Results Matrix – Volume I”. [↑](#footnote-ref-248)
248. The two equations are provided to show how savings are determined during the initial phase of the measure (existing to efficient) and the remaining phase (new baseline to efficient). In practice, the screening tools used may either require a First Year savings (using the first equation) and then a “number of years to adjustment” and “savings adjustment” input which would be the (new base to efficient savings)/(existing to efficient savings). [↑](#footnote-ref-249)
249. Navigant, ComEd PY3 Multi-Family Home Energy Savings Program Evaluation Report Final, May 16, 2012. [↑](#footnote-ref-250)
250. [Maureen](http://portal.veic.org/projects/illinoistrm/Lists/TRM%20Request%20Tracker/Attachments/287/%20Maureen) Hodgins, email message to TAC/SAG, August 26, 2014 [↑](#footnote-ref-251)
251. US DOE Building America Program. Building America Analysis Spreadsheet. For Chicago, IL [http://www1.eere.energy.gov/buildings/building\_america/analysis\_spreadsheets.html](http://www.energystar.gov/ia/products/appliances/refrig/NAECA_calculation.xls) [↑](#footnote-ref-252)
252. IECC 2012, Table C404.2, Minimum Performance of Water-Heating Equipment [↑](#footnote-ref-253)
253. Based upon DCEO data provided 10/2014; average age adjusted efficiency of existing units replaced through the program. Efficiency age adjustment of 0.5% per year based upon NREL “Building America Performance Analysis Procedures for Existing Homes”. [↑](#footnote-ref-254)
254. Stand-by loss is provided in 2012 International Energy Conservation Code (IECC2012), Table C404.2, Minimum Performance of Water-Heating Equipment [↑](#footnote-ref-255)
255. Benningfield Group. (2009). *PY 2009 Monitoring Report: Demand Control for Multifamily Central Domestic Hot Water.* Folsom, CA: Prepared for Southern California Gas Company, October 30, 2009. [↑](#footnote-ref-256)
256. Gas Technology Institute. (2014). *1003: Demand-based domestic hot water recirculation Public project report.* Des Plaines, IL: Prepared for Nicor Gas, January 7, 2014. [↑](#footnote-ref-257)
257. See Illinois\_Statewide\_TRM\_Workpaper\_Demand Control Central DHW for more details [↑](#footnote-ref-258)
258. Based on results from the Nicor Gas Emerging Technology Program study, this value is the average kWh saved per pump. Note this value does not reflect savings from electric units but electrical savings from gas-fired units. [↑](#footnote-ref-259)
259. Based on results from the Nicor Gas Emerging Technology Program study, this value is the average therms saved per dwelling unit. [↑](#footnote-ref-260)
260. A full description of the ComEd model development is found in “ComEd Portfolio Modeling Report. Energy Center of Wisconsin July 30, 2010” [↑](#footnote-ref-261)
261. Ibid. [↑](#footnote-ref-262)
262. Ibid. [↑](#footnote-ref-263)
263. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The AC load during the utility’s peak hour is divided by the maximum AC load during the year. [↑](#footnote-ref-264)
264. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year [↑](#footnote-ref-265)
265. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The AC load during the utility’s peak hour is divided by the maximum AC load during the year. [↑](#footnote-ref-266)
266. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year [↑](#footnote-ref-267)
267. High Impact Measure [↑](#footnote-ref-268)
268. Act on Energy Commercial Technical Reference Manual No. 2010-4, 9.2.2 Gas Boiler Tune-up [↑](#footnote-ref-269)
269. Act on Energy Commercial Technical Reference Manual No. 2010-4, 9.2.2 Gas Boiler Tune-up [↑](#footnote-ref-270)
270. Work Paper – Tune up for Boilers serving Space Heating and Process Load by Resource Solutions Group, January 2012 [↑](#footnote-ref-271)
271. Act on Energy Commercial Technical Reference Manual No. 2010-4, 9.2.2 Gas Boiler Tune-up [↑](#footnote-ref-272)
272. Act on Energy Commercial Technical Reference Manual No. 2010-4, 9.2.2 Gas Boiler Tune-up [↑](#footnote-ref-273)
273. Work Paper – Tune up for Boilers serving Space Heating and Process Load by Resource Solutions Group, January 2012 [↑](#footnote-ref-274)
274. Work Paper – Tune up for Boilers serving Space Heating and Process Load by Resource Solutions Group, January 2012 [↑](#footnote-ref-275)
275. CLEAResultreferences the Brooklyn Union Gas Company, High Efficiency Heating and Water and Controls, Gas Energy Efficiency Program Implementation Plan. [↑](#footnote-ref-276)
276. Nexant. Questar DSM Market Characterization Report. August 9, 2006. [↑](#footnote-ref-277)
277. Savings factor is the estimate of annual gas consumption that is saved due to adding boiler reset controls. The CLEAResultuses a boiler tuneup savings value derived from Xcel Energy "DSM Biennial Plan-Technical Assumptions," Colorado. Focus on Energy uses 8%, citing multiple sources. Vermont Energy Investment Corporation's boiler reset savings estimates for custom projects further indicate 8% savings estimate is better reflection of actual expected savings. [↑](#footnote-ref-278)
278. DEER 2008 [↑](#footnote-ref-279)
279. ENERGY STAR and CEE do not currently provide calculators for this type of equipment therefore deemed values from Nicor Gas were used. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011 [↑](#footnote-ref-280)
280. 2008 Database for Energy-Efficiency Resources (DEER), Version 2008.2.05, “Effective/Remaining Useful Life Values”, California Public Utilities Commission, December 16, 2008 (http://deeresources.com/deer0911planning/downloads/EUL\_Summary\_10-1-08.xls) [↑](#footnote-ref-281)
281. 2008 Database for Energy-Efficiency Resources (DEER), Version 2008.2.05, “Cost Values and Summary Documentation”, California Public Utilities Commission, December 16, 2008 (http://deeresources.com/deer0911planning/downloads/DEER2008\_Costs\_ValuesAndDocumentation\_080530Rev1.zip) [↑](#footnote-ref-282)
282. Calculated as the simple average of screw and reciprocating air-cooled chiller incremental costs from DEER2008. This assumes that baseline shift from IECC 2009 to IECC 2012 carries the same incremental costs. Values should be verified during evaluation [↑](#footnote-ref-283)
283. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The AC load during the utility’s peak hour is divided by the maximum AC load during the year. [↑](#footnote-ref-284)
284. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year [↑](#footnote-ref-285)
285. Integrated Part Load Value is a seasonal average efficiency rating calculated in accordance with ARI Standard 550/590. It may be calculated using any measure of efficiency (EER, kW/ton, COP), but for consistency with IECC 2012, it is expressed in terms of IPLV here. [↑](#footnote-ref-286)
286. Can determine IPLV from standard testing or looking at engineering specs for design conditions. Standard data is available from AHRnetI.org. http://www.ahrinet.org/ [↑](#footnote-ref-287)
287. International Energy Conservation Code (IECC)2012 [↑](#footnote-ref-288)
288. [http://www.energystar.gov/index.cfm?c=roomac.pr\_crit\_room\_ac](http://neep.org/uploads/EMV%20Forum/EMV%20Studies/CT-UI_CLP_2010_PSD.pdf?c=roomac.pr_crit_room_ac) and [http://www.cee1.org/resid/seha/rm-ac/rm-ac\_specs.pdf](http://www.icc.illinois.gov/downloads/public/edocket/303834.pdf)

     Side louvers that extend from a room air conditioner model in order to position the unit in a window. A model without louvered sides is placed in a built-in wall sleeve and are commonly referred to as "through-the-wall" or "built-in" models.

     Casement-only refers to a room air conditioner designed for mounting in a casement window of a specific size.

     Casement-slider refers to a room air conditioner with an encased assembly designed for mounting in a sliding or casement window of a specific size.

     Reverse cycle refers to the heating function found in certain room air conditioner models. [http://www.energystar.gov/ia/partners/product\_specs/program\_reqs/room\_air\_conditioners\_prog\_req.pdf](http://ilsag.org/yahoo_site_admin/assets/docs/ComEd_Res_Lighting_PY2_Evaluation_Report_2010-12-21_Final.12113928.pdf) [↑](#footnote-ref-289)
289. Energy Star Room Air Conditioner Savings Calculator, http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=AC

     [http://neep.org/uploads/EMV%20Forum/EMV%20Studies/measure\_life\_GDS%5B1%5D.pdf](http://www.icc.illinois.gov/downloads/public/edocket/303835.pdf) [↑](#footnote-ref-290)
290. Based on field study conducted by Efficiency Vermont [↑](#footnote-ref-291)
291. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The AC load during the utility’s peak hour is divided by the maximum AC load during the year. [↑](#footnote-ref-292)
292. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year [↑](#footnote-ref-293)
293. Full load hours for room AC is significantly lower than for central AC. The average ratio of FLH for Room AC (provided in RLW Report: Final Report Coincidence Factor Study Residential Room Air Conditioners, June 23, 2008: [http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117\_RLW\_CF%20Res%20RAC.pdf](http://www.bpa.gov/energy/n/reports/evaluation/residential/faucet_aerator.cfm)) to FLH for Central Cooling for the same location (provided by AHRI: [http://www.energystar.gov/ia/business/bulk\_purchasing/bpsavings\_calc/Calc\_CAC.xls](http://www.ahrinet.org/ARI/util/showdoc.aspx)) is 31%. This ratio has been applied to the FLH from the unitary and split system air conditioning measure. [↑](#footnote-ref-294)
294. Based on maximum capacity average from the RLW Report: Final Report Coincidence Factor Study Residential Room Air Conditioners, June 23, 2008 [↑](#footnote-ref-295)
295. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The AC load during the utility’s peak hour is divided by the maximum AC load during the year. [↑](#footnote-ref-296)
296. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year [↑](#footnote-ref-297)
297. DEER 2008 value for energy management systems [↑](#footnote-ref-298)
298. This value was extracted from Smart Ideas projects in PY1 and PY2. [↑](#footnote-ref-299)
299. For motels, see S. Keates, ADM Associates Workpaper: “Suggested Revisions to Guest Room Energy Management (PTAC & PTHP)”, 11/14/2013 and spreadsheet summarizing the results: ‘GREM Savings Summary\_IL TRM\_1\_22\_14.xlsx’. In 2014 the hotel models were also run to compile results, rather than by applying adjustment factors to the motel results as had been done in V3.0 of the TRM. The updated values can be found in ‘GREM Savings Summary (Hotel)\_IL TRM\_10\_16\_14.xls’. [↑](#footnote-ref-300)
300. Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, Inc., June 2007. [↑](#footnote-ref-301)
301. Based on a review of TRM incremental cost assumptions from Vermont, Wisconsin, and California. [↑](#footnote-ref-302)
302. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The AC load during the utility’s peak hour is divided by the maximum AC load during the year. [↑](#footnote-ref-303)
303. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year [↑](#footnote-ref-304)
304. International Energy Conservation Code (IECC) 2012 [↑](#footnote-ref-305)
305. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The AC load during the utility’s peak hour is divided by the maximum AC load during the year. [↑](#footnote-ref-306)
306. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year [↑](#footnote-ref-307)
307. The Federal baseline for boilers <300,000 btu/hr changes from 80% to 82% in September 2012. To prevent a change in baseline mid-program, the increase in efficiency is delayed until June 2013 when a new program year starts. [↑](#footnote-ref-308)
308. Ibid. [↑](#footnote-ref-309)
309. The Technical support documents for federal residential appliance standards: http://www1.eere.energy.gov/buildings/appliance\_standards/residential/pdfs/fb\_fr\_tsd/appendix\_e.pdf Note that this value is below the 20 years used by CA's DEER and the range of 20-40 year estimate made by the Consortium for Energy Efficiency in 2010 [↑](#footnote-ref-310)
310. Average of low and high incremental cost based on Nicor Gas program data for non-condensing and condensing boilers. Nicor Gas Energy Efficiency Plan 2011 - 2014, May 27, 2011 $1,470 for ≤ 300,000 Btu/hr for non-condensing hydronic boilers >85% AFUE & $3,365 for condensing boilers > 90% AFUE. The exception is $4,340 for AFUE ≥ 96% AFUE which was obtained from extrapolation above the size range that Nicor Gas Energy Efficiency Plan provided for incremental cost. [↑](#footnote-ref-311)
311. Average of 15-18 year lifetime estimate made by the Consortium for Energy Efficiency in 2010. [↑](#footnote-ref-312)
312. Assumed to be one third of effective useful life [↑](#footnote-ref-313)
313. Based on data from Appendix E of the Appliance Standards Technical Support Documents including equipment cost and installation labor (http://www1.eere.energy.gov/buildings/appliance\_standards/residential/pdfs/fb\_fr\_tsd/appendix\_e.pdf). Where efficiency ratings are not provided, the values are interpolated from those that are. [↑](#footnote-ref-314)
314. To estimate heating, cooling and shoulder season savings for Illinois, VEIC adapted results from a 2009 Focus on Energy study of BPM blower motor savings in Wisconsin. This study included effects of behavior change based on the efficiency of new motor greatly increasing the amount of people that run the fan continuously. The savings from the Wisconsin study were adjusted to account for different run hour assumptions (average values used) for Illinois. See: FOE to IL Blower Savings.xlsx. [↑](#footnote-ref-315)
315. The weighted average value is based on assumption that 75% of buildings installing BPM furnace blower motors have Central AC. [↑](#footnote-ref-316)
316. ComEd Trm June 1, 2010 page 139. The Office hours is based upon occupancy from the eQuest model developed for EFLH, since it was agreed the ComEd value was too low. [↑](#footnote-ref-317)
317. Based on DEER 2008 values [↑](#footnote-ref-318)
318. The two equations are provided to show how savings are determined during the initial phase of the measure (existing to efficient) and the remaining phase (new baseline to efficient). In practice, the screening tools used may either require a First Year savings (using the first equation) and then a “number of years to adjustment” and “savings adjustment” input which would be the (new base to efficient savings)/(existing to efficient savings). [↑](#footnote-ref-319)
319. Average nameplate efficiencies of all Early Replacement qualifying equipment in Ameren PY3-PY4. [↑](#footnote-ref-320)
320. Though the Federal Minimum AFUE is 78%, there were only 50 models listed in the AHRI database at that level. At AFUE 79% the total rises to 308. There are 3,548 active furnace models listed with AFUE ratings between 78 and 80. [↑](#footnote-ref-321)
321. Minimum ENERGY STAR efficiency after 2.1.2012. [↑](#footnote-ref-322)
322. ENERGY STAR and CEE do not currently provide calculators for this type of equipment therefore deemed values from Nicor Gas were used. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011 [↑](#footnote-ref-323)
323. Ibid. [↑](#footnote-ref-324)
324. Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011.These deemed values should be compared to PY evaluation and revised as necessary. [↑](#footnote-ref-325)
325. Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, Inc., June 2007 [↑](#footnote-ref-326)
326. Standard assumption of one third of effective useful life. [↑](#footnote-ref-327)
327. DEER 2008. This assumes that baseline shift from IECC 2006 to IECC 2012 carries the same incremental costs. Values should be verified during evaluation [↑](#footnote-ref-328)
328. Based on DCEO – IL PHA Efficient Living Program data. [↑](#footnote-ref-329)
329. Based on subtracting TOS incremental cost from the DCEO data. [↑](#footnote-ref-330)
330. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The AC load during the utility’s peak hour is divided by the maximum AC load during the year. [↑](#footnote-ref-331)
331. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year [↑](#footnote-ref-332)
332. There are no heating efficiency improvements for PTACs since although some do provide heating, it is always through electric resistance and therefore the COPbase and COPee would be 1.0. [↑](#footnote-ref-333)
333. Estimated using the IECC building energy code up until year 2003 (p107; https://law.resource.org/pub/us/code/ibr/icc.iecc.2000.pdf) and assuming a 1 ton unit; EER = 10 – (0.16 \* 12,000/1,000) = 8.1. [↑](#footnote-ref-334)
334. Estimated using the IECC building energy code up until year 2003 (p107; https://law.resource.org/pub/us/code/ibr/icc.iecc.2000.pdf) and assuming a 1 ton unit; COP = 2.9 – (0.026 \* 12,000/1,000) = 2.6 [↑](#footnote-ref-335)
335. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The AC load during the utility’s peak hour is divided by the maximum AC load during the year. [↑](#footnote-ref-336)
336. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year [↑](#footnote-ref-337)
337. *ASHRAE Handbook—Fundamentals*, 23.14; Hart, G., “Saving energy by insulating pipe components on steam and hot water distribution systems”, *ASHRAE Journal*, October 2011 [↑](#footnote-ref-338)
338. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007.

     <http://neep.org/uploads/EMV%20Forum/EMV%20Studies/measure_life_GDS%5B1%5D.pdf> [↑](#footnote-ref-339)
339. RS Means 2008. Mechanical Cost Data, pages 106 to 119 [↑](#footnote-ref-340)
340. RS Means 2010: “for fittings, add 3 linear feet for each fitting plus 4 linear feet for each flange of the fitting” [↑](#footnote-ref-341)
341. This value comes from the reference table “Savings Summary by Building Type and System Type.” The formula and the input tables in this section document assumptions used in calculation spreadsheet “Pipe Insulation Savings 2013-11-12.xlsx” [↑](#footnote-ref-342)
342. Average efficiencies of units from the California Energy Commission (CEC). [↑](#footnote-ref-343)
343. Ibid. [↑](#footnote-ref-344)
344. Katrakis, J. and T.S. Zawacki. “Field-Measured Seasonal Efficiency of Intermediate-sized Low-Pressure Steam Boilers”. ASHRAE V99, pt. 2, 1993. [↑](#footnote-ref-345)
345. Thermal regain for *residential* pipe insulation measures is discussed in Home Energy Services Impact Evaluation, prepared for the Massachusetts Residential Retrofit and Low Income Program Area Evaluation, Cadmus Group, Inc., August 2012 and Andrews, John, Better Duct Systems for Home Heating and Cooling, U.S. Department of Energy, 2001. Recognizing the differences between residential and commercial heating systems, the factors have been adjusted based on professional judgment. This factor would benefit from additional study and evaluation. [↑](#footnote-ref-346)
346. Thermal Regain Factor\_4-30-14.docx [↑](#footnote-ref-347)
347. 3E Plus is a heat loss calculation software provided by the NAIMA (North American Insulation Manufacturer Association). [↑](#footnote-ref-348)
348. DOE Weather Data. <http://apps1.eere.energy.gov/buildings/energyplus/weatherdata/4_north_and_central_america_wmo_region_4/1_usa/USA_IL_Aurora.Muni.AP.744655_TMY3.stat> Ibid. [↑](#footnote-ref-349)
349. Ibid. [↑](#footnote-ref-350)
350. Based on the dimensions for diameter, long radius, and short radius given by ANSI/ASME 36.19 [↑](#footnote-ref-351)
351. Based on the center to face and diameter dimensions given by ANSI/ASME B36.19 [↑](#footnote-ref-352)
352. Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, Inc., June 2007. [↑](#footnote-ref-353)
353. Based on a review of TRM incremental cost assumptions from Vermont, Wisconsin, and California. This assumes that baseline shift from IECC 2009 to IECC 2012 carries the same incremental costs. Values should be verified during evaluation [↑](#footnote-ref-354)
354. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The AC load during the utility’s peak hour is divided by the maximum AC load during the year. [↑](#footnote-ref-355)
355. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year [↑](#footnote-ref-356)
356. International Energy Conservation Code (IECC) 2012 [↑](#footnote-ref-357)
357. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The AC load during the utility’s peak hour is divided by the maximum AC load during the year. [↑](#footnote-ref-358)
358. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year [↑](#footnote-ref-359)
359. High Impact Measure [↑](#footnote-ref-360)
360. Source paper is the CLEAResult"Steam Traps Revision #1" dated August 2011. Primary studies used to prepare the source paper include Enbridge Steam Trap Survey, KW Engineering Steam Trap Survey, Enbridge Steam Saver Program 2005, Armstrong Steam Trap Survey, DOE Federal Energy Management Program Steam Trap Performance Assessment, Oak Ridge National Laboratory Steam System Survey Guide, KEMA Evaluation of PG&E's Steam Trap Program, Sept. 2007. Communication with vendors suggested a inverted bucket steam trap life typically in the range of 5 - 7 years, float and thermostatic traps 4- 6 years, float and thermodynamic disc traps of 1 - 3 years. Cost does not include installation. [↑](#footnote-ref-361)
361. Ibid. [↑](#footnote-ref-362)
362. CLEAResult"Steam Traps Revision #1" dated August 2011. [↑](#footnote-ref-363)
363. Heat of vaporization of steam at the inlet pressure to the steam trap. Implicit assumption that the average boiler nominal pressure where the vaporization occurs, is essentially that same pressure. Reference CLEAResult"Steam Traps Revision #1" dated August 2011. [↑](#footnote-ref-364)
364. California Energy Commission Efficiency Data for Steam Boilers as sited in CLEAResult"Steam Traps Revision #1" dated August 2011. [↑](#footnote-ref-365)
365. CLEAResult"Steam Traps Revision #1" dated August 2011, which references Enbridge service territory data and kW Engineering study. [↑](#footnote-ref-366)
366. Since commercial LPS reflect heating systems, Hours/yr are equivalent to HDD55 zone table [↑](#footnote-ref-367)
367. Enbridge adjustment factor used as referenced in CLEAResult"Steam Traps Revision #1" dated August 2011 and DOE Federal Energy Management Program Steam Trap Performance Assessment. [↑](#footnote-ref-368)
368. Dry cleaners survey data as referenced in CLEAResult"Steam Traps Revision #1" dated August 2011. [↑](#footnote-ref-369)
369. Efficiency Vermont TRM 10/26/11 for HVAC VSD motors [↑](#footnote-ref-370)
370. DEER 2008 [↑](#footnote-ref-371)
371. Ohio TRM 8/6/2010 varies by motor/fan size based on equipment costs from Granger 2008 Catalog pp 286-289, average across available voltages and models. Labor costs from RS Means Data 2008 Ohio average cost adjustment applied. [↑](#footnote-ref-372)
372. Del Balso, Ryan J. “Investigation into the Reliability of Energy Efficiency/Demand Side Management Savings Estimates for Variable Frequency Drives in Commercial Applications”, University of Colorado, Department of Civil, Environmental and Architectural Engineering, 2013. [↑](#footnote-ref-373)
373. Ohio TRM 8/6/2010 pp207-209, Com Ed TRM June 1, 2010. [↑](#footnote-ref-374)
374. ComEd Trm June 1, 2010 page 139. The Office hours is based upon occupancy from the eQuest model developed for EFLH, since it was agreed the ComEd value was too low. [↑](#footnote-ref-375)
375. Ibid. [↑](#footnote-ref-376)
376. Ibid [↑](#footnote-ref-377)
377. Table 1, HVAC Controls, Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, 2007 [↑](#footnote-ref-378)
378. Future evaluation is strongly encouraged to inform the persistence of savings to further refine measure life assumption. As this characterization depends heavily upon a large scale but only 2-year study of the energy impacts of programmable thermostats, the longer term impacts should be assessed. [↑](#footnote-ref-379)
379. Nicor Rider 30 Business EER Program Database, Paid Rebates with Programmable Thermostat Installation Costs, Program to Date as of January 11, 2013. [↑](#footnote-ref-380)
380. Savings equations and factors determined by regression of results of a series of eQuest simulations. See Programmable T-Stat Work Paper\_PECI\_FinalDraft\_140730\_Redline.docx for details. [↑](#footnote-ref-381)
381. Climate Zones Refrenced in Section 3.7, Table 3.6 [↑](#footnote-ref-382)
382. During the course of conversations with vendors and Building Automation System (BAS) contractors, it was determined that sensors have to be functional for up to 10 years. It is recommended that they are part of a normal preventive maintenance program in which calibration is an important part of extending useful life. Although they are not subject to mechanical failure, they do fall out of tolerance over time. [↑](#footnote-ref-383)
383. Discussion with vendors [↑](#footnote-ref-384)
384. The electric energy savings was calculated using TMY3 weather data and methodology consistent with ASHRAE standards. Savings are calculated on an annual basis for each given temperature zone in Illinois. Energy savings for DCV were developed utilizing standards, inputs and approaches as set forth by ASHRAE 62.1and 90.1, respectively. Building input parameters like square footage, equipment efficiencies and occupancy match those used in the EFLH calculations. Reference calculation found in Demand Control Ventilation 12-30-13.xls. [↑](#footnote-ref-385)
385. The natural gas energy savings was calculated using TMY3 weather data and methodology consistent with ASHRAE standards. Savings are calculated on an annual basis for each given temperature zone in Illinois. Energy savings for DCV were developed utilizing standards, inputs and approaches as set forth by ASHRAE 62.1 and 90.1, respectively. Building input parameters like square footage, equipment efficiencies and occupancy match those used in the EFLH calculations. Reference calculation found in Demand Control Ventilation 12-30-13.xls. [↑](#footnote-ref-386)
386. The standard turndown ratio for boilers is 6:1. Understanding Fuel Savings in the Boiler Room, ASHRAE Journal, David Eoff, December, 2008 p 38 [↑](#footnote-ref-387)
387. Focus on Energy Evaluation, Business Programs: Deemed Savings Manual V1.0, March 22, 2010. This factor implies that boilers are 30% oversized on average. [↑](#footnote-ref-388)
388. FES Analysis of bin hours based upon a 30% oversizing factor. [↑](#footnote-ref-389)
389. “Burner,” Obtained from a nation-wide survey conducted by ASHRAE TC 1.8 (Akalin 1978). Data changed by TC 1.8 in 1986. [↑](#footnote-ref-390)
390. FES review of PY2/PY3 costs for custom People’s and North Shore high turndown burner projects. See High Turndown Costs.xlsx for details. [↑](#footnote-ref-391)
391. Release 3.0 Operations & Maintenance Best Practices A Guide to Achieving Operational Efficiency, August 2010, Federal Energy Management Program, US Department of Energy. The equation was determined by plotting the values in Table 9.2.1 – Boiler Cycling Energy Loss. [↑](#footnote-ref-392)
392. PA Consulting, KEMA, Focus on Energy Evaluation, Business Programs: Deemed Savings Manual V1.0, March 22, 2010, Page 4-12. [↑](#footnote-ref-393)
393. Ibid. [↑](#footnote-ref-394)
394. 10:1 ratio used to qualify for efficient equipment. [↑](#footnote-ref-395)
395. Total number of hours for heating with a base temperature of 55°F for Chicago, IL as noted by National Climate Data Center [↑](#footnote-ref-396)
396. [↑](#footnote-ref-397)
397. Available and Emerging Technologies for Reducing Greenhouse Gas Emissions from Industrial, Commercial, and Institutional Boilers, Prepared by the Sector Policies and Programs Division Office of Air Quality Planning and Standards U.S. Environmental Protection Agency Research Triangle Park, North Carolina 27711, October 2010, Table 1. ICI Boilers – Summary of Greenhouse Gas Emission Reduction Measures, pg. 8 [↑](#footnote-ref-398)
398. Department of Energy (DOE). January 2012, Steam Tip Sheet #4, Improve Your Boiler’s Combustion Efficiency. Advanced Manufacturing Office. Washington, DC: U.S. Department of Energy. This value was determined as an appropriate average over the stack temperatures and excess air levels indicated. [↑](#footnote-ref-399)
399. State of Wisconsin Public Service Commission of Wisconsin Focus on Energy Evaluation Business Programs: Measure Life Study Final Report: August 25, 2009, Table 1-2. Recommended Measure Life by WISeerts Group Description, pg. 1-4. [↑](#footnote-ref-400)
400. CODES AND STANDARDS ENHANCEMENT INITIATIVE (CASE) PROCESS BOILERS, 2013 California Building Energy Efficiency Standards, California Utilities Statewide Codes and Standards Team, October 2011, pg. 22 [↑](#footnote-ref-401)
401. Department of Energy (DOE). 2009. Energy Matters newsletter. Fall 2009- Vol. 1, Iss. 1. Washington, DC: U.S. Department of Energy, Office of Energy Efficiency and Renewable Energy, Industrial Technologies Program. [↑](#footnote-ref-402)
402. Ibid. [↑](#footnote-ref-403)
403. [↑](#footnote-ref-404)
404. Department of Energy (DOE). January 2012, Steam Tip Sheet #4, Improving Your Boiler’s Combustion Efficiency. Advanced Manufacturing Office. Washington, DC: U.S. Department of Energy. This value was determined as an appropriate average over the stack temperatures and excess air levels indicated. [↑](#footnote-ref-405)
405. State of Wisconsin Public Service Commission of Wisconsin Focus on Energy Evaluation Business Programs: Measure Life Study Final Report: August 25, 2009, Table 1-2. Recommended Measure Life by WISeerts Group Description, pg. 1-4. [↑](#footnote-ref-406)
406. CODES AND STANDARDS ENHANCEMENT INITIATIVE (CASE) PROCESS BOILERS, 2013 California Building Energy Efficiency Standards, California Utilities Statewide Codes and Standards Team, October 2011, pg. 22 [↑](#footnote-ref-407)
407. Based on internet review of savings potential;

     “Up to 4%”: Use of Automatic Vent Dampers for New and Existing Boilers and Furnaces, Energy Innovators Initiative Technical Fact Sheet, Office of Energy Efficiency, Canada, 2002

     “Up to 1%”: Page 9, The Carbon Trust, “Steam and high temperature hot water boilers” <http://www.carbontrust.com/media/13332/ctv052_steam_and_high_temperature_hot_water_boilers.pdf>,

     “1 - 2%”: Page 2, Sustainable Energy Authority of Ireland “Steam Systems Technical Guide”, <http://www.seai.ie/Your_Business/Technology/Buildings/Steam_Systems_Technical_Guide.pdf>. [↑](#footnote-ref-408)
408. CODES AND STANDARDS ENHANCEMENT INITIATIVE (CASE) PROCESS BOILERS, 2013 California Building Energy Efficiency Standards, California Utilities Statewide Codes and Standards Team, October 2011, pg. 22 [↑](#footnote-ref-409)
409. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007. http://neep.org/uploads/EMV%20Forum/EMV%20Studies/measure\_life\_GDS%5B1%5D.pdf [↑](#footnote-ref-410)
410. A market survey was performed to determine these costs. [↑](#footnote-ref-411)
411. This value comes from the reference table “Savings Summary by Building Type and System Type.” The formula and the input tables in this section document assumptions used in calculation spreadsheet “Pipe Insulation Savings 2013-11-12.xlsx” [↑](#footnote-ref-412)
412. Average efficiencies of units from the California Energy Commission (CEC). [↑](#footnote-ref-413)
413. Ibid. [↑](#footnote-ref-414)
414. Katrakis, J. and T.S. Zawacki. “Field-Measured Seasonal Efficiency of Intermediate-sized Low-Pressure Steam Boilers”. ASHRAE V99, pt. 2, 1993. [↑](#footnote-ref-415)
415. Thermal regain for *residential* pipe insulation measures is discussed in Home Energy Services Impact Evaluation, prepared for the Massachusetts Residential Retrofit and Low Income Program Area Evaluation, Cadmus Group, Inc., August 2012 and Andrews, John, Better Duct Systems for Home Heating and Cooling, U.S. Department of Energy, 2001. Recognizing the differences between residential and commercial heating systems, the factors have been adjusted based on professional judgment. This factor would benefit from additional study and evaluation. [↑](#footnote-ref-416)
416. Thermal Regain Factor\_4-30-14.docx [↑](#footnote-ref-417)
417. Table 1, HVAC Controls, Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, 2007 [↑](#footnote-ref-418)
418. Future evaluation is strongly encouraged to inform the persistence of savings to further refine measure life assumption. [↑](#footnote-ref-419)
419. RSMeans, “Instrumentation and Control for HVAC”, Mechanical Cost Data , Kingston, MA: Reed Construction Data, 2010, pg. 255 & 632 [↑](#footnote-ref-420)
420. Savings equations and factors determined by regression of results of a series of eQuest simulations. See Programmable T-Stat Work Paper\_PECI\_FinalDraft\_140730\_Redline.docx for details. [↑](#footnote-ref-421)
421. Efficiency Vermont TRM 10/26/11 for HVAC VSD motors [↑](#footnote-ref-422)
422. DEER 2008 [↑](#footnote-ref-423)
423. Ohio TRM 8/6/2010 varies by motor/fan size based on equipment costs from Granger 2008 Catalog pp 286-289, average across available voltages and models. Labor costs from RS Means Data 2008 Ohio average cost adjustment applied. [↑](#footnote-ref-424)
424. Methodology developed and tested in Del Balso, Ryan Joseph. “Investigation into the Reliability of Energy Efficiency/Demand Side Management Savings Estimates for Variable Frequency Drives in Commercial Applications”. A project report submitted to the Faculty of the Graduate School of the University of Colorado, 2013. [↑](#footnote-ref-425)
425. Lawrence Berkeley National Laboratory, and Resource Dynamics Corporation. (2008). “Improving Motor and Drive System Performance; A Sourcebook for Industry”. U.S. Department of Energy, Office of Energy Efficiency and Renewable Energy. Golden, CO: National Renewable Energy Laboratory. [↑](#footnote-ref-426)
426. Douglass, J. (2005). Induction Motor Efficiency Standards. Washington State University and the Northwest Energy Efficiency Alliance, Extension Energy Program, Olympia, WA. Retrieved October 17, 2013, from <http://www1.eere.energy.gov/manufacturing/tech_assistance/pdfs/motor_efficiency_standards.pdf> [↑](#footnote-ref-427)
427. ComEd Trm June 1, 2010 page 139. The Office hours is based upon occupancy from the eQuest model developed for EFLH, since it was agreed the ComEd value was too low. [↑](#footnote-ref-428)
428. Assumed service life limited by controls -" Demand Control Ventilation Using CO2 Sensors", pg. 19, by US Department of Energy Efficiency and Renewable Energy [↑](#footnote-ref-429)
429. "Map to HVAC Solutions", by Michigan Air, Issue 3, 2006 [↑](#footnote-ref-430)
430. Weather Station Data, 99.6% Heating DB - 2013 Fundamentals, ASHRAE Handbook [↑](#footnote-ref-431)
431. Energy Recovery Fact Sheet - Center Point Energy, MN [↑](#footnote-ref-432)
432. PA Consulting, Focus on Energy Evaluation, Business Programs: Measure Life Study, August 25, 2009. [↑](#footnote-ref-433)
433. Cleaver Brooks. March 2012, Boiler Efficiency Guide, Pg. 7, Figure 1. [↑](#footnote-ref-434)
434. The minimum stack temperature for a non-condensing economizer is 250°F from Department of Energy (DOE). January 2012, Steam Tip Sheet #26A, Consider Installing a Condensing Economizer. Advanced Manufacturing Office. Washington, DC: U.S. Department of Energy. The average temperature drop is assumed to be ½ way between the existing and efficient temperature minimum, ( 425°F + 250°F ) / 2 = 338°F. [↑](#footnote-ref-435)
435. The minimum stack temperature for a non-condensing economizer is 250°F from Department of Energy (DOE). January 2012, Steam Tip Sheet #26A, Consider Installing a Condensing Economizer. Advanced Manufacturing Office. Washington, DC: U.S. Department of Energy. The average temperature drop is assumed to be ½ way between the existing and efficient temperature minimum, ( 480°F + 250°F ) / 2 = 365°F. [↑](#footnote-ref-436)
436. The minimum stack temperature for a condensing economizer is 250°F from Department of Energy (DOE). January 2012, Steam Tip Sheet #26A, Consider Installing a Condensing Economizer. Advanced Manufacturing Office. Washington, DC: U.S. Department of Energy. The average temperature drop is assumed to be ½ way between the existing and efficient temperature minimum, ( 425°F + 135°F ) / 2 = 280°F. [↑](#footnote-ref-437)
437. The minimum stack temperature for a condensing economizer is 250°F from Department of Energy (DOE). January 2012, Steam Tip Sheet #26A, Consider Installing a Condensing Economizer. Advanced Manufacturing Office. Washington, DC: U.S. Department of Energy. The average temperature drop is assumed to be ½ way between the existing and efficient temperature minimum, ( 480°F + 135°F ) / 2 = 308°F. [↑](#footnote-ref-438)
438. United States EPA, Climate Wise: Wise Rules for Industrial Efficiency, July 1998. The Wise Rules indicate savings range of 1-2% per 40°F reduction, so utilizing 1% is a conservative approach. [↑](#footnote-ref-439)
439. These average values should be utilized in absence of actual temperature data. An economizer with a zero temperature change between the existing and the efficient temperatures would not be installed, so these average values are conservative. [↑](#footnote-ref-440)
440. PA Consulting, Focus on Energy Evaluation, Business Programs: Measure Life Study, August 25, 2009. [↑](#footnote-ref-441)
441. Cleaver Brooks. March 2012, Boiler Efficiency Guide, Pg. 7, Figure 1. [↑](#footnote-ref-442)
442. The minimum stack temperature for a non-condensing economizer is 250°F from Department of Energy (DOE). January 2012, Steam Tip Sheet #26A, Consider Installing a Condensing Economizer. Advanced Manufacturing Office. Washington, DC: U.S. Department of Energy. The average temperature drop is assumed to be ½ way between the existing and efficient temperature minimum, ( 425°F + 250°F ) / 2 = 338°F. [↑](#footnote-ref-443)
443. The minimum stack temperature for a non-condensing economizer is 250°F from Department of Energy (DOE). January 2012, Steam Tip Sheet #26A, Consider Installing a Condensing Economizer. Advanced Manufacturing Office. Washington, DC: U.S. Department of Energy. The average temperature drop is assumed to be ½ way between the existing and efficient temperature minimum, ( 480°F + 250°F ) / 2 = 365°F. [↑](#footnote-ref-444)
444. The minimum stack temperature for a condensing economizer is 250°F from Department of Energy (DOE). January 2012, Steam Tip Sheet #26A, Consider Installing a Condensing Economizer. Advanced Manufacturing Office. Washington, DC: U.S. Department of Energy. The average temperature drop is assumed to be ½ way between the existing and efficient temperature minimum, ( 425°F + 135°F ) / 2 = 280°F. [↑](#footnote-ref-445)
445. The minimum stack temperature for a condensing economizer is 250°F from Department of Energy (DOE). January 2012, Steam Tip Sheet #26A, Consider Installing a Condensing Economizer. Advanced Manufacturing Office. Washington, DC: U.S. Department of Energy. The average temperature drop is assumed to be ½ way between the existing and efficient temperature minimum, ( 480°F + 135°F ) / 2 = 308°F. [↑](#footnote-ref-446)
446. United States EPA, Climate Wise: Wise Rules for Industrial Efficiency, July 1998. The Wise Rules indicate savings range of 1-2% per 40°F reduction, so utilizing 1% is a conservative approach. [↑](#footnote-ref-447)
447. These average values should be utilized in absence of actual temperature data. An economizer with a zero temperature change between the existing and the efficient temperatures would not be installed, so these average values are conservative. [↑](#footnote-ref-448)
448. Work Paper – Tune up for Boilers serving Space Heating and Process Load by Resource Solutions Group, January 2012 [↑](#footnote-ref-449)
449. "Gates Corporation Announces New EPDM Molded Notch V-Belts,” The Gates Rubber Co., June 2010 (Assumed 3% efficiency improvement) <https://ww2.gates.com/news/index.cfm?id=11296&show=newsitem&location_id=753&view=Gates> [↑](#footnote-ref-450)
450. “[Synchronous Belt Drives Offer Low Cost Energy Savings](#3.5 Synchronous Belt Drives Offer Low Cost Energy Savings),” Baldor., February 2009. (attached in Reference Documents) [↑](#footnote-ref-451)
451. "Energy Savings from Synchronous Belts," The Gates Rubber Co., February 2014. (Assumed 5% efficiency improvement) <http://www.gates.com/~/media/Files/Gates/Industrial/Power%20Transmission/White%20Papers/Energy%20Savings%20from%20Synchronous%20Belt%20Drives.pdf> [↑](#footnote-ref-452)
452. “Motor System Tip Sheet #5, Replace V-Belts with Cogged or Synchronous Belt Drives,” USDOE-EERE, September 2005. (Assumed 2% efficiency improvement) <http://www1.eere.energy.gov/industry/bestpractices/pdfs/replace_vbelts_motor_systemts5.pdf> [↑](#footnote-ref-453)
453. ComEd Trm June 1, 2010 page 139. The Office hours is based upon occupancy from the eQuest model developed for EFLH, since it was agreed the ComEd value was too low. [↑](#footnote-ref-454)
454. “[DEER2014-EUL-table-update\_2014-02-05.xlsx](#3.4 DEER2014-EUL-table-update_2014-02-05.xlsx),” Database for Energy Efficiency Resources (DEER), Deer 2014. [www.deerresources.com](file:///\\peci.org\files\Secure\Programs\14984%20-%20ComEd%20AirCare%20Plus\Engineering\Cogged%20v-belt\Work%20Paper\www.deerresources.com) (attached in Reference Documents) [↑](#footnote-ref-455)
455. Grainger catalog on-line web-site for Dayton v-belt pricing

     <http://www.grainger.com/Grainger/ecatalog/N-1z0r596/Ntt-v-belts> [↑](#footnote-ref-456)
456. Com Ed TRM June 1, 2010 [↑](#footnote-ref-457)
457. Efficiency values for motors less than one HP taken from Baldor Electric Catalog 501: <http://www.baldor.com/pdf/501_Catalog/CA501.pdf> [↑](#footnote-ref-458)
458. ComEd Trm June 1, 2010 page 139. The Office hours is based upon occupancy from the eQuest model developed for EFLH, since it was agreed the ComEd value was too low. [↑](#footnote-ref-459)
459. American Standard Maintenance for Indoor Units: http://www.americanstandardair.com/owner-support/maintenance.html [↑](#footnote-ref-460)
460. Act on Energy Commercial Technical Reference Manual No. 2010-4, 9.2.3 Gas Forced-Air Furnace Tune-up. [↑](#footnote-ref-461)
461. Fe is not one of the AHRI certified ratings provided for residential furnaces, but can be reasonably estimated from a calculation based on the certified values for fuel energy (Ef in MMBtu/yr) and Eae (kWh/yr). An average of a 300 record sample (non-random) out of 1495 was 3.14%. This is, appropriately, ~50% greater than the Energy Star version 3 criteria for 2% Fe. See “Programmable Thermostats Furnace Fan Analysis.xlsx” for reference. [↑](#footnote-ref-462)
462. Fixtures hours of use are primarily derived from the default EPY4 values developed for ComEd based on DEER 2005, DEER 2008, EPY1 and EPY2 evaluation results. ‘Lighting intro wp.doc’. Values for office, grocery, light industry, restaurant, retail/service and warehouse are an average of the EPY4 values and AmerEn Missouri, March 2011 Final Report: Evaluation of Business Energy Efficiency Program Custom and Standard Incentives. Hotel/Motel common areas is the DEER 2008 average across all non-guest room spaces and guest rooms is the average of hotel and motel guest room values from DEER 2008. Elementary School is from Ameren Missouri evaluation results. Multi-family common area value based on Focus on Energy Evaluation, ACES Deemed Savings Desk Review, November 2010. Miscellaneous is an average of all indoor spaces. [↑](#footnote-ref-463)
463. Hours of use for screw based bulbs are derived from DEER 2008 by building type for cfls. Garage, exterior and multi-family common area values are from the Hours of Use Table in this document. Miscellaneous is an average of interior space values. Some building types are averaged when DEER has two values: these include office, restaurant and retail. Healthcare clinic uses the hospital value. [↑](#footnote-ref-464)
464. The Waste Heat Factor for Energy is developed using EQuest models for various building types averaged across 5 climate zones for Illinois. Exterior and garage values are 1, miscellaneous is an average of all indoor spaces. [↑](#footnote-ref-465)
465. Waste Heat Factor for Demand are not yet complete. [↑](#footnote-ref-466)
466. Coincident diversity factors are from the EPY4 values developed for ComEd based on DEER 2005, DEER 2008, EPY1 and EPY2 evaluation results. Miscellaneous value for Coincident Diversity Factor is from DEER 2008. [↑](#footnote-ref-467)
467. IF Therms value is developed using EQuest models consistent with methodology for Waste Heat Factor for Energy. [↑](#footnote-ref-468)
468. Electric heat penalty assumptions are based on converting the IFTherm multiplier value in to kWh and then applying relative heating system efficiencies. The gas efficiency was assumed to be 78% AFUE based upon standard TRM assumption for existing unit average efficiency, and the electric resistance is assumed to be 100%:

     IFElectricHeat = IFTherms \* 29.3 kWh/therm \* 78% (Gas Heating Equipment Efficiency) / 100% (Electric Resistance Efficiency) [↑](#footnote-ref-469)
469. RES v C&I split is based on a weighted (by sales volume) average of ComEd PY4-6 and Ameren PY5-6 in store intercept survey results. [↑](#footnote-ref-470)
470. Based upon final weighted (by sales volume) average of the BILD program (ComEd’s commercial lighting program) for PY 4 and PY5 and PY6. [↑](#footnote-ref-471)
471. Energy Star bulbs have a rated life of at least 8000 hours. In commercial settings you expect significantly less on/off switching than residential and so a rated life assumption of 10,000 hours is used. [↑](#footnote-ref-472)
472. Based upon pricing forecast developed by Applied Proactive Technologies Inc (APT) based on industry input and provided to Ameren. [↑](#footnote-ref-473)
473. Illinois evaluation of PY1 through PY3 has not found that fixtures or lamps placed into storage to be a significant enough issue to warrant including an “In-Service Rate” when commercial customers complete an application form. [↑](#footnote-ref-474)
474. 1st year in service rate is based upon review of PY4-6 evaluations from ComEd’s commercial lighting program (BILD) (see ‘IL Commercial Lighting ISR\_2014.xls’ for more information. The average first year ISR was calculated weighted by the number of bulbs sold. [↑](#footnote-ref-475)
475. The 98% Lifetime ISR assumption is based upon review of two evaluations:

     ‘Nexus Market Research, RLW Analytics and GDS Associates study; “New England Residential Lighting Markdown Impact Evaluation, January 20, 2009’ and ‘KEMA Inc, Feb 2010, Final Evaluation Report:, Upstream Lighting Program, Volume 1.’ This implies that only 2% of bulbs purchased are never installed. The second and third year installations are based upon Ameren analysis of the Californian KEMA study showing that 54% of future installs occur in year 2 and 46% in year 3. The 2nd and 3rd year installations should be counted as part of those future program year savings. Note that this Final Install Rate does NOT account for leakage of purchased bulbs being installed outside of the utility territory. EM&V should assess how and if data from evaluation should adjust this final installation rate to account for this impact [↑](#footnote-ref-476)
476. Based on ComEd analysis taking DEER 2008 values and averaging with PY1 and PY2 evaluation results. [↑](#footnote-ref-477)
477. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-478)
478. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-479)
479. Based upon pricing forecast developed by Applied Proactive Technologies Inc (APT) based on industry input and provided to Ameren. [↑](#footnote-ref-480)
480. The manufacturers of the new minimally compliant EISA Halogens are using regular incandescent lamps with halogen fill gas rather than halogen infrared to meet the standard and so the component rated life is equal to the standard incandescent. [↑](#footnote-ref-481)
481. Based on ComEd’s estimate of lamp type saturation. [↑](#footnote-ref-482)
482. Based on the assessment of active projects in the 2008-09 ComEd Smart Ideas Program. See files “ltg costs 12-10-10.xl.” and “Lighting Unit Costs 102605.doc” [↑](#footnote-ref-483)
483. Default wattage reducetion is based on averaging the savings from moving from a 2 to 1, 3 to 2 and 4 to 3 lamp fixture, as provided in the Standard Performance Contract Procedures Manual: Appendix B: Table of Standard Fixture Wattages (<http://www.sce.com/NR/rdonlyres/7A3455F0-A337-439B-9607-10A016D32D4B/0/spc_B_Std_Fixture_Watts.pdf>). An adjustment is made to the T8 delamped fixture to account for the significant increase in ballast factor. See ‘Delamping calculation.xls’ for details. [↑](#footnote-ref-484)
484. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-485)
485. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-486)
486. Based on weighted average of Final ComEd’s BILD program data from PY5 and PY6. For Residential installations, hours of use assumptions from ‘5.5 Interior Hardwired Compact Fluorescent Lamp (CFL) Fixture’ measure should be used. [↑](#footnote-ref-487)
487. 15 years from GDS Measure Life Report, June 2007 [↑](#footnote-ref-488)
488. ibid [↑](#footnote-ref-489)
489. Illinois evaluation of PY1 through PY3 has not found that fixtures or lamps placed into storage to be a significant enough issue to warrant including an “In-Service Rate” when commercial customers complete an application form. [↑](#footnote-ref-490)
490. 1st year in service rate is based upon review of PY5-6 evaluations from ComEd’s commercial lighting program (BILD) (see ‘IL Commercial Lighting ISR\_2014.xls’ for more information [↑](#footnote-ref-491)
491. The 98% Lifetime ISR assumption is based upon review of two evaluations:

     ‘Nexus Market Research, RLW Analytics and GDS Associates study; “New England Residential Lighting Markdown Impact Evaluation, January 20, 2009’ and ‘KEMA Inc, Feb 2010, Final Evaluation Report:, Upstream Lighting Program, Volume 1.’ This implies that only 2% of bulbs purchased are never installed. The second and third year installations are based upon Ameren analysis of the Californian KEMA study showing that 54% of future installs occur in year 2 and 46% in year 3. The 2nd and 3rd year installations should be counted as part of those future program year savings. Note that this Final Install Rate does NOT account for leakage of purchased bulbs being installed outside of the utility territory. EM&V should assess how and if data from evaluation should adjust this final installation rate to account for this impact [↑](#footnote-ref-492)
492. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-493)
493. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-494)
494. Adapted from Efficiency Vermont Technical Reference User Manual (TRM) Measure Savings Algorithms and Cost Assumptions, October 26, 2011. [↑](#footnote-ref-495)
495. Adapted from Efficiency Vermont Technical Reference User Manual (TRM) Measure Savings Algorithms and Cost Assumptions, October 26, 2011. [↑](#footnote-ref-496)
496. Ibid. [↑](#footnote-ref-497)
497. Efficiency Vermont Technical Reference User Manual (TRM) Measure Savings Algorithms and Cost Assumptions, January 2012. [↑](#footnote-ref-498)
498. Adapted from EVT Technical Resource Manual, 2012-75, page 85. [↑](#footnote-ref-499)
499. Efficiency Vermont Technical Reference User Manual (TRM) Measure Savings Algorithms and Cost Assumptions, October 26, 2011

     EPE Program Downloads. Web accessed [http://www.epelectricefficiency.com/downloads.asp?section=ci](http://www.eia.gov/consumption/residential/data/2009/xls/HC7.9%20Air%20Conditioning%20in%20Midwest%20Region.xls?section=ci) download Copy of LSF\_2012\_v4.04\_250rows.xls.

     Kuiken et al, Focus on Energy Evaluation. Business Programs: Deemed Savings Manual v1.0, Kema, march 22, 2010 available at [http://www.focusonenergy.com/files/Document\_Management\_System/Evaluation/bpdeemedsavingsmanuav10\_evaluationreport.pdf](http://www.deeresources.com) Based on ComEd’s BILD program data from PY4 and PY5. For Residential installations, hours of use assumptions from ‘5.5.6 LED Downlights’ should be used for LED fixtures and ‘5.5.8 LED Screw Based Omnidirectional Bulbs’ should be used for LED bulbs. [↑](#footnote-ref-500)
500. Based on final ComEd’s BILD program data from PY4,PY5 and PY6. For Residential installations, hours of use assumptions from ‘5.5.6 LED Downlights’ should be used for LED fixtures and ‘5.5.8 LED Screw Based Omnidirectional Bulbs’ should be used for LED bulbs. [↑](#footnote-ref-501)
501. Based on ENERGY STAR specs – minimum luminous efficacy for Omnidirectional Lamps. For LED lamp power <10W = 50lm/W and for LED lamp power >=10W = 55lm/W. [↑](#footnote-ref-502)
502. Calculated as 45lm/W for all EISA non-exempt bulbs. [↑](#footnote-ref-503)
503. [↑](#footnote-ref-504)
504. The upper bounds for these categories depends on the lower bound of the next higher wattage, which varies by bulb type. [↑](#footnote-ref-505)
505. Illinois evaluation of PY1 through PY3 has not found that fixtures or lamps placed into storage to be a significant enough issue to warrant including an “In-Service Rate” when commercial customers complete an application form. [↑](#footnote-ref-506)
506. Based on ComEd’s BILD program data from PY5 and PY6, see “IL Commercial Lighting ISR\_2014.xls”. [↑](#footnote-ref-507)
507. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-508)
508. See “LED reference tables.xls” for breakdown of component cost assumptions. [↑](#footnote-ref-509)
509. Based upon pricing forecast developed by Applied Proactive Technologies Inc (APT) based on industry input and provided to Ameren. [↑](#footnote-ref-510)
510. The manufacturers of the new minimally compliant EISA Halogens are using regular incandescent lamps with halogen fill gas rather than halogen infrared to meet the standard and so the component rated life is equal to the standard incandescent. [↑](#footnote-ref-511)
511. Data is based on Efficiency Vermont derived cost and actual installed wattage information. [↑](#footnote-ref-512)
512. LED Refrigeration Case Ltg Workpaper 053007 rev1, May 30, 2007 [↑](#footnote-ref-513)
513. Note some measures have blended baselines. All values are provided to enable calculation of appropriate O&M impacts. Total costs include lamp, labor and disposal cost assumptions where applicable, see “LED reference tables.xls” for more information. [↑](#footnote-ref-514)
514. 2008 Database for Energy-Efficiency Resources (DEER), Version 2008.2.05, “Effective/Remaining Useful Life Values”, California Public Utilities Commission, December 16, 2008. [↑](#footnote-ref-515)
515. NYSERDA Deemed Savings Database, Labor cost assumes 25 minutes @ $18/hr. [↑](#footnote-ref-516)
516. Assuming continuous operation of an LED exit sign, the Summer Peak Coincidence Factor is assumed to equal 1.0. [↑](#footnote-ref-517)
517. Based on review of available product. [↑](#footnote-ref-518)
518. Efficiency Vermont Technical Reference User Manual (TRM) Measure Savings Algorithms and Cost Assumptions, February, 19, 2010 [↑](#footnote-ref-519)
519. ComEd has been using a weighted baseline of 70 percent incandescent and 30 percent compact fluorescent, reflecting program experience and a limited sample of evaluation verification findings that we consider to be reasonable (Navigant, through comment period February 2013) [↑](#footnote-ref-520)
520. Efficiency Vermont Technical Reference User Manual (TRM) Measure Savings Algorithms and Cost Assumptions, February, 19, 2010 [↑](#footnote-ref-521)
521. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-522)
522. Consistent with assumption for a Standard CFL bulb with an estimated labor cost of $4.50 (assuming $18/hour and a task time of 15 minutes). [↑](#footnote-ref-523)
523. Assumes a lamp life of 12,000 hours and 8766 run hours 12000/8766 = 1.37 years. [↑](#footnote-ref-524)
524. ACEEE, (1998) A Market Transformation Opportunity Assessment for LED Traffic Signals, [http://www.cee1.org/gov/led/led-ace3/ace3led.pdf](http://www.aquacraft.com/sites/default/files/pub/DeOreo-(2001)-Disaggregated-Hot-Water-Use-in-Single-Family-Homes-Using-Flow-Trace-Analysis.pdf) [↑](#footnote-ref-525)
525. Ibid [↑](#footnote-ref-526)
526. Technical Reference Manual for Pennsylvania Act 129 Energy Efficiency and Conservation Program and Act 213 Alternative Energy Portfolio Standards. Pennsylvania Public Utility Commission. May 2009 [↑](#footnote-ref-527)
527. Technical Reference Manual for Ohio, August 6, 2010 [↑](#footnote-ref-528)
528. Refer to the referenced code documents for specifics on calculating lighting power density using either the whole building method (IECC) or the Space by Space method (ASHRAE 90.1). [↑](#footnote-ref-529)
529. Measure Life Report, Residential and Commercial/Industrial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007. [↑](#footnote-ref-530)
530. IECC 2012 - Reference Code documentation for additional information. [↑](#footnote-ref-531)
531. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-532)
532. IECC 2012 in cases where both a general building area type and a more specific building area type are listed, the more specific building area type shall apply. [↑](#footnote-ref-533)
533. Where lighting equipment is specified to be installed to highlight specific merchandise in addition to lighting equipment specified for general lighting and is switched or dimmed on circuits different from the circuits for general lighting, the small of the actual wattage of the lighting equipment installed specifically for merchandise, or additional lighting power as determined below shall be added to the interior lighting power determined in accordance with this line item. [↑](#footnote-ref-534)
534. 15 years from GDS Measure Life Report, June 2007 [↑](#footnote-ref-535)
535. Illinois evaluation of PY1 through PY3 has not found that fixtures or lamps placed into storage to be a significant enough issue to warrant including an “In-Service Rate” when commercial customers complete an application form. [↑](#footnote-ref-536)
536. 1st year in service rate is based upon review of PY4-5 evaluations from ComEd’s commercial lighting program (BILD) (see ‘IL Commercial Lighting ISR.xls’ for more information. The average first year ISR was calculated weighted by the number of bulbs sold. [↑](#footnote-ref-537)
537. The 98% Lifetime ISR assumption is based upon review of two evaluations:

     ‘Nexus Market Research, RLW Analytics and GDS Associates study; “New England Residential Lighting Markdown Impact Evaluation, January 20, 2009’ and ‘KEMA Inc, Feb 2010, Final Evaluation Report:, Upstream Lighting Program, Volume 1.’ This implies that only 2% of bulbs purchased are never installed. The second and third year installations are based upon Ameren analysis of the Californian KEMA study showing that 54% of future installs occur in year 2 and 46% in year 3. The 2nd and 3rd year installations should be counted as part of those future program year savings. [↑](#footnote-ref-538)
538. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-539)
539. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-540)
540. Consistent with Occupancy Sensor control measure. [↑](#footnote-ref-541)
541. Goldberg et al, State of Wisconsin Public Service Commission of Wisconsin, Focus on Energy Evaluation, Business Programs: Incremental Cost Study, KEMA, October 28, 2009. [↑](#footnote-ref-542)
542. Based on results from “Lighting Controls Effectiveness Assessment: Final Report on Bi-Level Lighting Study” published by the California Public Utilities Commission (CPUC), prepared by ADM Associates.

     <http://lightingcontrolsassociation.org/bi-level-switching-study-demonstrates-energy-savings/> [↑](#footnote-ref-543)
543. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-544)
544. By applying the ESF and the same coincidence factor for general lighting savings we are in essence assuming that the savings from multi-level switching are as likely during peak periods as any other time. In the absence of better information this seems like a reasonable assumption and if anything may be on the conservative side since you might expect the peak periods to be generally sunnier and therefore more likely to have lower light levels. It is also consistent with the control type reducing the wattage lighting load, the same as the general lighting measures. [↑](#footnote-ref-545)
545. DEER 2008 [↑](#footnote-ref-546)
546. Goldberg et al, State of Wisconsin, Public Service Commission of Wisconsin, Focus on Energy Evaluation Business programs Incremental Cost Study, KEMA, October 28, 2009 [↑](#footnote-ref-547)
547. Ibid [↑](#footnote-ref-548)
548. Efficiency Vermont TRM, October 26, 2011. [↑](#footnote-ref-549)
549. Goldberg et al, State of Wisconsin Public Service Commission of Wisconsin, Focus on Energy Evaluation, Business Programs, Incremental Cost Study, KEMA, October 28, 2009 [↑](#footnote-ref-550)
550. Ibid [↑](#footnote-ref-551)
551. Efficiency Vermont TRM 2/19/2010 [↑](#footnote-ref-552)
552. Kuiken, Tammy eta al, State of Wisconsin/Public Service Commission of Wisconsin, Focus on Energy Evaluation, Business Programs, Deemed Savings Manual V1.0, PA Consulting Group and KEMA, March 22, 2010 pp 4-192-194. [↑](#footnote-ref-553)
553. Papamichael, Konstantions, Bi-Level Switching in Office Spaces, California Lighting Technology Center, February 1,2010. Note: See Figure 8 on page 10 for relevant study results. The study shows a 30% extra savings above a typical occupancy sensor; 41% \* 1.3 = 53%.. [↑](#footnote-ref-554)
554. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-555)
555. Coincidence Factor Study Residential and Commercial Industrial Lighting Measures, RLW Analytics, Spring 2007. Note, the connected load used in the calculation of the CF for occupancy sensor lights includes the average ESF. [↑](#footnote-ref-556)
556. Equal to the manufacturers standard warranty [↑](#footnote-ref-557)
557. The savings from solar light tubes are only realized during the sunlight hours. It is therefore appropriate to apply the single shift (8/5) loadshape to this measure. [↑](#footnote-ref-558)
558. Solatube Test Report (2005). http://www.mainegreenbuilding.com/files/file/solatube/stb\_lumens\_datasheet.pdf [↑](#footnote-ref-559)
559. Ibid. The lumen values presented in the kW table represent the average of the lightest 2400 hours. [↑](#footnote-ref-560)
560. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-561)
561. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-562)
562. Based on ComEd’s BILD program data from PY5. For Residential installations, hours of use assumptions from ‘5.5 Interior Hardwired Compact Fluorescent Lamp (CFL) Fixture’ measure should be used. [↑](#footnote-ref-563)
563. 15 years from GDS Measure Life Report, June 2007 [↑](#footnote-ref-564)
564. Illinois evaluation of PY1 through PY3 has not found that fixtures or lamps placed into storage to be a significant enough issue to warrant including an “In-Service Rate” when commercial customers complete an application form. [↑](#footnote-ref-565)
565. 1st year in service rate is based upon review of PY4-5 evaluations from ComEd’s commercial lighting program (BILD) (see ‘IL Commercial Lighting ISR.xls’ for more information [↑](#footnote-ref-566)
566. The 98% Lifetime ISR assumption is based upon review of two evaluations:

     ‘Nexus Market Research, RLW Analytics and GDS Associates study; “New England Residential Lighting Markdown Impact Evaluation, January 20, 2009’ and ‘KEMA Inc, Feb 2010, Final Evaluation Report:, Upstream Lighting Program, Volume 1.’ This implies that only 2% of bulbs purchased are never installed. The second and third year installations are based upon Ameren analysis of the Californian KEMA study showing that 54% of future installs occur in year 2 and 46% in year 3. The 2nd and 3rd year installations should be counted as part of those future program year savings. [↑](#footnote-ref-567)
567. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-568)
568. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-569)
569. Adapted from Efficiency Vermont Technical Reference User Manual (TRM) Measure Savings Algorithms and Cost Assumptions, October 26, 2011. [↑](#footnote-ref-570)
570. Ibid. [↑](#footnote-ref-571)
571. Adapted from Efficiency Vermont Technical Reference User Manual (TRM) Measure Savings Algorithms and Cost Assumptions, October 26, 2011. [↑](#footnote-ref-572)
572. Efficiency Vermont Technical Reference User Manual (TRM) Measure Savings Algorithms and Cost Assumptions, October 26, 2011

     EPE Program Downloads. Web accessed [http://www.epelectricefficiency.com/downloads.asp?section=ci](http://www.icc.illinois.gov/downloads/public/edocket/303835.pdf?section=ci) download Copy of LSF\_2012\_v4.04\_250rows.xls.

     Kuiken et al, Focus on Energy Evaluation. Business Programs: Deemed Savings Manual v1.0, Kema, march 22, 2010 available at [http://www.focusonenergy.com/files/Document\_Management\_System/Evaluation/bpdeemedsavingsmanuav10\_evaluationreport.pdf](http://www1.eere.energy.gov/buildings/appliance_standards/residential/pdfs/water_heater_fr.pdf) [↑](#footnote-ref-573)
573. DEER 2008. [↑](#footnote-ref-574)
574. Consistent with the Multi-level Fixture measure with reference to Goldberg et al, State of Wisconsin Public Service Commission of Wisconsin, Focus on Energy Evaluation, Business Programs: Incremental Cost Study, KEMA, October 28, 2009. Also consistent with field experience of about $250 per fixture and $25 install labor. [↑](#footnote-ref-575)
575. Average found from the four buildings in the State of California Energy Commission Lighting Research Program

     Bi-Level Stairwell Fixture Performance Final Report: <http://www.archenergy.com/lrp/lightingperf_standards/project_5_1_reports.htm> [↑](#footnote-ref-576)
576. Value determined from the Pacific Gas and Electric Company: Bi-Level Lighting Control Credits study for Interior Corridors of Hotels, Motels and High Rise Residential.

     <http://www.energy.ca.gov/title24/2005standards/archive/documents/2002-07-18_workshop/2002-07-18_BILEVEL_LIGHTING.PDF> [↑](#footnote-ref-577)
577. Conservative estimate. [↑](#footnote-ref-578)
578. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-579)
579. Coincidence Factor Study Residential and Commercial Industrial Lighting Measures, RLW Analytics, Spring 2007. Note, the connected load used in the calculation of the CF for occupancy sensor lights includes the average ESF. [↑](#footnote-ref-580)
580. Source: DEER 2008 [↑](#footnote-ref-581)
581. Ibid. [↑](#footnote-ref-582)
582. Measure savings from ComEd TRM developed by KEMA. June 1, 2010 [↑](#footnote-ref-583)
583. Measure Life Study, prepared for the Massachusetts Joint Utilities, Energy & Resource Solutions, November 2005. [↑](#footnote-ref-584)
584. ComEd workpapers, 8—15-11.pdf [↑](#footnote-ref-585)
585. Assumed that the peak period is coincident with periods of high traffic diminishing the demand reduction potential of occupancy based controls. [↑](#footnote-ref-586)
586. USA Technologies Energy Management Product Sheets, July 2006; cited September 2009. <http:// http://www.usatech.com/energy\_management/energy\_productsheets.php> [↑](#footnote-ref-587)
587. Ibid. [↑](#footnote-ref-588)
588. 2008 Database for Energy-Efficiency Resources (DEER), Version 2008.2.05, “Effective/Remaining Useful Life Values”, California Public Utilities Commission, December 16, 2008. [↑](#footnote-ref-589)
589. Efficiency Vermont Technical Reference User Manual (TRM) Measure Savings Algorithms and Cost Assumptions, February, 19, 2010 [↑](#footnote-ref-590)
590. Source partial list from DEER 2008 [↑](#footnote-ref-591)
591. Based on the assumption that humidity levels will most likely be relatively high during the peak period, reducing the likelihood of demand savings from door heater controls. [↑](#footnote-ref-592)
592. A review of TRM methodologies from Vermont, New York, Wisconsin, and Connecticut reveals several different sources for this factor. Connecticut requires site-specific information, whereas New York’s characterization does not explicitly identify the kWbase. Connecticut and Vermont provide values that are very consistent, and the simple average of these two values has been used for the purposes of this characterization. [↑](#footnote-ref-593)
593. A review of TRM methodologies from Vermont, New York, Wisconsin, and Connecticut reveals several different estimates of ESF. Vermont is the only TRM that provides savings estimates dependent on the control type. Additionally, these estimates are the most conservative of all TRMs reviewed. These values have been adopted for the purposes of this characterization. [↑](#footnote-ref-594)
594. Efficiency Vermont Technical Reference User Manual (TRM) Measure Savings Algorithms and Cost Assumptions, February, 19, 2010 [↑](#footnote-ref-595)
595. Energy Efficiency Supermarket Refrigeration, Wisconsin Electric Power Company, July 23, 1993 [↑](#footnote-ref-596)
596. DEER [↑](#footnote-ref-597)
597. Act on Energy Commercial Technical Reference Manual No. 2010-4 [↑](#footnote-ref-598)
598. “Efficient Evaporator Fan Motors (Shaded Pole to ECM),” Workpaper WPSCNRRN0011. Southern California Edison Company. 2007. [↑](#footnote-ref-599)
599. ENERGY STAR [↑](#footnote-ref-600)
600. ENERGY STAR [↑](#footnote-ref-601)
601. Savings from Vending Machine Calculator: http://www.energystar.gov/index.cfm?fuseaction=find\_a\_product.showProductGroup&pgw\_code=VMC [↑](#footnote-ref-602)
602. Source: DEER [↑](#footnote-ref-603)
603. Source: DEER [↑](#footnote-ref-604)
604. 2005 Database for Energy Efficiency Resources (DEER) Update Study Final Report [↑](#footnote-ref-605)
605. See “Ca Climate Zone Translation.docx” and “CDD Base 80 zone comparison.xlsx” [↑](#footnote-ref-606)
606. M. Goldberg, J. Ryan Barry, B. Dunn, M. Ackley, J. Robinson, and D. Deangelo-Woolsey, KEMA. “Focus on Energy: Business Programs – Measure Life Study”, August 2009. [↑](#footnote-ref-607)
607. Assume average walk in door size is 3.5 feet wide and 8 feet tall or 28 square feet. The reference for incremental cost is $10.22 per square foot of door opening (includes material and labor). 2008 Database for Energy-Efficiency Resources (DEER), Version 2008.2.05, “Cost Values and Summary Documentation”, California Public Utilities Commission, December 16, 2008, Therefore incremental cost per door is $286.16 [↑](#footnote-ref-608)
608. The summer coincident peak demand reduction is assumed as the total annual savings divided by the total number of hours per year, effectively assuming the average demand reduction is realized during the peak period. This is a reasonable assumption for refrigeration savings. [↑](#footnote-ref-609)
609. Values based on analysis prepared by ADM for FirstEnergy utilities in Pennsylvania, provided via personal communication with Diane Rapp of FirstEnergy on June 4, 2010. Based on a review of deemed savings assumptions and methodologies from Oregon and California, the values from Pennsylvania appear reasonable and are the most applicable. [↑](#footnote-ref-610)
610. Estimated life from Efficiency Vermont TRM [↑](#footnote-ref-611)
611. Based on average of costs from Freeaire, Natural Cool, and Cooltrol economizer systems. [↑](#footnote-ref-612)
612. Based on the assumption that humidity levels will most likely be relatively high during the peak period, reducing the likelihood of demand savings. [↑](#footnote-ref-613)
613. Savings table uses Economizer Calc.xls. Assume 5HP compressor size used to develop kWh/Hp value. No floating head pressure controls and compressor is located outdoors [↑](#footnote-ref-614)
614. In the source TRM (VT) this value was 2,996 hrs based on 38° F cooler setpoint, Burlington VT weather data, and 5 degree economizer deadband. The IL numbers were calculated by using weather bin data for each location (number of hours < 38F at each location is the Hours value). [↑](#footnote-ref-615)
615. A 50% duty cycle is assumed based on examination of duty cycle assumptions from Richard Travers (35%-65%), Cooltrol (35%-65%), Natural Cool (70%), Pacific Gas & Electric (58%). Also, manufacturers typically size equipment with a built-in 67% duty factor and contractors typically add another 25% safety factor, which results in a 50% overall duty factor. (as referenced by the Efficiency Vermont, Technical Reference User Manual) [↑](#footnote-ref-616)
616. Based on an a weighted average of 80% shaded pole motors at 132 watts and 20% PSC motors at 88 watts [↑](#footnote-ref-617)
617. Wattage of fan used by Freeaire and Cooltrol. This fan is used to circulate air in the cooler when the evaporator fan is turned off. As such, it is not used when fan control is not present [↑](#footnote-ref-618)
618. Average of two manufacturer estimates of 50% and 75%. [↑](#footnote-ref-619)
619. Bonus factor (1+ 1/3.5) assumes COP of 3.5, based on the average of standard reciprocating and discus compressor efficiencies with a Saturated Suction Temperature of 20°F and a condensing temperature of 90°F [↑](#footnote-ref-620)
620. The 227 watts for an economizer is calculated from the average of three manufacturers: Freeaire (186 Watts), Cooltrol (285 Watts), and Natural Cool (218 Watts). [↑](#footnote-ref-621)
621. 2014 Database for Energy-Efficiency Resources (DEER), Version 2014, “Cost Values and Summary Documentation”, California Public Utilities Commission, January, 2014. [↑](#footnote-ref-622)
622. 2014 Database for Energy-Efficiency Resources (DEER), Version 2014, “Cost Values and Summary Documentation”, California Public Utilities Commission, January, 2014. [↑](#footnote-ref-623)
623. Energy Conservation Standards for Commercial Refrigeration Equipment: Technical Support Document, U.S. Department of Energy, September 2013. The information required to estimate annual energy savings for refrigerated display cases is taken from the 2013-2014 U.S. Department of Energy (DOE) energy conservation standard rulemaking for Commercial Refrigerated Equipment. During the rulemaking process, DOE estimates the energy savings specific to night covers through extensive simulation and energy models that are validated by both manufacturers of night covers and refrigerated cases. The information is also referenced from a study done by Southern California Edison and testing by Technischer Uberwachungs-Verein Rheinland, which are used by DOE for the rulemaking process. [↑](#footnote-ref-624)
624. Southern California Edison Refrigeration Technology and Test Center. Effects of the Low Emissivity Shields on Performance and Power Use of a Refrigerated Display Case. 1997. Southern California Edison, Rancho Cucamonga, CA. [↑](#footnote-ref-625)
625. Technischer Uberwachungs-Verein Rheinland E.V. Laboratory test results for energy savings on refrigerated dairy case, conducted for Econofrost. [↑](#footnote-ref-626)
626. Conversion factor and offset based on a linear regression analysis of the relationship between air compressor motor nominal horsepower and incremental cost. Several Vermont vendors were surveyed to determine the cost of equipment. See “Compressed Air Analysis.xls” and “Compiled Data ReQuest Results.xls” for incremental cost details. [↑](#footnote-ref-627)
627. Conversion factor based on a linear regression analysis of the relationship between air compressor motor nominal horsepower and full load kW from power measurements of 72 compressors at 50 facilities on Long Island. See "BHP Weighted Compressed Air Load Profiles v2.xls". [↑](#footnote-ref-628)
628. Compressor factors were developed using DOE part load data for different compressor control types as well as load profiles from 50 facilities employing air compressors less than or equal to 40 hp. “See “BHP Weighted Compressed Air Load Profiles.xls” for source data and calculations (The “variable speed drive” compressor factor has been adjusted up from the 0.675 presented in the analysis to 0.705 to account for the additional power draw of the VSD). [↑](#footnote-ref-629)
629. Ibid. [↑](#footnote-ref-630)
630. Incremental cost research found in LPDF Costs. xlsx [↑](#footnote-ref-631)
631. See “Industrial System Standard Deemed Saving Analysis.xls” [↑](#footnote-ref-632)
632. See “Industrial System Standard Deemed Saving Analysis.xls” [↑](#footnote-ref-633)
633. Assumed pressure will be reduced from a roughly 3 psi pressure drop through a filter to less than 1 psi, for a 2 psi savings [↑](#footnote-ref-634)
634. “Optimizing pneumatic systems for extra savings,” 10, 2010, <http://www.compressedairchallenge.org/library/articles/2010-10-CABP.pdf> [↑](#footnote-ref-635)
635. Industrial System Standard Deemed Saving Analysis.xls [↑](#footnote-ref-636)
636. Based on empirical project data from ComEd Comprehensive Compressed Air Study program and VEIC review of pricing data found in CAS Cost Data.xls [↑](#footnote-ref-637)
637. Reduced CFM consumption is based on an a timer drain opening for 10 seconds every 300 seconds as the baseline. See “Industrial System Standard Deemed Saving Analysis.xls” [↑](#footnote-ref-638)
638. Calculated based on the type of compressor control. This assumes the compressor will be between 40% and 100% capacity before and after the changes to the system demand. See “Industrial System Standard Deemed Saving Analysis.xls” [↑](#footnote-ref-639)
639. US DOE, Evaluation of the Compressed Air Challenge® Training Program, Page 19 [↑](#footnote-ref-640)
640. Martin, N. et al., Emerging Energy-Efficient Industrial Technologies: New York State Edition, American Council for an Energy Efficient Economy (ACEEE), March 2001 (as stated in the OH State TRM, page 269) [↑](#footnote-ref-641)
641. Summer Peak Coincidence Factor has been preserved from the “Technical Reference Manual” (TRM) for Ohio Senate Bill 221 Energy Efficiency and Conservation Program and 09-512-GE-UNC,” October 15, 2009. This is likely a conservative estimate, but is recommended for further study (as stated in the OH State TRM, page 269) [↑](#footnote-ref-642)
642. “Measured Loading of Energy Efficient Motors - the Missing Link in Engineering Estimates of Savings,” ACEEE 1994 Summer Study Conference, Asilomar, CA. [↑](#footnote-ref-643)
643. Published estimates of typical pumping efficiency improvements range from 5 to 40%. For analysis purposes, assume 15%.

     United States Industrial Electric Motor Systems Market Opportunities Assessment December 2002, Table E-7, Page 18, <https://www1.eere.energy.gov/manufacturing/tech_assistance/pdfs/mtrmkt.pdf> [↑](#footnote-ref-644)
644. Summer Peak Coincidence Factor has been preserved from the “Technical Reference Manual” (TRM) for Ohio Senate Bill 221 Energy Efficiency and Conservation Program and 09-512-GE-UNC,” October 15, 2009. This is likely a conservative estimate, but is recommended for further study (as stated in the OH State TRM, page 269) [↑](#footnote-ref-645)
645. PA Consulting Group (2009). Business Programs: Measure Life Study. Prepared for State of Wisconsin Public Service Commission. [↑](#footnote-ref-646)
646. Costs are from EXAIR’s website and are an average of nozzles that meet the flow requirements. Models include Atto Super, Pico Super, Nano Super, Micro Super, Mini Super, Super and Large Super nozzles. www.exair.com. Accessed March 20, 2014 [↑](#footnote-ref-647)
647. Review of manufacturer’s information [↑](#footnote-ref-648)
648. Technical Reference Manual (TRM) for Ohio Senate Bill 221”Energy Efficiency and Conservation Program” and 09-512-GE-UNC, October 15,

     2009. Pgs 170-171 [↑](#footnote-ref-649)
649. Conservative estimate based on average values provided by the Compressed Air Challenge Training Program, Machinery’s Handbook 25th

     Edition, and manufacturers’ catalog. [↑](#footnote-ref-650)
650. Calculated based on the type of compressor control. This assumes the compressor will be between 40% and 100% capacity before and after the changes to the system demand. See “Industrial System Standard Deemed Saving Analysis.xls” [↑](#footnote-ref-651)
651. Weighting of 16% single shift, 23% two shift, 25% three shift and 36% continual based on DOE evaluation of the Compressed Air Challenge, section 2.1.5 Facility Operating Schedules [↑](#footnote-ref-652)
652. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The AC load during the utility’s peak hour is divided by the maximum AC load during the year. [↑](#footnote-ref-653)
653. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year [↑](#footnote-ref-654)
654. National Solar Radiation Data Base -- 1991- 2005 Update: Typical Meteorological Year 3

     <http://rredc.nrel.gov/solar/old_data/nsrdb/1991-2005/tmy3/by_state_and_city.html> [↑](#footnote-ref-655)
655. National Solar Radiation Data Base -- 1991- 2005 Update: Typical Meteorological Year 3

     <http://rredc.nrel.gov/solar/old_data/nsrdb/1991-2005/tmy3/by_state_and_city.html> [↑](#footnote-ref-656)
656. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The AC load during the utility’s peak hour is divided by the maximum AC load during the year. [↑](#footnote-ref-657)
657. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year [↑](#footnote-ref-658)
658. The following reference uses 10 years, however, given the rapid changes in the technology industry, there is quite a lot of uncertainty about the measure life and a more conservative value was used (i.e. half the published measure life): Table VI.1: Dimetrosky, S., Luedtke, J. S., & Seiden, K. (2005). Surveyor Network Energy Manager: Market Progress Evaluation Report, No. 2 (Northwest Energy Efficiency Alliance report #E05-136). Portland, OR: Quantec LLC;). [↑](#footnote-ref-659)
659. Work Paper WPSCNROE0003 Revision 1, Power Management Software for Networked Computers. Southern California Edison [↑](#footnote-ref-660)
660. Based on average energy savings/computer from the following sources:

     South California Edison, Work Paper WPSCNROE0003 (200k Wh)

     Surveyor Network Energy Manager Evaluation Report , NEEA (68, 100, and 128kWh)

     Regional Technical Forum <http://rtf.nwcouncil.org/measures/measure.asp?id=95> (200 kWh)

     EnergySTAR Computer Power Management Savings Calculator (~190 kWh for a mix of laptop/desktop and assuming 30% are already turned off at night)

     <http://www.energystar.gov/ia/products/power_mgt/LowCarbonITSavingsCalc.xlsx?78c1-120e&78c1-120e>

     Power Management for Networked Computers: A Review of Utility Incentive Programs J. Michael Walker, Beacon Consultants Network Inc., 2009 ACEEE Summer Study on Energy Efficiency in Industry (330 kWh) [↑](#footnote-ref-661)
661. Power Management for Networked Computers: A Review of Utility Incentive Programs J. Michael Walker, Beacon Consultants Network Inc., 2009 ACEEE Summer Study on Energy Efficiency in Industry [↑](#footnote-ref-662)
662. Based on PY6 ComEd Computer Software Program data showing a split of 74% desktop to 26% laptop. [↑](#footnote-ref-663)
663. Dimetrosky, S., Luedtke, J. S., & Seiden, K. (2005). Surveyor Network Energy Manager: Market Progress Evaluation Report, No. 2 (Northwest Energy Efficiency Alliance report #E05-136). Portland, OR: Quantec LLC [↑](#footnote-ref-664)
664. Measured according to the latest ANSI/AHAM AC-1 (AC-1) Standard [↑](#footnote-ref-665)
665. As defined as the average of non-ENERGY STAR products found in EPA research, 2008, ENERGY STAR Qualified Room Air Cleaner Calculator,

     [http://www.energystar.gov/ia/business/bulk\_purchasing/bpsavings\_calc/CalculatorRoomAirCleaner.xls?8ed7-275b](http://www.energystar.gov/ia/business/bulk_purchasing/bpsavings_calc/Calc_CAC.xls?8ed7-275b). [↑](#footnote-ref-666)
666. ENERGY STAR Qualified Room Air Cleaner Calculator,

     [http://www.energystar.gov/ia/business/bulk\_purchasing/bpsavings\_calc/CalculatorRoomAirCleaner.xls?8ed7-275b](http://www.icc.illinois.gov/downloads/public/edocket/303834.pdf?8ed7-275b). [↑](#footnote-ref-667)
667. Ibid [↑](#footnote-ref-668)
668. ENERGY STAR Qualified Room Air Cleaner Calculator, [http://www.energystar.gov/ia/business/bulk\_purchasing/bpsavings\_calc/CalculatorRoomAirCleaner.xls?8ed7-275b](http://www.energystar.gov/ia/partners/product_specs/program_reqs/room_air_conditioners_prog_req.pdf?8ed7-275b) [↑](#footnote-ref-669)
669. Ibid. [↑](#footnote-ref-670)
670. Consistent with ENERGY STAR Qualified Room Air Cleaner Calculator. [↑](#footnote-ref-671)
671. Some types of room air cleaners require filter replacement or periodic cleaning, but this is likely to be true for both efficient and baseline units and so no difference in cost is assumed. [↑](#footnote-ref-672)
672. See http://www1.eere.energy.gov/buildings/appliance\_standards/product.aspx/productid/39. [↑](#footnote-ref-673)
673. Based on DOE Life-Cycle Cost and Payback Period Excel-based analytical tool, available online at:

     [http://www1.eere.energy.gov/buildings/appliance\_standards/residential/clothes\_washers\_support\_stakeholder\_negotiations.html](http://www.ahrinet.org/ARI/util/showdoc.aspx) [↑](#footnote-ref-674)
674. Cost estimates are based on Navigant analysis for the Department of Energy (see CW Analysis\_09092014.xls). This analysis looked at incremental cost and shipment data from manufacturers and the Association of Home Appliance Manufacturers and attempts to find the costs associated only with the efficiency improvements. The ENERGY STAR level in this analysis was made the baseline (as it is now equivalent), the CEE Tier 3 level was made ENERGY STAR and ENERGY STAR Most efficient was extrapolated based on equal rates. Note these assumptions should be reviewed as qualifying product becomes available. [↑](#footnote-ref-675)
675. Calculated from Itron eShapes, 8760 hourly data by end use for Missouri, as provided by Ameren. [↑](#footnote-ref-676)
676. Definition provided on the Energy star website. [↑](#footnote-ref-677)
677. Tsavings represents total kWh only when water heating and drying are 100% electric. [↑](#footnote-ref-678)
678. Based on the average clothes washer volume of all units that pass the new Federal Standard on the California Energy Commission (CEC) database of Clothes Washer products accessed on 08/28/2014. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used. [↑](#footnote-ref-679)
679. Weighted average IMEF of Federal Standard rating for Front Loading and Top Loading units. Weighting is based upon the relative top v front loading percentage of available non-ENERGY STAR product in the CEC database. [↑](#footnote-ref-680)
680. Weighted average of 295 clothes washer cycles per year (based on 2009 Residential Energy Consumption Survey (RECS) national sample survey of housing appliances section, state of IL: [http://www.eia.gov/consumption/residential/data/2009/](http://www.focusonenergy.com/files/Document_Management_System/Evaluation/bpdeemedsavingsmanuav10_evaluationreport.pdf)

     If utilities have specific evaluation results providing a more appropriate assumption for single-family or multi-family homes, in a particular market, or geographical area then that should be used. [↑](#footnote-ref-681)
681. IMEF values are the weighted average of the new ENERGY STAR specifications. Weighting is based upon the relative top v front loading percentage of available ENERGY STAR and ENERGY STAR Most Efficient product in the CEC database. See “CW Analysis\_09092014.xls” for the calculation. [↑](#footnote-ref-682)
682. The percentage of total energy consumption that is used for the machine, heating the hot water or by the dryer is different depending on the efficiency of the unit. Values are based on a weighted average of top loading and front loading units based on data from Life-Cycle Cost and Payback Period Excel-based analytical tool, available online at: [http://www1.eere.energy.gov/buildings/appliance\_standards/residential/clothes\_washers\_support\_stakeholder\_negotiations.html](http://www.energystar.gov/ia/business/bulk_purchasing/bpsavings_calc/CalculatorConsumerDehumidifier.xls). See “CW Analysis\_09092014.xls” for the calculation. [↑](#footnote-ref-683)
683. Default assumption for unknown fuel is based on EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used [↑](#footnote-ref-684)
684. Default assumption for unknown is based on percentage of homes with electric dryer from EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used. [↑](#footnote-ref-685)
685. Based on a weighted average of 295 clothes washer cycles per year assuming an average load runs for one hour (2009 Residential Energy Consumption Survey (RECS) national sample survey of housing appliances section: [http://www.eia.gov/consumption/residential/data/2009/](http://ilsag.org/yahoo_site_admin/assets/docs/ComEd_PY2_CACES_Evaluation_Report_2010-10-18.299122020.pdf)) [↑](#footnote-ref-686)
686. Calculated from Itron eShapes, 8760 hourly data by end use for Missouri, as provided by Ameren. [↑](#footnote-ref-687)
687. To account for the different efficiency of electric and Natural Gas hot water heaters (gas water heater: recovery efficiencies ranging from 0.74 to 0.85 (0.78 used), and electric water heater with 0.98 recovery efficiency ([http://www.energystar.gov/ia/partners/bldrs\_lenders\_raters/downloads/Waste\_Water\_Heat\_Recovery\_Guidelines.pdf](http://www.energystar.gov) ). Therefore a factor of 0.98/0.78 (1.26) is applied. [↑](#footnote-ref-688)
688. Default assumption for unknown fuel is based on percentage of homes with gas dryer from EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used [↑](#footnote-ref-689)
689. Ibid. [↑](#footnote-ref-690)
690. Weighted average IWF of Federal Standard rating for Front Loading and Top Loading units. Weighting is based upon the relative top v front loading percentage of available non-ENERGY STAR product in the CEC database. [↑](#footnote-ref-691)
691. IWF values are the weighted average of the new ENERGY STAR specifications. Weighting is based upon the relative top v front loading percentage of available ENERGY STAR and ENERGY STAR Most Efficient product in the CEC database. See “CW Analysis\_09092014.xls” for the calculation. [↑](#footnote-ref-692)
692. Energy Star Version 3.0 will become effective 10/1/12 [↑](#footnote-ref-693)
693. <http://www.energystar.gov/ia/partners/prod_development/revisions/downloads/dehumid/ES_Dehumidifiers_Final_V3.0_Eligibility_Criteria.pdf?d70c-99b0> [↑](#footnote-ref-694)
694. The Federal Standard for Dehumidifiers changed as of October 2012; https://www.federalregister.gov/articles/2010/12/02/2010-29756/energy-conservation-program-for-consumer-products-test-procedures-for-residential-dishwashers#h-11 [↑](#footnote-ref-695)
695. ENERGY STAR Dehumidifier Calculator <http://www.energystar.gov/ia/business/bulk_purchasing/bpsavings_calc/CalculatorConsumerDehumidifier.xls> [↑](#footnote-ref-696)
696. Based on extrapolating available data from the Department of Energy’s Life Cycle Cost analysis spreadsheet and weighting based on volume of units available:

     <http://www1.eere.energy.gov/buildings/appliance_standards/residential/docs/lcc_dehumidifier.xls>

     See ‘DOE life cycle cost\_dehumidifier.xls’ for calculation. [↑](#footnote-ref-697)
697. Assume usage is evenly distributed day vs. night, weekend vs. weekday and is used between April through the end of September (4392 possible hours). 1620 operating hours from ENERGY STAR Dehumidifier Calculator. Coincidence peak during summer peak is therefore 1620/4392 = 36.9% [↑](#footnote-ref-698)
698. ENERGY STAR Dehumidifier Calculator <http://www.energystar.gov/ia/business/bulk_purchasing/bpsavings_calc/CalculatorConsumerDehumidifier.xls> [↑](#footnote-ref-699)
699. [↑](#footnote-ref-700)
700. Based on 68 days of 24 hour operation; ENERGY STAR Dehumidifier Calculator <http://www.energystar.gov/ia/business/bulk_purchasing/bpsavings_calc/appliance_calculator.xlsx?f3f7-6a8b&f3f7-6a8b> [↑](#footnote-ref-701)
701. Assume usage is evenly distributed day vs. night, weekend vs. weekday and is used between April through the end of September (4392 possible hours). 1620 operating hours from ENERGY STAR Dehumidifier Calculator. Coincidence peak during summer peak is therefore 1620/4392 = 36.9% [↑](#footnote-ref-702)
702. As of May 30, 2013 the Federal Baseline specification for compact units is equal to the ENERGY STAR specification. [↑](#footnote-ref-703)
703. http://www1.eere.energy.gov/buildings/appliance\_standards/product.aspx/productid/67 [↑](#footnote-ref-704)
704. Koomey, Jonathan et al. (Lawrence Berkeley National Lab), Projected Regional Impacts of Appliance Efficiency Standards for the U.S. Residential Sector, February 1998. [↑](#footnote-ref-705)
705. Estimate based on review of Energy Star stakeholder documents [↑](#footnote-ref-706)
706. Calculated from Itron eShapes, 8760 hourly data by end use for Missouri, as provided by Ameren. [↑](#footnote-ref-707)
707. The Federal Standard and ENERGY STAR annual consumption values include electric consumption for both the operation of the machine and for heating the water that is used by the machine. [↑](#footnote-ref-708)
708. ENERGY STAR Dishwasher Calculator ([http://www.energystar.gov/ia/business/bulk\_purchasing/bpsavings\_calc/CalculatorConsumerDishwasher.xls](http://www.energystar.gov/ia/business/bulk_purchasing/bpsavings_calc/CalculatorConsumerDehumidifier.xls)) [↑](#footnote-ref-709)
709. Ibid. [↑](#footnote-ref-710)
710. Default assumption for unknown fuel is based on EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used. [↑](#footnote-ref-711)
711. Assuming one and a half hours per cycle and 168 cycles per year therefore 252 operating hours per year; 168 cycles per year is based on a weighted average of dishwasher usage in Illinois derived from the 2009 RECs data; [http://205.254.135.7/consumption/residential/data/2009/](http://mn.gov/commerce/energy/images/ElectricFoodService_v03.2.xls) [↑](#footnote-ref-712)
712. End use data from Ameren representing the average DW load during peak hours/peak load. [↑](#footnote-ref-713)
713. Default assumption for unknown fuel is based on EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used. [↑](#footnote-ref-714)
714. To account for the different efficiency of electric and Natural Gas hot water heaters (gas water heater: recovery efficiencies ranging from 0.74 to 0.85 (0.78 used), and electric water heater with 0.98 recovery efficiency ([http://www.energystar.gov/ia/partners/bldrs\_lenders\_raters/downloads/Waste\_Water\_Heat\_Recovery\_Guidelines.pdf](http://www.eia.gov/consumption/residential/data/2009/xls/HC7.9%20Air%20Conditioning%20in%20Midwest%20Region.xls)). Therefore a factor of 0.98/0.78 (1.26) is applied. [↑](#footnote-ref-715)
715. Assuming 5 gallons/cycle (maximum allowed) and 168 cycles per year based on a weighted average of dishwasher usage in Illinois derived from the 2009 RECs data; [http://205.254.135.7/consumption/residential/data/2009/](http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls) [↑](#footnote-ref-716)
716. Assuming 4.25gallons/cycle (maximum allowed) and 168 cycles per year based on a weighted average of dishwasher usage in Illinois derived from the 2009 RECs data; [http://205.254.135.7/consumption/residential/data/2009/](http://www.energystar.gov/ia/business/bulk_purchasing/bpsavings_calc/Consumer_Residential_Refrig_Sav_Calc.xls) [↑](#footnote-ref-717)
717. http://www1.eere.energy.gov/buildings/appliance\_standards/product.aspx/productid/43 [↑](#footnote-ref-718)
718. [http://www.energystar.gov/ia/products/appliances/refrig/NAECA\_calculation.xls?c827-f746](http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls?c827-f746) [↑](#footnote-ref-719)
719. http://www1.eere.energy.gov/buildings/appliance\_standards/product.aspx/productid/43 [↑](#footnote-ref-720)
720. http://www.energystar.gov/products/specs/sites/products/files/ENERGY%20STAR%20Final%20Version%205.0%20Residential%20Refrigerators%20and%20Freezers%20Specification.pdf [↑](#footnote-ref-721)
721. Energy Star Freezer Calculator; [http://www.energystar.gov/ia/business/bulk\_purchasing/bpsavings\_calc/Consumer\_Residential\_Freezer\_Sav\_Calc.xls?570a-f000](http://mn.gov/commerce/energy/images/ElectricFoodService_v03.2.xls?570a-f000) [↑](#footnote-ref-722)
722. Based on review of data from the Northeast Regional ENERGY STAR Consumer Products Initiative; “2009 ENERGY STAR Appliances Practices Report”, submitted by Lockheed Martin, December 2009. [↑](#footnote-ref-723)
723. Based on eShapes Residential Freezer load data as provided by Ameren. [↑](#footnote-ref-724)
724. Volume is based on ENERGY STAR Calculator assumption of 16.14 ft3 average volume, converted to Adjusted volume by multiplying by 1.73. [↑](#footnote-ref-725)
725. Calculated from eShapes Residential Freezer load data as provided by Ameren by dividing total annual load by the maximum kW in any one hour. [↑](#footnote-ref-726)
726. Based on eShapes Residential Freezer load data as provided by Ameren. [↑](#footnote-ref-727)
727. http://www1.eere.energy.gov/buildings/appliance\_standards/product.aspx/productid/43 [↑](#footnote-ref-728)
728. [http://www.energystar.gov/ia/products/appliances/refrig/NAECA\_calculation.xls?c827-f746](http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls?c827-f746) [↑](#footnote-ref-729)
729. http://www1.eere.energy.gov/buildings/appliance\_standards/product.aspx/productid/43 [↑](#footnote-ref-730)
730. http://www.energystar.gov/products/specs/sites/products/files/ENERGY%20STAR%20Final%20Version%205.0%20Residential%20Refrigerators%20and%20Freezers%20Specification.pdf [↑](#footnote-ref-731)
731. From ENERGY STAR calculator: http://www.energystar.gov/buildings/sites/default/uploads/files/appliance\_calculator.xlsx?7224-046c=&7224-\_\_046ceiling\_fan\_calculator\_xlsx=&f7d8-39dd&f7d8-39dd [↑](#footnote-ref-732)
732. Standard assumption of one third of effective useful life. [↑](#footnote-ref-733)
733. From ENERGY STAR calculator linked above. [↑](#footnote-ref-734)
734. Based on weighted average of units participating in Efficiency Vermont program and retail cost data provided in Department of Energy, “TECHNICAL REPORT: Analysis of Amended Energy Conservation Standards for Residential Refrigerator-Freezers”, October 2005; [http://www1.eere.energy.gov/buildings/appliance\_standards/pdfs/refrigerator\_report\_1.pdf](http://www.bpa.gov/energy/n/reports/evaluation/residential/faucet_aerator.cfm) [↑](#footnote-ref-735)
735. ENERGY STAR full cost is based upon IL PHA Efficient Living Program data on sample size of 910 replaced units finding average cost of $430 plus an average recycling/removal cost of $21. The CEE Tier 2 estimate uses the delta from the Time of Sale estimate. [↑](#footnote-ref-736)
736. Calculated using incremental cost from Time of Sale measure. [↑](#footnote-ref-737)
737. Volume is based on the ENERGY STAR calculator average assumption of 14.75 ft3 fresh volume and 6.76 ft3 freezer volume. [↑](#footnote-ref-738)
738. Estimates of existing unit consumption are based on using the 5.1.8 Refrigerator and Freezer Recycling algorithm and the inputs described here: Age = 10 years, Pre-1990 = 0, Size = 21.5 ft3 (from ENERGY STAR calc and consistent with AV of 25.8), Single Door = 0, Side by side = 1 for classifications stating side by side, 0 for classifications stating top/bottom, and 0.5 for classifications that do not distinguish, Primary appliances = 1, unconditioned = 0, Part use factor = 0. [↑](#footnote-ref-739)
739. Estimates of existing unit consumption are based on using the 5.1.8 Refrigerator and Freezer Recycling algorithm and the inputs described here: Age = 10 years, Pre-1990 = 0, Size = 21.5 ft3 (from ENERGY STAR calc and consistent with AV of 25.8), Single Door = 0, Side by side = 1 for classifications stating side by side, 0 for classifications stating top/bottom, and 0.5 for classifications that do not distinguish, Primary appliances = 1, unconditioned = 0, Part use factor = 0. [↑](#footnote-ref-740)
740. Average temperature adjustment factor (to account for temperature conditions during peak period as compared to year as a whole) based on Blasnik, Michael, "Measurement and Verification of Residential Refrigerator Energy Use, Final Report, 2003-2004 Metering Study", July 29, 2004 (p. 47). It assumes 90 °F average outside temperature during peak period, 71°F average temperature in kitchens and 65°F average temperature in basement, and uses assumption that 66% of homes in Illinois having central cooling (CAC saturation: "Table HC7.9 Air Conditioning in Homes in Midwest Region, Divisions, and States, 2009 from Energy Information Administration", 2009 Residential Energy Consumption Survey; [http://www.eia.gov/consumption/residential/data/2009/xls/HC7.9%20Air%20Conditioning%20in%20Midwest%20Region.xls](http://www1.eere.energy.gov/buildings/appliance_standards/residential/clothes_washers_support_stakeholder_negotiations.html) ) [↑](#footnote-ref-741)
741. Daily load shape adjustment factor (average load in peak period /average daily load) also based on Blasnik, Michael, "Measurement and Verification of Residential Refrigerator Energy Use, Final Report, 2003-2004 Metering Study", July 29, 2004 (p. 48, using the average Existing Units Summer Profile for hours 13 through 17) [↑](#footnote-ref-742)
742. http://www.energystar.gov/ia/partners/downloads/unit\_shipment\_data/2010\_USD\_Summary\_Report.pdf?3193-51e7 [↑](#footnote-ref-743)
743. http://www.energystar.gov/ia/partners/downloads/unit\_shipment\_data/2011\_USD\_Summary\_Report.pdf?3193-51e7 [↑](#footnote-ref-744)
744. http://www.energystar.gov/ia/partners/prod\_development/revisions/downloads/roomac/RAC\_ProgramRequirements\_1105.pdf?c2df-6034 [↑](#footnote-ref-745)
745. http://www.energystar.gov/index.cfm?c=roomac.pr\_crit\_room\_ac [↑](#footnote-ref-746)
746. http://library.cee1.org/sites/default/files/library/9296/CEE\_ResApp\_RoomAirConditionerSpecification\_2003\_Updated.pdf [↑](#footnote-ref-747)
747. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007.

     http://neep.org/uploads/EMV%20Forum/EMV%20Studies/measure\_life\_GDS%5B1%5D.pdf [↑](#footnote-ref-748)
748. Standard assumption of one third of effective useful life. [↑](#footnote-ref-749)
749. CEE Tier 1 based on field study conducted by Efficiency Vermont and Tier 2 based on professional judgement. [↑](#footnote-ref-750)
750. Based on IL PHA Efficient Living Prgroam Data for 810 replaced units showing $416 per unit plus $32 average recycling/removal cost. [↑](#footnote-ref-751)
751. Estimate based upon Time of Sale incremental costs. [↑](#footnote-ref-752)
752. Consistent with coincidence factors found in: RLW Report: Final Report Coincidence Factor Study Residential Room Air Conditioners, June 23, 2008 ([http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117\_RLW\_CF%20Res%20RAC.pdf](http://www.ctsavesenergy.org/files/Measure%20Life%20Report%202007.pdf)) [↑](#footnote-ref-753)
753. Full load hours for room AC is significantly lower than for central AC. The average ratio of FLH for Room AC (provided in RLW Report: Final Report Coincidence Factor Study Residential Room Air Conditioners, June 23, 2008: [http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117\_RLW\_CF%20Res%20RAC.pdf](http://www.icc.illinois.gov/downloads/public/edocket/303834.pdf)) to FLH for Central Cooling for the same location (provided by AHRI: [http://www.energystar.gov/ia/business/bulk\_purchasing/bpsavings\_calc/Calc\_CAC.xls](http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117_RLW_CF%20Res%20RAC.pdf)) is 31%. This ratio is applied to those IL cities that have FLH for Central Cooling provided in the Energy Star calculator. For other cities this is extrapolated using the FLH assumptions VEIC have developed for Central AC. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-754)
754. Weighted based on number of residential occupied housing units in each zone. [↑](#footnote-ref-755)
755. Based on maximum capacity average from the RLW Report: Final Report Coincidence Factor Study Residential Room Air Conditioners, June 23, 2008 [↑](#footnote-ref-756)
756. Based on Nexus Market Research Inc, RLW Analytics, December 2005; “Impact, Process, and Market Study of the Connecticut Appliance Retirement Program: Overall Report.” [↑](#footnote-ref-757)
757. Consistent with coincidence factors found in: RLW Report: Final Report Coincidence Factor Study Residential Room Air Conditioners, June 23, 2008 ([http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117\_RLW\_CF%20Res%20RAC.pdf](http://www.energystar.gov/ia/business/bulk_purchasing/bpsavings_calc/Calc_CAC.xls)) [↑](#footnote-ref-758)
758. KEMA “Residential refrigerator recycling ninth year retention study”, 2004 [↑](#footnote-ref-759)
759. Based on similar Efficiency Vermont program. [↑](#footnote-ref-760)
760. Based on the specified regression, a small number of units may have negative energy and demand consumption. These are a function of the unit size and age, and should comprise a very small fraction of the population. While on an individual basis this result is counterintuitive it is important that these negative results remain such that as a population the average savings is appropriate. [↑](#footnote-ref-761)
761. Energy savings are based on an average 30-year TMY temperature of 51.1 degrees. Coefficients provided in July 30, 2014 memo from Cadmus: “Appliance Recycling Update no single door July 30 2014”. [↑](#footnote-ref-762)
762. National Climatic Data Center, calculated from 1981-2010 climate normals with a base temp of 65°F. [↑](#footnote-ref-763)
763. National Climatic Data Center, calculated from 1981-2010 climate normals with a base temp of 65°F. [↑](#footnote-ref-764)
764. For example, the part-use factor that shall be applied to the current program year t (PYt) for savings verification purposes should be determined through the PYt-2 participant surveys conducted in the respective utility’s service territory, if available. If an evaluation was not performed in PYt-2 the latest available evaluation should be used.   [↑](#footnote-ref-765)
765. Most recent refrigerator part-use factor from Ameren Illinois PY5 evaluation. [↑](#footnote-ref-766)
766. Energy savings are based on an average 30-year TMY temperature of 51.1 degrees. Coefficients provided in January 31, 2013 memo from Cadmus: “Appliance Recycling Update”. [↑](#footnote-ref-767)
767. For example, the part-use factor that shall be applied to the current program year t (PYt) for savings verification purposes should be determined through the PYt-2 participant surveys conducted in the respective utility’s service territory, if available. If an evaluation was not performed in PYt-2 the latest available evaluation should be used.   [↑](#footnote-ref-768)
768. Most recent freezer part-use factor from Ameren Illnois Company PY5 evaluation. [↑](#footnote-ref-769)
769. Cadmus memo, February 12, 2013; “Appliance Recycling Update” [↑](#footnote-ref-770)
770. A third of assumed measure life for Room AC. [↑](#footnote-ref-771)
771. Consistent with coincidence factors found in: RLW Report: Final Report Coincidence Factor Study Residential Room Air Conditioners, June 23, 2008 ([http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117\_RLW\_CF%20Res%20RAC.pdf](http://205.254.135.7/consumption/residential/data/2009/)) [↑](#footnote-ref-772)
772. The average ratio of FLH for Room AC (provided in RLW Report: Final Report Coincidence Factor Study Residential Room Air Conditioners, June 23, 2008: [http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117\_RLW\_CF%20Res%20RAC.pdf](http://neep.org/uploads/EMV%20Forum/EMV%20Studies/measure_life_GDS%5b1%5d.pdf)) to FLH for Central Cooling for the same location (provided by AHRI: [http://www.energystar.gov/ia/business/bulk\_purchasing/bpsavings\_calc/Calc\_CAC.xls](http://publicservice.vermont.gov/energy/ee_files/efficiency/eval/marivtreportfinal100104.pdf)) is 31%. This ratio is applied to those IL cities that have FLH for Central Cooling provided in the Energy Star calculator. For other cities this is extrapolated using the FLH assumptions VEIC have developed for Central AC. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-773)
773. Weighted based on number of residential occupied housing units in each zone. [↑](#footnote-ref-774)
774. Based on maximum capacity average from the RLW Report: Final Report Coincidence Factor Study Residential Room Air Conditioners, June 23, 2008 [↑](#footnote-ref-775)
775. Based on Nexus Market Research Inc, RLW Analytics, December 2005; “Impact, Process, and Market Study of the Connecticut Appliance Retirement Program: Overall Report.” [↑](#footnote-ref-776)
776. Consistent with coincidence factors found in:

     RLW Report: Final Report Coincidence Factor Study Residential Room Air Conditioners, June 23, 2008 ([http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117\_RLW\_CF%20Res%20RAC.pdf](http://www1.eere.energy.gov/buildings/appliance_standards/residential/pdfs/hvac_ch_08_lcc_2011-06-24.pdf)) [↑](#footnote-ref-777)
777. ENERGY STAR Market & Industry Scoping Report. Residential Clothes Dryers. Table 8. November 2011. <http://www.energystar.gov/ia/products/downloads/ENERGY_STAR_Scoping_Report_Residential_Clothes_Dryers.pdf> [↑](#footnote-ref-778)
778. Based on an average estimated range of 12-16 years. ENERGY STAR Market & Industry Scoping Report. Residential Clothes Dryers. November 2011. <http://www.energystar.gov/ia/products/downloads/ENERGY_STAR_Scoping_Report_Residential_Clothes_Dryers.pdf> [↑](#footnote-ref-779)
779. Based on the difference in installed cost for an efficient dryer ($716) and standard dryer ($564). <http://www.aceee.org/files/proceedings/2012/data/papers/0193-000286.pdf> [↑](#footnote-ref-780)
780. Based on coincidence factor of 3.8% for clothes washers [↑](#footnote-ref-781)
781. Based on ENERGY STAR test procedures. <https://www.energystar.gov/index.cfm?c=clothesdry.pr_crit_clothes_dryers> [↑](#footnote-ref-782)
782. ENERGY STAR Draft 2 Version 1.0 Clothes Dryers Data and Analysis [↑](#footnote-ref-783)
783. Federal standards report CEF for gas clothes dryers in terms of lbs/kWh. To determine gas savings, this number is later converted to therms. [↑](#footnote-ref-784)
784. ENERGY STAR Clothes Dryers Key Product Criteria. <https://www.energystar.gov/index.cfm?c=clothesdry.pr_crit_clothes_dryers> [↑](#footnote-ref-785)
785. Appendix D to Subpart B of Part 430 – Uniform Test Method for Measuring the Energy Consumption of Dryers. [↑](#footnote-ref-786)
786. %Electric accounts for the fact that some of the savings on gas dryers comes from electricity (motors, controls, etc). 16% was determined using a ratio of the electric to total savings from gas dryers given by ENERGY STAR Draft 2 Version 1.0 Clothes Dryers Data and Analysis. [↑](#footnote-ref-787)
787. ENERGY STAR qualified dryers have a maximum test cycle time of 80 minutes. Assume one hour per dryer cycle. [↑](#footnote-ref-788)
788. Based on coincidence factor of 3.8% for clothes washers. [↑](#footnote-ref-789)
789. %Gas accounts for the fact that some of the savings on gas dryers comes from electricity (motors, controls, etc). 84% was determined using a ratio of the gas to total savings from gas dryers given by ENERGY STAR Draft 2 Version 1.0 Clothes Dryers Data and Analysis. [↑](#footnote-ref-790)
790. David Rogers, Power Smart Engineering, October 2008; “Smart Strip electrical savings and usability”, p22. [↑](#footnote-ref-791)
791. Price survey performed in NYSERDA Measure Characterization for Advanced Power Strips, p4 [↑](#footnote-ref-792)
792. Efficiency Vermont coincidence factor for smart strip measure –in the absence of empirical evaluation data, this was based on assumptions of the typical run pattern for televisions and computers in homes. [↑](#footnote-ref-793)
793. NYSERDA Measure Characterization for Advanced Power Strips. Study based on review of:

     Smart Strip Electrical Savings and Usability, Power Smart Engineering, October 27, 2008.

     Final Field Research Report, Ecos Consulting, October 31, 2006. Prepared for California Energy Commission’s PIER Program.

     Developing and Testing Low Power Mode Measurement Methods, Lawrence Berkeley National Laboratory (LBNL), September 2004. Prepared for California Energy Commission’s Public Interest Energy Research (PIER) Program.

     2005 Intrusive Residential Standby Survey Report, Energy Efficient Strategies, March, 2006.

     Smart Strip Portfolio of the Future, Navigant Consulting for San Diego G&E, March 31, 2009. [↑](#footnote-ref-794)
794. Ibid. [↑](#footnote-ref-795)
795. Average of hours for controlled TV and computer from; NYSERDA Measure Characterization for Advanced Power Strips [↑](#footnote-ref-796)
796. Efficiency Vermont coincidence factor for smart strip measure –in the absence of empirical evaluation data, this was based on assumptions of the typical run pattern for televisions and computers in homes. [↑](#footnote-ref-797)
797. Based upon research from “Home Energy Efficiency Rebate Program GPY2 Evaluation Report” which outlines early replacement rates for both primary and secondary central air cooling (CAC) and residential furnaces. This is used as a reasonable proxy for ASHP installations since ASHP specific data is not available. Report presented to Nicor Gas Company February 27, 2014, available at http://www.ilsag.info/evaluation-documents.html. [↑](#footnote-ref-798)
798. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007,

     <http://www.ctsavesenergy.org/files/Measure%20Life%20Report%202007.pdf> [↑](#footnote-ref-799)
799. Assumed to be one third of effective useful life [↑](#footnote-ref-800)
800. Based on costs derived from DEER 2008 Database Technology and Measure Cost Data ([www.deeresources.com](http://www.deeresources.com)). [↑](#footnote-ref-801)
801. Ibid. See ‘ASHP\_Revised DEER Measure Cost Summary.xls’ for calculation. [↑](#footnote-ref-802)
802. Ibid. [↑](#footnote-ref-803)
803. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-804)
804. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-805)
805. The two equations are provided to show how savings are determined during the initial phase of the measure (existing to efficient) and the remaining phase (new baseline to efficient). In practice, the screening tools used may either require a First Year savings (using the first equation) and then a “number of years to adjustment” and “savings adjustment” input which would be the (new base to efficient savings)/(existing to efficient savings). [↑](#footnote-ref-806)
806. Full load hours for Chicago, Moline and Rockford are provided in “Final Evaluation Report: Central Air Conditioning Efficiency Services (CACES), 2010, Navigant Consulting”, <http://ilsag.org/yahoo_site_admin/assets/docs/ComEd_PY2_CACES_Evaluation_Report_2010-10-18.299122020.pdf>, p.33. An average FLH/Cooling Degree Day (from NCDC) ratio was calculated for these locations and applied to the CDD of the other locations in order to estimate FLH. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-807)
807. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-808)
808. Average nameplate efficiencies of all Early Replacement qualifying equipment in Ameren PY3-PY4. [↑](#footnote-ref-809)
809. If there is no central cooling in place but the incentive encourages installation of a new ASHP with cooling, the added cooling load should be subtracted from any heating benefit. [↑](#footnote-ref-810)
810. Based on Minimum Federal Standard effective 1/1/2015;

     http://www.gpo.gov/fdsys/pkg/CFR-2012-title10-vol3/pdf/CFR-2012-title10-vol3-sec430-32.pdf. [↑](#footnote-ref-811)
811. Full load heating hours for heat pumps are provided for Rockford, Chicago and Springfield in the Energy Star Calculator. Estimates for the other locations were calculated based on the FLH to Heating Degree Day (from NCDC) ratio. VEIC consider Energy Star estimates to be high due to oversizing not being adequately addressed. Using average Illinois billing data (from <http://www.icc.illinois.gov/ags/consumereducation.aspx>) VEIC estimated the average gas heating load and used this to estimate the average home heating output (using 83% average gas heat efficiency). Dividing this by a typical 36,000 Btu/hr ASHP gives an estimate of average ASHP FLH\_heat of 1821 hours. We used the ratio of this value to the average of the locations using the Energy Star data (1994 hours) to scale down the Energy Star estimates. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-812)
812. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-813)
813. HSPF ratings for Heat Pumps account for the seasonal average efficiency of the units and are based on testing within zone 4 which encompasses most of Illinois. Furthermore, a recent Cadmus/Opinion Dynamics metering study, “Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)”, found no significant variance between metered performance and that presented in the TRM [↑](#footnote-ref-814)
814. This is estimated based on finding the average HSPF/SEER ratio from the AHRI directory data (using the least efficient models – SEER 12 and SEER 13) – 0.596, and applying to the average nameplate SEER rating of all Early Replacement qualifying equipment in Ameren PY3-PY4. This estimation methodology appears to provide a result within 10% of actual HSPF. [↑](#footnote-ref-815)
815. Electric resistance has a COP of 1.0 which equals 1/0.293 = 3.41 HSPF. [↑](#footnote-ref-816)
816. Based on Minimum Federal Standard effective 1/1/2015;

     http://www.gpo.gov/fdsys/pkg/CFR-2012-title10-vol3/pdf/CFR-2012-title10-vol3-sec430-32.pdf [↑](#footnote-ref-817)
817. The two equations are provided to show how savings are determined during the initial phase of the measure (existing to efficient) and the remaining phase (new baseline to efficient). In practice, the screening tools used may either require a First Year savings (using the first equation) and then a “number of years to adjustment” and “savings adjustment” input which would be the (new base to efficient savings)/(existing to efficient savings). [↑](#footnote-ref-818)
818. From Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder. [↑](#footnote-ref-819)
819. Average nameplate efficiencies of all Early Replacement qualifying equipment in Ameren PY3-PY4. [↑](#footnote-ref-820)
820. If there is no central cooling in place but the incentive encourages installation of a new ASHP with cooling, the added cooling load should be subtracted from any heating benefit. [↑](#footnote-ref-821)
821. The Federal Standard does not include an EER requirement, so it is approximated with this formula: (-0.02 \* SEER2) + (1.12 \* SEER) Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder. Note this is appropriate for single speed units only. [↑](#footnote-ref-822)
822. Based on Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder. Note this is appropriate for single speed units only. [↑](#footnote-ref-823)
823. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-824)
824. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-825)
825. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007.

     [http://www.ctsavesenergy.org/files/Measure%20Life%20Report%202007.pdf](http://mn.gov/commerce/energy/images/ElectricFoodService_v03.2.xls) [↑](#footnote-ref-826)
826. Consistent with DEER 2008 Database Technology and Measure Cost Data ([www.deeresources.com](http://www.ctsavesenergy.org/files/Measure%20Life%20Report%202007.pdf)). [↑](#footnote-ref-827)
827. Assumption based on data obtained from the 3E Plus heat loss calculation software provided by the NAIMA (North American Insulation Manufacturer Association) and derived from Table 15 and Table 16 of 2009 ASHRAE Fundamentals Handbook, Chapter 23 Insulation for Mechanical Systems, page 23.17. [↑](#footnote-ref-828)
828. Full load heating hours for heat pumps are provided for Rockford, Chicago and Springfield in the Energy Star Calculator. Estimates for the other locations were calculated based on the FLH to Heating Degree Day (from NCDC) ratio. VEIC consider Energy Star estimates to be high due to oversizing not being adequately addressed. Using average Illinois billing data (from <http://www.icc.illinois.gov/ags/consumereducation.aspx>) VEIC estimated the average gas heating load and used this to estimate the average home heating output (using 83% average gas heat efficiency). Dividing this by a typical 36,000 Btu/hr ASHP gives an estimate of average ASHP FLH\_heat of 1821 hours. We used the ratio of this value to the average of the locations using the Energy Star data (1994 hours) to scale down the Energy Star estimates. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-829)
829. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-830)
830. Assumes 160°F water temp for a boiler without reset control, 120°F for a boiler with reset control, and 50°F air temperature for pipes in unconditioned basements and the following average heating season outdoor temperatures as the air temperature in crawl spaces: Zone 1 – 33.1, Zone 2 – 34.4, Zone 3 – 37.7, Zone 4 – 40.0, Zone 5 – 39.8, Weighted Average – 35.3 (NCDC 1881-2010 Normals, average of monthly averages Nov – Apr for zones 1-3 and Nov-March for zones 4 and 5). [↑](#footnote-ref-831)
831. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-832)
832. Average efficiency of boiler units found in Ameren PY3-PY4 data. [↑](#footnote-ref-833)
833. Based upon research from “Home Energy Efficiency Rebate Program GPY2 Evaluation Report” which outlines early replacement rates for both primary and secondary central air cooling (CAC) and residential funaces. The unit (furnace or CAC unit) that initially caused the customer to contact a trade ally is defined as the “primary unit”. The furnace or CAC unit that was also replaced but did not initially prompt the customer to contact a trade ally is defined as the “secondary unit”. This evaluation used different criteria for early replacement due to the availability of data after the fact; cost of any repairs < $550 and age of unit < 20 years. Report presented to Nicor Gas Company February 27, 2014, available at http://www.ilsag.info/evaluation-documents.html. [↑](#footnote-ref-834)
834. Baseline SEER and EER should be updated when new minimum federal standards become effective. [↑](#footnote-ref-835)
835. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007.

     [http://www.ctsavesenergy.org/files/Measure%20Life%20Report%202007.pdf](http://www.energystar.gov/ia/products/appliances/refrig/NAECA_calculation.xls)

     The "lifespan" of a central air conditioner is about 15 to 20 years (US DOE: [http://www.energysavers.gov/your\_home/space\_heating\_cooling/index.cfm/mytopic=12440](http://www.energystar.gov/ia/business/bulk_purchasing/bpsavings_calc/CalculatorRoomAirCleaner.xls)). [↑](#footnote-ref-836)
836. Assumed to be one third of effective useful life [↑](#footnote-ref-837)
837. DEER 2008 Database Technology and Measure Cost Data (www.deeresources.com) [↑](#footnote-ref-838)
838. Based on 3 ton initial cost estimate for an ENERGY STAR unit from ENERGY STAR Central AC calculator ([http://www.energystar.gov/ia/business/bulk\_purchasing/bpsavings\_calc/Calc\_CAC.xls](http://www.energystar.gov/ia/partners/prod_development/revisions/downloads/dehumid/ES_Dehumidifiers_Final_V3.0_Eligibility_Criteria.pdf)). [↑](#footnote-ref-839)
839. Based on 3 ton initial cost estimate for a conventional unit from ENERGY STAR Central AC calculator ([http://www.energystar.gov/ia/business/bulk\_purchasing/bpsavings\_calc/Calc\_CAC.xls](http://www1.eere.energy.gov/buildings/appliance_standards/residential/residential_cac_hp.html)). While baselines are likely to shift in the future, there is currently no good indication of what the cost of a new baseline unit will be in 6 years. In the absence of this information, assuming a constant federal baseline cost is within the range of error for this prescriptive measure. [↑](#footnote-ref-840)
840. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-841)
841. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-842)
842. The two equations are provided to show how savings are determined during the initial phase of the measure (existing to efficient) and the remaining phase (new baseline to efficient). In practice, the screening tools used may either require a First Year savings (using the first equation) and then a “number of years to adjustment” and “savings adjustment” input which would be the (new base to efficient savings)/(existing to efficient savings). [↑](#footnote-ref-843)
843. Full load hours for Chicago, Moline and Rockford are provided in “Final Evaluation Report: Central Air Conditioning Efficiency Services (CACES), 2010, Navigant Consulting”, [http://ilsag.org/yahoo\_site\_admin/assets/docs/ComEd\_PY2\_CACES\_Evaluation\_Report\_2010-10-18.299122020.pdf](http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117_RLW_CF%20Res%20RAC.pdf), p.33. An average FLH/Cooling Degree Day (from NCDC) ratio was calculated for these locations and applied to the CDD of the other locations in order to estimate FLH. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-844)
844. Weighted based on number of residential occupied housing units in each zone. [↑](#footnote-ref-845)
845. Actual unit size required for multi-family building, no size assumption provided because the unit size and resulting savings can vary greatly depending on the number of units. [↑](#footnote-ref-846)
846. Based on Minimum Federal Standard; [http://www1.eere.energy.gov/buildings/appliance\_standards/residential/residential\_cac\_hp.html](http://www.ilga.gov/legislation/ilcs/ilcs5.asp). [↑](#footnote-ref-847)
847. VEIC estimate based on Department of Energy Federal Standard between 1992 and 2006. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used. [↑](#footnote-ref-848)
848. The two equations are provided to show how savings are determined during the initial phase of the measure (existing to efficient) and the remaining phase (new baseline to efficient). In practice, the screening tools used may either require a First Year savings (using the first equation) and then a “number of years to adjustment” and “savings adjustment” input which would be the (new base to efficient savings)/(existing to efficient savings). [↑](#footnote-ref-849)
849. The federal Standard does not currently include an EER component. The value is approximated based on the SEER standard (13) and equals EER 11.2. To perform this calculation we are using this formula: (-0.02 \* SEER2) + (1.12 \* SEER) (from Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder). [↑](#footnote-ref-850)
850. Based on SEER of 10,0, using formula above to give 9.2 EER. [↑](#footnote-ref-851)
851. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-852)
852. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-853)
853. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007.

     [http://neep.org/uploads/EMV%20Forum/EMV%20Studies/measure\_life\_GDS%5B1%5D.pdf](http://www.eia.gov/consumption/residential/data/2009/) [↑](#footnote-ref-854)
854. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-855)
855. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-856)
856. 25 Pascals is the standard assumption for typical pressures experienced in the duct system under normal operating conditions. To convert CFM50 to CFM25 you multiply by 0.64 (inverse of the “Can’t Reach Fifty” factor for CFM25; see Energy Conservatory Blower Door Manual). [↑](#footnote-ref-857)
857. Assumes that for each percent of supply air loss there is one percent annual energy penalty. This assumes supply side leaks are direct losses to the outside and are not recaptured back to the house. This could be adjusted downward to reflect regain of usable energy to the house from duct leaks. For example, during the winter some of the energy lost from supply leaks in a crawlspace will probably be regained back to the house (sometimes 1/2 or more may be regained). More information provided in “Appendix E Estimating HVAC System Loss From Duct Airtightness Measurements” from <http://www.energyconservatory.com/download/dbmanual.pdf> [↑](#footnote-ref-858)
858. Assumes 50% of leaks are in supply ducts. [↑](#footnote-ref-859)
859. Assumes that for each percent of return air loss there is a half percent annual energy penalty. Note that this assumes that return leaks contribute less to energy losses than do supply leaks. This value could be adjusted upward if there was reason to suspect that the return leaks contribute significantly more energy loss than “average” (e.g. pulling return air from a super heated attic), or can be adjusted downward to represent significantly less energy loss (e.g. pulling return air from a moderate temperature crawl space) . More information provided in “Appendix E Estimating HVAC System Loss From Duct Airtightness Measurements” from [http://www.energyconservatory.com/download/dbmanual.pdf](http://www.energysavers.gov/your_home/space_heating_cooling/index.cfm/mytopic=12440) [↑](#footnote-ref-860)
860. Assumes 50% of leaks are in return ducts. [↑](#footnote-ref-861)
861. This conversion is an industry rule of thumb; e.g. see http://www.hvacsalesandsupply.com/Linked%20Documents/Tech%20Tips/61-Why%20400%20CFM%20per%20ton.pdf [↑](#footnote-ref-862)
862. Based on Full Load Hours from ENERGY Star with adjustments made in a Navigant Evaluation, other cities were scaled using those results and CDD. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-863)
863. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-864)
864. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Central AC was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-865)
865. Fe is not one of the AHRI certified ratings provided for residential furnaces, but can be reasonably estimated from a calculation based on the certified values for fuel energy (Ef in MMBtu/yr) and Eae (kWh/yr). An average of a 300 record sample (non-random) out of 1495 was 3.14%. This is, appropriately, ~50% greater than the Energy Star version 3 criteria for 2% Fe. See “Programmable Thermostats Furnace Fan Analysis.xlsx” for reference. [↑](#footnote-ref-866)
866. Heating EFLH based on ENERGY Star EFLH for Rockford, Chicago, and Springfield and on NCDC/NOAA HDD for the other two cities. In all cases, the hours were adjusted based on average natural gas heating consumption in IL. [↑](#footnote-ref-867)
867. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-868)
868. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Heat Pumps was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-869)
869. Based on Full Load Hours from ENERGY Star with adjustments made in a Navigant Evaluation, other cities were scaled using those results and CDD. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-870)
870. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-871)
871. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Central AC was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-872)
872. Heating EFLH based on ENERGY Star EFLH for Rockford, Chicago, and Springfield and on NCDC/NOAA HDD for the other two cities. In all cases, the hours were adjusted based on average natural gas heating consumption in IL. [↑](#footnote-ref-873)
873. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-874)
874. Note that the HSPF of a heat pump is equal to the COP \* 3.413. [↑](#footnote-ref-875)
875. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Heat Pumps was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-876)
876. Based on Full Load Hours from ENERGY Star with adjustments made in a Navigant Evaluation, other cities were scaled using those results and CDD. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-877)
877. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-878)
878. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-879)
879. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-880)
880. Based on Natural Draft Furnaces requiring 100 CFM per 10,000 Btu, Induced Draft Furnaces requiring 130CFM per 10,000Btu and Condensing Furnaces requiring 150 CFM per 10,000 Btu (rule of thumb from [http://contractingbusiness.com/enewsletters/cb\_imp\_43580/](http://ilsag.org/yahoo_site_admin/assets/docs/ComEd_PY2_CACES_Evaluation_Report_2010-10-18.299122020.pdf)). Data provided by GAMA during the federal rule-making process for furnace efficiency standards, suggested that in 2000, 24% of furnaces purchased in Illinois were condensing units. Therefore a weighted average required airflow rate is calculated assuming a 50:50 split of natural v induced draft non-condensing furnaces, as 123 per 10,000Btu or 0.0123/Btu. [↑](#footnote-ref-881)
881. Heating EFLH based on ENERGY Star EFLH for Rockford, Chicago, and Springfield and on NCDC/NOAA HDD for the other two cities. In all cases, the hours were adjusted based on average natural gas heating consumption in IL. [↑](#footnote-ref-882)
882. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-883)
883. The Equipment Efficiency can be obtained either by recording the AFUE of the unit, or performing a steady state efficiency test.

     If there are more than one heating systems, the weighted (by consumption) average efficiency should be used.

     If the heating system or distribution is being upgraded within a package of measures together with the insulation upgrade, the new average heating system efficiency should be used. [↑](#footnote-ref-884)
884. This has been estimated assuming that natural gas central furnace heating is typical for Illinois residences (66% of Illinois homes have a Natural Gas Furnace (based on Energy Information Administration, 2009 Residential Energy Consumption Survey: [http://www.eia.gov/consumption/residential/data/2009/xls/HC6.9%20Space%20Heating%20in%20Midwest%20Region.xls](http://www.ctsavesenergy.org/files/Measure%20Life%20Report%202007.pdf)))

     In 2000, 24% of furnaces purchased in Illinois were condensing (based on data from GAMA, provided to Department of Energy during the federal standard setting process for residential heating equipment - see Furnace Penetration.xls). Furnaces tend to last up to 20 years and so units purchased 10 years ago provide a reasonable proxy for the current mix of furnaces in the State. Assuming typical efficiencies for condensing and non-condensing furnaces and duct losses, the average heating system efficiency is estimated as follows:

     (0.24\*0.92) + (0.76\*0.8) = 0.829 [↑](#footnote-ref-885)
885. The Distribution Efficiency can be estimated via a visual inspection and by referring to a look up table such as that provided by the Building Performance Institute: ([http://www.bpi.org/files/pdf/DistributionEfficiencyTable-BlueSheet.pdf](http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117_RLW_CF%20Res%20RAC.pdf)) or by performing duct blaster testing. [↑](#footnote-ref-886)
886. Estimated as follows: 0.829 \* (1-0.15) = 0.70 [↑](#footnote-ref-887)
887. Consistent with assumed life of a new gas furnace. Table 8.3.3 The Technical support documents for federal residential appliance standards: [http://www1.eere.energy.gov/buildings/appliance\_standards/residential/pdfs/fb\_fr\_tsd/chapter\_8.pdf](http://www.energystar.gov/ia/business/bulk_purchasing/bpsavings_calc/CalculatorConsumerDishwasher.xls) [↑](#footnote-ref-888)
888. Adapted from Tables 8.2.3 and 8.2.13 in [http://www1.eere.energy.gov/buildings/appliance\_standards/residential/pdfs/hvac\_ch\_08\_lcc\_2011-06-24.pdf](http://mn.gov/commerce/energy/images/ElectricFoodService_v03.2.xls) [↑](#footnote-ref-889)
889. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-890)
890. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-891)
891. To estimate heating, cooling and shoulder season savings for Illinois, VEIC adapted results from a 2009 Focus on Energy study of BPM blower motor savings in Wisconsin. This study included effects of behavior change based on the efficiency of new motor greatly increasing the amount of people that run the fan continuously. The savings from the Wisconsin study were adjusted to account for different run hour assumptions (average values used) for Illinois. See: FOE to IL Blower Savings.xlsx. [↑](#footnote-ref-892)
892. The weighted average value is based on assumption that 75% of homes installing BPM furnace blower motors have Central AC. 66% of IL housing units have CAC and 66% have gas furnaces. It is logical these two groups overlap to a large extent (like the 95% in the FOE study above). [↑](#footnote-ref-893)
893. Full load hours for Chicago, Moline and Rockford are provided in “Final Evaluation Report: Central Air Conditioning Efficiency Services (CACES), 2010, Navigant Consulting”, [http://ilsag.org/yahoo\_site\_admin/assets/docs/ComEd\_PY2\_CACES\_Evaluation\_Report\_2010-10-18.299122020.pdf](http://www.ctsavesenergy.org/files/Measure%20Life%20Report%202007.pdf), p.33. An average FLH/Cooling Degree Day (from NCDC) ratio was calculated for these locations and applied to the CDD of the other locations in order to estimate FLH. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-894)
894. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-895)
895. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-896)
896. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-897)
897. The blower fan is in the heating duct so all, or very nearly all, of its waste heat is delivered to the conditioned space. [↑](#footnote-ref-898)
898. Negative value since this measure will increase the heating load due to reduced waste heat. [↑](#footnote-ref-899)
899. Based upon research from “Home Energy Efficiency Rebate Program GPY2 Evaluation Report” which outlines early replacement rates for both primary and secondary central air cooling (CAC) and residential furnaces. This is used as a reasonable proxy for boiler installations since boiler specific data is not available. Report presented to Nicor Gas Company February 27, 2014, available at http://www.ilsag.info/evaluation-documents.html. [↑](#footnote-ref-900)
900. There will be some delay to the baseline shift while existing stocks of lower efficiency equipment is sold. [↑](#footnote-ref-901)
901. Table 8.3.3 The Technical support documents for federal residential appliance standards: <http://www1.eere.energy.gov/buildings/appliance_standards/residential/pdfs/fb_fr_tsd/chapter_8.pdf> [↑](#footnote-ref-902)
902. Assumed to be one third of effective useful life [↑](#footnote-ref-903)
903. Based on data provided in Appendix E of the Appliance Standards Technical Support Documents including equipment cost and installation labor (<http://www1.eere.energy.gov/buildings/appliance_standards/residential/pdfs/fb_fr_tsd/appendix_e.pdf>). Where efficiency ratings are not provided, the values are interpolated from those that are. [↑](#footnote-ref-904)
904. The two equations are provided to show how savings are determined during the initial phase of the measure (existing to efficient) and the remaining phase (new baseline to efficient). In practice, the screening tools used may either require a First Year savings (using the first equation) and then a “number of years to adjustment” and “savings adjustment” input which would be the (new base to efficient savings)/(existing to efficient savings). [↑](#footnote-ref-905)
905. Boiler consumption values are informed by an evaluation which did not identify any fraction of heating load due to domestic hot water (DHW) provided by the boiler. Thus these values are an average of both homes with boilers only providing heat, and homes with boilers that also provide DHW. Heating load is used to describe the household heating need, which is equal to (gas heating consumption \* AFUE ) [↑](#footnote-ref-906)
906. Values are based on household heating consumption values and inferred average AFUE results from Table 3-4, Program Sample Analysis, *Nicor R29 Res Rebate Evaluation Report 092611\_REV FINAL to Nicor*). Adjusting to a statewide average using relative HDD values to adjust for the evaluation results focus on northern region. Values for individual cities are then calculated by comparing average HDD to the individual city’s HDD. [↑](#footnote-ref-907)
907. The Air Conditioning Contractors of America Manual J, Residential Load Calculation 8th Edition produces equipment sizing loads for Single Family, Multi-single, and Condominiums using input characteristics of the home. A best practice for equipment selection and installation of Heating and Air Conditioning, load calculations should be completed by contractors during the selection process and may be readily available for program data purposes. [↑](#footnote-ref-908)
908. Average nameplate efficiencies of all Early Replacement qualifying equipment in Ameren PY3-PY4. [↑](#footnote-ref-909)
909. Default values per tier selected based upon the average AFUE value for the tier range except for the top tier where the minimum is used due to proximity to the maximum possible. [↑](#footnote-ref-910)
910. Based upon research from “Home Energy Efficiency Rebate Program GPY2 Evaluation Report” which outlines early replacement rates for both primary and secondary central air cooling (CAC) and residential funaces. The unit (furnace or CAC unit) that initially caused the customer to contact a trade ally is defined as the “primary unit”. The furnace or CAC unit that was also replaced but did not initially prompt the customer to contact a trade ally is defined as the “secondary unit”. This evaluation used different criteria for early replacement due to the availability of data after the fact; cost of any repairs < $550 and age of unit < 20 years. Report presented to Nicor Gas Company February 27, 2014, available at http://www.ilsag.info/evaluation-documents.html. [↑](#footnote-ref-911)
911. Table 8.3.3 The Technical support documents for federal residential appliance standards: <http://www1.eere.energy.gov/buildings/appliance_standards/residential/pdfs/fb_fr_tsd/chapter_8.pdf> [↑](#footnote-ref-912)
912. Assumed to be one third of effective useful life [↑](#footnote-ref-913)
913. Based on data from Table E.1.1 of Appendix E of the Appliance Standards Technical Support Documents including equipment cost and installation labor.(<http://www1.eere.energy.gov/buildings/appliance_standards/residential/pdfs/fb_fr_tsd/appendix_e.pdf>). Where efficiency ratings are not provided, the values are interpolated from those that are. Note that ECM furnace fan cost (refer to other measure in TRM) has been deducted from the 93%-96% AFUE values to avoid double counting. [↑](#footnote-ref-914)
914. The two equations are provided to show how savings are determined during the initial phase of the measure (existing to efficient) and the remaining phase (new baseline to efficient). In practice, the screening tools used may either require a First Year savings (using the first equation) and then a “number of years to adjustment” and “savings adjustment” input which would be the (new base to efficient savings)/(existing to efficient savings). [↑](#footnote-ref-915)
915. Heating load is used to describe the household heating need, which is equal to (gas consumption \* AFUE ) [↑](#footnote-ref-916)
916. Values are based on household heating consumption values and inferred average AFUE results from Table 2-1, *Energy Efficiency / Demand Response Nicor Gas Plan Year 1 (6/1/2011-5/31/2012) Research Report: Furnace Metering Study* (August 1, 2013) (prepared by Navigant Consulting, Inc.) and adjusting to a statewide average using relative HDD values to adjust for the evaluation results focus on northern region. Values for individual cities are then calculated by comparing average HDD to the individual city’s HDD. [↑](#footnote-ref-917)
917. The Air Conditioning Contractors of America Manual J, Residential Load Calculation 8th Edition produces equipment sizing loads for Single Family, Multi-single, and Condominiums using input characteristics of the home. A best practice for equipment selection and installation of Heating and Air Conditioning, load calculations are commonly completed by contractors during the selection process and may be readily available for program data purposes. [↑](#footnote-ref-918)
918. Multifamily household heating consumption relative to single-family households is affected by overall household square footage and exposure to the exterior. This 65% reduction factor is applied to MF homes with electric resistance, based on professional judgment that average household size, and heat loads of MF households are smaller than single-family homes [↑](#footnote-ref-919)
919. Program-specific household factors may be utilized on the basis of sufficiently validated program evaluations. [↑](#footnote-ref-920)
920. Average nameplate efficiencies of all Early Replacement qualifying equipment in Ameren PY3-PY4. [↑](#footnote-ref-921)
921. Though the Federal Minimum AFUE is 78%, there were only 50 models listed in the AHRI database at that level. At AFUE 79% the total rises to 308. There are 3,548 active furnace models listed with AFUE ratings between 78 and 80. [↑](#footnote-ref-922)
922. Minimum ENERGY STAR efficiency after 2.1.2012. [↑](#footnote-ref-923)
923. The Federal Standard does not include an EER requirement, so it is approximated with this formula: (-0.02 \* SEER2) + (1.12 \* SEER) Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder. [↑](#footnote-ref-924)
924. Minimum Federal Standard as of 4/1/2015;

     http://www.gpo.gov/fdsys/pkg/CFR-2012-title10-vol3/pdf/CFR-2012-title10-vol3-sec430-32.pdf [↑](#footnote-ref-925)
925. System life of indoor components as per DOE estimate http://energy.gov/energysaver/articles/geothermal-heat-pumps. The ground loop has a much longer life, but the compressor and other mechanical components are the same as an ASHP.

     <http://neep.org/uploads/EMV%20Forum/EMV%20Studies/measure_life_GDS%5B1%5D.pdf> [↑](#footnote-ref-926)
926. Assumed to be one third of effective useful life [↑](#footnote-ref-927)
927. Based on data provided in ‘Results of HomE geothermal and air source heat pump rebate incentives documented by IL electric cooperatives’. [↑](#footnote-ref-928)
928. Based on data provided on Home Advisor website, providing national average ASHP cost based on 2465 cost submittals. <http://www.homeadvisor.com/cost/heating-and-cooling/install-a-heat-pump/> [↑](#footnote-ref-929)
929. Furnace and boiler costs are based on data provided in Appendix E of the Appliance Standards Technical Support Documents including equipment cost and installation labor (<http://www1.eere.energy.gov/buildings/appliance_standards/residential/pdfs/fb_fr_tsd/appendix_e.pdf>). Where efficiency ratings are not provided, the values are interpolated from those that are. [↑](#footnote-ref-930)
930. Based on 3 ton initial cost estimate for a conventional unit from ENERGY STAR Central AC calculator ([http://www.energystar.gov/ia/business/bulk\_purchasing/bpsavings\_calc/Calc\_CAC.xls](http://www1.eere.energy.gov/buildings/appliance_standards/residential/residential_cac_hp.html)). While baselines are likely to shift in the future, there is currently no good indication of what the cost of a new baseline unit will be in 6 years. In the absence of this information, assuming a constant federal baseline cost is within the range of error for this prescriptive measure. [↑](#footnote-ref-931)
931. Based on data from Table E.1.1 of Appendix E of the Appliance Standards Technical Support Documents including equipment cost and installation labor.(<http://www1.eere.energy.gov/buildings/appliance_standards/residential/pdfs/fb_fr_tsd/appendix_e.pdf>). [↑](#footnote-ref-932)
932. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-933)
933. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-934)
934. The two equations are provided to show how savings are determined during the initial phase of the measure (existing to efficient) and the remaining phase (new baseline to efficient). In practice, the screening tools used may either require a First Year savings (using the first equation) and then a “number of years to adjustment” and “savings adjustment” input which would be the (new base to efficient savings)/(existing to efficient savings). [↑](#footnote-ref-935)
935. Based on Full Load Hours from ENERGY Star with adjustments made in a Navigant Evaluation, other cities were scaled using those results and CDD. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-936)
936. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-937)
937. Minimum Federal Standard as of 1/1/2015;

     http://www.gpo.gov/fdsys/pkg/CFR-2012-title10-vol3/pdf/CFR-2012-title10-vol3-sec430-32.pdf [↑](#footnote-ref-938)
938. Minimum Federal Standard; Federal Register, Vol. 66, No. 14, Monday, January 22, 2001/Rules and Regulations, p. 7170-7200. [↑](#footnote-ref-939)
939. Assumes that the decision to replace existing systems includes desire to add cooling. [↑](#footnote-ref-940)
940. Average nameplate efficiencies of all Early Replacement qualifying equipment in Ameren PY3-PY4. [↑](#footnote-ref-941)
941. Ibid. [↑](#footnote-ref-942)
942. Assumes that the decision to replace existing systems includes desire to add cooling. [↑](#footnote-ref-943)
943. Minimum Federal Standard as of 1/1/2015;

     http://www.gpo.gov/fdsys/pkg/CFR-2012-title10-vol3/pdf/CFR-2012-title10-vol3-sec430-32.pdf [↑](#footnote-ref-944)
944. As per conversations with David Buss territory manager for Connor Co, the SEER and COP ratings of an ASHP equate most appropriately with the part load EER and COP of a GSHP. [↑](#footnote-ref-945)
945. Heating EFLH based on ENERGY Star EFLH for Rockford, Chicago, and Springfield and on NCDC/NOAA HDD for the other two cities. In all cases, the hours were adjusted based on average natural gas heating consumption in IL. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-946)
946. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-947)
947. Electric resistance has a COP of 1.0 which equals 1/0.293 = 3.41 HSPF. [↑](#footnote-ref-948)
948. Minimum Federal Standard as of 1/1/2015;

     http://www.gpo.gov/fdsys/pkg/CFR-2012-title10-vol3/pdf/CFR-2012-title10-vol3-sec430-32.pdf [↑](#footnote-ref-949)
949. As per conversations with David Buss territory manager for Connor Co, the SEER and COP ratings of an ASHP equate most appropriately with the part load EER and COP of a GSHP. [↑](#footnote-ref-950)
950. Assumes that the desuperheater can provide two thirds of hot water needs for eight months of the year (2/3 \* 2/3 = 44%). Based on input from Doug Dougherty, Geothermal Exchange Organization. [↑](#footnote-ref-951)
951. Minimum Federal Standard as of 4/1/2015;

     http://www.gpo.gov/fdsys/pkg/CFR-2012-title10-vol3/pdf/CFR-2012-title10-vol3-sec430-32.pdf [↑](#footnote-ref-952)
952. [Maureen](http://portal.veic.org/projects/illinoistrm/Lists/TRM%20Request%20Tracker/Attachments/287/%20Maureen) Hodgins, email message to TAC/SAG, August 26, 2014 [↑](#footnote-ref-953)
953. ComEd Energy Efficiency/ Demand Response Plan: Plan Year 2 (6/1/2009-5/31/2010) Evaluation Report: All Electric Single Family Home Energy Performance Tune-Up Program citing 2006-2008 American Community Survey data from the US Census Bureau for Illinois cited on p. 17 of the PY2 Evaluation report. 2.75 \* 93% evaluation adjustment [↑](#footnote-ref-954)
954. Bedrooms are suitable proxies for household occupancy, and may be preferable to actual occupancy due to turnover rates in residency and non-adult population impacts. [↑](#footnote-ref-955)
955. US DOE Building America Program. Building America Analysis Spreadsheet. For Chicago, IL [http://www1.eere.energy.gov/buildings/building\_america/analysis\_spreadsheets.html](http://www.energystar.gov/ia/products/appliances/refrig/NAECA_calculation.xls) [↑](#footnote-ref-956)
956. The Federal Standard does not include an EER requirement, so it is approximated with the conversion formula from Wassmer, M. 2003 thesis refererenced below. [↑](#footnote-ref-957)
957. Minimum Federal Standard; Federal Register, Vol. 66, No. 14, Monday, January 22, 2001/Rules and Regulations, p. 7170-7200. [↑](#footnote-ref-958)
958. Assumes that the decision to replace existing systems includes desire to add cooling. [↑](#footnote-ref-959)
959. From Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder. [↑](#footnote-ref-960)
960. Average nameplate efficiencies of all Early Replacement qualifying equipment in Ameren PY3-PY4. [↑](#footnote-ref-961)
961. Ibid. [↑](#footnote-ref-962)
962. Assumes that the decision to replace existing systems includes desire to add cooling. [↑](#footnote-ref-963)
963. As per conversations with David Buss territory manager for Connor Co, the EER rating of an ASHP equate most appropriately with the full load EER of a GSHP. [↑](#footnote-ref-964)
964. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-965)
965. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-966)
966. Heating load is used to describe the household heating need, which is equal to (gas consumption \* AFUE ) [↑](#footnote-ref-967)
967. The Air Conditioning Contractors of America Manual J, Residential Load Calculation 8th Edition produces equipment sizing loads for Single Family, Multi-single, and Condominiums using input characteristics of the home. A best practice for equipment selection and installation of Heating and Air Conditioning, load calculations are commonly completed by contractors during the selection process and may be readily available for program data purposes. [↑](#footnote-ref-968)
968. Values are based on household heating consumption values and inferred average AFUE results from Table 2-1, *Energy Efficiency / Demand Response Nicor Gas Plan Year 1 (6/1/2011-5/31/2012) Research Report: Furnace Metering Study* (August 1, 2013) (prepared by Navigant Consulting, Inc.) and adjusting to a statewide average using relative HDD values to adjust for the evaluation results focus on northern region. Values for individual cities are then calculated by comparing average HDD to the individual city’s HDD. [↑](#footnote-ref-969)
969. Boiler consumption values are informed by an evaluation which did not identify any fraction of heating load due to domestic hot water (DHW) provided by the boiler. Thus these values are an average of both homes with boilers only providing heat, and homes with boilers that also provide DHW. Values are based on household heating consumption values and inferred average AFUE results from Table 3-4, Program Sample Analysis, *Nicor R29 Res Rebate Evaluation Report 092611\_REV FINAL to Nicor*). Adjusting to a statewide average using relative HDD values to adjust for the evaluation results focus on northern region. Values for individual cities are then calculated by comparing average HDD to the individual city’s HDD. [↑](#footnote-ref-970)
970. Average nameplate efficiencies of all Early Replacement qualifying equipment in Ameren PY3-PY4. [↑](#footnote-ref-971)
971. Assumes that Federal Standard will have been increased to 90% by the time the existing unit would have to have been replaced. [↑](#footnote-ref-972)
972. The values provided are based on the average fossil heat rate for the EPA eGRID subregion multiplied by a factor (5.82%) that takes into account T&D losses. These values were provided by Stefano Galiasso, University of Illinois, Chicago. [↑](#footnote-ref-973)
973. Minimum Federal Standard as of 4/1/2015;

     http://www.gpo.gov/fdsys/pkg/CFR-2012-title10-vol3/pdf/CFR-2012-title10-vol3-sec430-32.pdf [↑](#footnote-ref-974)
974. Note AFUEbase in the algorithm should be replaced with AFUEexist for early replacement measures. [↑](#footnote-ref-975)
975. Note SEERbase in the algorithm should be replaced with SEERexist for early replacement measures. [↑](#footnote-ref-976)
976. VEIC analysis looking at average efficient fan (i.e. Brushless Permanent Magnet) efficacies at static pressures of 0.1 and 0.25 inches of water column for quiet fans rated for 50 CFM. [↑](#footnote-ref-977)
977. Bi-level controls may be used by efficient fans larger than 50 CFM [↑](#footnote-ref-978)
978. VEIC analysis looking at average baseline fan (i.e. non-Brushless Permanent Magnet) efficacies at static pressures of 0.1 and 0.25 inches of water column for quiet fans rated for 50 CFM. [↑](#footnote-ref-979)
979. On/off cycling controls may be required of baseline fans larger than 50CFM. [↑](#footnote-ref-980)
980. Conservative estimate based upon GDS Associates Measure Life Report “Residential and C&I Lighting and HVAC measures” 25 years for whole-house fans, and 19 for thermostatically-controlled attic fans. [↑](#footnote-ref-981)
981. VEIC analysis using cost data collected from wholesale vendor; [http://www.westsidewholesale.com/](http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117_RLW_CF%20Res%20RAC.pdf) . [↑](#footnote-ref-982)
982. 50CFM is the closest available fan size to ASHRAE 62.2 Section 4.1 Whole House Ventilation rates based upon typical square footage and bedrooms. [↑](#footnote-ref-983)
983. VEIC analysis looking at average baseline fan (i.e. non-Brushless Permanent Magnet) efficacies at static pressures of 0.1 and 0.25 inches of water column for quiet fans rated for 50 CFM. [↑](#footnote-ref-984)
984. VEIC analysis looking at average efficient fan (i.e. Brushless Permanent Magnet) efficacies at static pressures of 0.1 and 0.25 inches of water column for quiet fans rated for 50 CFM. [↑](#footnote-ref-985)
985. Based on VEIC professional judgment. [↑](#footnote-ref-986)
986. Based on personal communication with HVAC efficiency program consultant Buck Taylor or Roltay Inc., 6/21/10, who estimated the cost of tune up at $125 to $225, depending on the market and the implementation details. [↑](#footnote-ref-987)
987. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-988)
988. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-989)
989. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-990)
990. Based on Full Load Hours from ENERGY Star with adjustments made in a Navigant Evaluation, other cities were scaled using those results and CDD. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-991)
991. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-992)
992. Use actual SEER rating where it is possible to measure or reasonably estimate. Unknown default of 10 SEER is a VEIC estimate of existing unit efficiency, based on minimum federal standard between the years of 1992 and 2006. [↑](#footnote-ref-993)
993. Energy Center of Wisconsin, May 2008; “Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research.” [↑](#footnote-ref-994)
994. Use actual SEER rating where it is possible to measure or reasonably estimate. Unknown default of 10 SEER is a VEIC estimate of existing unit efficiency, based on minimum federal standard between the years of 1992 and 2006. [↑](#footnote-ref-995)
995. Full load heating hours for heat pumps are provided for Rockford, Chicago and Springfield in the Energy Star Calculator. Estimates for the other locations were calculated based on the FLH to Heating Degree Day (from NCDC) ratio. VEIC consider Energy Star estimates to be high due to oversizing not being adequately addressed. Using average Illinois billing data (from [http://www.icc.illinois.gov/ags/consumereducation.aspx](http://www.ctsavesenergy.com/files/Final%202008%20Program%20Savings%20Document.pdf)) VEIC estimated the average gas heating load and used this to estimate the average home heating output (using 83% average gas heat efficiency). Dividing this by a typical 36,000 Btu/hr ASHP gives an estimate of average ASHP FLH\_heat of 1821 hours. We used the ratio of this value to the average of the locations using the Energy Star data (1994 hours) to scale down the Energy Star estimates. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-996)
996. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-997)
997. Use actual HSPF rating where it is possible to measure or reasonably estimate. Unknown default of 6.8 HSPF is a VEIC estimate based on minimum Federal Standard between 1992 and 2006. [↑](#footnote-ref-998)
998. Based on Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder. Note this is appropriate for single speed units only. [↑](#footnote-ref-999)
999. Based on June 2010 personal conversation with Scott Pigg, author of Energy Center of Wisconsin, May 2008; “Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research” suggesting the average WI unit system draw of 2.8kW under peak conditions, and average peak savings of 50W. [↑](#footnote-ref-1000)
1000. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-1001)
1001. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-1002)
1002. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-1003)
1003. The EnergyStar program discontinued its support for this measure category effective 12/31/09, and is presently developing a new specification for ‘Residential Climate Controls’.  [↑](#footnote-ref-1004)
1004. Table 1, HVAC Controls, Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, 2007 [↑](#footnote-ref-1005)
1005. Future evaluation is strongly encouraged to inform the persistence of savings to further refine measure life assumption. As this characterization depends heavily upon a large scale but only 2-year study of the energy impacts of programmable thermostats, the longer term impacts should be assessed. [↑](#footnote-ref-1006)
1006. Market prices vary significantly in this category, generally increasing with thermostat capability and sophistication. The basic functions required by this measure's eligibility criteria are available on units readily available in the market for the listed price. [↑](#footnote-ref-1007)
1007. Note the second part of the algorithm relates to furnace fan savings if the heating system is Natural Gas. [↑](#footnote-ref-1008)
1008. Average (default) value of 13% electric space heating from 2010 Residential Energy Consumption Survey for Illinois. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used. [↑](#footnote-ref-1009)
1009. Values in table are based on converting an average household heating load (834 therms) for Chicago based on ‘Table E-1, Energy Efficiency/Demand Response Nicor Gas Plan Year 1: Research Report: Furnace Metering Study, Draft, Navigant, August 1 2013 to an electric heat load (divide by 0.03413) to electric resistance and ASHP heat load (resistance load reduced by 15% to account for distribution losses that occur in furnace heating but not in electric resistance while ASHP heat is assumed to suffer from similar distribution losses) and then to electric consumption assuming efficiencies of 100% for resistance and 200% for HP (see ‘Household Heating Load Summary Calculations\_11062013.xls’). Finally these values were adjusted to a statewide average using relative HDD assumptions to adjust for the evaluation results focus on northern region. Values for individual cities are then calculated by comparing average HDD to the individual city’s HDD. [↑](#footnote-ref-1010)
1010. Assumption that 1/2 of electrically heated homes have electric resistance and 1/2 have Heat Pump, based on 2010 Residential Energy Consumption Survey for Illinois. [↑](#footnote-ref-1011)
1011. The savings from programmable thermostats are highly susceptible to many factors best addressed, so far for this category, by a study that controlled for the most significant issues with a very large sample size. To the extent that the treatment group is representative of the program participants for IL, this value is suitable. Higher and lower values would be justified based upon clear dissimilarities due to program and product attributes. Future evaluation work should assess program specific impacts associated with penetration rates, baseline levels, persistence, and other factors which this value represents. [↑](#footnote-ref-1012)
1012. Multifamily household heating consumption relative to single-family households is affected by overall household square footage and exposure to the exterior. This 65% reduction factor is applied to MF homes based on professional judgment that average household size, and heat loads of MF households are smaller than single-family homes [↑](#footnote-ref-1013)
1013. Program-specific household factors may be utilized on the basis of sufficiently validated program evaluations. [↑](#footnote-ref-1014)
1014. “Programmable Thermostats. Report to KeySpan Energy Delivery on Energy Savings and Cost Effectiveness,” GDS Associates, Marietta, GA. 2002GDS [↑](#footnote-ref-1015)
1015. Fe is not one of the AHRI certified ratings provided for residential furnaces, but can be reasonably estimated from a calculation based on the certified values for fuel energy (Ef in MMBtu/yr) and Eae (kWh/yr). An average of a 300 record sample (non-random) out of 1495 was 3.14%. This is, appropriately, ~50% greater than the Energy Star version 3 criteria for 2% Fe. See “Programmable Thermostats Furnace Fan Analysis.xlsx” for reference. [↑](#footnote-ref-1016)
1016. Average (default) value of 87% electric space heating from 2010 Residential Energy Consumption Survey for Illinois. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used. [↑](#footnote-ref-1017)
1017. Values are based on adjusting the average household heating load (834 therms) for Chicago based on ‘Table E-1, Energy Efficiency / Demand Response Nicor Gas Plan Year 1, Research Report: Furnace Metering Study’, divided by standard assumption of existing unit efficiency of 83% (estimate based on 24% of furnaces purchased in Illinois were condensing in 2000 (based on data from GAMA, provided to Department of Energy), assuming typical efficiencies: (0.24\*0.92) + (0.76\*0.8) = 0.83) to give 1005 therms. This Chicago value was then adjusted to a statewide average using relative HDD assumptions to adjust for the evaluation results focus on northern region. Values for individual cities are then calculated by comparing average HDD to the individual city’s HDD. [↑](#footnote-ref-1018)
1018. The whole purpose of installing ductless heat pumps is to conserve energy, so the installer can be assumed to be capable of recommending an appropriate controls strategy. For most applications, the heating setpoint for the ductless heat pump should be at least 2F higher than any remaining existing system and the cooling setpoint for the ductless heat pump should be at least 2F cooler than the existing system (this should apply to all periods of a programmable schedule, if applicable). This helps ensure that the ductless heat pump will be used to meet as much of the load as possible before the existing system operates to meet the remaining load. Ideally, the new ductless heat pump controls should be set to the current comfort settings, while the existing system setpoints should be adjusted down (heating) and up (cooling) to capture savings. [↑](#footnote-ref-1019)
1019. Minimum Federal Standard as of 1/1/2015;

      http://www.gpo.gov/fdsys/pkg/CFR-2012-title10-vol3/pdf/CFR-2012-title10-vol3-sec430-32.pdf [↑](#footnote-ref-1020)
1020. Additional heat pumps will achieve additional savings, but not as much as the first one. [↑](#footnote-ref-1021)
1021. Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, Inc., June 2007 [↑](#footnote-ref-1022)
1022. *Ductless Heat Pumps for Residential Customers in Connecticut*,  Swift, Joseph R and Rebecca A. Meyer, The Connecticut Light & Power Company, 2010 ACEEE Summer Study on Energy Efficiency in Buildings (2-292) [↑](#footnote-ref-1023)
1023. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-1024)
1024. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-1025)
1025. PLD values calculated in “DHP Savings Model 12-31-13.xls”. To verify that the proposed algorithm generates reasonable savings, we compared the results to metering studies done to measure ductless heat pump savings.

      Ecotope Study, prepared for Bonneville Power Administration, “Residential Ductless Mini-Split Heat Pump Retrofit Monitoring,” Monmouth, Oregon, June, 2009.

      Ecotope Study, Prepared for Bonneville Power Administration, “Ductless Heat Pump Retrofits in Multifamily and Small Commercial Buildings,” December, 2012.

      KEMA Study, Prepared for NSTAR Electric and Gas Corporation et al. “Ductless Mini Pilot Study,” Middletown, Connecticut, June, 2009 [↑](#footnote-ref-1026)
1026. Values in table are based on converting an average household heating load (834 therms) for Chicago based on ‘Table E-1, Energy Efficiency/Demand Response Nicor Gas Plan Year 1: Research Report: Furnace Metering Study, Draft, Navigant, August 1 2013 to an electric heat load (divide by 0.03413) to electric resistance and ASHP heat load (resistance load reduced by 15% to account for distribution losses that occur in furnace heating but not in electric resistance while ASHP heat is assumed to suffer from similar distribution losses) (see ‘Household Heating Load Summary Calculations\_11062013.xls’). Finally these values were adjusted to a statewide average using relative HDD assumptions to adjust for the evaluation results focus on northern region. Values for individual cities are then calculated by comparing average HDD to the individual city’s HDD. [↑](#footnote-ref-1027)
1027. Multifamily household heating consumption relative to single-family households is affected by overall household square footage and exposure to the exterior. This 65% reduction factor is applied to MF homes with electric resistance, based on professional judgment that average household size, and heat loads of MF households are smaller than single-family homes [↑](#footnote-ref-1028)
1028. Program-specific household factors may be utilized on the basis of sufficiently validated program evaluations. [↑](#footnote-ref-1029)
1029. 1 Ton = 12 kBtu/hr [↑](#footnote-ref-1030)
1030. Electric resistance has a COP of 1.0 which equals 1/0.293 = 3.41 HSPF. [↑](#footnote-ref-1031)
1031. This is from the ASHP measure which estimated HSPF based on finding the average HSPF/SEER ratio from the AHRI directory data (using the least efficient models – SEER 12 and SEER 13) – 0.596, and applying to the average nameplate SEER rating of all Early Replacement qualifying equipment in Ameren PY3-PY4. This estimation methodology appears to provide a result within 10% of actual HSPF. [↑](#footnote-ref-1032)
1032. Note that if only an EER rating is available, a conversion factor of SEER=1.1\*EER can be used [↑](#footnote-ref-1033)
1033. Converted from EER using formula EER = 1.1 SEER [↑](#footnote-ref-1034)
1034. Residential EFLH for room AC [↑](#footnote-ref-1035)
1035. Weighted based on number of residential occupied housing units in each zone. [↑](#footnote-ref-1036)
1036. Same EER as PTAC recycling. Estimated using the IECC building energy code up until year 2003 (p107; https://law.resource.org/pub/us/code/ibr/icc.iecc.2000.pdf) and assuming a 1 ton unit; EER = 10 – (0.16 \* 12,000/1,000) = 8.1. [↑](#footnote-ref-1037)
1037. Same method to calculate EER as PTAC recycling. Estimated using the IECC building energy code up until year 2003 (p107; https://law.resource.org/pub/us/code/ibr/icc.iecc.2000.pdf) and assuming a 1 ton unit; EER = 10 – (0.16 \* 12,000/1,000) = 8.1. [↑](#footnote-ref-1038)
1038. The quoted efficiency rating in the IECC was given in EER and was translated to SEER using a conversion factor of SEER=1.1\*EER. [↑](#footnote-ref-1039)
1039. Ibid. [↑](#footnote-ref-1040)
1040. Same EER as Window AC recycling. Based on Nexus Market Research Inc, RLW Analytics, December 2005; “Impact, Process, and Market Study of the Connecticut Appliance Retirement Program: Overall Report.” [↑](#footnote-ref-1041)
1041. The Federal Standard does not include an EER requirement, so it is approximated with this formula: (-0.02 \* SEER2) + (1.12 \* SEER) Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder. Note this is appropriate for single speed units only. [↑](#footnote-ref-1042)
1042. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-1043)
1043. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-1044)
1044. American Standard Maintenance for Indoor Units: http://www.americanstandardair.com/owner-support/maintenance.html [↑](#footnote-ref-1045)
1045. Act on Energy Commercial Technical Reference Manual No. 2010-4, 9.2.3 Gas Forced-Air Furnace Tune-up. [↑](#footnote-ref-1046)
1046. Fe is not one of the AHRI certified ratings provided for residential furnaces, but can be reasonably estimated from a calculation based on the certified values for fuel energy (Ef in MMBtu/yr) and Eae (kWh/yr). An average of a 300 record sample (non-random) out of 1495 was 3.14%. This is, appropriately, ~50% greater than the Energy Star version 3 criteria for 2% Fe. See “Programmable Thermostats Furnace Fan Analysis.xlsx” for reference. [↑](#footnote-ref-1047)
1047. Heating load is used to describe the household heating need, which is equal to (gas consumption \* AFUE ) [↑](#footnote-ref-1048)
1048. Values are based on household heating consumption values and inferred average AFUE results from Table 2-1, Energy Efficiency / Demand Response Nicor Gas Plan Year 1 (6/1/2011-5/31/2012) Research Report: Furnace Metering Study (August 1, 2013) (prepared by Navigant Consulting, Inc.) and adjusting to a statewide average using relative HDD values to adjust for the evaluation results focus on northern region. Values for individual cities are then calculated by comparing average HDD to the individual city’s HDD. [↑](#footnote-ref-1049)
1049. The Air Conditioning Contractors of America Manual J, Residential Load Calculation 8th Edition produces equipment sizing loads for Single Family, Multi-single, and Condominiums using input characteristics of the home. [↑](#footnote-ref-1050)
1050. Multifamily household heating consumption relative to single-family households is affected by overall household square footage and exposure to the exterior. This 65% reduction factor is applied to MF homes with electric resistance, based on professional judgment that average household size, and heat loads of MF households are smaller than single-family homes [↑](#footnote-ref-1051)
1051. Program-specific household factors may be utilized on the basis of sufficiently validated program evaluations. [↑](#footnote-ref-1052)
1052. Energy Solutions Center, a consortium of natural gas utilities, equipment manufacturers and vendors. Boiler Reset Control, accessed at http://naturalgasefficiency.org/residential/Boiler\_Reset\_Control.htm [↑](#footnote-ref-1053)
1053. CLEAResultreferences the Brooklyn Union Gas Company, High Efficiency Heating and Water and Controls, Gas Energy Efficiency Program Implementation Plan. [↑](#footnote-ref-1054)
1054. Nexant. Questar DSM Market Characterization Report. August 9, 2006. [↑](#footnote-ref-1055)
1055. Boiler consumption values are informed by an evaluation which did not identify any fraction of heating load due to domestic hot water (DHW) provided by the boiler. Thus these values are an average of both homes with boilers only providing heat, and homes with boilers that also provide DHW. Heating load is used to describe the household heating need, which is equal to (gas heating consumption \* AFUE ) [↑](#footnote-ref-1056)
1056. Values are based on household heating consumption values and inferred average AFUE results from Table 3-4, Program Sample Analysis, *Nicor R29 Res Rebate Evaluation Report 092611\_REV FINAL to Nicor*). Adjusting to a statewide average using relative HDD values to adjust for the evaluation results focus on northern region. Values for individual cities are then calculated by comparing average HDD to the individual city’s HDD. [↑](#footnote-ref-1057)
1057. The Air Conditioning Contractors of America Manual J, Residential Load Calculation 8th Edition produces equipment sizing loads for Single Family, Multi-single, and Condominiums using input characteristics of the home. A best practice for equipment selection and installation of Heating and Air Conditioning, load calculations should be completed by contractors during the selection process and may be readily available for program data purposes. [↑](#footnote-ref-1058)
1058. Energy Solutions Center, a consortium of natural gas utilities, equipment manufacturers and vendors. Boiler Reset Control, accessed at http://naturalgasefficiency.org/residential/Boiler\_Reset\_Control.htm [↑](#footnote-ref-1059)
1059. <http://www.energystar.gov/products/certified-products/detail/ceiling-fans> [↑](#footnote-ref-1060)
1060. ENERGY STAR Ceiling Fan Savings Calculator

      <http://www.energystar.gov/buildings/sites/default/uploads/files/light_fixture_ceiling_fan_calculator.xlsx?8178-e52c> [↑](#footnote-ref-1061)
1061. Assuming that the CF same as a Room AC. Consistent with coincidence factors found in: RLW Report: Final Report Coincidence Factor Study Residential Room Air Conditioners, June 23, 2008 ([http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117\_RLW\_CF%20Res%20RAC.pdf](http://www.ctsavesenergy.org/files/Measure%20Life%20Report%202007.pdf)) [↑](#footnote-ref-1062)
1062. All fan default assumptions are based upon assumptions provided in the ENERGY STAR Ceiling Fan Savings Calculator;

      <http://www.energystar.gov/buildings/sites/default/uploads/files/light_fixture_ceiling_fan_calculator.xlsx?8178-e52c> [↑](#footnote-ref-1063)
1063. Assuming that the CF same as a Room AC. Consistent with coincidence factors found in: RLW Report: Final Report Coincidence Factor Study Residential Room Air Conditioners, June 23, 2008 ([http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117\_RLW\_CF%20Res%20RAC.pdf](http://www.ctsavesenergy.org/files/Measure%20Life%20Report%202007.pdf)) [↑](#footnote-ref-1064)
1064. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1065)
1065. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007.

      [http://www.ctsavesenergy.org/files/Measure%20Life%20Report%202007.pdf](http://mn.gov/commerce/energy/images/ElectricFoodService_v03.2.xls) [↑](#footnote-ref-1066)
1066. Consistent with DEER 2008 Database Technology and Measure Cost Data ([www.deeresources.com](http://www.ctsavesenergy.org/files/Measure%20Life%20Report%202007.pdf)). [↑](#footnote-ref-1067)
1067. Navigant Consulting Inc., April 2009; “Measures and Assumptions for Demand Side Management (DSM) Planning; Appendix C Substantiation Sheets”, p77. [↑](#footnote-ref-1068)
1068. Assumes 125°F water leaving the hot water tank and average temperature of basement of 65°F. [↑](#footnote-ref-1069)
1069. Electric water heaters have recovery efficiency of 98%: <http://www.ahridirectory.org/ahridirectory/pages/home.aspx> [↑](#footnote-ref-1070)
1070. Review of AHRI Directory suggests range of recovery efficiency ratings for new Gas DHW units of 70-87%. Average of existing units is estimated at 78% [↑](#footnote-ref-1071)
1071. Minimum Federal Standard as of 4/1/2015;

      http://www.gpo.gov/fdsys/pkg/CFR-2012-title10-vol3/pdf/CFR-2012-title10-vol3-sec430-32.pdf [↑](#footnote-ref-1072)
1072. DOE, 2010 Residential Heating Products Final Rule Technical Support Document, Table 8.2.14 http://www1.eere.energy.gov/buildings/appliance\_standards/residential/pdfs/htgp\_finalrule\_ch8.pdf Note: This source is used to support this category in aggregate. For all water heaters, life expectancy will depend on local variables such as water chemistry and homeowner maintenance. Some categories, including condensing storage and tankless water heaters do not yet have sufficient field data to support separate values. Preliminary data show lifetimes may exceed 20 years, though this has yet to be sufficiently demonstrated. [↑](#footnote-ref-1073)
1073. Assumed to be one third of effective useful life [↑](#footnote-ref-1074)
1074. Source for cost info; DOE, 2010 Residential Heating Products Final Rule Technical Support Document, Table 8.2.14 (http://www1.eere.energy.gov/buildings/appliance\_standards/residential/pdfs/htgp\_finalrule\_ch8.pdf) [↑](#footnote-ref-1075)
1075. The deemed install cost of a Gas Storage heater is based upon DCEO Efficient Living Program Data for a sample size of 157 gas water heaters. [↑](#footnote-ref-1076)
1076. The two equations are provided to show how savings are determined during the initial phase of the measure (existing to efficient) and the remaining phase (new baseline to efficient). In practice, the screening tools used may either require a First Year savings (using the first equation) and then a “number of years to adjustment” and “savings adjustment” input which would be the (new base to efficient savings)/(existing to efficient savings). [↑](#footnote-ref-1077)
1077. The disconnect between rated energy factor and in-situ energy consumption is markedly different for tankless units due to significantly higher contributions to overall household hot water usage from short draws. In tankless units the large burner and unit heat exchanger must fire and heat up for each draw. The additional energy losses incurred when the mass of the unit cools to the surrounding space in-between shorter draws was found to be 9% in a study prepared for Lawrence Berkeley National Laboratory by Davis Energy Group, 2006. “Field and Laboratory Testing of Tankless Gas Water Heater Performance” Due to the similarity (storage) between the other categories and the baseline, this derating factor is applied only to the tankless category. [↑](#footnote-ref-1078)
1078. Based on DCEO Efficient Living Program Data for a sample size of 157 gas water heaters. [↑](#footnote-ref-1079)
1079. [Maureen](http://portal.veic.org/projects/illinoistrm/Lists/TRM%20Request%20Tracker/Attachments/287/Maureen) Hodgins, Email to SAG/TAC on August 26, 2017 [↑](#footnote-ref-1080)
1080. ComEd Energy Efficiency/ Demand Response Plan: Plan Year 2 (6/1/2009-5/31/2010) Evaluation Report: All Electric Single Family Home Energy Performance Tune-Up Program citing 2006-2008 American Community Survey data from the US Census Bureau for Illinois cited on p. 17 of the PY2 Evaluation report. 2.75 \* 93% evaluation adjustment [↑](#footnote-ref-1081)
1081. Navigant, ComEd PY3 Multi-Family Home Energy Savings Program Evaluation Report Final, May 16, 2012. [↑](#footnote-ref-1082)
1082. Bedrooms are suitable proxies for household occupancy, and may be preferable to actual occupancy due to turnover rates in residency and non-adult population impacts. [↑](#footnote-ref-1083)
1083. US DOE Building America Program. Building America Analysis Spreadsheet. For Chicago, IL [http://www1.eere.energy.gov/buildings/building\_america/analysis\_spreadsheets.html](http://www.bpi.org/files/pdf/DistributionEfficiencyTable-BlueSheet.pdf) [↑](#footnote-ref-1084)
1084. Table C-6, Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007. "http://neep.org/uploads/EMV%20Forum/EMV%20Studies/measure\_life\_GDS%5B1%5D.pdf" [↑](#footnote-ref-1085)
1085. Direct-install price per faucet assumes cost of aerator and install time. (2011, Market research average of $3 and assess and install time of $5 (20min @ $15/hr) [↑](#footnote-ref-1086)
1086. Calculated as follows: Assume 18% aerator use takes place during peak hours (based on: <http://www.aquacraft.com/sites/default/files/pub/DeOreo-%282001%29-Disaggregated-Hot-Water-Use-in-Single-Family-Homes-Using-Flow-Trace-Analysis.pdf>) There are 65 days in the summer peak period, so the percentage of total annual aerator use in peak period is 0.18\*65/365 = 3.21%. The number of hours of recovery during peak periods is therefore assumed to be 3.21% \*180 = 5.8 hours of recovery during peak period where 180 equals the average annual electric DHW recovery hours for faucet use including SF and MF homes. There are 260 hours in the peak period so the probability you will see savings during the peak period is 5.8/260 = 0.022 [↑](#footnote-ref-1087)
1087. This algorithm calculates the amount of energy saved per aerator by determining the fraction of water consumption savings for the upgraded fixture. [↑](#footnote-ref-1088)
1088. Default assumption for unknown fuel is based on EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used [↑](#footnote-ref-1089)
1089. [Maureen](http://portal.veic.org/projects/illinoistrm/Lists/TRM%20Request%20Tracker/Attachments/287/Maureen) Hodgins, email to SAG/TAC on August 26, 2014 [↑](#footnote-ref-1090)
1090. Measurement should be based on actual average flow consumed over a period of time rather than a onetime spot measurement for maximum flow. Studies have shown maximum flow rates do not correspond well to average flow rate due to occupant behavior which does not always use maximum flow. [↑](#footnote-ref-1091)
1091. 2008, Schultdt, Marc, and Debra Tachibana. Energy related Water Fixture Measurements: Securing the Baseline for Northwest Single Family Homes. 2008 ACEEE Summer Study on Energy Efficiency in Buildings. Page 1-265. www.seattle.gov/light/Conserve/Reports/paper\_10.pdf [↑](#footnote-ref-1092)
1092. Average retrofit flow rate for kitchen and bathroom faucet aerators from sources 2, 4, 5, and 7(see source table at end of characterization). This accounts for all throttling and differences from rated flow rates. Assumes all kitchen aerators at 2.2 gpm or less and all bathroom aerators at 1.5 gpm or less. The most comprehensive available studies did not disaggregate kitchen use from bathroom use, but instead looked at total flow and length of use for all faucets. This makes it difficult to reliably separate kitchen water use from bathroom water use. It is possible that programs installing low flow aerators lower than the 2.2 gpm for kitchens and 1.5 gpm for bathrooms will see a lower overall average retrofit flow rate. [↑](#footnote-ref-1093)
1093. Measurement should be based on actual average flow consumed over a period of time rather than a onetime spot measurement for maximum flow. Studies have shown maximum flow rates do not correspond well to average flow rate due to occupant behavior which does not always use maximum flow. [↑](#footnote-ref-1094)
1094. 2008, Schultdt, Marc, and Debra Tachibana. Energy related Water Fixture Measurements: Securing the Baseline for Northwest Single Family Homes. 2008 ACEEE Summer Study on Energy Efficiency in Buildings. Page 1-265. www.seattle.gov/light/Conserve/Reports/paper\_10.pdf [↑](#footnote-ref-1095)
1095. Cadmus and Opinion Dynamics Showerhead and Faucet Aerator Meter Study Memorandum dated June 2013, directed to Michigan Evaluation Working Group. This study of 135 single and multi-family homes in Michigan metered energy parameters for efficient showerhead and faucet aerators. [↑](#footnote-ref-1096)
1096. Ibid. [↑](#footnote-ref-1097)
1097. One kitchen faucet plus 2.83 bathroom faucets. Based on findings from a 2009 ComEd residential survey of 140 sites, provided by Cadmus. [↑](#footnote-ref-1098)
1098. One kitchen faucet plus 1.5 bathroom faucets. Based on findings from a 2009 ComEd residential survey of 140 sites, provided by Cadmus. [↑](#footnote-ref-1099)
1099. Cadmus and Opinion Dynamics Showerhead and Faucet Aerator Meter Study Memorandum dated June 2013, directed to Michigan Evaluation Working Group. [↑](#footnote-ref-1100)
1100. Ibid. [↑](#footnote-ref-1101)
1101. One kitchen faucet plus 2.83 bathroom faucets. Based on findings from a 2009 ComEd residential survey of 140 sites, provided by Cadmus. [↑](#footnote-ref-1102)
1102. One kitchen faucet plus 1.5 bathroom faucets. Based on findings from a 2009 ComEd residential survey of 140 sites, provided by Cadmus. [↑](#footnote-ref-1103)
1103. ComEd Energy Efficiency/ Demand Response Plan: Plan Year 2 (6/1/2009-5/31/2010) Evaluation Report: All Electric Single Family Home Energy Performance Tune-Up Program citing 2006-2008 American Community Survey data from the US Census Bureau for Illinois cited on p. 17 of the PY2 Evaluation report. 2.75 \* 93% evaluation adjustment [↑](#footnote-ref-1104)
1104. Navigant, ComEd PY3 Multi-Family Home Energy Savings Program Evaluation Report Final, May 16, 2012. [↑](#footnote-ref-1105)
1105. Bedrooms are suitable proxies for household occupancy, and may be preferable to actual occupancy due to turnover rates in residency and non-adult population impacts. [↑](#footnote-ref-1106)
1106. Because faucet usages are at times dictated by volume, only usage of the sort that would go straight down the drain will provide savings. VEIC is unaware of any metering study that has determined this specific factor and so through consensus with the Illinois Technical Advisory Group have deemed these values to be 75% for the kitchen and 90% for the bathroom. If the aerator location is unknown an average of 79.5% should be used which is based on the assumption that 70% of household water runs through the kitchen faucet and 30% through the bathroom (0.7\*0.75)+(0.3\*0.9)=0.795. [↑](#footnote-ref-1107)
1107. Based on findings from a 2009 ComEd residential survey of 140 sites, provided by Cadmus. [↑](#footnote-ref-1108)
1108. Ibid. [↑](#footnote-ref-1109)
1109. Cadmus and Opinion Dynamics Showerhead and Faucet Aerator Meter Study Memorandum dated June 2013, directed to Michigan Evaluation Working Group. If the aerator location is unknown an average of 91% should be used which is based on the assumption that 70% of household water runs through the kitchen faucet and 30% through the bathroom (0.7\*93)+(0.3\*86)=0.91. [↑](#footnote-ref-1110)
1110. US DOE Building America Program. Building America Analysis Spreadsheet. For Chicago, IL <http://www1.eere.energy.gov/buildings/building_america/analysis_spreadsheets.html>. [↑](#footnote-ref-1111)
1111. Electric water heaters have recovery efficiency of 98%: <http://www.ahridirectory.org/ahridirectory/pages/home.aspx> [↑](#footnote-ref-1112)
1112. ComEd Energy Efficiency/ Demand Response Plan: Plan Year 2 (6/1/2009-5/31/2010) Evaluation Report: All Electric Single Family Home Energy Performance Tune-Up Program Table 3-8 [↑](#footnote-ref-1113)
1113. Navigant, ComEd-Nicor Gas EPY4/GPY1 Multi-Family Home Energy Savings Program Evaluation Report DRAFT 2013-01-28 [↑](#footnote-ref-1114)
1114. Ibid. [↑](#footnote-ref-1115)
1115. 54.5% is the proportion of hot 120F water mixed with 54.1F supply water to give 90F mixed faucet water. [↑](#footnote-ref-1116)
1116. Calculated as follows: Assume 18% aerator use takes place during peak hours (based on: <http://www.aquacraft.com/sites/default/files/pub/DeOreo-%282001%29-Disaggregated-Hot-Water-Use-in-Single-Family-Homes-Using-Flow-Trace-Analysis.pdf>) There are 65 days in the summer peak period, so the percentage of total annual aerator use in peak period is 0.18\*65/365 = 3.21%. The number of hours of recovery during peak periods is therefore assumed to be 3.21% \*180 = 5.8 hours of recovery during peak period where 180 equals the average annual electric DHW recovery hours for faucet use including SF and MF homes. There are 260 hours in the peak period so the probability you will see savings during the peak period is 5.8/260 = 0.022 [↑](#footnote-ref-1117)
1117. Default assumption for unknown fuel is based on EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used [↑](#footnote-ref-1118)
1118. DOE Final Rule discusses Recovery Efficiency with an average around 0.76 for Gas Fired Storage Water heaters and 0.78 for standard efficiency gas fired tankless water heaters up to 0.95 for the highest efficiency gas fired condensing tankless water heaters. These numbers represent the range of new units however, not the range of existing units in stock. Review of AHRI Directory suggests range of recovery efficiency ratings for new Gas DHW units of 70-87%. Average of existing units is estimated at 78%. [↑](#footnote-ref-1119)
1119. Water heating in multi-family buildings is often provided by a larger central boiler. This suggests that the average recovery efficiency is somewhere between a typical central boiler efficiency of 0.59 and the 0.75 for single family homes. An average efficiency of 0.67 is used for this analysis as a default for multi-family buildings. [↑](#footnote-ref-1120)
1120. Table C-6, Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007. "http://neep.org/uploads/EMV%20Forum/EMV%20Studies/measure\_life\_GDS%5B1%5D.pdf" [↑](#footnote-ref-1121)
1121. Direct-install price per faucet assumes cost of aerator and install time. (2011, Market research average of $3 and assess and install time of $5 (20min @ $15/hr) [↑](#footnote-ref-1122)
1122. Calculated as follows: Assume 18% aerator use takes place during peak hours (based on: <http://www.aquacraft.com/sites/default/files/pub/DeOreo-%282001%29-Disaggregated-Hot-Water-Use-in-Single-Family-Homes-Using-Flow-Trace-Analysis.pdf>) There are 65 days in the summer peak period, so the percentage of total annual aerator use in peak period is 0.18\*65/365 = 3.21%. The number of hours of recovery during peak periods is therefore assumed to be 3.21% \*180 = 5.8 hours of recovery during peak period where 180 equals the average annual electric DHW recovery hours for faucet use including SF and MF homes. There are 260 hours in the peak period so the probability you will see savings during the peak period is 5.8/260 = 0.022 [↑](#footnote-ref-1123)
1123. This algorithm calculates the amount of energy saved per aerator by determining the fraction of water consumption savings for the upgraded fixture. [↑](#footnote-ref-1124)
1124. Default assumption for unknown fuel is based on EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used [↑](#footnote-ref-1125)
1125. Table 56, DeOreo, William B., Mayer, Peter W., Residential End Uses of Water Study Update, 2013. http://www.aquacraft.com/sites/default/files/img/REUWS2%20Project%20Report%2020131204.pdf [↑](#footnote-ref-1126)
1126. Measurement should be based on actual average flow consumed over a period of time rather than a onetime spot measurement for maximum flow. Studies have shown maximum flow rates do not correspond well to average flow rate due to occupant behavior which does not always use maximum flow. [↑](#footnote-ref-1127)
1127. 2008, Schultdt, Marc, and Debra Tachibana. Energy related Water Fixture Measurements: Securing the Baseline for Northwest Single Family Homes. 2008 ACEEE Summer Study on Energy Efficiency in Buildings. Page 1-265. www.seattle.gov/light/Conserve/Reports/paper\_10.pdf [↑](#footnote-ref-1128)
1128. Average retrofit flow rate for kitchen and bathroom faucet aerators from sources 2, 4, 5, and 7(see source table at end of characterization). This accounts for all throttling and differences from rated flow rates. Assumes all kitchen aerators at 2.2 gpm or less and all bathroom aerators at 1.5 gpm or less. The most comprehensive available studies did not disaggregate kitchen use from bathroom use, but instead looked at total flow and length of use for all faucets. This makes it difficult to reliably separate kitchen water use from bathroom water use. It is possible that programs installing low flow aerators lower than the 2.2 gpm for kitchens and 1.5 gpm for bathrooms will see a lower overall average retrofit flow rate. [↑](#footnote-ref-1129)
1129. Measurement should be based on actual average flow consumed over a period of time rather than a onetime spot measurement for maximum flow. Studies have shown maximum flow rates do not correspond well to average flow rate due to occupant behavior which does not always use maximum flow. [↑](#footnote-ref-1130)
1130. 2008, Schultdt, Marc, and Debra Tachibana. Energy related Water Fixture Measurements: Securing the Baseline for Northwest Single Family Homes. 2008 ACEEE Summer Study on Energy Efficiency in Buildings. Page 1-265. www.seattle.gov/light/Conserve/Reports/paper\_10.pdf [↑](#footnote-ref-1131)
1131. Cadmus and Opinion Dynamics Showerhead and Faucet Aerator Meter Study Memorandum dated June 2013, directed to Michigan Evaluation Working Group. This study of 135 single and multi-family homes in Michigan metered energy parameters for efficient showerhead and faucet aerators. [↑](#footnote-ref-1132)
1132. Ibid. [↑](#footnote-ref-1133)
1133. One kitchen faucet plus 2.83 bathroom faucets. Based on findings from a 2009 ComEd residential survey of 140 sites, provided by Cadmus. [↑](#footnote-ref-1134)
1134. One kitchen faucet plus 1.5 bathroom faucets. Based on findings from a 2009 ComEd residential survey of 140 sites, provided by Cadmus. [↑](#footnote-ref-1135)
1135. Cadmus and Opinion Dynamics Showerhead and Faucet Aerator Meter Study Memorandum dated June 2013, directed to Michigan Evaluation Working Group. [↑](#footnote-ref-1136)
1136. Ibid. [↑](#footnote-ref-1137)
1137. One kitchen faucet plus 2.83 bathroom faucets. Based on findings from a 2009 ComEd residential survey of 140 sites, provided by Cadmus. [↑](#footnote-ref-1138)
1138. One kitchen faucet plus 1.5 bathroom faucets. Based on findings from a 2009 ComEd residential survey of 140 sites, provided by Cadmus. [↑](#footnote-ref-1139)
1139. ComEd Energy Efficiency/ Demand Response Plan: Plan Year 2 (6/1/2009-5/31/2010) Evaluation Report: All Electric Single Family Home Energy Performance Tune-Up Program citing 2006-2008 American Community Survey data from the US Census Bureau for Illinois cited on p. 17 of the PY2 Evaluation report. 2.75 \* 93% evaluation adjustment [↑](#footnote-ref-1140)
1140. Navigant, ComEd PY3 Multi-Family Home Energy Savings Program Evaluation Report Final, May 16, 2012. [↑](#footnote-ref-1141)
1141. Bedrooms are suitable proxies for household occupancy, and may be preferable to actual occupancy due to turnover rates in residency and non-adult population impacts. [↑](#footnote-ref-1142)
1142. Because faucet usages are at times dictated by volume, only usage of the sort that would go straight down the drain will provide savings. VEIC is unaware of any metering study that has determined this specific factor and so through consensus with the Illinois Technical Advisory Group have deemed these values to be 75% for the kitchen and 90% for the bathroom. If the aerator location is unknown an average of 79.5% should be used which is based on the assumption that 70% of household water runs through the kitchen faucet and 30% through the bathroom (0.7\*0.75)+(0.3\*0.9)=0.795. [↑](#footnote-ref-1143)
1143. Based on findings from a 2009 ComEd residential survey of 140 sites, provided by Cadmus. [↑](#footnote-ref-1144)
1144. Ibid. [↑](#footnote-ref-1145)
1145. Cadmus and Opinion Dynamics Showerhead and Faucet Aerator Meter Study Memorandum dated June 2013, directed to Michigan Evaluation Working Group. If the aerator location is unknown an average of 91% should be used which is based on the assumption that 70% of household water runs through the kitchen faucet and 30% through the bathroom (0.7\*93)+(0.3\*86)=0.91. [↑](#footnote-ref-1146)
1146. US DOE Building America Program. Building America Analysis Spreadsheet. For Chicago, IL <http://www1.eere.energy.gov/buildings/building_america/analysis_spreadsheets.html>. [↑](#footnote-ref-1147)
1147. Electric water heaters have recovery efficiency of 98%: <http://www.ahridirectory.org/ahridirectory/pages/home.aspx> [↑](#footnote-ref-1148)
1148. ComEd Energy Efficiency/ Demand Response Plan: Plan Year 2 (6/1/2009-5/31/2010) Evaluation Report: All Electric Single Family Home Energy Performance Tune-Up Program Table 3-8 [↑](#footnote-ref-1149)
1149. Navigant, ComEd-Nicor Gas EPY4/GPY1 Multi-Family Home Energy Savings Program Evaluation Report DRAFT 2013-01-28 [↑](#footnote-ref-1150)
1150. Ibid. [↑](#footnote-ref-1151)
1151. 54.5% is the proportion of hot 120F water mixed with 54.1F supply water to give 90F mixed faucet water. [↑](#footnote-ref-1152)
1152. Calculated as follows: Assume 18% aerator use takes place during peak hours (based on: <http://www.aquacraft.com/sites/default/files/pub/DeOreo-%282001%29-Disaggregated-Hot-Water-Use-in-Single-Family-Homes-Using-Flow-Trace-Analysis.pdf>) There are 65 days in the summer peak period, so the percentage of total annual aerator use in peak period is 0.18\*65/365 = 3.21%. The number of hours of recovery during peak periods is therefore assumed to be 3.21% \*180 = 5.8 hours of recovery during peak period where 180 equals the average annual electric DHW recovery hours for faucet use including SF and MF homes. There are 260 hours in the peak period so the probability you will see savings during the peak period is 5.8/260 = 0.022 [↑](#footnote-ref-1153)
1153. Default assumption for unknown fuel is based on EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used [↑](#footnote-ref-1154)
1154. DOE Final Rule discusses Recovery Efficiency with an average around 0.76 for Gas Fired Storage Water heaters and 0.78 for standard efficiency gas fired tankless water heaters up to 0.95 for the highest efficiency gas fired condensing tankless water heaters. These numbers represent the range of new units however, not the range of existing units in stock. Review of AHRI Directory suggests range of recovery efficiency ratings for new Gas DHW units of 70-87%. Average of existing units is estimated at 78%. [↑](#footnote-ref-1155)
1155. Water heating in multi-family buildings is often provided by a larger central boiler. This suggests that the average recovery efficiency is somewhere between a typical central boiler efficiency of 0.59 and the 0.75 for single family homes. An average efficiency of 0.67 is used for this analysis as a default for multi-family buildings. [↑](#footnote-ref-1156)
1156. Table C-6, Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007. Evaluations indicate that consumer dissatisfaction may lead to reductions in persistence, particularly in Multi-Family , "http://neep.org/uploads/EMV%20Forum/EMV%20Studies/measure\_life\_GDS%5B1%5D.pdf" [↑](#footnote-ref-1157)
1157. Direct-install price per showerhead assumes cost of showerhead (Market research average of $7 and assess and install time of $5 (20min @ $15/hr) [↑](#footnote-ref-1158)
1158. Calculated as follows: Assume 11% showers take place during peak hours (based on: <http://www.aquacraft.com/sites/default/files/pub/DeOreo-%282001%29-Disaggregated-Hot-Water-Use-in-Single-Family-Homes-Using-Flow-Trace-Analysis.pdf>). There are 65 days in the summer peak period, so the percentage of total annual aerator use in peak period is 0.11\*65/365 = 1.96%. The number of hours of recovery during peak periods is therefore assumed to be 1.96% \* 369 = 7.23 hours of recovery during peak period, where 369 equals the average annual electric DHW recovery hours for showerhead use including SF and MF homes with Direct Install and Retrofit/TOS measures. There are 260 hours in the peak period so the probability you will see savings during the peak period is 7.23/260 = 0.0278 [↑](#footnote-ref-1159)
1159. Default assumption for unknown fuel is based on EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used [↑](#footnote-ref-1160)
1160. Based on measured data from Ameren IL EM&V of Direct-Install program. Program targets showers that are rated 2.5 GPM or above. [↑](#footnote-ref-1161)
1161. Representative value from sources 1, 2, 4, 5, 6 and 7 (See Source Table at end of measure section) adjusted slightly upward to account for program participation which is expected to target customers with existing higher flow devices rather than those with existing low flow devices. [↑](#footnote-ref-1162)
1162. Note that actual values may be either a) program-specific minimum flow rate, or b) program-specific evaluation-based value of actual effective flow-rate due to increased duration or temperatures. The latter increases in likelihood as the rated flow drops and may become significant at or below rated flows of 1.5 GPM. The impact can be viewed as the inverse of the throttling described in the footnote for baseline flowrate. [↑](#footnote-ref-1163)
1163. Cadmus and Opinion Dynamics Showerhead and Faucet Aerator Meter Study Memorandum dated June 2013, directed to Michigan Evaluation Working Group. This study of 135 single and multi-family homes in Michigan metered energy parameters for efficient showerhead and faucet aerators. [↑](#footnote-ref-1164)
1164. Ibid. [↑](#footnote-ref-1165)
1165. If household type is unknown, as may be the case for time of sale measures, then single family deemed value shall be used. [↑](#footnote-ref-1166)
1166. ComEd Energy Efficiency/ Demand Response Plan: Plan Year 2 (6/1/2009-5/31/2010) Evaluation Report: All Electric Single Family Home Energy Performance Tune-Up Program citing 2006-2008 American Community Survey data from the US Census Bureau for Illinois cited on p. 17 of the PY2 Evaluation report. 2.75 \* 93% evaluation adjustment [↑](#footnote-ref-1167)
1167. ComEd PY3 Multi-Family Evaluation Report REVISED DRAFT v5 2011-12-08.docx [↑](#footnote-ref-1168)
1168. Bedrooms are suitable proxies for household occupancy, and may be preferable to actual occupancy due to turnover rates in residency and non-adult population impacts. [↑](#footnote-ref-1169)
1169. Cadmus and Opinion Dynamics Showerhead and Faucet Aerator Meter Study Memorandum dated June 2013, directed to Michigan Evaluation Working Group. [↑](#footnote-ref-1170)
1170. Based on findings from a 2009 ComEd residential survey of 140 sites, provided by Cadmus. [↑](#footnote-ref-1171)
1171. Ibid. [↑](#footnote-ref-1172)
1172. Cadmus and Opinion Dynamics Showerhead and Faucet Aerator Meter Study Memorandum dated June 2013, directed to Michigan Evaluation Working Group. [↑](#footnote-ref-1173)
1173. US DOE Building America Program. Building America Analysis Spreadsheet. For Chicago, IL <http://www1.eere.energy.gov/buildings/building_america/analysis_spreadsheets.html>. [↑](#footnote-ref-1174)
1174. Electric water heaters have recovery efficiency of 98%: <http://www.ahridirectory.org/ahridirectory/pages/home.aspx> [↑](#footnote-ref-1175)
1175. Deemed values are from ComEd Energy Efficiency/ Demand Response Plan: Plan Year 2 (6/1/2009-5/31/2010) Evaluation Report: All Electric Single Family Home Energy Performance Tune-Up Program Table 3-8. Alternative ISRs may be developed for program delivery methods based on evaluation results. [↑](#footnote-ref-1176)
1176. Navigant, ComEd-Nicor Gas EPY4/GPY1 Multi-Family Home Energy Savings Program Evaluation Report FINAL 2013-06-05 [↑](#footnote-ref-1177)
1177. 71.2% is the proportion of hot 120F water mixed with 54.1F supply water to give 101F shower water. [↑](#footnote-ref-1178)
1178. Calculated as follows: Assume 11% showers take place during peak hours (based on: <http://www.aquacraft.com/sites/default/files/pub/DeOreo-%282001%29-Disaggregated-Hot-Water-Use-in-Single-Family-Homes-Using-Flow-Trace-Analysis.pdf>). There are 65 days in the summer peak period, so the percentage of total annual aerator use in peak period is 0.11\*65/365 = 1.96%. The number of hours of recovery during peak periods is therefore assumed to be 1.96% \* 369 = 7.23 hours of recovery during peak period where 369 equals the average annual electric DHW recovery hours for showerhead use including SF and MF homes with Direct Install and Retrofit/TOS measures. There are 260 hours in the peak period so the probability you will see savings during the peak period is 7.23/260 = 0.0278 [↑](#footnote-ref-1179)
1179. Default assumption for unknown fuel is based on EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used [↑](#footnote-ref-1180)
1180. DOE Final Rule discusses Recovery Efficiency with an average around 0.76 for Gas Fired Storage Water heaters and 0.78 for standard efficiency gas fired tankless water heaters up to 0.95 for the highest efficiency gas fired condensing tankless water heaters. These numbers represent the range of new units however, not the range of existing units in stock. Review of AHRI Directory suggests range of recovery efficiency ratings for new Gas DHW units of 70-87%. Average of existing units is estimated at 78%. [↑](#footnote-ref-1181)
1181. Water heating in multi-family buildings is often provided by a larger central boiler. This suggests that the average recovery efficiency is somewhere between a typical central boiler efficiency of 0.59 and the 0.75 for single family homes. An average efficiency of 0.67 is used for this analysis as a default for multi-family buildings. [↑](#footnote-ref-1182)
1182. Note this algorithm provides savings only from reduction in standby losses. The TAC considered avoided energy from not heating the water to the higher temperature but determined that dishwashers are likely to boost the temperature within the unit (roughly canceling out any savings), faucet and shower use is likely to be at the same temperature so there would need to be more lower temperature hot water being used (cancelling any savings) and clothes washers will only see savings if the water from the tank is taken without any temperature control. It was felt the potential impact was too small to be characterized. [↑](#footnote-ref-1183)
1183. Assumptions from PA TRM. Area values were calculated from average dimensions of several commercially available units, with radius values measured to the center of the insulation. [↑](#footnote-ref-1184)
1184. Electric water heaters have recovery efficiency of 98%: <http://www.ahridirectory.org/ahridirectory/pages/home.aspx> [↑](#footnote-ref-1185)
1185. DOE Final Rule discusses Recovery Efficiency with an average around 0.76 for Gas Fired Storage Water heaters and 0.78 for standard efficiency gas fired tankless water heaters up to 0.95 for the highest efficiency gas fired condensing tankless water heaters. These numbers represent the range of new units however, not the range of existing units in stock. Review of AHRI Directory suggests range of recovery efficiency ratings for new Gas DHW units of 70-87%. Average of existing units is estimated at 78%. [↑](#footnote-ref-1186)
1186. Water heating in multi-family buildings is often provided by a larger central boiler. This suggests that the average recovery efficiency is somewhere between a typical central boiler efficiency of 0.59 and the 0.75 for single family homes. An average efficiency of 0.67 is used for this analysis as a default for multi-family buildings. [↑](#footnote-ref-1187)
1187. Visually determine whether it is insulated by foam (newer, rigid, and more effective) or fiberglass (older, gives to gently pressure, and not as effective) [↑](#footnote-ref-1188)
1188. This estimate assumes the tank wrap is installed on an existing unit with 5 years remaining life. [↑](#footnote-ref-1189)
1189. Area includes tank sides and top to account for typical wrap coverage. [↑](#footnote-ref-1190)
1190. Ibid. [↑](#footnote-ref-1191)
1191. Assumes 125°F water leaving the hot water tank and average temperature of basement of 65°F. [↑](#footnote-ref-1192)
1192. Electric water heaters have recovery efficiency of 98%: <http://www.ahridirectory.org/ahridirectory/pages/home.aspx> [↑](#footnote-ref-1193)
1193. Assumptions from PA TRM. Area values were calculated from average dimensions of several commercially available units, with radius values measured to the center of the insulation. Area includes tank sides and top to account for typical wrap coverage. [↑](#footnote-ref-1194)
1194. Assumptions from PA TRM. Ainsul was calculated by assuming that the water heater wrap is a 2” thick fiberglass material. [↑](#footnote-ref-1195)
1195. Assumptions based on NY TRM, Pacific Gas and Electric Company Work Paper PGECODHW113, and measure life of low-flow showerhead [↑](#footnote-ref-1196)
1196. Based on actual cost of the SS-1002CP-SB Ladybug Water-Saving Shower-Head adapter from Evolve showerheads [↑](#footnote-ref-1197)
1197. Calculated as follows: Assume 11% showers take place during peak hours (based on: <http://www.aquacraft.com/sites/default/files/pub/DeOreo-%282001%29-Disaggregated-Hot-Water-Use-in-Single-Family-Homes-Using-Flow-Trace-Analysis.pdf>). There are 65 days in the summer peak period, so the percentage of total annual use in peak period is 0.11\*65/365 = 1.96%. The number of hours of recovery during peak periods is therefore assumed to be 1.96% \* 29.5 = 0.577 hours of recovery during peak period, where 29.5 equals the average annual electric DHW recovery hours for showerhead use prevented by the device including SF and MF homes with Direct Install and Retrofit/TOS measures. There are 260 hours in the peak period so the probability you will see savings during the peak period is 0.577/260 = 0.0022 [↑](#footnote-ref-1198)
1198. Default assumption for unknown fuel is based on EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used [↑](#footnote-ref-1199)
1199. Based on measured data from Ameren IL EM&V of Direct-Install program. Program targets showers that are rated 2.5 GPM or above. Assumes low flow showerhead not included in direct installation. [↑](#footnote-ref-1200)
1200. Representative value from sources 1, 2, 4, 5, 6 and 7 (See Source Table at end of measure section) adjusted slightly upward to account for program participation which is expected to target customers with existing higher flow devices rather than those with existing low flow devices. [↑](#footnote-ref-1201)
1201. Average of the following sources: ShowerStart LLC survey; “Identifying, Quantifying and Reducing Behavioral Waste in the Shower: Exploring the Savings Potential of ShowerStart”, City of San Diego Water Department survey; “Water Conservation Program: ShowerStart Pilot Project White Paper”, and PG&E Work Paper PGECODHW113. [↑](#footnote-ref-1202)
1202. If household type is unknown, as may be the case for time of sale measures, then single family deemed value shall be used. [↑](#footnote-ref-1203)
1203. ComEd Energy Efficiency/ Demand Response Plan: Plan Year 2 (6/1/2009-5/31/2010) Evaluation Report: All Electric Single Family Home Energy Performance Tune-Up Program citing 2006-2008 American Community Survey data from the US Census Bureau for Illinois cited on p. 17 of the PY2 Evaluation report. 2.75 \* 93% evaluation adjustment [↑](#footnote-ref-1204)
1204. ComEd PY3 Multi-Family Evaluation Report REVISED DRAFT v5 2011-12-08.docx [↑](#footnote-ref-1205)
1205. Bedrooms are suitable proxies for household occupancy, and may be preferable to actual occupancy due to turnover rates in residency and non-adult population impacts. [↑](#footnote-ref-1206)
1206. Cadmus and Opinion Dynamics Showerhead and Faucet Aerator Meter Study Memorandum dated June 2013, directed to Michigan Evaluation Working Group. [↑](#footnote-ref-1207)
1207. Based on findings from a 2009 ComEd residential survey of 140 sites, provided by Cadmus. [↑](#footnote-ref-1208)
1208. Ibid. [↑](#footnote-ref-1209)
1209. Cadmus and Opinion Dynamics Showerhead and Faucet Aerator Meter Study Memorandum dated June 2013, directed to Michigan Evaluation Working Group. [↑](#footnote-ref-1210)
1210. US DOE Building America Program. Building America Analysis Spreadsheet. For Chicago, IL <http://www1.eere.energy.gov/buildings/building_america/analysis_spreadsheets.html>. [↑](#footnote-ref-1211)
1211. Electric water heaters have recovery efficiency of 98%: <http://www.ahridirectory.org/ahridirectory/pages/home.aspx> [↑](#footnote-ref-1212)
1212. Deemed values are from ComEd Energy Efficiency/ Demand Response Plan: Plan Year 2 (6/1/2009-5/31/2010) Evaluation Report: All Electric Single Family Home Energy Performance Tune-Up Program Table 3-8. Alternative ISRs may be developed for program delivery methods based on evaluation results. [↑](#footnote-ref-1213)
1213. Navigant, ComEd-Nicor Gas EPY4/GPY1 Multi-Family Home Energy Savings Program Evaluation Report FINAL 2013-06-05 [↑](#footnote-ref-1214)
1214. 71.2% is the proportion of hot 120F water mixed with 54.1F supply water to give 101F shower water. [↑](#footnote-ref-1215)
1215. Calculated as follows: Assume 11% showers take place during peak hours (based on: <http://www.aquacraft.com/sites/default/files/pub/DeOreo-%282001%29-Disaggregated-Hot-Water-Use-in-Single-Family-Homes-Using-Flow-Trace-Analysis.pdf>). There are 65 days in the summer peak period, so the percentage of total annual use in peak period is 0.11\*65/365 = 1.96%. The number of hours of recovery during peak periods is therefore assumed to be 1.96% \* 29.5 = 0.577 hours of recovery during peak period, where 29.5 equals the average annual electric DHW recovery hours for showerhead use prevented by the device including SF and MF homes with Direct Install and Retrofit/TOS measures. There are 260 hours in the peak period so the probability you will see savings during the peak period is 0.577/260 = 0.0022 [↑](#footnote-ref-1216)
1216. Default assumption for unknown fuel is based on EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used [↑](#footnote-ref-1217)
1217. DOE Final Rule discusses Recovery Efficiency with an average around 0.76 for Gas Fired Storage Water heaters and 0.78 for standard efficiency gas fired tankless water heaters up to 0.95 for the highest efficiency gas fired condensing tankless water heaters. These numbers represent the range of new units however, not the range of existing units in stock. Review of AHRI Directory suggests range of recovery efficiency ratings for new Gas DHW units of 70-87%. Average of existing units is estimated at 78%. [↑](#footnote-ref-1218)
1218. Water heating in multi-family buildings is often provided by a larger central boiler. This suggests that the average recovery efficiency is somewhere between a typical central boiler efficiency of 0.59 and the 0.75 for single family homes. An average efficiency of 0.67 is used for this analysis as a default for multi-family buildings. [↑](#footnote-ref-1219)
1219. RES v C&I split is based on a weighted (by sales volume) average of ComEd PY4, PY5 and PY6 and Ameren PY5 and PY6 in store intercept survey results. See ‘RESvCI Split\_122014.xls’. [↑](#footnote-ref-1220)
1220. Jump et al 2008: "Welcome to the Dark Side: The Effect of Switching on CFL Measure Life" indicates that the “observed life” of CFLs with an average rated life of 8000 hours (8000 hours is the average rated life of ENERGY STAR bulbs (<http://www.energystar.gov/index.cfm?c=cfls.pr_crit_cfls>) is 5.2 years. [↑](#footnote-ref-1221)
1221. Since the replacement baseline bulb from 2020 on will be equivalent to a CFL, no additional savings should be claimed from that point. Due to expected delay in clearing stock from retail outlets and to account for the operating life of a halogen incandescent potentially spanning over 2020, this shift is assumed not to occur until mid-2020. [↑](#footnote-ref-1222)
1222. Based on using 8,000 hour rated life assumption since more switching and use outdoors. 8,000/2475 = 3.2years [↑](#footnote-ref-1223)
1223. Based upon pricing forecast developed by Applied Proactive Technologies Inc (APT) based on industry input and provided to Ameren. [↑](#footnote-ref-1224)
1224. Based on 15 minutes at $20 an hour. Includes some portion of travel time to site. [↑](#footnote-ref-1225)
1225. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1226)
1226. Based on lighting logger study conducted as part of the PY5/PY6 ComEd Residential Lighting Program evaluation and excluding all logged bulbs installed in closets. [↑](#footnote-ref-1227)
1227. 1st year in service rate is based upon review of PY4-6 evaluations from ComEd and PY5-6 for Ameren (see ‘IL RES Lighting ISR\_122014.xls’ for more information. The average first year ISR for each utility was calculated weighted by the number of bulbs in the each year’s survey. This was then weighted by annual sales to give a statewide assumption. [↑](#footnote-ref-1228)
1228. The 98% Lifetime ISR assumption is based upon review of two evaluations:

      ‘Nexus Market Research, RLW Analytics and GDS Associates study; “New England Residential Lighting Markdown Impact Evaluation, January 20, 2009’ and ‘KEMA Inc, Feb 2010, Final Evaluation Report:, Upstream Lighting Program, Volume 1.’ This implies that only 2% of bulbs purchased are never installed. The second and third year installations are based upon Ameren analysis of the Californian KEMA study showing that 54% of future installs occur in year 2 and 46% in year 3. The 2nd and 3rd year installations should be counted as part of those future program year savings. [↑](#footnote-ref-1229)
1229. Based upon review of the PY2 and PY3 ComEd Direct Install program surveys. This value includes bulb failures in the 1st year to be consistent with the Commission approval of annualization of savings for first year savings claims. ComEd PY2 All Electric Single Family Home Energy Performance Tune-Up Program Evaluation, Navigant Consulting, December 21, 2010. <http://www.icc.illinois.gov/downloads/public/edocket/287090.pdf>. [↑](#footnote-ref-1230)
1230. In Service Rates provided are for the CFL bulb within a kit only. Given the significant differences in program design and the level of education provided through Efficiency Kits programs, the evaluators should apply the ISR estimated through evaluations (either past evaluations or the current program year evaluation) of the specific Efficiency Kits program.  In cases where program-specific evaluation results for an ISR are unavailable, the default ISR values for Efficiency Kits provide may be used. [↑](#footnote-ref-1231)
1231. Free bulbs provided without request, with little or no education. Based on ‘Impact and Process Evaluation of 2013 (PY6) Ameren Illinois Company Residential CFL Distribution Program’, Report Table 11 and Appendix B. [↑](#footnote-ref-1232)
1232. Kits provided free to students through school, with education program. Based on ‘Impact and Process Evaluation of 2013 (PY6) Ameren Illinois Company Residential Efficiency Kits Program’, table 10. Final ISR assumptions are based upon comparing with CFL Distribution First year ISR and multiplying by the CFL Distribution Final ISR value, and second and third year estimates based on same proportion of future installs. [↑](#footnote-ref-1233)
1233. Opt-in program to receive kits via mail, with little or no education. Based on ‘Impact and Process Evaluation of 2013 (PY6) Ameren Illinois Company Residential Efficiency Kits Program’, table 10, as above. [↑](#footnote-ref-1234)
1234. Using a leakage estimate from the current program year evaluation, from past evaluation results, or a rolling average of leakage estimates from previous years. [↑](#footnote-ref-1235)
1235. Except where noted, based on lighting logger study conducted as part of the PY5/PY6 ComEd Residential Lighting Program evaluation. Direct Install value excludes all logged bulbs installed in closets. [↑](#footnote-ref-1236)
1236. Based on secondary research conducted as part of the PY5/PY6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1237)
1237. Assumes 5% exterior lighting, based on PYPY5/PY6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1238)
1238. The value is estimated at 1.06 (calculated as 1 + (0.66\*(0.27 / 2.8)). Based on cooling loads decreasing by 27% of the lighting savings (average result from REMRate modeling of several different configurations and IL locations of homes), assuming typical cooling system operating efficiency of 2.8 COP (starting from standard assumption of SEER 10.5 central AC unit, converted to 9.5 EER using algorithm (-0.02 \* SEER2) + (1.12 \* SEER) (from Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder), converted to COP = EER/3.412 = 2.8COP) and 66% of homes in Illinois having central cooling ("Table HC7.9 Air Conditioning in Homes in Midwest Region, Divisions, and States, 2009 from Energy Information Administration", 2009 Residential Energy Consumption Survey; <http://www.eia.gov/consumption/residential/data/2009/xls/HC7.9%20Air%20Conditioning%20in%20Midwest%20Region.xls> ) [↑](#footnote-ref-1239)
1239. As above but using estimate of 45% of multi family buildings in Illinois having central cooling (based on data from “Table HC7.1 Air Conditioning in U.S. Homes, By Housing Unit Type, 2009” which is for the whole of the US, scaled to IL air conditioning prevalence compared to US average); <http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls> [↑](#footnote-ref-1240)
1240. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-1241)
1241. This means that heating loads increase by 49% of the lighting savings. This is based on the average result from REMRate modeling of several different configurations and IL locations of homes. [↑](#footnote-ref-1242)
1242. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Heat Pumps was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-1243)
1243. The value is estimated at 1.11 (calculated as 1 + (0.66 \* 0.466 / 2.8)). See footnote relating to WHFe for details. Note the 46.6% factor represents the average Residential cooling coincidence factor calculated by dividing average load during the peak hours divided by the maximum cooling load. [↑](#footnote-ref-1244)
1244. As above but using estimate of 45% of multi family buildings in Illinois having central cooling (based on data from “Table HC7.1 Air Conditioning in U.S. Homes, By Housing Unit Type, 2009” which is for the whole of the US, scaled to IL air conditioning prevalence compared to US average); <http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls>. [↑](#footnote-ref-1245)
1245. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. Direct Install value is based on resut excluding all logged bulbs installed in closets. [↑](#footnote-ref-1246)
1246. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-1247)
1247. This means that heating loads increase by 49% of the lighting savings. This is based on the average result from REMRate modeling of several different configurations and IL locations of homes. [↑](#footnote-ref-1248)
1248. This has been estimated assuming that natural gas central furnace heating is typical for Illinois residences (66% of Illinois homes have a Natural Gas Furnace (based on Energy Information Administration, 2009 Residential Energy Consumption Survey: http://www.eia.gov/consumption/residential/data/2009/xls/HC6.9%20Space%20Heating%20in%20Midwest%20Region.xls))

      In 2000, 24% of furnaces purchased in Illinois were condensing (based on data from GAMA, provided to Department of Energy during the federal standard setting process for residential heating equipment - see Furnace Penetration.xls). Furnaces tend to last up to 20 years and so units purchased 10 years ago provide a reasonable proxy for the current mix of furnaces in the State. Assuming typical efficiencies for condensing and non-condensing furnaces and duct losses, the average heating system efficiency is estimated as follows:

      (0.24\*0.92) + (0.76\*0.8) \* (1-0.15) = 0.70 [↑](#footnote-ref-1249)
1249. Based upon pricing forecast developed by Applied Proactive Technologies Inc (APT) based on industry input and provided to Ameren. [↑](#footnote-ref-1250)
1250. The manufacturers of the new minimally compliant EISA Halogens are using regular incandescent lamps with halogen fill gas rather than halogen infrared to meet the standard and so the component rated life is equal to the standard incandescent. [↑](#footnote-ref-1251)
1251. RES v C&I split is based on a weighted (by sales volume) average of ComEd PY4, PY5 and PY6 and Ameren PY5 and PY6 in store intercept survey results. See ‘RESvCI Split\_122014.xls’. [↑](#footnote-ref-1252)
1252. The assumed measure life for the specialty bulb measure characterization was reported in "Residential Lighting Measure Life Study", Nexus Market Research, June 4, 2008 (measure life for markdown bulbs). Measure life estimate does not distinguish between equipment life and measure persistence. Measure life includes products that were installed and operated until failure (i.e., equipment life) as well as those that were retired early and permanently removed from service for any reason, be it early failure, breakage, or the respondent not liking the product (i.e., measure persistence). [↑](#footnote-ref-1253)
1253. Based on using 8,000 hour rated life assumption since more switching and use ourdoors. 8,000/2475 = 3.2years [↑](#footnote-ref-1254)
1254. NEEP Residential Lighting Survey, 2011 [↑](#footnote-ref-1255)
1255. Based on 15 minutes at $20 per hour. [↑](#footnote-ref-1256)
1256. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1257)
1257. Based upon the draft ENERGY STAR specification for lamps (<http://energystar.gov/products/specs/sites/products/files/ENERGY_STAR_Lamps_V1_0_Draft%203.pdf>) and the Energy Policy and Conservation Act of 2012. [↑](#footnote-ref-1258)
1258. A 2006-2008 California Upstream Lighting Evaluation found an average incandescent wattage of 61.7 Watts (KEMA, Inc, The Cadmus Group, Itron, Inc, PA Consulting Group, Jai J. Mitchell Analytics, Draft Evaluation Report: Upstream Lighting Program. Prepared for the California Public Utilities Commission, Energy Division. December 10, 2009) [↑](#footnote-ref-1259)
1259. The upper bounds for these categories depends on the lower bound of the next higher wattage, which varies by bulb type. [↑](#footnote-ref-1260)
1260. As above. [↑](#footnote-ref-1261)
1261. An evaluation (Energy Efficiency / Demand Response Plan: Plan Year 2 (6/1/2009-5/31/2010) Evaluation Report: Residential Energy Star ® Lighting

      <http://ilsag.org/yahoo_site_admin/assets/docs/ComEd_Res_Lighting_PY2_Evaluation_Report_2010-12-21_Final.12113928.pdf> ) reported 13-17W as the most common specialty CFL wattage (69% of program bulbs). 2009 California data also reported an average CFL wattage of 15.5 Watts (KEMA, Inc, The Cadmus Group, Itron, Inc, PA Consulting Group, Jai J. Mitchell Analytics, Draft Evaluation Report: Upstream Lighting Program, Prepared for the California Public Utilities Commission, Energy Division. December 10, 2009). [↑](#footnote-ref-1262)
1262. 1st year in service rate is based upon review of PY4-6 evaluations from ComEd and PY5-6 from Ameren (see ‘IL RES Lighting ISR\_122014.xls’ for more information. The average first year ISR was calculated weighted by the number of bulbs in the each year’s survey. [↑](#footnote-ref-1263)
1263. The 98% Lifetime ISR assumption is consistent with the assumption for standard CFLs (in the absence of evidence that it should be different for this bulb type) based upon review of two evaluations:

      ‘Nexus Market Research, RLW Analytics and GDS Associates study; “New England Residential Lighting Markdown Impact Evaluation, January 20, 2009’ and ‘KEMA Inc, Feb 2010, Final Evaluation Report:, Upstream Lighting Program, Volume 1.’ This implies that only 2% of bulbs purchased are never installed. The second and third year installations are based upon Ameren analysis of the Californian KEMA study showing that 54% of future installs occur in year 2 and 46% in year 3. The 2nd and 3rd year installations should be counted as part of those future program year savings. [↑](#footnote-ref-1264)
1264. Consistent with assumption for standard CFLs (in the absence of evidence that it should be different for this bulb type). Based upon review of the PY2 and PY3 ComEd Direct Install program surveys. This value includes bulb failures in the 1st year to be consistent with the Commission approval of annualization of savings for first year savings claims. ComEd PY2 All Electric Single Family Home Energy Performance Tune-Up Program Evaluation, Navigant Consulting, December 21, 2010. <http://www.icc.illinois.gov/downloads/public/edocket/287090.pdf>. [↑](#footnote-ref-1265)
1265. In Service Rates provided are for the bulb within a kit only. Given the significant differences in program design and the level of education provided through Efficiency Kits programs, the evaluators should apply the ISR estimated through evaluations (either past evaluations or the current program year evaluation) of the specific Efficiency Kits program.  In cases where program-specific evaluation results for an ISR are unavailable, the default ISR values for Efficiency Kits provide may be used. [↑](#footnote-ref-1266)
1266. Free bulbs provided without request, with little or no education. Consistent with Standard CFL assumptions. [↑](#footnote-ref-1267)
1267. Kits provided free to students through school, with education program. Consistent with Standard CFL assumptions. [↑](#footnote-ref-1268)
1268. Opt-in program to receive kits via mail, with little or no education. Consistent with Standard CFL assumptions. [↑](#footnote-ref-1269)
1269. Using a leakage estimate from the current program year evaluation, from past evaluation results, or a rolling average of leakage estimates from previous years. [↑](#footnote-ref-1270)
1270. Hours of use by specialty bulb type calculated using the average hours of use in locations or rooms where each type of specialty bulb is most commonly found. Values for Reflector, Decorative and Globe are taken directly from the lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. All other hours have been updated based on the room specific hours of use from the PY5/PY6 logger study. [↑](#footnote-ref-1271)
1271. The value is estimated at 1.06 (calculated as 1 + (0.66\*(0.27 / 2.8)). Based on cooling loads decreasing by 27% of the lighting savings (average result from REMRate modeling of several different configurations and IL locations of homes), assuming typical cooling system operating efficiency of 2.8 COP (starting from standard assumption of SEER 10.5 central AC unit, converted to 9.5 EER using algorithm (-0.02 \* SEER2) + (1.12 \* SEER) (from Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder), converted to COP = EER/3.412 = 2.8COP) and 66% of homes in Illinois having central cooling ("Table HC7.9 Air Conditioning in Homes in Midwest Region, Divisions, and States, 2009 from Energy Information Administration", 2009 Residential Energy Consumption Survey; <http://www.eia.gov/consumption/residential/data/2009/xls/HC7.9%20Air%20Conditioning%20in%20Midwest%20Region.xls> ) [↑](#footnote-ref-1272)
1272. As above but using estimate of 45% of multi family buildings in Illinois having central cooling (based on data from “Table HC7.1 Air Conditioning in U.S. Homes, By Housing Unit Type, 2009” which is for the whole of the US, scaled to IL air conditioning prevalence compared to US average); <http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls> [↑](#footnote-ref-1273)
1273. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-1274)
1274. This means that heating loads increase by 49% of the lighting savings. This is based on the average result from REMRate modeling of several different configurations and IL locations of homes. [↑](#footnote-ref-1275)
1275. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Heat Pumps was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-1276)
1276. The value is estimated at 1.11 (calculated as 1 + (0.66 \* 0.466 / 2.8)). See footnote relating to WHFe for details. Note the 46.6% factor represents the average Residential cooling coincidence factor calculated by dividing average load during the peak hours divided by the maximum cooling load. [↑](#footnote-ref-1277)
1277. As above but using estimate of 45% of multifamily buildings in Illinois having central cooling (based on data from “Table HC7.1 Air Conditioning in U.S. Homes, By Housing Unit Type, 2009” which is for the whole of the US, scaled to IL air conditioning prevalence compared to US average); <http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls>. [↑](#footnote-ref-1278)
1278. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1279)
1279. Based on average of bedroom, dining room, office and living room results from the lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1280)
1280. Ibid [↑](#footnote-ref-1281)
1281. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-1282)
1282. This means that heating loads increase by 49% of the lighting savings. This is based on the average result from REMRate modeling of several different configurations and IL locations of homes. [↑](#footnote-ref-1283)
1283. This has been estimated assuming that natural gas central furnace heating is typical for Illinois residences (66% of Illinois homes have a Natural Gas Furnace (based on EIA Residential Energy Consumption Survey (RECS) 2009 for Midwest Region, data for the state of IL. If utilities have specific evaluation results providing a more appropriate assumption for homes in a particular market or geographical area then that should be used.)

      In 2000, 24% of furnaces purchased in Illinois were condensing (based on data from GAMA, provided to Department of Energy during the federal standard setting process for residential heating equipment - see Furnace Penetration.xls). Furnaces tend to last up to 20 years and so units purchased 10 years ago provide a reasonable proxy for the current mix of furnaces in the State. Assuming typical efficiencies for condensing and non-condensing furnaces and duct losses, the average heating system efficiency is estimated as follows:

      (0.24\*0.92) + (0.76\*0.8) \* (1-0.15) = 0.70 [↑](#footnote-ref-1284)
1284. Assuming 1000 hour rated life for incandescent bulb: 1000/759 = 1.32 [↑](#footnote-ref-1285)
1285. NEEP Residential Lighting Survey, 2011 [↑](#footnote-ref-1286)
1286. Assuming 1000 hour rated life for halogen bulb: 1000/759 = 1.32 [↑](#footnote-ref-1287)
1287. NEEP Residential Lighting Survey, 2011 [↑](#footnote-ref-1288)
1288. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007. [↑](#footnote-ref-1289)
1289. DEER 2008 Database Technology and Measure Cost Data ([www.deeresources.com](http://www1.eere.energy.gov/buildings/building_america/analysis_spreadsheets.html)) and consistent with Efficiency Vermont TRM. [↑](#footnote-ref-1290)
1290. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1291)
1291. Nexus Market Research, “Impact Evaluation of the Massachusetts, Rhode Island and Vermont 2003 Residential Lighting Programs”, Final Report, October 1, 2004, p. 43 (Table 4-9) [↑](#footnote-ref-1292)
1292. Nexus Market Research, RLW Analytics “Impact Evaluation of the Massachusetts, Rhode Island, and Vermont 2003 Residential Lighting Programs” table 6-3 on p63 indicates that 86% torchieres were installed in year one. [http://publicservice.vermont.gov/energy/ee\_files/efficiency/eval/marivtreportfinal100104.pdf](http://www1.eere.energy.gov/buildings/building_america/analysis_spreadsheets.html) [↑](#footnote-ref-1293)
1293. Using a leakage estimate from the current program year evaluation, from past evaluation results, or a rolling average of leakage estimates from previous years. [↑](#footnote-ref-1294)
1294. Nexus Market Research, “Impact Evaluation of the Massachusetts, Rhode Island and Vermont 2003 Residential Lighting Programs”, Final Report, October 1, 2004, p. 104 (Table 9-7) [↑](#footnote-ref-1295)
1295. The value is estimated at 1.06 (calculated as 1 + (0.66\*(0.27 / 2.8)). Based on cooling loads decreasing by 27% of the lighting savings (average result from REMRate modeling of several different configurations and IL locations of homes), assuming typical cooling system operating efficiency of 2.8 COP (starting from standard assumption of SEER 10.5 central AC unit, converted to 9.5 EER using algorithm (-0.02 \* SEER2) + (1.12 \* SEER) (from Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder), converted to COP = EER/3.412 = 2.8COP) and 66% of homes in Illinois having central cooling ("Table HC7.9 Air Conditioning in Homes in Midwest Region, Divisions, and States, 2009 from Energy Information Administration", 2009 Residential Energy Consumption Survey; [http://www.eia.gov/consumption/residential/data/2009/xls/HC7.9%20Air%20Conditioning%20in%20Midwest%20Region.xls](http://www.epelectricefficiency.com/downloads.asp) ) [↑](#footnote-ref-1296)
1296. As above but using estimate of 45% of multi family buildings in Illinois having central cooling (based on data from “Table HC7.1 Air Conditioning in U.S. Homes, By Housing Unit Type, 2009” which is for the whole of the US, scaled to IL air conditioning prevalence compared to US average); [http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls](http://www.ilsag.org/) [↑](#footnote-ref-1297)
1297. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-1298)
1298. This means that heating loads increase by 49% of the lighting savings. This is based on the average result from REMRate modeling of several different configurations and IL locations of homes. [↑](#footnote-ref-1299)
1299. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Heat Pumps was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-1300)
1300. The value is estimated at 1.11 (calculated as 1 + (0.66 \* 0.466 / 2.8)). See footnote relating to WHFe for details. Note the 46.6% factor represents the average Residential cooling coincidence factor calculated by dividing average load during the peak hours divided by the maximum cooling load. [↑](#footnote-ref-1301)
1301. As above but using estimate of 45% of multi family buildings in Illinois having central cooling (based on data from “Table HC7.1 Air Conditioning in U.S. Homes, By Housing Unit Type, 2009” which is for the whole of the US, scaled to IL air conditioning prevalence compared to US average); [http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls](http://www1.eere.energy.gov/buildings/appliance_standards/residential/pdfs/htgp_finalrule_ch8.pdf). [↑](#footnote-ref-1302)
1302. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1303)
1303. This means that heating loads increase by 49% of the lighting savings. This is based on the average result from REMRate modeling of several different configurations and IL locations of homes. [↑](#footnote-ref-1304)
1304. This has been estimated assuming that natural gas central furnace heating is typical for Illinois residences (66% of Illinois homes have a Natural Gas Furnace (based on Energy Information Administration, 2009 Residential Energy Consumption Survey: www.eia.gov/consumption/residential/data/2009/xls/HC6.9%20Space%20Heating%20in%20Midwest%20Region.xls) In 2000, 24% of furnaces purchased in Illinois were condensing (based on data from GAMA, provided to Department of Energy during the federal standard setting process for residential heating equipment - see Furnace Penetration.xls). Furnaces tend to last up to 20 years and so units purchased 10 years ago provide a reasonable proxy for the current mix of furnaces in the State. Assuming typical efficiencies for condensing and non-condensing furnaces and duct losses, the average heating system efficiency is estimated as follows:

      (0.24\*0.92) + (0.76\*0.8) \* (1-0.15) = 0.70 [↑](#footnote-ref-1305)
1305. Based on VEIC assumption of baseline bulb (mix of incandescent and halogen) average rated life of 2000 hours, 2000/1095 = 1.83 years. [↑](#footnote-ref-1306)
1306. Derived from Efficiency Vermont TRM. [↑](#footnote-ref-1307)
1307. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007 (<http://www.ctsavesenergy.org/files/Measure%20Life%20Report%202007.pdf>) gives 20 years for an interior fluorescent fixture. [↑](#footnote-ref-1308)
1308. Due to expected delay in clearing stock from retail outlets and to account for the operating life of a halogen incandescent potentially spanning over 2020, this shift is assumed not to occur until mid-2020. [↑](#footnote-ref-1309)
1309. ENERGY STAR Qualified Lighting Savings Calculator default incremental cost input for exterior fixture (http://www.energystar.gov/buildings/sites/default/uploads/files/light\_fixture\_ceiling\_fan\_calculator.xlsx?4349-303e=&b6b3-3efd&b6b3-3efd) [↑](#footnote-ref-1310)
1310. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1311)
1311. 1st year in service rate is based upon review of PY2-3 evaluations from ComEd (see ‘IL RES Lighting ISR.xls’ for more information. The average first year ISR was calculated weighted by the number of bulbs in the each year’s survey. [↑](#footnote-ref-1312)
1312. The 98% Lifetime ISR assumption is consistent with the assumption for standard CFLs (in the absence of evidence that it should be different for this bulb type) based upon review of two evaluations:

      ‘Nexus Market Research, RLW Analytics and GDS Associates study; “New England Residential Lighting Markdown Impact Evaluation, January 20, 2009’ and ‘KEMA Inc, Feb 2010, Final Evaluation Report:, Upstream Lighting Program, Volume 1.’ This implies that only 2% of bulbs purchased are never installed. The second and third year installations are based upon Ameren analysis of the Californian KEMA study showing that 54% of future installs occur in year 2 and 46% in year 3. The 2nd and 3rd year installations should be counted as part of those future program year savings. [↑](#footnote-ref-1313)
1313. In the absence of evaluation results for Direct Install Fixtures specifically, this is made consistent with the Direct Install CFL measure which is based upon review of the PY2 and PY3 ComEd Direct Install program surveys. [↑](#footnote-ref-1314)
1314. Using a leakage estimate from the current program year evaluation, from past evaluation results, or a rolling average of leakage estimates from previous years. [↑](#footnote-ref-1315)
1315. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1316)
1316. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1317)
1317. Based upon pricing forecast developed by Applied Proactive Technologies Inc (APT) based on industry input and provided to Ameren. [↑](#footnote-ref-1318)
1318. The manufacturers of the new minimally compliant EISA Halogens are using regular incandescent lamps with halogen fill gas rather than halogen infrared to meet the standard and so the component rated life is equal to the standard incandescent. [↑](#footnote-ref-1319)
1319. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007 (<http://www.ctsavesenergy.org/files/Measure%20Life%20Report%202007.pdf> ) gives 20 years for an interior fluorescent fixture. [↑](#footnote-ref-1320)
1320. Due to expected delay in clearing stock from retail outlets and to account for the operating life of a halogen incandescent potentially spanning over 2020, this shift is assumed not to occur until mid-2020. [↑](#footnote-ref-1321)
1321. ENERGY STAR Qualified Lighting Savings Calculator default incremental cost input for interior fixture (http://www.energystar.gov/buildings/sites/default/uploads/files/light\_fixture\_ceiling\_fan\_calculator.xlsx?4349-303e=&b6b3-3efd&b6b3-3efd) [↑](#footnote-ref-1322)
1322. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1323)
1323. 1st year in service rate is based upon review of PY2-3 evaluations from ComEd (see ‘IL RES Lighting ISR.xls’ for more information. The average first year ISR was calculated weighted by the number of bulbs in the each year’s survey. [↑](#footnote-ref-1324)
1324. The 98% Lifetime ISR assumption is consistent with the assumption for standard CFLs (in the absence of evidence that it should be different for this bulb type) based upon review of two evaluations:

      ‘Nexus Market Research, RLW Analytics and GDS Associates study; “New England Residential Lighting Markdown Impact Evaluation, January 20, 2009’ and ‘KEMA Inc, Feb 2010, Final Evaluation Report:, Upstream Lighting Program, Volume 1.’ This implies that only 2% of bulbs purchased are never installed. The second and third year installations are based upon Ameren analysis of the Californian KEMA study showing that 54% of future installs occur in year 2 and 46% in year 3. The 2nd and 3rd year installations should be counted as part of those future program year savings. [↑](#footnote-ref-1325)
1325. In the absence of evaluation results for Direct Install Fixtures specifically, this is made consistent with the Direct Install CFL measure which is based upon review of the PY2 and PY3 ComEd Direct Install program surveys. [↑](#footnote-ref-1326)
1326. Using a leakage estimate from the current program year evaluation, from past evaluation results, or a rolling average of leakage estimates from previous years. [↑](#footnote-ref-1327)
1327. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1328)
1328. The value is estimated at 1.06 (calculated as 1 + (0.66\*(0.27 / 2.8)). Based on cooling loads decreasing by 27% of the lighting savings (average result from REMRate modeling of several different configurations and IL locations of homes), assuming typical cooling system operating efficiency of 2.8 COP (starting from standard assumption of SEER 10.5 central AC unit, converted to 9.5 EER using algorithm (-0.02 \* SEER2) + (1.12 \* SEER) (from Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder), converted to COP = EER/3.412 = 2.8COP) and 66% of homes in Illinois having central cooling ("Table HC7.9 Air Conditioning in Homes in Midwest Region, Divisions, and States, 2009 from Energy Information Administration", 2009 Residential Energy Consumption Survey; <http://www.eia.gov/consumption/residential/data/2009/xls/HC7.9%20Air%20Conditioning%20in%20Midwest%20Region.xls>) [↑](#footnote-ref-1329)
1329. As above but using estimate of 45% of multi family buildings in Illinois having central cooling (based on data from “Table HC7.1 Air Conditioning in U.S. Homes, By Housing Unit Type, 2009” which is for the whole of the US, scaled to IL air conditioning prevalence compared to US average); <http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls> [↑](#footnote-ref-1330)
1330. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-1331)
1331. This means that heating loads increase by 49% of the lighting savings. This is based on the average result from REMRate modeling of several different configurations and IL locations of homes. [↑](#footnote-ref-1332)
1332. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Heat Pumps was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-1333)
1333. The value is estimated at 1.11 (calculated as 1 + (0.66 \* 0.466 / 2.8)). See footnote relating to WHFe for details. Note the 46.6% factor represents the average Residential cooling coincidence factor calculated by dividing average load during the peak hours divided by the maximum cooling load. [↑](#footnote-ref-1334)
1334. As above but using estimate of 45% of multi family buildings in Illinois having central cooling (based on data from “Table HC7.1 Air Conditioning in U.S. Homes, By Housing Unit Type, 2009” which is for the whole of the US, scaled to IL air conditioning prevalence compared to US average); <http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls> . [↑](#footnote-ref-1335)
1335. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1336)
1336. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-1337)
1337. This means that heating loads increase by 49% of the lighting savings. This is based on the average result from REMRate modeling of several different configurations and IL locations of homes. [↑](#footnote-ref-1338)
1338. This has been estimated assuming that natural gas central furnace heating is typical for Illinois residences (66% of Illinois homes have a Natural Gas Furnace (based on Energy Information Administration, 2009 Residential Energy Consumption Survey: <http://www.eia.gov/consumption/residential/data/2009/xls/HC6.9%20Space%20Heating%20in%20Midwest%20Region.xls>))

      In 2000, 24% of furnaces purchased in Illinois were condensing (based on data from GAMA, provided to Department of Energy during the federal standard setting process for residential heating equipment - see Furnace Penetration.xls). Furnaces tend to last up to 20 years and so units purchased 10 years ago provide a reasonable proxy for the current mix of furnaces in the State. Assuming typical efficiencies for condensing and non-condensing furnaces and duct losses, the average heating system efficiency is estimated as follows:

      (0.24\*0.92) + (0.76\*0.8) \* (1-0.15) = 0.70 [↑](#footnote-ref-1339)
1339. Based upon pricing forecast developed by Applied Proactive Technologies Inc (APT) based on industry input and provided to Ameren. [↑](#footnote-ref-1340)
1340. The manufacturers of the new minimally compliant EISA Halogens are using regular incandescent lamps with halogen fill gas rather than halogen infrared to meet the standard and so the component rated life is equal to the standard incandescent. [↑](#footnote-ref-1341)
1341. Limited by persistence. NEEP EMV Emerging Technologies Research Report (December 2011) [↑](#footnote-ref-1342)
1342. Costs are provided as the best estimate from VEIC and are based on review of available product and of price reports provided to Efficiency Vermont by a number of manufacturers and retailers. [↑](#footnote-ref-1343)
1343. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1344)
1344. The upper bounds for these categories depends on the lower bound of the next higher wattage, which varies by bulb type. [↑](#footnote-ref-1345)
1345. NEEP EMV Emerging Technologies Research Report (December 2011) [↑](#footnote-ref-1346)
1346. Using a leakage estimate from the current program year evaluation, from past evaluation results, or a rolling average of leakage estimates from previous years. [↑](#footnote-ref-1347)
1347. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluations. [↑](#footnote-ref-1348)
1348. The value is estimated at 1.06 (calculated as 1 + (0.66\*(0.27 / 2.8)). Based on cooling loads decreasing by 27% of the lighting savings (average result from REMRate modeling of several different configurations and IL locations of homes), assuming typical cooling system operating efficiency of 2.8 COP (starting from standard assumption of SEER 10.5 central AC unit, converted to 9.5 EER using algorithm (-0.02 \* SEER2) + (1.12 \* SEER) (from Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder), converted to COP = EER/3.412 = 2.8COP) and 66% of homes in Illinois having central cooling ("Table HC7.9 Air Conditioning in Homes in Midwest Region, Divisions, and States, 2009 from Energy Information Administration", 2009 Residential Energy Consumption Survey; [http://www.eia.gov/consumption/residential/data/2009/xls/HC7.9%20Air%20Conditioning%20in%20Midwest%20Region.xls](http://www.energystar.gov/ia/partners/bldrs_lenders_raters/downloads/Waste_Water_Heat_Recovery_Guidelines.pdf)) [↑](#footnote-ref-1349)
1349. As above but using estimate of 45% of multi family buildings in Illinois having central cooling (based on data from “Table HC7.1 Air Conditioning in U.S. Homes, By Housing Unit Type, 2009” which is for the whole of the US, scaled to IL air conditioning prevalence compared to US average); [http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls](http://205.254.135.7/consumption/residential/data/2009/) [↑](#footnote-ref-1350)
1350. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-1351)
1351. This means that heating loads increase by 49% of the lighting savings. This is based on the average result from REMRate modeling of several different configurations and IL locations of homes. [↑](#footnote-ref-1352)
1352. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Heat Pumps was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-1353)
1353. The value is estimated at 1.11 (calculated as 1 + (0.66 \* 0.466 / 2.8)). See footnote relating to WHFe for details. Note the 46.6% factor represents the average Residential cooling coincidence factor calculated by dividing average load during the peak hours divided by the maximum cooling load. [↑](#footnote-ref-1354)
1354. As above but using estimate of 45% of multi family buildings in Illinois having central cooling (based on data from “Table HC7.1 Air Conditioning in U.S. Homes, By Housing Unit Type, 2009” which is for the whole of the US, scaled to IL air conditioning prevalence compared to US average); [http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls](http://www.homeenergy.org/archive/hem.dis.anl.gov/eehem/94/940111.html). [↑](#footnote-ref-1355)
1355. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1356)
1356. Average result from REMRate modeling of several different configurations and IL locations of homes [↑](#footnote-ref-1357)
1357. This has been estimated assuming that natural gas central furnace heating is typical for Illinois residences (66% of Illinois homes have a Natural Gas Furnace (based on Energy Information Administration, 2009 Residential Energy Consumption Survey: http://www.eia.gov/consumption/residential/data/2009/xls/HC6.9%20Space%20Heating%20in%20Midwest%20Region.xls))

      In 2000, 24% of furnaces purchased in Illinois were condensing (based on data from GAMA, provided to Department of Energy during the federal standard setting process for residential heating equipment - see Furnace Penetration.xls). Furnaces tend to last up to 20 years and so units purchased 10 years ago provide a reasonable proxy for the current mix of furnaces in the State. Assuming typical efficiencies for condensing and non-condensing furnaces and duct losses, the average heating system efficiency is estimated as follows:

      (0.24\*0.92) + (0.76\*0.8) \* (1-0.15) = 0.70 [↑](#footnote-ref-1358)
1358. 2008 Database for Energy-Efficiency Resources (DEER), Version 2008.2.05, “Effective/Remaining Useful Life Values”, California Public Utilities Commission, December 16, 2008. [↑](#footnote-ref-1359)
1359. NYSERDA Deemed Savings Database, Labor cost assumes 25 minutes @ $18/hr. [↑](#footnote-ref-1360)
1360. Assuming continuous operation of an LED exit sign, the Summer Peak Coincidence Factor is assumed to equal 1.0. [↑](#footnote-ref-1361)
1361. Based on review of available product. [↑](#footnote-ref-1362)
1362. Efficiency Vermont Technical Reference User Manual (TRM) Measure Savings Algorithms and Cost Assumptions, February, 19, 2010 [↑](#footnote-ref-1363)
1363. Efficiency Vermont Technical Reference User Manual (TRM) Measure Savings Algorithms and Cost Assumptions, February, 19, 2010 [↑](#footnote-ref-1364)
1364. The value is estimated at 1.04 (calculated as 1 + (0.45\*(0.27 / 2.8)). Based on cooling loads decreasing by 27% of the lighting savings (average result from REMRate modeling of several different configurations and IL locations of homes), assuming typical cooling system operating efficiency of 3.1 COP (starting from standard assumption of SEER 10.5 central AC unit, converted to 9.5 EER using algorithm (-0.02 \* SEER2) + (1.12 \* SEER) (from Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder), converted to COP = EER/3.412 = 2.8COP) and estimate of 45% of multi family buildings in Illinois having central cooling (based on data from “Table HC7.1 Air Conditioning in U.S. Homes, By Housing Unit Type, 2009” which is for the whole of the US, scaled to IL air conditioning prevalence compared to US average); http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls [↑](#footnote-ref-1365)
1365. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-1366)
1366. This means that heating loads increase by 49% of the lighting savings. This is based on the average result from REMRate modeling of several different configurations and IL locations of homes. [↑](#footnote-ref-1367)
1367. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Heat Pumps was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-1368)
1368. The value is estimated at 1.11 (calculated as 1 + (0.45 \* 0.466 / 2.8)). See footnote relating to WHFe for details. Note the 46.6% factor represents the average Residential cooling coincidence factor calculated by dividing average load during the peak hours divided by the maximum cooling load. [↑](#footnote-ref-1369)
1369. Average result from REMRate modeling of several different configurations and IL locations of homes [↑](#footnote-ref-1370)
1370. This has been estimated assuming that natural gas central furnace heating is typical for Illinois residences (66% of Illinois homes have a Natural Gas Furnace (based on Energy Information Administration, 2009 Residential Energy Consumption Survey: http://www.eia.gov/consumption/residential/data/2009/xls/HC6.9%20Space%20Heating%20in%20Midwest%20Region.xls))

      In 2000, 24% of furnaces purchased in Illinois were condensing (based on data from GAMA, provided to Department of Energy during the federal standard setting process for residential heating equipment - see Furnace Penetration.xls). Furnaces tend to last up to 20 years and so units purchased 10 years ago provide a reasonable proxy for the current mix of furnaces in the State. Assuming typical efficiencies for condensing and non-condensing furnaces and duct losses, the average heating system efficiency is estimated as follows:

      (0.24\*0.92) + (0.76\*0.8) \* (1-0.15) = 0.70 [↑](#footnote-ref-1371)
1371. Consistent with assumption for a Standard CFL bulb with an estimated labor cost of $4.50 (assuming $18/hour and a task time of 15 minutes). [↑](#footnote-ref-1372)
1372. Assumes a lamp life of 12,000 hours and 8766 run hours 12000/8766 = 1.37 years. [↑](#footnote-ref-1373)
1373. Based on recommendation in the Dunsky Energy Consulting, Livingston Energy Innovations and Opinion Dynamics Corporation; NEEP Emerging Technology Research Report: <https://www.neep.org/Assets/uploads/files/emv/emv-products/NEEP_EMV_EmergingTechResearch_Report_Final.pdf>, p 6-18. [↑](#footnote-ref-1374)
1374. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1375)
1375. Based on ENERGY STAR specs – minimum luminous efficacy for Omnidirectional Lamps. For LED lamp power <10W = 50lm/W and for LED lamp power >=10W = 55lm/W. [↑](#footnote-ref-1376)
1376. Calculated as 45lm/W for all EISA non-exempt bulbs. [↑](#footnote-ref-1377)
1377. 1st year in service rate is based upon analysis of ComEd PY7 intercept data. [↑](#footnote-ref-1378)
1378. The 98% Lifetime ISR assumption is based upon the standard CFL measure in the absence of any better reference. This value is based upon review of two evaluations:

      ‘Nexus Market Research, RLW Analytics and GDS Associates study; “New England Residential Lighting Markdown Impact Evaluation, January 20, 2009’ and ‘KEMA Inc, Feb 2010, Final Evaluation Report:, Upstream Lighting Program, Volume 1.’ This implies that only 2% of bulbs purchased are never installed. The second and third year installations are based upon Ameren analysis of the Californian KEMA study showing that 54% of future installs occur in year 2 and 46% in year 3. The 2nd and 3rd year installations should be counted as part of those future program year savings. [↑](#footnote-ref-1379)
1379. Based upon Standard CFL assumption in the absence of better data, and is based upon review of the PY2 and PY3 ComEd Direct Install program surveys. This value includes bulb failures in the 1st year to be consistent with the Commission approval of annualization of savings for first year savings claims. ComEd PY2 All Electric Single Family Home Energy Performance Tune-Up Program Evaluation, Navigant Consulting, December 21, 2010. <http://www.icc.illinois.gov/downloads/public/edocket/287090.pdf>. [↑](#footnote-ref-1380)
1380. In Service Rates provided are for the bulb within a kit only. Given the significant differences in program design and the level of education provided through Efficiency Kits programs, the evaluators should apply the ISR estimated through evaluations (either past evaluations or the current program year evaluation) of the specific Efficiency Kits program.  In cases where program-specific evaluation results for an ISR are unavailable, the default ISR values for Efficiency Kits provide may be used. [↑](#footnote-ref-1381)
1381. Free bulbs provided without request, with little or no education. Consistent with Standard CFL assumptions. [↑](#footnote-ref-1382)
1382. Kits provided free to students through school, with education program. Consistent with Standard CFL assumptions. [↑](#footnote-ref-1383)
1383. Opt-in program to receive kits via mail, with little or no education. Consistent with Standard CFL assumptions. [↑](#footnote-ref-1384)
1384. Using a leakage estimate from the current program year evaluation, from past evaluation results, or a rolling average of leakage estimates from previous years. [↑](#footnote-ref-1385)
1385. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluation. [↑](#footnote-ref-1386)
1386. The value is estimated at 1.06 (calculated as 1 + (0.66\*(0.27 / 2.8)). Based on cooling loads decreasing by 27% of the lighting savings (average result from REMRate modeling of several different configurations and IL locations of homes), assuming typical cooling system operating efficiency of 2.8 COP (starting from standard assumption of SEER 10.5 central AC unit, converted to 9.5 EER using algorithm (-0.02 \* SEER2) + (1.12 \* SEER) (from Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder), converted to COP = EER/3.412 = 2.8COP) and 66% of homes in Illinois having central cooling ("Table HC7.9 Air Conditioning in Homes in Midwest Region, Divisions, and States, 2009 from Energy Information Administration", 2009 Residential Energy Consumption Survey; <http://www.eia.gov/consumption/residential/data/2009/xls/HC7.9%20Air%20Conditioning%20in%20Midwest%20Region.xls> ) [↑](#footnote-ref-1387)
1387. As above but using estimate of 45% of multi family buildings in Illinois having central cooling (based on data from “Table HC7.1 Air Conditioning in U.S. Homes, By Housing Unit Type, 2009” which is for the whole of the US, scaled to IL air conditioning prevalence compared to US average); <http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls> [↑](#footnote-ref-1388)
1388. Negative value because this is an increase in heating consumption due to the efficient lighting. [↑](#footnote-ref-1389)
1389. This means that heating loads increase by 49% of the lighting savings. This is based on the average result from REMRate modeling of several different configurations and IL locations of homes. [↑](#footnote-ref-1390)
1390. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Heat Pumps was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-1391)
1391. The value is estimated at 1.11 (calculated as 1 + (0.66 \* 0.466 / 2.8)). See footnote relating to WHFe for details. Note the 46.6% factor represents the average Residential cooling coincidence factor calculated by dividing average load during the peak hours divided by the maximum cooling load. [↑](#footnote-ref-1392)
1392. As above but using estimate of 45% of multi family buildings in Illinois having central cooling (based on data from “Table HC7.1 Air Conditioning in U.S. Homes, By Housing Unit Type, 2009” which is for the whole of the US, scaled to IL air conditioning prevalence compared to US average); <http://205.254.135.7/consumption/residential/data/2009/xls/HC7.1%20Air%20Conditioning%20by%20Housing%20Unit%20Type.xls>. [↑](#footnote-ref-1393)
1393. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluations. [↑](#footnote-ref-1394)
1394. Based upon pricing forecast developed by Applied Proactive Technologies Inc (APT) based on industry input and provided to Ameren. [↑](#footnote-ref-1395)
1395. Based on lighting logger study conducted as part of the PY5/6 ComEd Residential Lighting Program evaluations. [↑](#footnote-ref-1396)
1396. The manufacturers of the new minimally compliant EISA Halogens are using regular incandescent lamps with halogen fill gas rather than halogen infrared to meet the standard and so the component rated life is equal to the standard incandescent. [↑](#footnote-ref-1397)
1397. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, 2007 [↑](#footnote-ref-1398)
1398. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-1399)
1399. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-1400)
1400. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-1401)
1401. N-factor is used to convert 50-pascal blower door air flows to natural air flows and is dependent on geographic location and exposure of the home to wind (impacts of stack effect based on height of building will not be significant because of reduced delta T during the cooling season) , based on methodology developed by Lawrence Berkeley Laboratory (LBL). [N-factor](http://www.homeenergy.org/archive/hem.dis.anl.gov/eehem/94/940111.html#94011122) values copied from J. Krigger, C. Dorsi; “Residential Energy: Cost Savings and Comfort for Existing Buildings”, p284. [↑](#footnote-ref-1402)
1402. National Climatic Data Center, calculated from 1981-2010 climate normals with a base temp of 65°F. [↑](#footnote-ref-1403)
1403. This factor's source is: Energy Center of Wisconsin, May 2008 metering study; “Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research”, p31. [↑](#footnote-ref-1404)
1404. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Central AC was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-1405)
1405. The Latent Multiplier is used to convert the sensible cooling savings calculated to a value representing sensible and latent cooling loads. The values are derived from Harriman et al "Dehumidification and Cooling Loads From Ventilation Air", ASHRAE Journal, by adding the latent and sensible loads to determine the total, then dividing the total by the sensible load. Where this specialized data was not available, a nearby city was chosen. [↑](#footnote-ref-1406)
1406. N-factor is used to convert 50-pascal blower door air flows to natural air flows and is dependent on geographic location, height of building (stack effect) and exposure of the home to wind, based on methodology developed by Lawrence Berkeley Laboratory (LBL). [N-factor](http://www.homeenergy.org/archive/hem.dis.anl.gov/eehem/94/940111.html#94011122) values copied from J. Krigger, C. Dorsi; “Residential Energy: Cost Savings and Comfort for Existing Buildings”, p284. [↑](#footnote-ref-1407)
1407. National Climatic Data Center, calculated from 1981-2010 climate normals with a base temp of 65°F. The base temperature was selected to account for the fact that homes receiving airsealing efforts are likely to be more leaky homes where the inside and outside air temperature is more consistent and therefore is more likely to require heating as temperatures drop below 65 degrees. Using this base temperature also reconciles the resulting savings estimates with the results of more sophisticated modeling software. [↑](#footnote-ref-1408)
1408. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Heat Pumps was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time means that using the minimum standard is appropriate. An 85% distribution efficiency is then applied to account for duct losses for heat pumps. [↑](#footnote-ref-1409)
1409. Fe is not one of the AHRI certified ratings provided for residential furnaces, but can be reasonably estimated from a calculation based on the certified values for fuel energy (Ef in MMBtu/yr) and Eae (kWh/yr). An average of a 300 record sample (non-random) out of 1495 was 3.14%. This is, appropriately, ~50% greater than the Energy Star version 3 criteria for 2% Fe. See “Programmable Thermostats Furnace Fan Analysis.xlsx” for reference. [↑](#footnote-ref-1410)
1410. Full load hours for Chicago, Moline and Rockford are provided in “Final Evaluation Report: Central Air Conditioning Efficiency Services (CACES), 2010, Navigant Consulting”, <http://ilsag.org/yahoo_site_admin/assets/docs/ComEd_PY2_CACES_Evaluation_Report_2010-10-18.299122020.pdf> p.33. An average FLH/Cooling Degree Day (from NCDC) ratio was calculated for these locations and applied to the CDD of the other locations in order to estimate FLH. [↑](#footnote-ref-1411)
1411. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-1412)
1412. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-1413)
1413. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-1414)
1414. N-factor is used to convert 50-pascal blower door air flows to natural air flows and is dependent on geographic location, height of building (stack effect) and exposure of the home to wind, based on methodology developed by Lawrence Berkeley Laboratory (LBL). [N-factor](http://www.homeenergy.org/archive/hem.dis.anl.gov/eehem/94/940111.html#94011122) values copied from J. Krigger, C. Dorsi; “Residential Energy: Cost Savings and Comfort for Existing Buildings”, p284. [↑](#footnote-ref-1415)
1415. National Climatic Data Center, calculated from 1981-2010 climate normals with a base temp of 60°F, consistent with the findings of Belzer and Cort, Pacific Northwest National Laboratory in “Statistical Analysis of Historical State-Level Residential Energy Consumption Trends,” 2004.. [↑](#footnote-ref-1416)
1416. Ideally, the System Efficiency should be obtained either by recording the AFUE of the unit, or performing a steady state efficiency test. The Distribution Efficiency can be estimated via a visual inspection and by referring to a look up table such as that provided by the Building Performance Institute: (<http://www.bpi.org/files/pdf/DistributionEfficiencyTable-BlueSheet.pdf> or by performing duct blaster testing. [↑](#footnote-ref-1417)
1417. This has been estimated assuming that natural gas central furnace heating is typical for Illinois residences (66% of Illinois homes have a Natural Gas Furnace (based on Energy Information Administration, 2009 Residential Energy Consumption Survey: <http://www.eia.gov/consumption/residential/data/2009/xls/HC6.9%20Space%20Heating%20in%20Midwest%20Region.xls> )

      In 2000, 24% of furnaces purchased in Illinois were condensing (based on data from GAMA, provided to Department of Energy during the federal standard setting process for residential heating equipment - see Furnace Penetration.xls). Furnaces tend to last up to 20 years and so units purchased 10 years ago provide a reasonable proxy for the current mix of furnaces in the State. Assuming typical efficiencies for condensing and non-condensing furnaces and duct losses, the average heating system efficiency is estimated as follows:

      (0.24\*0.92) + (0.76\*0.8) \* (1-0.15) = 0.70 [↑](#footnote-ref-1418)
1418. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, 2007 [↑](#footnote-ref-1419)
1419. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-1420)
1420. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-1421)
1421. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-1422)
1422. ORNL Builders Foundation Handbook, crawl space data from Table 5-5: Initial Effective R-values for Uninsulated Foundation System and Adjacent Soil, 1991, http://www.ornl.gov/sci/roofs+walls/foundation/ORNL\_CON-295.pdf [↑](#footnote-ref-1423)
1423. ASHREA, 2001, “Characterization of Framing Factors for New Low-Rise Residential Building Envelopes (904-RP),” Table 7.1 [↑](#footnote-ref-1424)
1424. National Climatic Data Center, calculated from 1981-2010 climate normals with a base temp of 65°F. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-1425)
1425. Five year average cooling degree days with 75F base temp from DegreeDays.net were used in this table because the 30 year climate normals from NCDC used elsewhere are not available at base temps above 72F. [↑](#footnote-ref-1426)
1426. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-1427)
1427. This factor's source is: Energy Center of Wisconsin, May 2008 metering study; “Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research”, p31. [↑](#footnote-ref-1428)
1428. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Central AC was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-1429)
1429. Adapted from Table 1, page 24.4, of the 1977 ASHRAE Fundamentals Handbook [↑](#footnote-ref-1430)
1430. National Climatic Data Center, calculated from 1981-2010 climate normals with a base temp of 60°F for a conditioned basement and 50°F for an unconditioned basement), consistent with the findings of Belzer and Cort, Pacific Northwest National Laboratory in “Statistical Analysis of Historical State-Level Residential Energy Consumption Trends,” 2004. There is a county mapping table in the front of the TRM providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-1431)
1431. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-1432)
1432. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Heat Pumps was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time means that using the minimum standard is appropriate. An 85% distribution efficiency is then applied to account for duct losses for heat pumps. [↑](#footnote-ref-1433)
1433. Based upon comparing algorithm derived savings estimate and evaluated bill analysis estimate in the following 2012 Massachusetts report: “Home Energy Services Impact Evaluation”, August 2012. See “Insulation ADJ calculations.xls” for details or calculation. [↑](#footnote-ref-1434)
1434. Fe is not one of the AHRI certified ratings provided for residential furnaces, but can be reasonably estimated from a calculation based on the certified values for fuel energy (Ef in MMBtu/yr) and Eae (kWh/yr). An average of a 300 record sample (non-random) out of 1495 was 3.14%. This is, appropriately, ~50% greater than the Energy Star version 3 criteria for 2% Fe. See “Programmable Thermostats Furnace Fan Analysis.xlsx” for reference. [↑](#footnote-ref-1435)
1435. Full load hours for Chicago, Moline and Rockford are provided in “Final Evaluation Report: Central Air Conditioning Efficiency Services (CACES), 2010, Navigant Consulting”, <http://ilsagfiles.org/SAG_files/Evaluation_Documents/ComEd/ComEd%20EPY2%20Evaluation%20Reports/ComEd_Central_AC_Efficiency_Services_PY2_Evaluation_Report_Final.pdf>, p.33. An average FLH/Cooling Degree Day (from NCDC) ratio was calculated for these locations and applied to the CDD of the other locations in order to estimate FLH. There is a county mapping table in the front of the TRM providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-1436)
1436. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-1437)
1437. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-1438)
1438. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-1439)
1439. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-1440)
1440. This has been estimated assuming that natural gas central furnace heating is typical for Illinois residences (66% of Illinois homes have a Natural Gas Furnace (based on Energy Information Administration, 2009 Residential Energy Consumption Survey: http://www.eia.gov/consumption/residential/data/2009/xls/HC6.9%20Space%20Heating%20in%20Midwest%20Region.xls))

      In 2000, 24% of furnaces purchased in Illinois were condensing (based on data from GAMA, provided to Department of Energy during the federal standard setting process for residential heating equipment - see Furnace Penetration.xls). Furnaces tend to last up to 20 years and so units purchased 10 years ago provide a reasonable proxy for the current mix of furnaces in the State. Assuming typical efficiencies for condensing and non-condensing furnaces and duct losses, the average heating system efficiency is estimated as follows:

      (0.24\*0.92) + (0.76\*0.8) \* (1-0.15) = 0.70 [↑](#footnote-ref-1441)
1441. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, 2007 [↑](#footnote-ref-1442)
1442. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-1443)
1443. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-1444)
1444. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-1445)
1445. Based on 2005 ASHRAE Handbook – Fundamentals: assuming 2x8 joists, 16” OC, ¾” subfloor, ½” carpet with rubber pad, and accounting for a still air film above and below: 1/ [(0.85 cavity share of area / (0.68 + 0.94 + 1.23 + 0.68)) + (0.15 framing share / (0.68 + 7.5” \* 1.25 R/in + 0.94 + 1.23 + 0.68))] = 3.96 [↑](#footnote-ref-1446)
1446. ASHRAE, 2001, “Characterization of Framing Factors for New Low-Rise Residential Building Envelopes (904-RP),” Table 7.1 [↑](#footnote-ref-1447)
1447. Five year average cooling degree days with 75F base temp from DegreeDays.net were used in this table because the 30 year climate normals from NCDC used elsewhere are not available at base temps above 72F. [↑](#footnote-ref-1448)
1448. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-1449)
1449. Energy Center of Wisconsin, May 2008 metering study; “Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research”, p31. [↑](#footnote-ref-1450)
1450. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Central AC was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-1451)
1451. National Climatic Data Center, Heating Degree Days with a base temp of 50°F to account for lower impact of unconditioned space on heating system. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-1452)
1452. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-1453)
1453. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Heat Pumps was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time means that using the minimum standard is appropriate. An 85% distribution efficiency is then applied to account for duct losses for heat pumps. [↑](#footnote-ref-1454)
1454. Based upon comparing algorithm derived savings estimate and evaluated bill analysis estimate in the following 2012 Massachusetts report: “Home Energy Services Impact Evaluation”, August 2012. See “Insulation ADJ calculations.xls” for details or calculation. Note that basement wall is used as a proxy for crawlspace ceiling. [↑](#footnote-ref-1455)
1455. Fe is not one of the AHRI certified ratings provided for residential furnaces, but can be reasonably estimated from a calculation based on the certified values for fuel energy (Ef in MMBtu/yr) and Eae (kWh/yr). An average of a 300 record sample (non-random) out of 1495 was 3.14%. This is, appropriately, ~50% greater than the Energy Star version 3 criteria for 2% Fe. See “Programmable Thermostats Furnace Fan Analysis.xlsx” for reference. [↑](#footnote-ref-1456)
1456. Full load hours for Chicago, Moline and Rockford are provided in “Final Evaluation Report: Central Air Conditioning Efficiency Services (CACES), 2010, Navigant Consulting”, <http://ilsag.org/yahoo_site_admin/assets/docs/ComEd_PY2_CACES_Evaluation_Report_2010-10-18.299122020.pdf>, p.33. An average FLH/Cooling Degree Day (from NCDC) ratio was calculated for these locations and applied to the CDD of the other locations in order to estimate FLH. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-1457)
1457. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-1458)
1458. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-1459)
1459. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-1460)
1460. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-1461)
1461. This has been estimated assuming that natural gas central furnace heating is typical for Illinois residences (66% of Illinois homes have a Natural Gas Furnace (based on Energy Information Administration, 2009 Residential Energy Consumption Survey: <http://www.eia.gov/consumption/residential/data/2009/xls/HC6.9%20Space%20Heating%20in%20Midwest%20Region.xls>))

      In 2000, 24% of furnaces purchased in Illinois were condensing (based on data from GAMA, provided to Department of Energy during the federal standard setting process for residential heating equipment - see Furnace Penetration.xls). Furnaces tend to last up to 20 years and so units purchased 10 years ago provide a reasonable proxy for the current mix of furnaces in the State. Assuming typical efficiencies for condensing and non-condensing furnaces and duct losses, the average heating system efficiency is estimated as follows:

      (0.24\*0.92) + (0.76\*0.8) \* (1-0.15) = 0.70 [↑](#footnote-ref-1462)
1462. Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, 2007 [↑](#footnote-ref-1463)
1463. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-1464)
1464. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-1465)
1465. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-1466)
1466. An estimate based on review of Madison Gas and Electric, Exterior Wall Insulation, R-value for no insulation in walls, and NREL's Building Energy Simulation Test for Existing Homes (BESTEST-EX). [↑](#footnote-ref-1467)
1467. ASHRAE, 2001, “Characterization of Framing Factors for New Low-Rise Residential Building Envelopes (904-RP),” Table 7.1 [↑](#footnote-ref-1468)
1468. Ibid. [↑](#footnote-ref-1469)
1469. National Climatic Data Center, Cooling Degree Days are based on a base temp of 65°F. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-1470)
1470. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-1471)
1471. This factor's source is: Energy Center of Wisconsin, May 2008 metering study; “Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research”, p31. [↑](#footnote-ref-1472)
1472. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Central AC was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time mean that using the minimum standard is appropriate. [↑](#footnote-ref-1473)
1473. National Climatic Data Center, calculated from 1981-2010 climate normals with a base temp of 60°F, consistent with the findings of Belzer and Cort, Pacific Northwest National Laboratory in “Statistical Analysis of Historical State-Level Residential Energy Consumption Trends,” 2004. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-1474)
1474. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-1475)
1475. These default system efficiencies are based on the applicable minimum Federal Standards. In 2006 the Federal Standard for Heat Pumps was adjusted. While one would expect the average system efficiency to be higher than this minimum, the likely degradation of efficiencies over time means that using the minimum standard is appropriate. An 85% distribution efficiency is then applied to account for duct losses for heat pumps. [↑](#footnote-ref-1476)
1476. Based upon comparing algorithm derived savings estimate and evaluated bill analysis estimate in the following 2012 Massachusetts report: “Home Energy Services Impact Evaluation”, August 2012. See “Insulation ADJ calculations.xls” for details or calculation. [↑](#footnote-ref-1477)
1477. Based upon comparing algorithm derived savings estimate and evaluated bill analysis estimate in the following 2012 Massachusetts report: “Home Energy Services Impact Evaluation”, August 2012. See “Insulation ADJ calculations.xls” for details or calculation. Note that basement walls is used as a proxy for crawlspace ceiling. [↑](#footnote-ref-1478)
1478. Fe is not one of the AHRI certified ratings provided for residential furnaces, but can be reasonably estimated from a calculation based on the certified values for fuel energy (Ef in MMBtu/yr) and Eae (kWh/yr). An average of a 300 record sample (non-random) out of 1495 was 3.14%. This is, appropriately, ~50% greater than the Energy Star version 3 criteria for 2% Fe. See “Programmable Thermostats Furnace Fan Analysis.xlsx” for reference. [↑](#footnote-ref-1479)
1479. Based on Full Load Hours from ENERGY Star with adjustments made in a Navigant Evaluation, other cities were scaled using those results and CDD. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-1480)
1480. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-1481)
1481. Based on metering of 24 homes with central AC during PY4 and PY5 in Ameren Illinois service territory. [↑](#footnote-ref-1482)
1482. Based on analysis of metering results from 24 heat pumps in Ameren Illinois service territory in PY5 coincident with AIC’s 2010 system peak; ‘Impact and Process Evaluation of Ameren Illinois Company’s Residential HVAC Program (PY5)’. [↑](#footnote-ref-1483)
1483. Based on analysis of Itron eShape data for Missouri, calibrated to Illinois loads, supplied by Ameren. The average AC load over the PJM peak period (1-5pm, M-F, June through August) is divided by the maximum AC load during the year. [↑](#footnote-ref-1484)
1484. National Climatic Data Center, calculated from 1981-2010 climate normals with a base temp of 60°F, consistent with the findings of Belzer and Cort, Pacific Northwest National Laboratory in “Statistical Analysis of Historical State-Level Residential Energy Consumption Trends,” 2004. There is a county mapping table in the Appendix providing the appropriate city to use for each county of Illinois. [↑](#footnote-ref-1485)
1485. Weighted based on number of occupied residential housing units in each zone. [↑](#footnote-ref-1486)
1486. Ideally, the System Efficiency should be obtained either by recording the AFUE of the unit, or performing a steady state efficiency test. The Distribution Efficiency can be estimated via a visual inspection and by referring to a look up table such as that provided by the Building Performance Institute: (<http://www.bpi.org/files/pdf/DistributionEfficiencyTable-BlueSheet.pdf>) or by performing duct blaster testing. [↑](#footnote-ref-1487)
1487. This has been estimated assuming that natural gas central furnace heating is typical for Illinois residences (66% of Illinois homes have a Natural Gas Furnace (based on Energy Information Administration, 2009 Residential Energy Consumption Survey: <http://www.eia.gov/consumption/residential/data/2009/xls/HC6.9%20Space%20Heating%20in%20Midwest%20Region.xls)>). In 2000, 24% of furnaces purchased in Illinois were condensing (based on data from GAMA, provided to Department of Energy during the federal standard setting process for residential heating equipment - see Furnace Penetration.xls). Furnaces tend to last up to 20 years and so units purchased 10 years ago provide a reasonable proxy for the current mix of furnaces in the State. Assuming typical efficiencies for condensing and non-condensing furnaces and duct losses, the average heating system efficiency is estimated as follows:

      (0.24\*0.92) + (0.76\*0.8) \* (1-0.15) = 0.70 [↑](#footnote-ref-1488)